



# Hydrogeology and Hydrology Characterization Report

## Glenmore Landfill



City of Kelowna

19 December 2023

→ The Power of Commitment





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# 1. Introduction

GHD Limited (GHD) was retained by the City of Kelowna (City) to complete this Hydrogeology and Hydrology Characterization Report (HHCR) for the Glenmore Landfill (Site). The Site operates under Operational Certificate 12218 (OC), issued by the British Columbia (BC) Ministry of Environment and Climate Change Strategy (Ministry) on December 8, 2000, and most recently amended on May 30, 2023. The Operational Certificate is presented in **Appendix A**.

For the purpose of this report, the term Landfill refers to the Glenmore Landfill waste footprint, including future fill areas, and the term Site refers to all facilities and works within the Site boundary, as defined by Section 1.5.1 of the OC.

## 1.1 Purpose and Scope of this Report

Section 3.2 of the OC states that an HHCR must be submitted to the Ministry on, or before December 31, 2024, and that an updated HHCR must be submitted at least once every ten years following December 31, 2024. The purpose of this report is to provide the 2024 HHCR for the Site. The scope of this report is to produce an HHCR that includes the required information specified in Section 10.1 *Hydrogeology and Hydrology Characterization Report* of the BC Landfill Criteria for Municipal Solid Waste (BC Ministry of Environment, 2016).

## 1.2 Limitations

*This report: has been prepared by GHD for City of Kelowna and may only be used and relied on by City of Kelowna and the Ministry of Environment and Climate Change Strategy for the purpose agreed between GHD and City of Kelowna as set out in section 1.1 of this report.*

*GHD otherwise disclaims responsibility to any person other than City of Kelowna arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.*

*The services undertaken by GHD in connection with preparing this report were limited to the information provided in historical documents provided by the City and publicly available information provided online at the date of preparing the report.*

*The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.*

*The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.*

## 1.3 Site Location

The Site is located in Kelowna, BC and is approximately 1.5 kilometres (km) east of Okanagan Lake and 9 km northeast of downtown Kelowna. The civic address of the scale house and public drop-off area is 2710 John Hindle Drive. A Site location map is presented on **Figure 1.1**.

## 1.4 Landfilling Operations

### 1.4.1 Municipal Waste

The Landfill accepts approximately 120,000 tonnes of municipal solid waste annually. The Landfill footprint is approximately 81 ha. Landfilling of municipal solid waste began in 1966 within Phase 1, Phase 2, and Phase 3. Phases 1 and 2 together are known as the North Landfill and Phase 3 is referred to as the Slough. Phases 1 and 2 are delineated by an east-west gravity drain that is part of the leachate collection system.

Each of the three areas relies largely on a natural control liner system (i.e., natural clay subsurface). In 2001, the footprint of the landfill was expanded to the north with construction of the lined North Expansion Area (now referred to as fill Area 2), and in 2019 a liner was installed at the former public drop-off area (fill Area 1). Additional liner was constructed in Area 2 in 2020.

Today, municipal waste is deposited in the lined and natural control liner portions of Phase 1 & Phase 2, with some select filling of construction and demolition waste in Phase 3 (the Slough). It should also be noted that the Municipality operates a Compost Facility (or Composting Facility) south of Phase 3.

For a detailed description of historical, active, and future municipal solid waste landfilling, refer to the 2023 Design, Operations, and Closure Plan (GHD, 2023). The Phases of the Landfill and the Compost Facility are briefly described below and presented on **Figure 1.2**.

- Phase 1: Historical and active disposal area located in the northern portion of the Landfill. This area is unlined except for the northwestern and southwestern areas of Phase 1 (see **Figure 1.2** for location of geomembrane liners).
- Phase 2: Historical and active disposal area located in the central portion of the Landfill. This area is unlined except for the historic public drop-off area in northwest corner of Phase 2.
- Phase 3: Historical disposal area located south of Phase 2. Active disposal in Phase 3 is limited to select construction and demolition materials. Historical landfilling in this area began by infilling the Slough, formally known as Alki Lake. Landfill cells were developed by excavating and infilling successive trenches. Trench depths have been inferred to be up to 10.4 m (SLR, 2011). The northern end of the Slough received two lifts of waste and the southern end received one lift of waste (CH2M Hill, 2008).
- Compost Facility: Located south of Phase 3. The composting infrastructure is currently being upgraded from a turned windrow system to an aerated static pile (ASP) system. Runoff from the compost facility has been managed by directing flow towards the landfill footprint. The ASP composting system will be equipped with a leachate management system that includes collection under the compost piles and discharge to the sewer via a new composting leachate lift station.

Groundwater monitoring wells are instrumented throughout and surrounding the Site to monitor groundwater elevation and quality. A map presenting historical investigation locations is presented on **Figure 1.3** and a map presenting the current groundwater, leachate, and surface water monitoring network is presented on **Figure 1.4**.

## 1.4.2 Biosolids

According to the City, biosolids organic waste (roughly 3% solids) were accepted at the Site for land spreading in the northern end of Phase 1 between 2000 and 2008. The organic waste was generated at the Brandt's Creek Trade Waste Treatment Plant and was high in nitrogen and was used as a fertiliser replacement. It is estimated that approximately  $\frac{3}{4}$  of the organic waste received by the Landfill was spread in the northern end of Phase 1 and the remaining  $\frac{1}{4}$  was spread in the northeast corner of the Site. Available application records indicate that approximately 3,688,092 L were applied at the Site in 2005; 6,298,500 L in 2006; 4,870,500 L in 2007; and 1,759,500 L in 2008 (Golder, 2012).

Additionally, the City reports that between approximately 1990 and 1993, primary and tertiary biosolids (roughly 20% solids) were deposited in the form of liquid sludge at the northeast corner of the Site (northeast of Phase 2), as part of a biosolids composting program. The biosolids were deposited into above ground pits construction of hog fuel. Once the pits were filled, the sludge was mixed up and allowed to decompose for a period of at least one year, at which time it is inferred that the sludge was spread on the surface of the adjacent farmlands and to landscape the perimeter berms of the Landfill (Golder, 2012).



## 2. Land and Water Use

### 2.1 Zoning and Land Use

Figure 2.1 provides a map of the zoning and land use of the Site and within 1 kilometre (km) of the Site.

The majority of the Site is zoned as agricultural (A1) and forms part of the Agricultural Land Reserve (ALR). The operation of the Landfill is a legal non-conforming land use for the property. The Site entrance facilities are located at the south end of the Site on a lot zoned for public and institutional uses (P4).

The lands within 1 km of the Site are mainly undeveloped or active agricultural properties including Bredin Farm to the north and Tutt Farm to the west (zoned as agricultural A1). Residential and public lands are also present to the east southeast, and west of the Site. Directly east of the Site is Eagle View Park (zoned as park P), Quail Ridge subdivision (zoned as rural urban RU), and the Okanagan Golf Club (zoned as public and institutional P). Further to the southeast of the Site is another residential area along Glenmore Road (zoned as rural residential RR, mobile homes MH, and multi-dwelling zones MF). Directly west of the Site is North Glenmore Dog Park (zoned as park P).

### 2.2 Groundwater Use

Figure 2.2 illustrates the groundwater supply wells present within at least a 1 km radius of the Site. The groundwater well locations and detailed well records were sourced from iMapBC, which was accessed in September 2023. The detailed well records are in Appendix B.

There are six groundwater supply wells located within a 1 km radius of the Site. As presented in Table 1, one well is decommissioned and the remaining wells are unlicensed with unknown existing water use. Each of the wells are located hydraulically upgradient or cross-gradient from the Site. iMapBC does not show any groundwater supply wells within 1 km radius downgradient of the Site. Table 2.1, below, details the groundwater supply wells listed on iMapBC.

Additionally, SLR Consulting Canada Ltd. (SLR) completed a door-to-door survey in March 2014 to locate any water wells within a 500 m radius of the Site. SLR did not identify any existing water wells during the door-to-door survey (SLR Consulting Canada Ltd., 2015).

Table 2.1 Groundwater Supply Well Details for Wells Located within 1 km of the Site

Well Tag	Installation Date	Screened Geologic Unit	Well Yield (GPM)	Use; driller notes
23247	1970	Bedrock	9	Unknown/other/not listed
99677	2005	Hardpan (likely clay)	Not applicable	Decommissioned (2018)
19830	1966	Bedrock	0.5	No use; no suitable formation for a well
71857	1979	Bedrock	minimal	No use; well yield not suitable for use
20594	1967	Clay	5	Likely no use; due to the presence of thick black water that never cleared
2936	1948	Unknown	Not specified	Unknown/other/not listed

### 2.3 Surface Water Use

Figure 2.2 illustrates the surface water points of diversion present within a 1 km radius of the Site. The points of diversion and water use licenses were sourced from iMapBC, which was accessed in November 2023. The licenses are in Appendix B.

There are four surface water points of diversion within a 1 km radius of the Site. Surface water point of diversion C134394 (formerly C123789) is on-Site for pumping of water from the Northeast Pond (NE Pond) and the remaining

three are hydraulically upstream of the Site at the McKinley Reservoir. Surface water points of diversion C029197, C034631, and C061861 are all for the storage of water diverted from Kelowna Creek into the McKinley Reservoir.

It should be noted that clean water from the onsite ponds (NE Pond, Tutt Pond, and Bredin Pond) is used for irrigation by the farmers on the adjacent agricultural lands.

Downstream of the Site is Little Robert Lake and Robert Lake both of which are alkali lakes (or salt flats). Neither lake include surface water diversion points but are key surface water bodies to consider when assessing the hydrology of the Site. Robert Lake is situated within the Robert Lake Regional Park which is a 2 ha conservation area. There are no trails or access to the lake. Robert Lake is considered a sensitive ecosystem used by a number of wildlife species. Additional discussion of the Site’s hydrology is included in Section 3.3, below.

## 3. Site Physical Setting

### 3.1 Climate

The climate of the Central Okanagan is marked by hot, dry summers, and cool winters. Climatic data for the Site is based on Environment Canada’s 1981-2010 Climate Normals for the Kelowna Airport climate station (Climate ID 1123970). The Kelowna Airport climate station is located approximately 2.5 km to the east of the Site at an elevation of approximately 430 metres above mean sea level (m AMSL). The average annual temperature is 8.1 degrees Celsius. The average annual precipitation is 386.9 millimetres (mm). On average 89 centimetres (cm) of snowfall is recorded per year and 311.3 mm of rainfall is recorded. The average total monthly precipitation and average daily temperature records are presented in Table 3.1, below.

Table 3.1 Local Climate

Month	Daily Average Temperature (°C)	Average Monthly Precipitation (mm)
January	-2.5	31.0
February	-0.9	19.0
March	4.1	21.6
April	8.4	29.1
May	12.8	40.2
June	16.6	45.9
July	19.5	37.2
August	19.1	32.1
September	13.9	32.4
October	7.3	29.2
November	1.6	36.7
December	-2.6	32.6
Annual	8.1	386.9

Source: Environment Canada Canadian Climate Normals 1981-2010. Kelowna A Climate Station (Climate ID 1123970)

### 3.2 Topography

The Site is situated in the north-south trending Glenmore Valley. The Site is bordered by mountainous terrain to the north, west, east, and south-east of the Site. Quail Ridge is to the east, Tutt Mountain to the east, Bredin Hill to the



northeast, and Diamond Mountain to the southwest. A larger mountainous area is also present further west of the Site which contains Stephens Coyote Ridge.

The Site gradually slopes to the south ranging in elevation from approximately 475 m AMSL (at the north Site boundary) to 445 m AMSL (at the south Site boundary). The Landfill, which is located at the centre of the Site, is presently mounded to an elevation of 465 m AMSL at Phase 1. The Slough is the lowest lying area of the Site at 440 m AMSL. The Compost Facility is at an approximate elevation of 445 m AMSL.

Surrounding the Site, the topography rises to 520 m AMSL to the north, 560 m AMSL to the west, and 530 m AMSL to the east. South of the Site, lands slope gently down towards the south to an elevation of approximately 435 m AMSL at Robert Lake. A map presenting the topography in the vicinity of the Site is provided on **Figure 3.1**.

## 3.3 Hydrology and Drainage

### 3.3.1 Regional and Site Hydrology

The regional and Site hydrologic setting is illustrated on **Figure 3.2**.

The Site is situated within the Okanagan River watershed that includes six main lakes, the Okanagan, Kalamalka, Wood, Skaha, Vaseux and Osoyoos. Closest to the Landfill is Okanagan Lake, which is approximately 1.5 km west and upstream of the Site at 342 m AMSL. Okanagan Lake drains into the Okanagan River, which subsequently drains to Lake Skaha, Vaseux Lake, then Osoyoos Lake, and ultimately to the Columbia River.

As previously described, the Landfill is situated in the north-south trending Glenmore Valley. Stormwater from the surrounding mountainous terrain flows into the valley following topography. Stormwater that flows onto Site is managed by the Site stormwater management system, as described in Section 3.3.2. Stormwater that is not captured on-Site drains to the south following the topography of the valley floor and/or infiltrates into the subsurface.

North of the Site, the prominent surface water features include McKinley Reservoir (515 m AMSL), Bubna Slough (500 m AMSL), and Slough 2 (509 m AMSL). Ellison Lake, a smaller regional lake, is found 2.5 km northeast and upstream of the Site. South of the Site, the prominent surface water features include Little Robert Lake (440 m AMSL) and Robert Lake (434 m AMSL).

While not illustrated on **Figure 3.2**, a review of aerial photographs shows Little Robert Lake occasionally (during period of high precipitation) discharges at its south end and that discharge will flow into Robert Lake.

As illustrated on **Figure 3.2**, drainage from the McKinley Reservoir toe drain flows to the south and passes beneath Glenmore Road N. before discharging to the western Bredin Farm field. **Figure 3.2** also show drainage from Bubna Slough. Bubna Slough is subject to evaporative conditions; however, occasional discharge will also flow southwards and join the McKinley Reservoir discharge on Bredin Farm. Flow from both upstream sources, along with the majority of stormwater that falls or flows into Bredin Farm area ultimately enters Bredin Pond and joins the Site's drainage system.

**Figure 3.2** also shows surface water drainage to the northeast of Bredin Farm flows to the south and drains into the Northeast Pond.

### 3.3.2 Site Drainage

The Site drainage features are illustrated on **Figure 3.3**.

Site surface water and surface water run-on from the surrounding mountainous terrain is captured and managed by three constructed ponds: Northeast Pond (NE Pond), Bredin Pond and Tutt Pond. Surface water from the NE Pond flows to Bredin Pond, which flows into Tutt Pond. Water from Tutt Pond is pumped out for irrigation use on the farmlands located southwest of the Landfill. There is an overflow weir located between Tutt Pond and the Slough that allows for water to discharge from Tutt Pond to the Slough at high water levels.

The Slough does not have any overland outlet drainage points and is drained by the east-west gravity drain that separates the Phase 2 and Phase 3 area.

Precipitation that lands on Site areas outside the limit of waste or Landfill areas with intermediate cover is managed as clean surface water via the Surface Water Management System. The remaining precipitation that lands on the Site (in specific the Landfill areas without intermediate cover and Compost Facility) is managed as leachate.

During large storm events, run-off from the Glenmore Valley can cause excess Site stormwater. Excess run-off may flow into the on-Site ponds or infiltrate into the subsurface. Stormwater and excess run-off that flows onto the southeastern portion of the Site (i.e. from the administrative building area) can follow the drainage pathways that reach Little Robert Lake via a drainage culvert that flows under John Hindle Drive at the south end of the Site. The City reports that very little stormwater drainage has been observed discharging from the Site.

Stormwater that enters the on-Site ponds ultimately flow into Tutt Pond which is equipped with an emergency by-pass system whereby water can be pumped from Tutt Pond via temporary pumps and hoses, across the Compost Facility, and into the drainage system at the south end of the Site. From there water would flow into Little Robert Lake.

Throughout the Site's history, pumping from Tutt Pond to Little Robert Lake has only occurred twice, between April 15 and July 10, 2018 and April 29 to May 28, 2019. Typically, surface water is managed by evaporation or being used for irrigation (as described above).

### 3.4 Geologic Setting

The Site-specific geology presented below is based on a review of technical and investigative reports completed by others and borehole logs provided by the City. Historical investigative locations are presented on **Figure .3**. The available stratigraphic and instrumentation logs for the Site are provided in **Appendix C.1**.

Geology underlying the Site consists of overburden sediments of variable thickness which overlie volcanic and sedimentary bedrock. GHD has simplified the sequency of overburden sediments based on geologic deposition environments to support an understanding of the hydrogeologic function of the Site. Geologic units consist of glaciolacustrine silt and clay deposits which overlie glaciofluvial sands and gravels, which overlie a glacial till unit. Overburden material is primarily found in the valley floor and pinches out towards the sides of the Glenmore Valley. Bedrock underlies the glacial till unit.

Based on these results, four major stratigraphic units are present on Site:

1. Glaciolacustrine silt and clay (Clay Unit)
2. Glaciofluvial sand and gravel (Sand and Gravel Unit)
3. Glacial till (Till Unit)
4. Bedrock (Bedrock Unit)

Three cross-sections were prepared to illustrate the interpreted stratigraphy of the Site. The cross-section map is presented on **Figure 3.4**.

- Cross-section A-A' (**Figure 3.4A**) – stratigraphy in a north to south orientation across the length of the Site.
- Cross-section B-B' (**Figure 3.4B**) – stratigraphy in a west to east orientation across Bredin Pond, Phase 1, and the NE Pond.
- Cross-section C-C' (**Figure 3.4C**) – stratigraphy in a southwest to northeast orientation across the northern portion of the Compost Facility and southern portion of Phase 3.

Additional, historical, cross-sections illustrating the complex geology underlying the Site are presented in **Appendix C.2**.

## Clay Unit

As illustrated in the geologic cross-sections, a Clay Unit up to 15 m in thickness is present underlying the Ponds (Bredin, Northeast and likely Tutt), the Slough, and Compost Facility. The clay unit is not likely present underlying Phase 1 and the northern half of Phase 2. As illustrated on **Figure 3.4A**, the clay unit is relatively thin in the southern end of the Slough. These are glaciolacustrine sediments that include grey laminated (varved) silty clay with trace sand and gravel (USCS classification CH). The silty clays are described as highly plastic, (plasticity index >30%), suggesting that the clay unit may include volcanic ash (SLR, 2011). The trace gravels present within the clay unit are interpreted as dropstones. The silty clay deposits are overlain by more variable glaciofluvial sediments that include silty sands and (generally USCS classification SM, with one sample as SP-SM), lean clays (USCS classification CL), sandy silts (USCS classification ML), and highly plastic silty clays consistent with glaciolacustrine deposits (SLR, 2011).

Historical cross-sections included in **Appendix C.2** illustrate a rise in the Clay Unit along the southern Site boundary. This rise may create a natural berm to restrict very shallow groundwater flow from flowing off-Site. As illustrated in the cross-sections there is some uncertainty in this interpretation. It should be noted that a shallow Clay Unit berm would not prevent migration of impacted groundwater within the underlying geologic units.

A review of the stratigraphic logs for the Site shows occasional seams of more permeable sandy clays or clayey sands within the Clay Unit. The existing geologic data is insufficient to map these seams; however, it is possible that the seams represent preferential pathways for groundwater flow through the Clay Unit.

## Sand and Gravel Unit

Underlying the Clay Unit are glaciofluvial sands and gravels that, where present, range from 0.6 to 10 m in thickness, with the thickest sand and gravel deposits at the north end of the Site and the thinnest deposits at the Slough. The sand and gravel deposits did not appear in every borehole log, suggesting that the Sand and Gravel Unit forms a discontinuous deposit across the Site.

## Till Unit

A glacial till is present underlying the Sand and Gravel Unit (where present) or the Clay Unit. The glacial till which is estimated to range between 1.22 and 25 m in thickness (Gartner Lee Limited., 1990) is interpreted to be present across the Site. The till has been characterized as silty sand with gravel (USCS classification SM) and silty gravel with sand (USCS classification GM). Large (>0.5 m thickness) bedrock boulders were encountered near the base of the till underlying the Slough. Till soils were generally described as being dense to very dense (SLR, 2011). GHD's review of the Site's geology shows that the glacial Till Unit can vary across the Site in composition, density, and hydrogeologic character.

## Bedrock Unit

Bedrock is exposed at ground surface to the north, east, and west of the Site and slopes towards the centre of the Site. Two bedrock units were encountered. Bedrock in the north, centre, and east areas of the Site was formed in the early Cenozoic era and is composed of Kettle River Formation volcanic rocks, including dacite, obsidian, basalt, and breccia (Church, 1981). The bedrock has been described as weathered at and for several meters below its surface (SLR, 2011). A second bedrock unit was encountered below the volcanic rocks in the south, west and northeast areas of the Site and is composed of sedimentary deposits including siltstone, mudstones, and sandstones of the White Lake Formation (Golder, 2014). The White Lake Formation was noted to contain interbedded, light gray fine sand and thin coal lenses in the northeastern area of the Site.

Bedrock at the Site is inferred to have an undulating surface with a depression directly underlying the Slough. The cross-sections do not extend to the flanking mountains (Quail Ridge to the east and Stephens Coyote Ridge to the west) but would illustrate increasing bedrock elevations in both directions. The elevations of these small mountains are 560 and 630 m AMSL, respectively, and the mountains are comprised of thin overburden and bedrock outcroppings. Thus, the bedrock surface in Cross-Sections B-B' and C-C' would rise to form the valley walls. Cross-section B-B' and C-C' are located between Tutt Hill and Bredin Mountain and to the south of Tutt Mountain,

respectively. Bredin Hill and Tutt Mountain appear to form a north to south ridge of elevated bedrock. The City notes the White Lake Formation was encountered in Area 3 of Phase 1 when blasting and quarrying into Bredin Hill. A review of aerial photographs show thin overburden and bedrock outcrops are present over Tutt Mountain and Bredin Hill. Both cross-sections illustrate the interpreted rise in bedrock.

## 3.5 Hydrogeologic Setting

The BC aquifer classification system indicates Aquifer 469<sup>1</sup> and Aquifer 470<sup>2</sup> are present at the Site. The extent of these aquifers is illustrated on **Figure 3.5**. Aquifer 469 is an overburden aquifer composed of sands and gravels with moderate productivity, low vulnerability, and low demand. Aquifer 470 is a bedrock aquifer composed of volcanic rocks likely belonging to the Pentiction Group or Harper Ranch Group (BC Ministry of Environment, 2012). The bedrock of the White Lake Formation is found within the Pentiction Group (Church, 1981 and Hoy, 2021).

In general, the geologic units described in Section 3.4 may be grouped into the following hydrogeologic units identified in brackets:

1. Clay Unit (acts as a leaky aquitard)
2. Sand and Gravel Unit (Aquifer 469)
3. Till Unit (acts as a leaky aquitard)
4. Bedrock (Aquifer 470)

Horizontal groundwater flow at the Site occurs primarily in the Sand and Gravel Unit and the underlying Bedrock Unit. Groundwater flow is interpreted to be generally flowing from north to south, through the Landfill, the Slough, and the Compost Facility towards the mouth of the valley. It is likely that during periods of high precipitation, precipitation falling on the valley walls and mountains/hills to the east and west of the valley follow bedrock topography and flow towards the centre of the Site. Once flow reaches the centre of the Site, it joins the primary flow path to the south.

The Till Unit has a wide range of hydraulic conductivities and is inferred to vary in composition laterally across the Site. The Till Unit is considered a leaky aquitard, a confining unit with areas that transmits water at a very slow rate. The Till Unit partially separates the Sand and Gravel Unit from the Bedrock Unit below it. Flow within the Till Unit may be a combination of horizontal and vertical flow depending on the composition.

A portion of groundwater/leachate recharges the Slough, which acts as a hydraulic sink. From the Slough, groundwater/leachate slowly infiltrates the underlying silt and clay deposits and the Sand and Gravel Unit. A review of the 2022 inferred direction of groundwater flow figures indicate a portion of groundwater that does not recharge the Slough also flows south toward the Site boundary.

A review of the 2022 vertical hydraulic gradients on Site indicates that vertical groundwater flows upwards in the northern area of the Site, as well as near the eastern and western Site boundaries. Slight downward vertical gradients occur in the Slough and compost facility areas, specifically monitoring well nests GL-28, GL-29, GL-34, GL-35 and GL-39.

A detailed description of the Site hydrogeology, specifically hydraulically conductivity testing and horizontal and vertical groundwater flow direction, is presented in Sections 3.5.1 to 3.5.3.

### 3.5.1 Hydraulic Conductivity Testing

In support of this HHCR, GHD completed a field investigation at the Site between July 5 and 8, 2023. The purpose of the field investigation was to perform hydraulic conductivity testing at Site monitoring wells to estimate hydraulic conductivities of the overburden sediments and bedrock underlying the Site.

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<sup>1</sup> British Columbia Groundwater Wells and Aquifers, Aquifer 469 Summary. <https://apps.nrs.gov.bc.ca/gwells/aquifers/469>

<sup>2</sup> British Columbia Groundwater Wells and Aquifers, Aquifer 470 Summary. <https://apps.nrs.gov.bc.ca/gwells/aquifers/470>

GHD completed single wells response testing (SWRT) at 9 monitoring wells installed in the overburden and bedrock. The tests were completed using solid PVC slugs, Solinst™ water level meters, and Solinst™ Levellogger pressure transducers. Barometric pressure was simultaneously recorded using a Solinst™ Barologger pressure transducer.

Each test was completed by inducing a sudden change in the water level and measuring the response of the aquifer within the monitoring well being tested (i.e., measuring the change in water level over time). The water level change was induced by introducing or removing a known volume or “slug” into and out of each well. The change in water level over time is recorded using a pressure transducer installed in the well prior to beginning the test.

Prior to each test, GHD measured and recorded static water levels, removed all dedicated sampling equipment (e.g., tubing) from the monitoring well, and installed a Solinst™ Levellogger pressure transducer. The solid PVC slug was then quickly lowered into the well to displace the static water level. Following this near instantaneous change in static water level, the recovery of water level in the well to at least 90 percent of the total initial displacement was recorded by the pressure transducer. Manual water level measurements were also recorded with a water level meter to validate the pressure transducer measurements.

GHD analyzed the results of the recovery tests using the AQTESOLV® (v. 4.01) software. GHD used monitoring well/borehole specific data along with time-displacement data collected during the SWRT with the Bouwer-Rice (1976) and Hvorslev (1951) solutions for unconfined and confined aquifers to estimate hydraulic conductivity values for each test.

The estimated geometric mean hydraulic conductivities for each monitoring well are included in **Table 3.1**, below. Individual AQTESOLV solution output sheets are provided in **Appendix D**.

**Table 3.2** Estimated Hydraulic Conductivity Values

Monitoring Well ID	Stratigraphy	Screened Unit	Test Type	Analytical Solution	Number of Tests	Geometric Mean Hydraulic Conductivity (m/sec)
<i>Upgradient</i>						
GL-23-1	Sand, compact	Sand and Gravel	Falling and Rising Head	Bouwer and Rice, 1976	4	$1.1 \times 10^{-6}$
GL-24-1	Sand, compact followed by silty sand (till)	Sand and Gravel	Falling and Rising Head	Bouwer and Rice, 1976	4	$9.6 \times 10^{-6}$
GL-41-2	Gravel and silt, trace clay (till)	Till	Falling and Rising Head	Bouwer and Rice, 1976	6	$1.0 \times 10^{-3}$
GL-41-1	Bedrock	Bedrock	Rising Head	Bouwer and Rice, 1976	1*	$3.5 \times 10^{-9}$
<i>Landfill Vicinity</i>						
GL-5-2	Sand followed by gravelly silt (till)	Till	Falling and Rising Head	Bouwer and Rice, 1976	7	$1.2 \times 10^{-4}$
GL-26-2	Clayey silt	Till	Rising Head	Hvorslev, 1951	1**	$6.0 \times 10^{-8}$
GL-34-3	Lean clay, trace sand followed by fat clay, trace sand	Till	Falling and Rising Head	Bouwer and Rice, 1976	6	$7.5 \times 10^{-6}$
GL-35-3	Silty sand with gravel (till)	Till	Falling and Rising Head	Bouwer and Rice, 1976	6	$7.3 \times 10^{-6}$

Monitoring Well ID	Stratigraphy	Screened Unit	Test Type	Analytical Solution	Number of Tests	Geometric Mean Hydraulic Conductivity (m/sec)
<i>Compost Facility Vicinity</i>						
G-L27-1	Bedrock, some fractures	Bedrock	Falling and Rising Head	Hvorslev, 1951	1	$1.4 \times 10^{-6}$
GL-27-2	Silty clay, some sand and gravel (till)	Till	Falling and Rising Head	Bouwer and Rice, 1976	2	$4.3 \times 10^{-10}$
G-L29-2	Sand and silt (till)	Till	Falling and Rising Head	Bouwer and Rice, 1976	1	$5.0 \times 10^{-9}$
G-L40-2	Bedrock	Bedrock	Rising Head	Bouwer and Rice, 1976	1*	$7.9 \times 10^{-8}$
<i>Downgradient</i>						
GL-28-2	Silty sand	Till	Falling and Rising Head	Bouwer and Rice, 1976	4	$1.6 \times 10^{-6}$
GL-39-1	SILT, some sand and gravel	Till	Falling and Rising Head	Bouwer and Rice, 1976	2*	$1.7 \times 10^{-5}$
GL-39-2	SAND, fine to coarse, silty, trace coarse gravel	Sand and Gravel	Falling and Rising Head	Bouwer and Rice, 1976	2*	$1.5 \times 10^{-9}$
GL-42-1	(Till) SAND and GRAVEL, silty	Till	Rising Head	Bouwer and Rice, 1976	1*	$9.2 \times 10^{-9}$
Notes: * completed by SNC, ** completed by Golder						

In 2019, SNC Lavalin completed single wells response tests at monitoring wells GL-39-1, GL-39-2, GL-40-2, GL-41-1, and GL-42-1 (SNC Lavalin Inc., 2020). The hydraulic conductivity estimates are provided in **Table 3.1** for reference.

In summary, the hydraulic conductivity ranges for each unit include:

- Sand and Gravel Unit:  $1.5 \times 10^{-9}$  m/sec to  $9.6 \times 10^{-6}$  m/sec
- Till Unit:  $4.3 \times 10^{-10}$  m/sec to  $1.0 \times 10^{-3}$  m/sec
- Bedrock Unit:  $3.5 \times 10^{-9}$  m/sec to  $1.4 \times 10^{-6}$  m/sec

The Till Unit has a wide range of hydraulic conductivity values, which suggests that the composition of the till varies laterally across the Site. The till is inferred to be a leaky aquitard separating the Sand and Gravel Unit from the Bedrock Unit. Areas where the Till Unit is more permeable and is characterized by a higher hydraulic conductivity estimate may represent preferential pathways for vertical migration of Landfill derived impacts.

## 3.5.2 Horizontal Flow Direction

Groundwater elevations for Site monitoring wells from 2015 through 2022 are presented in **Table 2**. Hydrographs showing groundwater elevations between 2015 through 2022 at the upgradient, landfill vicinity, compost vicinity, and downgradient monitoring wells are presented in **Appendix E**.

The highest groundwater elevations in the overburden are observed at GL-41-3 (located upgradient to the north of the landfill) and GL-15-2 (located upgradient to the southwest west of the landfill). Groundwater elevations at GL-41-3 and GL-15-2 ranged from 448.26 to 449.02 m AMSL, and 448.09 to 448.20 m AMSL in 2022 respectively. The lowest groundwater elevations in the overburden are observed at 09BH06-S, which ranged from 435.67 to 435.76 m AMSL in 2022.

A review hydrographs and historical water elevation data shows that water elevations have been generally consistent over the past eight years with no overall decreasing or increasing trends. The hydrographs show some evidence of seasonal trends in groundwater elevations with high elevations occurring following the spring freshet and is associated with a period of groundwater recharge. This pattern is more apparent in the upgradient monitoring locations and locations in the central portion of the Site. Several of the downgradient monitoring wells have shown a slight increasing trend in groundwater elevations since 2015. These include GL-28-3, GL-28-1, 09BH03 and 09BH06-D. The reason for the increase is unclear.

Horizontal groundwater flow on Site occurs primarily in the Sand and Gravel Unit (Aquifer 469) and the underlying bedrock (Aquifer 470). Groundwater flow is interpreted to be generally flowing from north to south, through the Landfill vicinity, the Slough and the Compost Facility towards the mouth of the valley. It is likely that during periods of high precipitation, precipitation falling on the valley walls and small mountains/hills to the east and west of the valley follow bedrock topography and flow towards the centre of the Site. Once flow reaches the centre of the Site, it joins the primary flow path to the south.

It should be noted that the Sand and Gravel Unit is discontinuous throughout the Site or is unsaturated in portions of the Site and there may be some localized differences in groundwater flow which reflect this.

To illustrate the groundwater flow patterns at the Site, groundwater elevations were used to create groundwater contour maps for March, June, August, and October 2022. Groundwater contours were generated for the Sand and Gravel Unit as shown on **Figure 3.6A** through **Figure 3.6D** and the Till Unit on **Figure 3.7A** through **Figure 3.7D**. Groundwater contours for the Bedrock Unit were not generated due to an insufficient dataset.

The following observations are drawn based on a review of groundwater contour maps:

- Within both the Sand and Gravel Aquifer and Till Unit, the overall groundwater flow direction is to the south following Site topography (i.e., towards the mouth of the valley).
- Within the Sand and Gravel Aquifer, components of flow are directed from topographic high points into the center of the Site where hydraulic gradients are relatively flat. This pattern is not observed within the Till Unit.
- Within the Till Unit, a hydraulic high-point is present in the vicinity of well nest GL-29-1/2. Hydraulic conductivity testing at these wells shows relatively low permeability within the Till Unit. This zone of low permeability is likely to act as a barrier for downward flow which results in the hydraulic high point.
  - As previously described, the composition of the Till Unit varies significantly across the Site. It is likely that other low-permeable areas exist across the Site and that these areas would create localized hydraulic high points. Areas with high permeability are expected to promote flow which may result in localized hydraulic low points.
- Although groundwater flow in bedrock was not mapped, it is anticipated that groundwater flow would follow Site topography. Groundwater in bedrock would flow eastward and westward from the valley walls and flanking mountains/hills and then flow to the south down the valley.

A comparison between groundwater elevations and ground surface in the central portion of the Site shows that groundwater elevations are close to or even above grade. The presence of water elevations above grade supports this interpretation and shows that groundwater discharge to low-lying areas (i.e., the Slough) is likely still occurring particularly during periods of higher groundwater levels such as during the spring freshet. As shown on the geological cross-sections, the groundwater elevations measured in each of the geological units are not that dissimilar. This provides evidence that the Till Unit separating the Sand and Gravel Unit and Bedrock Unit may not provide a significant hydraulic barrier to vertical groundwater migration and is therefore considered a leaky aquitard. Flow within the till unit is inferred to be a combination of horizontal and vertical flow due to lateral variation in grain size across the Site.

### 3.5.3 Vertical Flow Direction

The vertical component of groundwater flow was determined from the nested wells at the Site as shown in Table 3.3 below. Vertical gradients are presented in an upgradient to downgradient and shallow to deep fashion.

Table 3.3 2022 Vertical Gradient Calculations

Nested Wells Location	Location	Hydrogeologic Units	March 2022 (m/m)	June 2022 (m/m)	August 2022 (m/m)	October 2022 (m/m)
GL-1-1 & GL-1-2	North of Phase 1	Till Unit & Till Unit	0.01	0.01	0.01	0.01
GL-41-1 & GL-41-3	North of Phase 1	Bedrock & Till Unit	-0.003	-0.003	-0.005	-0.005
GL-2-1 & GL-2-2	West of Phase 2	Clay Unit	0.08	0.08	0.07	0.06
GL-4-1 & GL-4-2	East of Phase 2	Sand and Gravel Unit & Clay Unit	0.14	0.15	0.13	0.13
GL-5-1 & GL-5-2	West of Phase 2	Till & Bedrock Unit	0.0004	0.0027	-0.0003	0.0002
GL-34-1 & GL-34-3	Phase 3 Slough	Fill and Clay Unit	-0.05	-0.04	-0.04	-0.04
GL-35-1 & GL-35-3	Phase 3 Slough	Fill and Clay Unit	-0.07	-0.10	-0.08	-0.08
GL-8-1 & GL-8-2	West of Phase 3 Slough	Clay Unit & Sand and Gravel Unit	0.07	0.03	0.11	0.11
GL-26-1 & GL-26-2	East of Phase 3	Bedrock & Till Unit	2.14*	2.26*	2.48*	2.32*
GL-26-1 & GL-26-4	East of Phase 3 Slough	Till/Bedrock & Bedrock Unit	0.13	0.14	0.15	0.14
GL-27-1 & GL-27-2	Compost Facility	Bedrock & Clay /Till Unit	0.12	0.13	0.14	0.15
GL-29-1 & GL-29-2	Compost Facility	Sand and Gravel & Till Unit	-0.02	-0.03	-0.02	-0.01
GL-42-1 & GL-42-2	South Perimeter	Till Unit	0.03	Damaged	Damaged	Damaged
GL-39-1 & GL-39-2	South perimeter	Till Unit	-0.01	-0.01	-0.01	-0.01
GL-28-1 & GL-28-2	South of Site	Sand and Gravel & Clay Unit	-0.03	-0.02	-0.02	-0.02
09BH06-D & 09BH06-S	South of Site	Sand and Gravel Unit & Clay Unit	Artesian	Artesian	0.06	0.06

Notes: Positive values are upward gradients; negative values are downward gradients.  
 \* - vertical gradients in GL-26-1/2 are unexpectedly large due to a small difference in screen mid-point elevations and larger differences in water elevations. This results may be anomalous or may indicate

The 2022 vertical hydraulic gradients indicate a spatial pattern where vertical groundwater flows upwards in the northern area of the Site, as well as near the eastern and western Site boundaries. Slight downward vertical gradients are observed in the Slough and Compost Facility, specifically at monitoring well nests GL-28, GL-29, GL-34, GL-35 and GL-39. This may be related to groundwater recharge from the topographic high areas to the north, east, and west of the Site. Historical reporting suggests that minimal vertical groundwater migration is observed near the sidewalls of Glenmore Valley, (Gartner Lee Limited, 1992). Additionally, a downward vertical gradient has been observed at the Site at the GL-6/GL-18, GL-8/GL-16, GL-15, GL-27, and GL-28 well series (Golder Associates Ltd., 2012). With the exception of GL-28, these groundwater monitoring locations are located in the vicinity of the Slough. Monitoring well nest GL28 is located immediately downgradient of the compost facility.

An assessment of Site bedrock hydrogeology completed by Golder Associates and SLR Consulting identified upward hydraulic gradients between the bedrock and overburden sediments and concluded that groundwater within the bedrock acts as a source of recharge for the overlying aquifer (Golder Associates and SLR Consulting, 2015). The 2022 monitoring results generally agree with this assessment. It's important to note that upwards vertical gradient from bedrock to the overburden sediments will prevent downward migration of landfill derived impacts into the Bedrock unit.



Vertical groundwater flow throughout the Site footprint is noted to be upwards provided the leachate level within the Landfill is maintained at an elevation at or below 437 m AMSL (Golder Associates Ltd., 2016). Provided the leachate collections systems are maintained and leachate mounding is prevented within the waste, vertical hydraulic gradients will be directed upwards from the underlying groundwater flow zones into the waste. Leachate mounding could result in a reversal of vertical hydraulic gradients surrounding the waste mound which may promote downward migration of leachate into the subsurface, particularly in the areas where the natural control liner is not present or thin.

### Artesian Conditions

A review of the groundwater elevations between 2012 and 2022, see Table 2, shows artesian conditions (groundwater levels above ground surface) at a number of monitoring locations. As shown in Table 3.4, below, artesian conditions are noted in many of the Phase 3/Slough area, Compost Facility, and downgradient monitoring wells. It is noted that artesian conditions are more prevalent during periods of high precipitation (i.e., March or the spring freshet).

As noted by Golder Associates and SLR, upward hydraulic gradients will limit the downward migration of landfill derived impacts into bedrock. Upward gradients will also limit downward migration of impacts into the overburden sediments.

The following provides a list of the monitoring wells, locations, screened hydrogeologic unit, and frequency of water levels above grade:

**Table 3.4** Wells Characterized by Artesian Conditions

Monitor	Frequency	Site Location	Hydrogeologic Unit
GL-2-2	1 out of 33	West of Phase 2	Clay Unit
GL-8-2	1 out of 34	West of Phase 3/Slough	Clay Unit
GL-42-1	1 out of 9	South Boundary	Till Unit
06BH02	3 out of 18	East of Compost Facility	Sand and Gravel Unit
GL-27-2	3 out of 33	Compost Facility	Till Unit
GL-10-1	4 out of 34	East of Phase 3/Slough	Clay Unit
09BH04	4 out of 9	Downgradient (South of Site)	Sand and Gravel Unit
GL-27-4	4 out of 32	Compost Facility	Surficial fill
GL-32-2	5 out of 7	Phase 3/Slough	Clay Unit/Till Unit
GL-32-3	6 out of 8	Phase 3/Slough	Till Unit
GL-27-3	7 out of 32	Compost Facility	Till Unit
GL-17-2	13 out of 34	Compost Facility	Till Unit
09BH06-D	13 out of 17	Downgradient (South of Site)	Sand and Gravel Unit
GL-8-1	14 out of 34	West of Phase 3/Slough	Sand and Gravel Unit
GL-35-1	18 out of 30	Phase 3/Slough	Fill material/Clay Unit
GL-17-1	25 out of 25	Compost Facility	Bedrock
GL-35-2	25 out of 28	Phase 3/Slough	Clay Unit
GL-27-1	26 out of 26	Compost Facility	Bedrock
GL-2-1	27 out of 33	West of Phase 2	Clay Unit
GL-26-1	27 out of 33	East of Phase 3/Slough	Bedrock
GL-35-3	28 out of 31	Phase 3/Slough	Till

## 4. Environmental Monitoring Program

As reported in the 2022 Annual Water Monitoring Report (Keltech, 2023), water quality at the Site is monitored at least semi-annually through a network of groundwater monitoring wells, leachate collection stations, and surface water monitoring stations.

The network includes groundwater monitoring wells located upgradient, in the vicinity of the Landfill and Compost Facility, and downgradient. The monitoring well network includes several sets of nested wells which monitor groundwater quality and water elevation in the Clay Unit, Sand and Gravel Unit, Till Unit, and Bedrock Unit.

The 2022 environmental monitoring program (EMP) included quarterly leachate quality monitoring at four locations: North Pumphouse Manhole (N. Pumphouse MH), P1 Leachate Manhole 2 (P1 Leachate MH-2), P2-A2 Leachate Manhole, and the South Leachate Wet Well (S. Leachate WW).

Surface water quality is currently monitored quarterly at eight (8) locations: Bredin Pond, the NE Pond, Tutt Pond, the Bubna Slough, the Slough, Slough #2, Little Robert Lake, and Robert Lake. As part of the EMP, background surface water quality is represented by the Bubna Slough, Slough #2, Little Robert Lake, and Robert Lake.

For the purposes of this HHCR, upgradient surface water quality is characterized by Bubna Slough and Slough #2 and downgradient surface water quality is represented by Little Robert Lake and Robert Lake. The remaining locations represent on-Site surface water quality.

The historical monitoring network is presented on **Figure 1.3** and the installation details are presented on **Table 1**. The 2022 EMP network is presented on **Figure 1.4**. The groundwater monitoring well network included in the EMP and referenced throughout this report is summarized in **Table 4.1**, below.

Table 4.1 includes a list of groundwater monitoring wells that are sampled for water quality. It should be noted that depth to water measurements is collected at all available groundwater monitoring wells.

**Table 4.1** Groundwater Quality Monitoring Well Network

Monitoring well ID	Lithology	Hydrogeologic Classification
<b>Upgradient Monitoring Wells</b>		
GL-41-1 (onsite at north Site boundary)	Volcanic bedrock, brown, hard	Bedrock Unit
GL-41-2 (onsite at north Site boundary)	Gravel and silt, trace clay (till)	Till Unit
GL-41-3 (onsite at north Site boundary)	Silt, some clay, sand, and trace silt	Sand and Gravel Unit
GL-23-1 (offsite northeast)	Sand, compact	Sand and Gravel Unit
GL-15-1 (offsite west)	Bedrock	Bedrock Unit
GL-15-2 (offsite west)	Sandy silt and gravel (till)	Till Unit
<b>Landfill Vicinity Monitoring Wells</b>		
GL-2-1 (artesian)	Silty clay followed by silty sand	Clay Unit
GL-2-2	Silty clay	Clay Unit
GL-4-1	Silty gravel and sand	Sand and Gravel Unit / Till Unit
GL-4-2	Silty clay	Clay Unit
GL-5-2	Sand followed by gravelly silt (till)	Till Unit
<b>Slough Monitoring Wells</b>		

Monitoring well ID	Lithology	Hydrogeologic Classification
GL-16-1	Very dense silt to laminated silt (weathered bedrock)	Bedrock Unit
GL-17-1 (artesian)	Bedrock	Bedrock Unit
GL-20-1	Silty sand, some gravel, and traces of clay and cobbles (till)	Till Unit
GL-35-3	Silty sand with gravel (till)	Till Unit
<b>Compost Monitoring Wells</b>		
GL-12-1	Silty sand (till)	Till Unit
GL-27-1 (artesian)	Bedrock, some fractures	Bedrock Unit
GL-27-3	Layered clay followed by silty clay (till)	Clay Unit / Till Unit
GL-29-1	Sand and silt followed by bedrock	Sand and Gravel Unit
GL-29-2	Sand and silt (till)	Till Unit
<b>Downgradient Monitoring Wells</b>		
GL-42-1	Sand and gravel, trace silt (till)	Till Unit
GL-42-2	Clayey silt	Till Unit
GL-39-1	Silt, some sand, clay and gravel (till)	Till Unit
GL-39-2	Silty sand, trace gravel and clay	Sand and Gravel Unit
GL-28-1 (offsite)	Sand, some gravel, bedrock	Sand and Gravel Unit
GL-28-2 (offsite)	Silty sand	Sand within Clay Unit
GL-28-3 (offsite)	Layered silty clay, some sand	Clay Unit
09BH03 (offsite)	Sand, trace silt	Sand and Gravel
09BH06-D (offsite)	Silty sand	Sand and Gravel
Notes: * - monitoring well is included in the groundwater compliance assessment		

## 5. Site Impact Assessment

The following sections provide a discussion of current water quality impacts as a result of the Site activities.

The Site impact assessment focuses on landfill leachate impacts to the surrounding environment under the assumption that the majority of impacts would originate from areas of the Landfill where the natural liner is thin or is not present. Leachate collection and liner systems would mitigate impacts to the underlying aquifer units and the majority of the compost leachate generated at the Compost Facility is collected and managed appropriately. Therefore, impacts to groundwater or surface water quality are most likely attributable to areas of the Landfill where the natural control line is thin or not present.

The section begins by describing the current monitoring program and focuses the discussion of water quality to key leachate impact indicator parameters and applicable water quality standards.

The discussion follows a lines of evidence approach broken out into geographic areas to assess the potential of leachate impacts. Lines of evidence include a comparison of key leachate indicator parameter concentrations between background, leachate, and downgradient groundwater, spatial and temporal distribution of key leachate indicator parameters with a comparison to interpreted groundwater flow paths and an investigation of major ion geochemical patterns.

## 5.1 Indicator Parameters

Historical analytical results, including a full list of parameter concentrations, are presented in **Appendix F**; however, a list of typical water quality indicator parameters has been selected to focus the discussion of water quality. Water quality indicator parameters were selected based on parameters that are typically elevated in landfill leachate and show notable increases in leachate impacted water as well as those that have been observed at elevated concentrations in water at the Site.

Many other analytical parameter concentrations also change in leachate impacted water, but not generally at the high levels of change. GHD has considered several secondary analytical parameters to provide supporting evidence to the key parameters.

Eight indicator parameters have been selected for the site to assess potential impacts to groundwater and surface water quality. The rationale for the leachate indicator parameters is presented in **Table 5.1**, below:

**Table 5.1** Leachate Indicator Parameters

Leachate Indicator Parameter	Rationale
Alkalinity	Alkalinity increases downgradient of landfills primarily due to elevated levels of dissolved carbon dioxide in affected water (produced by the biological breakdown of organic material) causing the dissolution of carbonate from natural geologic materials within the aquifer.
Chloride	Chloride is generally abundant in municipal waste and is formed in part by the degradation of various wastes. Chloride is a very useful leachate indicator parameter as it is not subject to retardation processes and thus migrates at essentially the same rate as groundwater flow. External factors such as road salt and dust suppressant may have impacts on background water quality levels of chloride.
Nitrate (as N) and/or Ammonia (as N)	<p>High concentrations of nitrate are observed when landfill leachate is in an aerobic environment. In this stage, the landfill is in a chemically oxidizing state where oxidized chemical species such as nitrate dominate and oxidized species such as nitrite decrease in concentrations. High concentrations of nitrate are also observed in water impacted by compost facilities.</p> <p>As the landfill enters a reducing state, nitrogen species are reduced to ammonia. Given the age of the historical portion of the Site, higher ammonia may be present.</p> <p>Elevated nitrate and ammonia concentrations can also be associated with compost and agricultural sources. Both should be considered when assessing nitrate and ammonia levels.</p>
Sulphate	<p>Construction and demolition waste landfills often generate elevated concentrations of sulphate in leachate-affected waters due to the abundance of sulphate available from drywall in the waste stream.</p> <p>It is noted that an increase in calcium may also be associated with drywall and can be used as a secondary indicator parameter. However, calcium ions are subject to move complex geochemical process while in groundwater (sorption, precipitation) and may not occur at comparable levels of impact.</p> <p>Potash fertilizer use may also increase sulphate concentrations in groundwater.</p>

Leachate Indicator Parameter	Rationale
Total Dissolved Solids (TDS)	TDS is caused by the increased cations and anions in solution due to the breakdown and dissolution of waste materials and salts.
Boron	Boron occurs naturally in borate minerals; however, it is relatively rare in the natural environment. Boron is an additive in fiberglass and various detergent and cleaning products. Elevated boron may be observed in municipal solid wastes leachate.
Iron and Manganese	Concentrations of metals typically increase in leachate-affected groundwater due to the alteration of redox conditions within the groundwater. The breakdown of dissolved organic matter within leachate consumes dissolved oxygen and related oxygen sources in groundwater and creates reducing conditions. Where conditions are reducing, naturally-occurring iron and manganese oxides within the geologic material are reduced to more soluble forms, which results in an increase in dissolved iron and manganese concentrations.

## 5.2 Applicable Background Concentrations

GHD completed a Site-Specific Background and Compliance Water Quality Review (GHD, 2023) to determine Site-specific background groundwater and surface concentrations and assess water quality compliance at the Landfill. Site-specific background concentrations were determined following CSR Protocol 9 *Establishing Local Background Concentrations in Groundwater*. GHD's technical memo is presented in **Appendix G**.

As presented in the technical memo, Site-specific background concentrations were determined for the parameters that exceeded both the CSR standards and regional background concentrations as well as parameters that are not included in Table 1 of Protocol 9.

The Site-specific background concentrations are listed in **Table 5.2**, below. To support this impact assessment, GHD has calculated Site-specific background concentrations for each of the leachate indicator parameters. These concentrations supplement the background groundwater dataset for the Sand and Gravel Unit background wells (GL-41-3, GL-23-1, and GL-0-3) and the Till Unit background wells (GL-41-2, GL-15-2, and GL-0-2).

**Table 5.2 Overall 95<sup>th</sup> Percentile Background Concentrations in Groundwater**

Exceedance Parameter	Units	Sand and Gravel Unit 95 <sup>th</sup> Percentile Concentration	Glacial Till Unit 95 <sup>th</sup> Percentile Concentration
Chloride	mg/L	556.4	717.4
Nitrate (as N)	mg/L	2.5	n/a
Sulphate	mg/L	763.7	347.6 (maximum*)
Sodium	mg/L	n/a	1,423
Lithium	ug/L	62.2	76.61
Strontium	ug/L	n/a	18,282
Alkalinity, total (as CaCO <sub>3</sub> )	mg/L	1,401.0	n/a
Total Dissolved Solids	mg/L	2,250.0	n/a
Uranium	µg/L	227.7	30.0 (maximum*)
Notes: n/a – not applicable; parameter not assessed as there were no exceedances.			

Exceedance Parameter	Units	Sand and Gravel Unit 95 <sup>th</sup> Percentile Concentration	Glacial Till Unit 95 <sup>th</sup> Percentile Concentration
* Only two values remained after removing outliers from the sulphate and uranium datasets for the glacial till wells. Therefore, it was not possible to calculate 95 <sup>th</sup> percentile concentrations and the maximum of the remaining values was used.			

## 5.3 Applicable Water Quality Standards

The BC Contaminated Site Regulation (CSR) standards are the applicable groundwater quality criteria for the Site (refer to OC Condition 3.7) and supersede previously used Site criteria. The applicability of BCs water quality classes is explained below.

The groundwater quality criteria applicable to the Site include:

- BC CSR Aquatic Freshwater Life (AW)
- BC CSR Drinking Water Use (DW)
- BC CSR Irrigation Water Use (IW)

The BC water quality guidelines (WQGs) were used as the most applicable water quality criteria for Little Robert Lake and Robert Lake. As mentioned in Section 3.3, these surface water bodies are natural alkaline lakes and so are unique environments that aren't necessarily applicable to freshwater aquatic life criteria. However, in the absence of Site-specific criteria, the following BC WQGs were applied:

- BC Water Quality Guidelines (WQG) Aquatic Life Long-Term Chronic (AW LT)
- BC WQG Aquatic Life Short-Term Acute (AW ST)
- BC WQG Irrigation Long-Term Chronic (IW LT)
- BC WQG Irrigation Short-Term Acute (IW ST)

The short-term chronic WQGs are the primary criteria. Where short-term chronic criteria are not available, long-term chronic WQGs were used.

### BC Water Quality Classes

#### BC Contaminated Sites Regulation (CSR)

As outlined in the BC MOE document Protocol 21 the applicability of BC groundwater quality classes depends on the potential for groundwater or surface water at the Site to flow to surface water bodies that may support aquatic life as well as the current and future water uses in the vicinity of the site.

#### CSR AW standards

Protocol 21 states that CSR AW standards apply to sites located within 500 m of an aquatic receiving environment (i.e., a surface water body containing aquatic life) unless it can be demonstrated that the groundwater discharges into a different surface water body (located greater than 500 m from the site) or that groundwater does not migrate to within 500 m of a surface water body that contains aquatic life. Little Robert Lake and Robert Lake are located within 500 m of the south Site boundary and are recharged by groundwater (Little Robert Lake may only become hydraulically connected to groundwater during flooding events) thus each lake represents an aquatic receiving environment.

The AW standards identified in Schedule 3.2 of the CSR apply to groundwater quality at the Site.

#### CSR DW standards

Protocol 21 states that both current and future drinking water use must be considered when determining whether CSR DW standards apply to a site. Future land use in the vicinity of the Site may include potable water supply from Aquifer 469 and Aquifer 470 thus; the drinking water exposure pathway is applicable for the Site.

The DW standards identified in Schedule 3.2 of the CSR apply to groundwater quality at the Site.

### **CSR IW standards**

Similar to drinking water, future groundwater use in the vicinity of the Site may include irrigation. Thus, the irrigation water exposure pathway is applicable for the Site.

The IW standards identified in Schedule 3.2 of the CSR apply to groundwater quality at the Site.

## **BC Water Quality Guidelines (WQG)**

### **WQG AW LT and WQG AW ST standards**

Technical Guidance 15: Concentration Limits for the Protection of Aquatic Receiving Environments (TG15) states that WQGs apply to water quality in aquatic receiving environments [surface water or porewater (i.e., groundwater)] located at or beyond 10 m of the high-water mark. Little Robert Lake and Robert Lake are downstream aquatic life environments and so WQGs apply to surface water samples collected from these lakes. WQGs do not apply to groundwater at the Site compliance wells since these lakes are located greater than 10 m from the Site.

### **WQG IW LT and WQG IW ST standards**

Surface water from the on-Site stormwater ponds is used for irrigation use on the adjacent farmland therefore the IW WQGs are applicable at these ponds. Surface water from Little Robert Lake and Robert Lake are not used for irrigation. These are alkaline lakes and so water quality is not suitable for irrigation therefore IW WQGs do not apply.

## **5.4 Overburden Groundwater Quality**

### **5.4.1 Background Water Quality Assessment**

Background groundwater quality at the Site is represented by monitoring wells installed north and north-east of the Phase 1 area. In the Sand and Gravel Unit this includes: GL-41-3, GL-23-1, and GL-0-3. In the Till Unit this includes monitoring wells: GL-41-2, GL-15-2 and GL-0-2 (historically monitored).

Monitoring wells have been selected to represent background water quality based on the following selection criteria:

- Hydraulically upgradient or cross-gradient of the Landfill footprint and Site activities,
- Historically used as a background location
- Stable water quality with no clear indication of impacts from the Landfill or Site activities
- Screened within a hydrogeologic unit present upgradient and downgradient of the Landfill footprint

Largely, the monitoring wells chosen to represent background are located in a clear upgradient position, north and north-east of the Landfill. Monitoring wells GL-15-2 is located southwest of the Phase 3 area; however, due to groundwater flow directed inward to the landfill, this location is in an upgradient position and is a suitable representative for background.

The locations of the background wells are illustrated on **Figure 1.2**.

There are no background wells screening the shallow silt and clay deposits (i.e., the Clay Unit). Groundwater availability is expected to be low (i.e., low well yield) and of poor water quality due to high fines content. It is recommended that a background well be installed or added to the monitoring program in order to complete a Protocol 9 assessment in the Clay Unit.

Background water quality in bedrock is represented by GL-41-1 (discussed in Section 4.6).

A summary of the available leachate indicator parameter concentrations reported at the upgradient wells are presented in **Table 5.3**, below. Historical results from 2015 to 2022 have been used to derive the ranges below.

Historical water quality data is presented in **Appendix F**. The Background Water Quality Memo, prepared by GHD, dated October 11, 2023, is presented in **Appendix G**.

**Table 5.3** 2015-2022 Concentrations Ranges of Leachate Indicator Parameters in Background Wells

Parameter	Units	Sand and Gravel Unit (Background)				Till Unit (Background)			
		GL-41-3	GL-23-1	GL-0-3	95 <sup>th</sup> Percentile	GL-15-2 <sup>(1)</sup>	GL-41-2	GL-0-2	95 <sup>th</sup> Percentile
Alkalinity, total	mg/L	533 - 622	962 – 1,180	396 – 525	1401.0	650 – 817	533 – 608	255 – 340	1,034
Ammonia, total	mg/L	ND – 0.141	ND – 0.04	ND – 0.274	0.163	ND – 0.0076	ND – 0.174	0.0926 – 0.317	0.221(2)
Chloride	mg/L	250 - 471	31.9 – 35	121 – 154	556.4	214 – 361	232 – 423	6.8 – 71.6	717.4
Nitrate (as N)	mg/L	1.18 – 1.78	ND – 0.066	ND – 1.88	2.5	1.79 – 7.69	1.46 – 2.14	ND - 0.049	82.23
Sulphate	mg/L	108 - 160	376 – 416	293 – 613	763.7	3,730 – 7,190	109 – 175	294 - 349	347.6(2)
TDS	mg/L	1010 – 1,580	1370 – 1,660	1420 – 2,060	2250.0	6,990 – 11,900	986 – 1,410	296 – 1,050	14,593
Boron	mg/L	0.0242 – 0.0322	0.0289 – 0.0379	0.0238 – 0.0377	0.0634	ND – 0.017	0.0236 – 0.0331	ND – 0.0568	0.07596
Iron	mg/L	ND – 0.0136	ND – 0.045	ND – 0.064	0.0801	ND	ND – 0.097	0.113 – 0.225	0.003(2)
Manganese	mg/L	0.00133 – 0.00731	0.00534 – 0.87	ND – 0.00191	1.69	ND – 0.00028	ND – 0.164	0.126 – 0.234	0.000382(2)

Notes: (ND) – non-detect; TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N  
 Boron, iron, and manganese are reported as dissolved concentrations  
 (1) Monitoring well GL-15-2 is located cross-gradient from the landfill footprint and has been previously identified as a suitable background well  
 (2) Only two values remained after removing outliers from the data set. Therefore, it was not possible to calculate 95<sup>th</sup> percentile concentrations and the maximum values was used.

In the Sand and Gravel Unit, background groundwater quality at the Site can be characterized by moderate to high alkalinity, sulphate, TDS concentrations with variable but, overall, moderately elevated chloride concentrations. Chloride is elevated at GL-41-3 and 09BH03 but only slightly elevated at GL-23-1 and GL-0-3. Low concentrations of boron, iron, and manganese are also noted.

Background water quality in the Till Unit can be characterized by elevated concentrations of alkalinity, chloride, nitrate, and sulphate. Concentrations of TDS are significantly elevated.

The presence of elevated concentrations of leachate indicator parameters in background water quality indicates generally poor natural water quality and this needs to be considered when assessing the potential for landfill impacts downgradient of the landfill. Using Protocol 9 is an appropriate approach to assessing water quality at the Site as it considers naturally elevated concentrations in background water quality.



## 5.4.2 Leachate Quality

A leachate management plan (LMP) has been implemented at the Site to provide short and long-term solutions to collect and dispose of leachate. Leachate generated within Phase 1 and Phase 2 areas of the Site is collected using gravity drains that convey leachate through a leachate forcemain, located along the west side of the Site, to the municipal sanitary sewer system. Leachate generated in the Phase 3 (Slough) area is collected via an east-west gravity drain that runs along the boundary between the Phase 2 and Phase 3 area. After flowing to the west, leachate collected from the Phase 3 (Slough) area flows north and is pumped off-Site to the municipal sanitary sewer system.

As previously described, portions of the Site are constructed with a natural control liner system which includes greater than 2 m of in-situ native clay (with hydraulic conductivity values between  $10^{-6}$  and  $10^{-9}$  cm/sec) (Keltech, 2023). The presence of the natural control liner system supports the collection of leachate via gravity drains. However, GHD has noted several areas where this natural or native clay liner is unlikely to be present or is thin. These areas may allow for downward migration of leachate into the underlying subsurface.

Vertical hydraulic gradients at the Site have historically been upwards provided leachate elevations are maintained at or below 437 mAMSL. Meaning groundwater flow, in general, is upwards into the landfill footprint not downwards. Maintaining and continuing to implement the LMP will continue to ensure that leachate levels are maintained, and that a leachate mound does not form in the Site's footprint. This will reduce the long-term risk of leachate impacts downgradient of the Site.

Leachate quality at the Site is currently monitored at four locations within the leachate collection system:

- P2 A2 Leachate MH, located along the west side of Phase 1
  - represents leachate from the lined area within Phase 1
- S Leachate WW, located at southwest corner of Phase 2
  - represents leachate collected from Phase 2 and Phase 3/Slough areas via the east-west gravity drain
- P1 Leachate MH-2, located at the southwest side of Phase 1
  - represents a combination of leachate from the lined area between Phase 1 and Phase 2 and S Leachate Wet Well (WW)
  - N Pumhouse MH, located at the west side of Phase 1
  - represents a composite of collected leachate from across the Site just before leachate flows into Leachate Lift Station #3 and is pumped off-Site

The locations of the leachate monitoring points are presented on **Figure 1.2**. The 2022 concentration ranges of the eight leachate indicator parameters, as well as four secondary parameters, observed at the Site are summarized in **Table 5.4**, below.

**Table 5.4** 2022 Concentrations of Leachate Indicator Parameters

Parameter	Unit	N Pumhouse MH	P1 Leachate MH-2	P2 A2 Leachate MH	S Leachate WW	Median Leachate Concentration	Sand and Gravel Unit 95 <sup>th</sup> Percentile	Till Unit 95 <sup>th</sup> Percentile
Alkalinity, total	mg/L	2,290 – 5,740	4,330 – 10,900	2,450 – 4,550	4,110 – 6,400	4,895	1,401.0	1,034
Ammonia, total	mg/L	23.3 – 52.9	465 – 1,320	69.8 – 212	38.9 – 68.3	69.55	0.163	0.221 <sup>(2)</sup>
Chloride	mg/L	439 – 792	719 – 2,050	934 – 1,480	654 – 859	832	556.4	717.4
Nitrate (as N)	mg/L	ND	ND	ND – 7.7	ND – 0.142	0.05	2.5	82.23
Sulphate	mg/L	754 – 1,850	ND - 451	ND - 410	1,620 – 1,880	602.5	763.7	347.6(2)
TDS	mg/L	4,310 – 9,140	4,670 – 10,300	4,200 – 6200	7,390 – 10,800	7,435	2,250.0	14,593
Boron	ug/L	947 – 1,850	3,310 – 14,800	3,870 – 6170	1,610 – 1,990	2,650	63.4	75.96

Parameter	Unit	N Pumphouse MH	P1 Leachate MH-2	P2 A2 Leachate MH	S Leachate WW	Median Leachate Concentration	Sand and Gravel Unit 95 <sup>th</sup> Percentile	Till Unit 95 <sup>th</sup> Percentile
Iron	ug/L	ND – 32.8	499 – 4,640	1,870 – 136,000	ND – 69.2	299.5	80.1	3 <sup>(2)</sup>
Manganese	ug/L	106 – 311	1,260 – 4,540	1,070 – 3,690	104 – 275	168.5	1,690	0.382 <sup>(2)</sup>

Notes: TDS - total dissolved solids  
Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
Boron, iron, and manganese are reported as dissolved concentrations.  
(2) Only two values remained after removing outliers from the data set. Therefore, it was not possible to calculate 95<sup>th</sup> percentile concentrations and the maximum values was used.

As summarized above, leachate quality at the Site varies between the four leachate sources. In general, concentrations of indicator parameters alkalinity, ammonia, chloride (in comparison to the Sand and Gravel Unit water quality), boron, manganese, and iron are elevated in comparison to background water quality. Median concentrations of nitrate were notably lower within the leachate collection system in comparison to background concentrations. Median concentrations of TDS in leachate were much less than the 95<sup>th</sup> percentile in the Till Unit. Median concentrations of sulphate were only moderately elevated in leachate in comparison to background concentrations in the Till Unit and are less than the 95<sup>th</sup> percentile in the Sand and Gravel Unit. It should be noted that sulphate concentrations in S Leachate WW contains high sulphate concentrations.

In comparison to the typical leachate strength listed in the BC Environmental Monitoring at Municipal Solid Waste Landfills, concentrations of total ammonia and total alkalinity are particularly elevated while chloride is moderately elevated. It should also be noted that concentrations of hardness, total phosphorus (as P), and sodium are elevated in leachate at the Site. Concentrations of BOD and COD are also moderately elevated.

The 2022 leachate quality data shows that leachate at the Site also contains a number of Polycyclic Aromatic Hydrocarbons (PAHs), fatty acids, aggregate hydrocarbons, and Volatile Organic Compounds (VOCs). Organic compounds are not included in the current groundwater or surface water monitoring programs at the Site. In particular, the 2022 monitoring results show elevated levels of BTEX (benzene, toluene, ethylbenzene, and xylene), chlorinated VOCs (1,1-DCA, 1,2-DCA, cis-1,2-DCE, TCE, and vinyl chloride).

With the exception of potentially naturally occurring fatty acids and aggregate hydrocarbons, organic compounds are anthropogenic in origin. These components may provide useful leachate indicator parameters during future water quality assessments. However, the concentrations reported in the 2022 Annual Water Monitoring Report (Keltech Environmental Ltd, 2023) are not significantly elevated and detectable concentrations in the surrounding environment may not exist.

### 5.4.3 Landfill Vicinity Groundwater Quality

Landfill vicinity groundwater quality at the Site is represented by monitoring wells installed within and directly surrounding the landfill in the Phase 1 and Phase 2 areas. In the clay unit this includes monitoring wells: GL-2-2 and GL-4-2. In the Sand and Gravel Unit this includes monitoring well: GL-4-1. In the Till Unit this includes monitoring wells: GL-2-1 and GL-5-2. The locations of the landfill vicinity wells are illustrated on **Figure 1.2**.

A summary of the available 2022 leachate indicator parameter concentrations reported at the landfill vicinity wells are presented in **Table 5.5A** and **Table 5.5B**, below. Each data set is compared to its corresponding 95<sup>th</sup> percentile background concentration. Note that GL-5-2 was only sampled once in 2022.

**Table 5.5A** 2022 Concentrations Ranges of Leachate Indicator Parameters at Landfill Vicinity Wells – Clay Unit and Sand and Gravel Unit

Parameters	Units	Clay Unit		Sand and Gravel Unit	
		GL-2-2	GL-4-2	GL-4-1	95 <sup>th</sup> Percentile
Alkalinity, total	mg/L	233 - 275	719 - 823	520 - 575	1401.0
Ammonia, total	mg/L	ND – 0.085	ND - ND	0.101 – 0.134	0.163
Chloride	mg/L	68.1 – 70.6	36.4 – 41.6	18.2 – 18.8	556.4
Nitrate (as N)	mg/L	ND	ND - ND	ND - ND	2.5
Sulphate	mg/L	465 - 473	440 - 488	507 - 551	763.7
TDS	mg/L	998 - 1030	1410 - 1410	1280 - 1300	2250.0
Boron	mg/L	0.0065 – 0.0084	0.0192 – 0.0217	0.0114 – 0.0124	0.0634
Iron	mg/L	0.0562 – 0.126	0.0063 – 0.0571	<b>0.586 – 0.687</b>	0.0801
Manganese	mg/L	0.135 – 0.311	0.0196 – 0.228	0.0727 – 0.0755	1.69

Notes: TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
 Boron, iron, and manganese are reported as dissolved concentrations  
 Bold text indicates concentrations above the 95<sup>th</sup> percentile criteria

There is insufficient background water quality data to calculate the 95<sup>th</sup> percentile for the Clay Unit; however, a general assessment of the leachate indicator parameters shows similar parameter concentrations in comparison to the Sand and Gravel water quality and Till Unit water quality (below). This provides evidence that landfill derived impacts are minor, if present, in the Clay Unit in the vicinity of the landfill.

In comparison to the 95<sup>th</sup> percentile of background, indicator parameter concentrations are low in the Sand and Gravel Unit in the vicinity of the landfill.

**Table 5.5B** 2022 Concentrations Ranges of Leachate Indicator Parameters at Landfill Vicinity Wells – Till Unit

Parameters	Units	Till Unit		
		GL-2-1	GL-5-2	95 <sup>th</sup> Percentile
Alkalinity, total	mg/L	201 - 227	425	1034
Ammonia, total	mg/L	0.058 – 0.075	ND	0.221 <sup>(2)</sup>
Chloride	mg/L	90.5 - 101	173	717.4
Nitrate (as N)	mg/L	ND - ND	ND - ND	82.23
Sulphate	mg/L	<b>573 - 632</b>	291	347.6 <sup>(2)</sup>
TDS	mg/L	1120 - 1220	1070	14593
Boron	mg/L	0.0077 – 0.0096	0.0248	0.07596
Iron	mg/L	<b>0.954 – 1.02</b>	ND	0.003 <sup>(2)</sup>
Manganese	mg/L	<b>0.112 – 0.119</b>	0.00023	0.000382 <sup>(2)</sup>

Notes: TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
 Boron, iron, and manganese are reported as dissolved concentrations  
 (2) Only two values remained after removing outliers from the data set. Therefore, it was not possible to calculate 95<sup>th</sup> percentile concentrations and the maximum values was used.  
 Bold text indicates concentrations above the 95<sup>th</sup> percentile criteria

Till Unit groundwater in the landfill vicinity is generally lower than or comparable to the 95<sup>th</sup> percentile of background water quality with the exception of sulphate, iron and manganese at GL-2-1. Iron exceedances were also noted at GL-4-1. These exceedances are likely due to naturally poor groundwater quality and potentially minor leachate derived impacts.

## 5.4.4 Phase 3/Slough Groundwater Quality

Slough groundwater quality at the Site is represented by three monitoring wells installed at or near the perimeter of the Slough in the Phase 3 area. In the Till Unit this includes monitoring wells: GL-20-1 and GL-35-3, both on the west Slough perimeter. In the bedrock unit, this includes well GL16-1, located immediately west of the Slough. The locations of these monitoring wells are illustrated on **Figure 1.2**.

A summary of the available 2022 leachate indicator parameter concentrations reported at the Slough wells are presented in **Table 5.6**, below. Each data set is compared to its corresponding 95<sup>th</sup> percentile background concentration. Note that GL-35-3 was only sampled once in 2022.

**Table 5.6** 2022 Concentration Ranges of Leachate Indicator Parameters – Slough Wells

Parameters	Units	Till Unit		
		GL-20-1	GL-35-3	95 <sup>th</sup> Percentile
Alkalinity, total	mg/L	<b>2,820 – 3,130</b>	<b>1,530</b>	1,034
Ammonia, total	mg/L	<b>70.4 – 85.7</b>	<b>1.36</b>	0.221 <sup>(2)</sup>
Chloride	mg/L	370 - 399	344	717.4
Nitrate (as N)	mg/L	ND - ND	ND - ND	82.23
Sulphate	mg/L	172 - 251	<b>2,940</b>	347.6 <sup>(2)</sup>
TDS	mg/L	4,210 – 4,510	6,730	14,593
Boron	mg/L	<b>1.89 – 2.8</b>	0.0588	0.07596
Iron	mg/L	<b>10.2 – 19.4</b>	<b>12.5</b>	0.003 <sup>(2)</sup>
Manganese	mg/L	<b>0.256 – 0.409</b>	<b>0.325</b>	0.000382 <sup>(2)</sup>

Notes: TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
 Boron, iron, and manganese are reported as dissolved concentrations  
 (2) Only two values remained after removing outliers from the data set. Therefore, it was not possible to calculate 95<sup>th</sup> percentile concentrations and the maximum values was used.  
**Bold** text indicates concentrations above the 95<sup>th</sup> percentile criteria

Groundwater in the Till Unit well GL-35-3 has elevated concentrations of some parameters compared to the 95<sup>th</sup> percentile, including alkalinity, ammonia, boron, iron and manganese. Sulphate concentrations at GL-35-3 also greatly exceeded the 95<sup>th</sup> percentile concentration for sulphate, which suggest leachate derived impacts.

Water quality at GL-20-1 is characterized by elevated concentrations of total alkalinity, ammonia, boron, iron, and manganese when compared to the 95<sup>th</sup> percentile background concentrations, suggesting groundwater in the Slough vicinity, particularly in the area surrounding GL-20-1, has moderate leachate-derived impacts. It is also noted that the groundwater at GL-20-1 has been physically described as resembling leachate.

## 5.4.5 Compost Facility Groundwater Quality

Compost Facility groundwater quality in the vicinity of the Compost Facility is represented by monitoring wells GL-27-3 and GL-29-2 (see **Figure 1.2**). As noted in Section 4.1, GL-27-3 is completed partially in the Clay Unit and the Till Unit. GL-29-2 is completed in the Till Unit. Given the low expected permeability of the Clay Unit, GL-27-3 has been considered a Till Unit well for this assessment.

A summary of the available 2022 leachate indicator parameter concentrations reported at the Compost Facility wells are presented in **Table 5.7**, below. Each data set is compared to its corresponding 95<sup>th</sup> percentile background concentration. Note that GL-27-3 was only sampled once in 2022.

**Table 5.7** 2022 Concentrations Ranges of Leachate Indicator Parameters – Compost Facility Vicinity Wells

Parameters	Units	Till Unit		
		GL-27-3	GL-29-2	95 <sup>th</sup> Percentile
Alkalinity, total	mg/L	479	293 – 316	1,034
Ammonia, total	mg/L	0.933	ND – ND	0.221(2)
Chloride	mg/L	585	220 – 232	717.4
Nitrate (as N)	mg/L	ND	ND - ND	82.23
Sulphate	mg/L	10,300	5,030 – 4,710	347.6(2)
TDS	mg/L	20,000	7,590 – 7,680	14,593
Boron	mg/L	0.0324	0.0368 – 0.0231	0.07596
Iron	mg/L	3.94	ND – 0.0223	0.003(2)
Manganese	mg/L	0.466	0.0258 – 0.432	0.000382(2)

Notes: TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
 Boron, iron, and manganese are reported as dissolved concentrations  
 (2) Only two values remained after removing outliers from the data set. Therefore, it was not possible to calculate 95<sup>th</sup> percentile concentrations and the maximum values was used.  
**Bold** text indicates concentrations above the 95<sup>th</sup> percentile criteria

The comparison of indicator parameter concentrations versus the 95<sup>th</sup> percentile background concentrations shows elevated concentrations of ammonia, sulphate, TDS, iron, and manganese at GL-27-3 which is indicative of water quality impacts. The 2022 results from GL-29-2 show elevated levels of sulphate, iron, and manganese while the other indicators are comparable or lower than the 95<sup>th</sup> percentile. This may indicate water quality impacts; however, if present, they are minor.

The Sand and Gravel Unit is discontinuous in the Compost Facility and is generally thin or above the water table where it does exist. There are currently no monitoring wells screened within the Sand and Gravel Unit in the compost facility. A review of the compost facility borehole logs suggests the Sand and Gravel Unit is thickest in the vicinity of historical monitoring well GL-40-2/3 at approximately 441.25 to 446.05 m AMSL, which is likely above the water table at this location.

## 5.4.6 Downgradient Groundwater Quality

Downgradient groundwater quality south of the southern site boundary is represented by monitoring well nest GL-28 and GL-39 (situated along the southern Site boundary north of Little Robert Lake), monitoring well 09BH03 (located in a down to cross-gradient position southeast of the Site boundary), and monitoring well nest 09BH06 (situated west of Robert Lake). Given that these wells are located immediately downgradient of the landfill boundary, water quality impacts may have originated from a combination of leachate from the Phase 1 and Phase 2 area, debris in the Slough, or the Compost Facility. The locations of the landfill vicinity wells are illustrated on **Figure 1.2**.

A summary of the available 2022 leachate indicator parameter concentrations reported at the downgradient vicinity wells are presented in **Table 5.8A** and **Table 5.8B**, below. Note that monitoring well 09BH06-S has not been monitored since 2015 and has therefore not been included in the downgradient water quality analysis. Monitoring wells 09BH03 and 09BH06-D were only sampled during the spring 2022 monitoring event. GL-42 is sampled quarterly; however, only the spring 2022 data was available at the time of writing this report and is sufficient to characterize water quality.

**Table 5.8A 2022 Concentration Ranges of Leachate Indicator Parameters – Downgradient Clay Unit and Sand and Gravel Unit Wells**

Parameter	Units	Clay Unit		Sand and Gravel Unit				
		GL-28-2*	GL-28-3	GL-28-1	GL-39-2	09BH03(1)	09BH06-D	95th Percentile
Alkalinity	mg/L	615 - 621	736 - 782	469 - 477	351 – 394	396 – 525	308	1,401.0
Ammonia	mg/L	ND - ND	ND – ND	0.051 – 0.09	ND – ND	ND – 0.274	0.147	0.163
Chloride	mg/L	57.8 – 62.1	67.2 – 80.8	84 – 93.5	126 – 158	121 – 154	6.5	556.4
Nitrate (as N)	mg/L	10.8 – 13.2	8.24 – 9.3	ND - 0.187	ND – ND	ND – 1.88	0.931	2.5
Sulphate	mg/L	3,120 – 3,160	4,510 – 4,640	2,070 – 2,130	951 – 1,410	293 – 613	294	763.7
TDS	mg/L	5,040 – 5,170	7,210 – 7,700	3,450 – 3,630	1,820 – 1,960	1420 – 2,060	730	2,250.0
Boron	mg/L	0.0164 – 0.0186	ND – 0.221	0.0151 – 0.0179	0.0067 - 0.0075	0.0238 – 0.0377	0.0104	0.0634
Iron	mg/L	ND – ND	ND - ND	0.0068 – 0.19	ND – ND	ND – 0.064	0.378	0.0801
Manganese	mg/L	0.0155 – 0.0204	0.12 – 0.364	0.154 – 0.279	0.00365 - 0.00407	ND – 0.00191	0.162	1.69

Notes: TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
 Boron, iron, and manganese are reported as dissolved concentrations  
**Bold** text indicates concentrations above the 95<sup>th</sup> percentile criteria  
 \* GL-28-2 is located within a sand lense in the Clay Unit

As shown above, there are elevated indicator parameters in GL-28-3 when compared to GL-28-2. This may be due to natural variation as GL-28-2 is screened within a sand lense in the Clay Unit and GL-28-3 is screened directly within the Clay Unit.

The results from the downgradient Sand and Gravel Unit well GL-28-2 shows elevated concentrations of nitrate, sulphate, TDS, and manganese. Slightly elevated levels of chloride in comparison to the 95<sup>th</sup> percentile of background are present at GL-39-2 and 09BH03. The remaining indicator parameter concentrations are generally comparable or lower than background. The comparison above provides evidence that water quality at GL-28-2 has been impacted by Site activities. The presence of chloride at elevated concentrations may indicate some water quality impacts; however, they are minor.

**Table 5.8B 2022 Concentration Ranges of Leachate Indicator Parameters – Downgradient Till Unit Wells**

Parameters	Units	Till Unit			
		GL-39-1	GL-42-1	GL-42-2	95th Percentile
Alkalinity	mg/L	546 – 637	900	1,040	1,034
Ammonia	mg/L	ND – ND	<b>0.624</b>	ND	0.221 <sup>(2)</sup>
Chloride	mg/L	145 – 149	48.6	81.5	717.4
Nitrate (as N)	mg/L	5.88	ND	9.08	82.23
Sulphate	mg/L	<b>2,670 – 2,740</b>	28.2	<b>2,790</b>	347.6 <sup>(2)</sup>

Parameters	Units	Till Unit			
		GL-39-1	GL-42-1	GL-42-2	95th Percentile
TDS	mg/L	4,700 – 4,720	3,380	5,080	14,593
Boron	mg/L	0.0137 – 0.0143	0.0731	0.0348	0.07596
Iron	mg/L	ND – ND	<b>1.82</b>	ND	0.003 <sup>(2)</sup>
Manganese	mg/L	<b>0.0114 – 0.0134</b>	<b>0.139</b>	<b>0.207</b>	0.000382 <sup>(2)</sup>

Notes: TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
 Boron, iron, and manganese are reported as dissolved concentrations  
 (2) Only two values remained after removing outliers from the data set. Therefore, it was not possible to calculate 95<sup>th</sup> percentile concentrations and the maximum values was used.  
**Bold** text indicates concentrations above the 95<sup>th</sup> percentile criteria

With the exception of GL-42-1, Till Unit groundwater quality south of the landfill property is characterized by elevated sulphate and manganese concentrations compared to the 95<sup>th</sup> percentile background water quality. Concentrations of ammonia and iron are elevated in GL-42-1. Other Till Unit indicator parameter concentrations are generally comparable to the 95<sup>th</sup> percentile in background. The collections of elevated parameters may indicate minor landfill-related water quality impacts. It should be noted that the GL-42-1 analytical results for the June 2022 monitoring event are described as being invalid due to surface water infiltration in the City of Kelowna’s *2022 Glenmore Landfill Annual Monitoring Report*. The 2022 analytical results are comparable to the historical monitoring record (June 2020 – June 2021), and as such, the 2022 analytical results were used in the downgradient water quality assessment.

### 5.4.7 Compliance - Groundwater Quality

The allowable contaminate concentrations in groundwater leaving a site need to account for upgradient water quality. Using the guidance provided in Protocol 9, Site-specific 95<sup>th</sup> percentile background concentrations have been calculated for the Sand and Gravel Unit and Till Unit (the monitoring well network does not include appropriate Clay Unit or Bedrock Unit background wells). As described in Section 4.3, an exceedance of the published water quality standards at the Site boundary needs to be confirmed with a comparison to the regional and then Site-specific background water quality. Where parameters exceed published water quality standards and regional and Site-specific background water quality, water quality exceedances are confirmed.

The use of Protocol 9 in assessing water quality leaving a Site is discussed in **Appendix G**.

**Table 5.9**, below, provides a summary of the water quality exceedances reported at the property boundary monitors in the 2022 water quality data set. The table also provides a summary of the exceedances which are confirmed using regional and Site-specific background concentrations.

Table 5.9 2022 Groundwater Compliance Exceedances

Compliance Location	Exceedances of Water Quality Criteria (2022)	Exceedances also above Regional Background Concentrations	Exceedances also above Site-Specific Background Concentrations
<b>Sand and Gravel Unit</b>			
GL-28-1	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(DW)</sup></li> </ul>
GL-28-2	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Nitrate (as N)<sup>(DW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Nitrate (as N)<sup>(DW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Nitrate (as N)<sup>(DW)(MAC)</sup></li> <li>- Sulphate<sup>(DW)(AO)</sup></li> </ul>
GL-39-2	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(DW)</sup></li> </ul>
<b>Glacial Till Unit</b>			
GL-42-2	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>
GL-39-1	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(DW)(AO)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> </ul>
GL-42-1	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> </ul>
<b>Clay Unit</b>			
GL-28-3	<ul style="list-style-type: none"> <li>- Arsenic<sup>(DW)</sup></li> <li>- Cobalt<sup>(DW)</sup></li> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Nickel<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Nickel<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> </ul>



Compliance Location	Exceedances of Water Quality Criteria (2022)	Exceedances also above Regional Background Concentrations	Exceedances also above Site-Specific Background Concentrations
	<ul style="list-style-type: none"> <li>– Nickel<sup>(DW)</sup></li> <li>– Sodium<sup>(DW)</sup></li> <li>– Strontium<sup>(DW)</sup></li> <li>– Uranium<sup>(DW)(IW)</sup></li> <li>– Sulphate<sup>(DW)(AW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>– Uranium<sup>(DW)(IW)</sup></li> <li>– Sulphate<sup>(DW)(AW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>– Uranium<sup>(DW)(IW)</sup></li> <li>– Sulphate<sup>(DW)(AW)</sup></li> </ul>
<p>Notes:</p> <p>DW: Schedule 3.2 Generic Numerical Water Standards Column 6 for the protection of Drinking Water.</p> <p>IW: Schedule 3.2 Generic Numerical Water Standards Column 4 for the protection of Irrigation Water.</p> <p>AW: Schedule 3.2 Generic Numerical Water Standards Column 3 for the protection of Aquatic Life.</p>			

In summary, confirmed water quality exceedances at compliance locations are listed below.

**Groundwater – Sand and Gravel Unit:**

- GL-28-1 (Sulphate)
- GL-39-2 (Sulphate)
- GL-28-2 (Nitrate, Sulphate)

**Groundwater –Till Unit:**

- GL-42-2 (Sulphate, Lithium, Uranium)
- GL-39-1 (Sulphate, Uranium)
- GL-42-1 (Lithium)

**Groundwater –Clay Unit:**

- GL-28-3: (Lithium, Molybdenum, Nickel, Sodium, Uranium, Sulphate)

Based on a comparison of water quality in the vicinity of the Site boundary against the CSR water quality standards, regional and Site-specific background water quality, a number of exceedances are present which may be landfill related. However, after comparing those exceedances to landfill leachate concentrations, the following conclusions were made:

1. The concentration of nitrate, lithium, and uranium reported at GL-28-2, GL-39-1, GL-41-1, and GL-42-2 are greater than the concentrations reported in leachate indicating that landfill leachate is not the cause or not solely the cause of nitrate, lithium, and uranium exceedances in groundwater at the property boundary:
  - a. The concentration of nitrate in leachate ranged from non-detect to 7.7 mg/L in 2022, which is below the CSR DW criteria of 10 mg/L. Nitrate in landfill leachate is below the CSR DW and so the nitrate exceedance at GL-28-2 is not resulting from leachate. Elevated nitrate may be related to the nearby agriculture activities.
  - b. The concentration of lithium in landfill leachate ranged from 31.9 to 290 µg/L in 2022, which is lower than the concentration reported at GL-41-1 (861 µg/L) and GL-42-2 (861 µg/L). As such, landfill leachate cannot solely be the cause of the lithium exceedance at GL-42-2. This is likely related to natural variation in water quality.
  - c. The concentration of uranium in leachate ranged from 1.98 to 32.2 ug/L in 2022, which is well below the concentrations measured at GL-39-1 (244 ug/L) and GL-42-2 (122 ug/L). As such, landfill leachate cannot solely be the cause of the uranium exceedance at GL-39-1 and GL-42-2. This is likely related to natural variation in water quality.
2. Sulphate concentrations in landfill leachate range significantly (<10 mg/L to 1,880 mg/L). Sulphate concentrations from the Phase 3 (Slough) area are elevated and reported at concentrations ranging from 1,620 to 1,880 mg/L in

2022. Groundwater at the property boundary was reported at concentrations ranging from 28.2 mg/L to 4,640 mg/L in 2022. This indicating that the source of sulphate in groundwater may be landfill derived. More elevated sulphate in groundwater at the property boundary in comparison to leachate show that some contribution from natural sources is also occurring.

- Monitoring well GL-28-3 is a shallow well screened in silt and clay. Concentrations of leachate indicator parameters reported at GL-28-3 are elevated above the Landfill Vicinity Clay Unit wells GL-2-2 and GL-4-2; however, without a proper background monitoring well to compare against, it is unclear if the metals exceedances are due to natural variation in the Clay Unit or leachate impacts.

## 5.5 Bedrock Unit Groundwater Quality

The Bedrock Unit groundwater monitoring network and key indicator parameter concentrations are presented in **Table 5.10**, below. Historical water quality results from decommissioned bedrock wells have not been considered when characterizing bedrock groundwater.

As previously described, there are no compliance wells screened in the Bedrock Unit and as such, Bedrock Unit groundwater has not been compared to 95<sup>th</sup> percentile concentrations.

**Table 5.10** 2022 Concentration Ranges of Leachate Indicator Parameters – Bedrock Wells

Parameter	Units	Background Wells		Landfill Vicinity			Compost Vicinity
		GL-41-1	GL-15-1	GL-16-1	GL-17-1	GL-27-1	GL-29-1
Alkalinity, total	mg/L	611 - 623	414	833	1,220 – 1,450	1,270 – 1,570	590 - 617
Ammonia, total	mg/L	ND - ND	ND	0.118	0.3 – 0.347	0.241 – 0.242	0.09 – 0.118
Chloride	mg/L	279 - 297	9.27	130	65.6 – 70.9	36.8 – 37.6	0.62 – 71.2
Sulphate	mg/L	183 - 204	292	1,410	ND – 1.9	13.2 – 17.3	2 - 213
TDS	mg/L	1,160 – 1,240	811	2,790	1,250 – 1,520	1,140 – 1,600	1,240 – 1,250
Boron	mg/L	0.0369 – 0.0391	0.0079	0.0765	0.0831 – 0.0849	0.0674 – 0.0735	0.366 – 0.403
Iron	mg/L	ND – 0.0022	ND	0.235	1.62 – 1.87	0.625 – 0.683	0.121 – 0.156
Manganese	mg/L	0.0018 – 0.00764	0.000794	0.153	0.0496 – 0.0499	0.0829 – 0.0923	0.469 – 0.478

Notes: TDS - total dissolved solids  
 Alkalinity, total is reported as CaCO<sub>3</sub>; ammonia, total is reported as N.  
 Boron, iron, and manganese are reported as dissolved concentrations.  
**Bold** text indicates concentrations that exceed the background concentrations

Background groundwater quality in bedrock is characterized by low concentrations of metals and ammonia with moderate concentrations of alkalinity, sulphate, and TDS.

Since there are no downgradient or compliance bedrock monitoring wells included in the EMP, the bedrock locations presented above were compared to CSR DW standards to assess potential Landfill related impact in Landfill Vicinity and Compost wells, as follows:

- At the background wells, at least one of lithium, sodium, strontium, uranium, and chloride concentrations exceed the CSR DW Standard during the monitoring period. The remaining concentrations were below standard.

- At the Landfill vicinity and Compost Facility wells, at least one of lithium, sodium, strontium, and arsenic concentrations exceed the CSR DW standard during the monitoring period. The remaining concentrations were below standard.
- At Landfill vicinity well GL-16-1, sulphate exceeded the CSR DW standard.

These results suggest that the presence of metals and chloride in Landfill vicinity and Compost Facility wells are not likely Landfill related. As mentioned in previous sections, the presence of sulphate in overburden groundwater may be attributable to Landfill leachate and so the presence of sulphate in bedrock at GL-16-1 (Compost Facility well) may also be landfill derived. A lines of evidence approach was taken to assess bedrock groundwater quality for sulphate:

- The highest sulphate concentrations are at overburden wells GL-27-3 (10,300 mg/L) and GL-29-2 (5,030 to 4710 mg/L), which are both located in the Compost Facility.
- The presence of sulphate in bedrock groundwater at GL-16-1 (1,410 mg/L) is similar in concentration to the neighbouring overburden wells GL-8-1 (1,200 mg/L in 2010) and GL-8-2 (1,900 to 3,200 in 2009-2015). These concentrations exceed the CSR DW standard (500 mg/L).
- Vertical gradients between these wells are variable with flow changing direction from upward to downward depending on the month. Since water elevations are variable between overburden and bedrock (meaning groundwater mixes between these units), the presence of sulphate in bedrock may be attributable to the presence of leachate in overburden.
- As shown in the concentration versus time plot (**Appendix H**), sulphate at GL-16-1 shows a decreasing trend over time. At overburden well GL-35-1, which is in the vicinity, a decreasing trend in sulphate is also occurring. Water quality trends are not apparent at GL-27-3 and GL-29-2.
- Trends for the remaining leachate indicator parameters do not indicate that water quality in bedrock is worsening over time in this area (i.e., no trend or decreasing trends are present).

Based on the above, sulphate in bedrock groundwater is likely attributable to the Landfill. Improvements in water quality is occurring.

## 5.6 Temporal Trends

Temporal trends in groundwater chemistry at the Site are evaluated using concentration versus time plots for each of the key leachate indicator parameter concentrations over time for the upgradient, landfill vicinity, compost vicinity and downgradient wells. Leachate indicator parameters alkalinity, ammonia, boron, chloride, COD, manganese, sulphate and TDS.

As discussed in Section 6.1, concentration versus time plots were created for select upgradient, landfill vicinity, compost vicinity and downgradient monitoring wells, as presented in **Appendix H**. Concentration versus time plots for alkalinity, ammonia, boron, chemical oxygen demand (COD), chloride, manganese, sulphate and TDS are provided. Changes in parameter concentrations are considered on aggregate to identify temporal trends that may indicate landfill derived impacts.

In general, concentrations in groundwater show consistent or decreasing parameter concentrations over time. The following exceptions are noted:

- GL-15-2: Chloride and sulphate concentrations have been increasing since 2011. TDS concentrations increased from 2011 through 2020 but have been decreasing since 2020. GL-15-2 is located upgradient of the Site and cannot be impacted by Site activities.
- GL-12-1: Chloride, OD and manganese concentrations have been increasing since 2013. Increasing ammonia concentrations are also noted since 2019.
- GL-28-2: Sulphate concentrations have been slightly increasing since 2015.
- GL-28-3: Sulphate TDS concentrations have been increasing since 2015.

Increasing trends in leachate indicator parameters can be correlated with the progressive migration of leachate within groundwater. Thus, increasing trends observed at GL-12-1 and GL-28-3 may indicate landfill derived impacts and fit the pattern of southern groundwater flow. The increasing chloride and TDS concentrations are likely derived from road salt use on Glenmore Road N. It should be noted that there is insufficient data to identify meaningful temporal trends in the monitoring wells installed in 2019. Further monitoring is recommended to establish trends.

Monitoring well GL-12-1 was identified in 2022 as having surface water infiltration impacts and was therefore decommissioned. The screened intervals of monitoring wells GL-13-1 (430.7 – 434.0 m AMSL) and GL-17-2 (430.5 – 434.0 m AMSL), in the same vicinity as monitoring well GL-12-1, are both screened with the till at a similar elevation to GL-12-1 (432.9 – 436.0 m AMSL). Groundwater analytical data from monitoring wells GL-13-1- and GL-17-2 can be utilized to assess groundwater quality in the till unit in this area.

## 5.7 Spatial Distribution Plots

The lateral extent of leachate in groundwater was evaluated through the use of chemical spatial distribution plots or isopleths. Leachate indicator parameters (alkalinity, chloride, nitrate, sulphate and TDS) were selected as these parameters provide an important framework for understanding the behaviour of leachate plume evolution.

**Appendix I** presents the isopleths for wells screened in Sand and Gravel Unit, Till Unit and Bedrock Units. The 2022 analytical data from the June and October 2022 monitoring events was averaged for each location to create the isopleths.

**Appendix I** presents the isopleth contours prepared for alkalinity, chloride, nitrate, sulphate and TDS in the Sand and Gravel Unit, Till Unit Sand and Bedrock Units. Gravel, Till and Bedrock units. The following observations are drawn based on the general spatial patterns illustrated in each of the hydrogeologic units.

### Sand and Gravel Unit

Chloride concentrations are highest in the GL-15 well nest, indicating that chloride impacts in the Sand and Gravel Unit are likely derived from road salt use on Glenmore Drive N, as opposed to being landfill derived. Sulphate and TDS concentrations are also highest at the GL-15 well nest, further suggesting off-Site sources of impacts are contributing to water quality alterations in the vicinity of and downgradient of the Site.

The isopleths indicate that in the alkalinity concentrations are highest in the vicinity of the Stage 3, Slough area and attenuate as groundwater flows towards the South.

### Till Unit

Chloride, TDS, and sulphate concentrations are highest in the Till Unit immediately downgradient of the Phase 3 Slough area. Concentrations of these parameters decrease as groundwater flows to the south. GL-35-1, located directly west of the Slough, has the highest alkalinity concentration, with concentrations also decreasing as groundwater flows south.

### Bedrock Unit

The highest concentrations of chloride in the Bedrock Unit are found in upgradient well GL-41-1. This suggests chloride impacts at this location are from off-Site sources. Sulphate is also elevated in the bedrock aquifer at upgradient monitoring wells GL-15-1 and GL-41-1. The spatial distribution plots provide some evidence that the bedrock aquifer has not been impacted by leachate derived impacts. The Bedrock Unit is considered to have little to no leachate derived impacts.

## 5.8 Surface Water Quality

Surface water quality on Site was monitored at eight locations in 2022. These locations include Bredin Pond, the NE Pond, Tutt Pond, the Bubna Slough, the Slough, and Slough #2. Little Robert Lake and Robert Lake are sampled to assess off-Site downgradient surface water bodies. **Table 5.11**, below, provides a comparison of select indicator

parameter concentrations ranges from 2022 compared against the 95<sup>th</sup> percentile background surface water quality calculated from the Bubna Slough and Slough #2.

**Table 5.1** 2022 Concentration Ranges of Leachate Indicator Parameters – Surface Water

Parameter	Units	95 <sup>th</sup> Percentile of Background Surface Water <sup>(1)</sup>	Bredin Pond	NE Pond	Tutt Pond	Slough	L. Robert Lake	Robert Lake
Alkalinity, total (as CaCO <sub>3</sub> )	mg/L	1037	584 – 688	907 – 1,020	652 – 745	1,170 – 2,240	656 – 719	1,290 – 1,930
Ammonia, total (as N)	mg/L	0.0411	ND – 0.16	ND - 0.27	0.03 – 0.33	0.15 – 4.12	0.03 – 0.20	0.09 – 0.22
Chloride	mg/L	812.1	167 – 185	173 – 220	218 – 284	367 – 1,000	82.2 - 120	188 – 350
Nitrate	mg/L	-	ND – 0.011	ND – 0.02	ND	ND	ND	ND
Sulphate	mg/L	1520	203 – 315	513 – 655	605 – 997	1,340 – 3,530	1,810 – 2,930	3,540 – 6,280
Phosphate, total (as P)	mg/L	0.0733	0.10 – 0.20	0.12 – 0.51	0.20 – 0.54	1.34 – 2.05	1.45 – 1.68	2.74 – 3.89
TDS	mg/L	4187	1,030 – 1,270	1,740 – 1,950	1,870 – 2,630	3,760 – 8,760	3,190 – 4,600	6,680 – 11,200
Field Conductivity	uS/cm	6438	1,784 – 2,044	2,640 – 2,915	2,597 – 3,393	2,695 – 11,216	4,227 – 5,528	8,300 – 12,671
Aluminium	mg/L	0.0411	0.0069 - 0.086	0.0582 – 210	0.0822 – 0.283	0.469 – 0.711	0.231 – 7.270	0.242 – 0.848
Arsenic	mg/L	0.00618	0.000699 – 0.00179	0.002 – 0.00411	0.00245 – 0.00478	0.0231 – 0.0475	0.00432 – 0.00898	0.0073 – 0.0121
Boron	mg/L	38.8	0.50 - 1.17	0.05 – 0.07	0.03 – 0.04	0.23 – 0.58	0.03 – 0.03	0.04 – 0.08
Chromium	mg/L	0.000345	0.00026 – 0.00078	ND – 0.00066	0.00032 – 0.00092	0.00172 – 0.00245	0.00054 – 0.0156	ND – 0.00185
Iron	mg/L	0.0785	0.01 – 0.08	0.07 – 0.30	0.09 – 0.43	0.62 – 1.00	0.24 – 10.30	0.26 – 1.06
Manganese	mg/L	0.0552	0.04 – 0.05	0.05 – 0.21	0.06 – 0.20	0.04 – 0.06	0.31 – 2.08	0.06 – 0.21
Uranium	mg/L	0.0329	0.0203 – 0.0245	0.0321 – 0.0403	0.0357 – 0.0535	0.038 – 0.0684	0.0287 – 0.0552	0.0882 – 0.109

Notes: (ND) – Non-detect; **Bold** – concentration is above the 95<sup>th</sup> percentile background.

Metals parameters are reported as total concentrations (aluminum, arsenic, boron, chromium, iron, manganese, and uranium)

<sup>(1)</sup> 95<sup>th</sup> percentile values calculated using Slough #2 and Bubna Slough analytical data

Background surface water quality at the Site (as represented by the Bubna Slough and Slough #2) can be characterized by high alkalinity, chloride, sulphate, and TDS concentrations. Concentrations of metals parameters are slightly elevated as well which, when combined with the general chemistry parameters indicate relatively poor surface water quality which is typical of sloughs. Similar to the groundwater assessment, the use of Protocol 9 is appropriate to assess surface water quality at the Site, to ensure that poor natural upgradient water quality is considered in the surface water assessment, as elevated contaminant concentrations in the upstream surface water adds to the contaminant mass downstream of the landfill.

The following observations are drawn based on the surface water quality comparison presented above:

- Indicator parameter concentrations in the NE Pond and Bredin Pond (located on either side of the Phase 1 area) are generally comparable to or better than background with the exception of occasionally elevated metals parameters. This provides evidence that there are no significant landfill impacts within these surface water bodies.
- Indicator parameter concentrations at Tutt Pond (located west of the Phase 3 area) are elevated in comparison to the NE Pond and Bredin Pond and more parameters are noted above the 95<sup>th</sup> percentile background concentrations. The comparison indicates that some landfill derived impacts maybe present within Tutt Pond.
- As expected, water quality in the Slough is significantly impacted by Site activities (and is managed as leachate). Water quality in the Slough is characterized by elevated TDS, chloride and sulphate concentrations that are significantly higher than background concentrations. Arsenic, aluminium, boron, and iron concentrations in the Slough are all significantly elevated compared to the 95<sup>th</sup> percentile background concentrations.
- Surface water quality at the downgradient receptors Little Robert Lake and Robert Lake are significantly lower than the Slough but many parameters, particularly metals parameters, remain higher than background concentrations and are higher than Bredin Pond and the NE Pond. This is likely due to the concentrative effect of seasonal evaporation on the lake. Both landfill-derived and naturally occurring metals do not evaporate seasonally with the surface water, leaving higher concentrations of metals in the surface water bodies during periods with low water levels. Over time, the cumulative effects of evaporation cycles cause the metal concentrations in surface water to slowly increase over time. Additional discussion on temporal trends in surface water quality is provided below.
- A comparison between the water quality in the two downgradient receptors shows increased parameter concentrations in Robert Lake. Little Robert Lake and Robert Lake are found at elevations of approximately 440 mAMSL and 434 mAMSL. Shallow groundwater in the vicinity of Little Robert Lake and Robert Lake is found between 437 and 436 mAMSL. Artesian conditions and a comparison of groundwater levels and the elevation of Robert Lake show that shallow groundwater is likely discharging into Robert Lake. Little Robert Lake is at an elevation that is higher (by approximately 3 m) than groundwater. Impacts to this lake may originate from the concentrative effect of evaporation cycles on the lake, as well as the occasional overflow from the southeastern corner of the Site which drains beneath John Hindle Drive or from surface water drainage in the ditching along John Hindle Drive.
- To better understand potential contaminant sources and how those sources may drain or flow to Little Robert Lake, it is recommended that the City add additional surface water monitoring locations to the EMP. A surface water monitoring point should be added within the ditch along John Hindle Drive, upstream of the culvert flowing into Little Robert Lake. A second additional surface water monitoring point should be added to characterize surface water runoff from the southeast corner of the Site. This point should be located before the confluence of the John Hindle Drive ditch. It is recognized that surface water flow in these bodies is limited. Monitoring will need to be completed during or immediately after rainfall events.
- In order to understand the potential connection between Little Robert Lake and Robert Lake and as groundwater discharge to Robert Lake may be the cause for increasing water quality issues in the lake, the Robert Lake monitoring point should be relocated to the landfill side of the lake (i.e., the northern end of the lake).

## 5.8.1 Temporal Trends – Surface Water

**Appendix H** includes concentration versus time plots that illustrates concentrations of select analytical parameters reported in the each of the surface water monitoring stations between 2015 and 2022. Concentration versus time plots for alkalinity, ammonia, boron, chemical oxygen demand (COD), chloride, manganese, sulphate, and TDS are provided. Changes in parameter concentrations are considered on aggregate to identify temporal trends that may indicate landfill derived impacts. Increasing trends in leachate indicator parameters are typically correlated with the progressive migration of leachate within groundwater and a thus a useful line of evidence to identify landfill related impacts.

In general, the Concentration versus Time plots show generally consistent concentrations over time. The following exceptions are noted:

- With the exception of ammonia, decreasing trends or improving water quality is seen in the Slough. While improvements in water quality are observed, concentrations are still well above background concentrations and there are notable impacts within the Slough.
- Concentrations of TDS, sulphate, manganese, and COD have followed increasing trends in Little Robert Lake since approximately 2018. Levels of each are now well above background and other landfill vicinity surface water bodies. The increasing trends may indicate landfill derived impacts within the lake are worsening; however, the remaining indicator parameters have remained consistent. Ongoing monitoring is recommended.

**Appendix J.1** presents a plot of Robert Lake water elevations and sulphate concentrations from March 2018 to October 2022 in Little Robert Lake and Robert Lake. **Appendix J-2** presents alkalinity and chloride concentrations with Rober Lake Elevations. The water elevation in Robert Lake fluctuates between 434.8 and 435.3 m AMSL, with the lowest elevations occurring during the late summer and fall months (August through December) and the highest elevations occurring during the winter and spring months (February through June). The sulphate concentration in Robert Lake has inverse relationship with the water elevation in the lake, with the highest sulphate concentrations occurring when water levels are lowest and the lowest concentrations occurring when water levels are highest. This suggests that evaporation has a significant seasonal influence on water quality in the lake. Hot, dry periods with high evaporation concentrate contaminants in the lake, while precipitation and surface runoff during wet periods dilute the contaminants in a cyclical pattern.

It is also noted that since the March 2018 monitoring event, sulphate concentrations have, overall, been increasing steadily in Robert Lake, suggesting a source of impacts in addition to evaporative effects is impacted surface water in the lake. This corresponds with increasing trends in sulphate concentrations in groundwater at the Site's southern/downgradient property boundary. However, the City has provided anecdotal evidence of a longer, 20-year cycle of high and low water levels in Robert Lake. The increasing trend may be related to a longer term trend of evaporation and increasing concentrations in the Robert Lake.

The monitoring wells located between Little Robert Lake, Robert Lake, and the Site boundary are not part of the current water quality monitoring program. It is recommended that monitoring wells 09BH05-S/D and 09BH04 be added to the monitoring program to provide additional spatial data between the lakes and the Site. If monitoring well nest 09BH05-S/D is not accessible, the City should consider adding a replacement monitoring well nest to east of Little Robert Lake. This will give a good spatial distribution of potential impacts flowing south from the Site boundary.

## 5.8.2 Downgradient – Surface Water Quality

Based on the results of the Protocol 9 assessment, several parameters were determined to exceed the applicable surface water quality criteria and the local 95<sup>th</sup> percentile background surface water concentrations at Little Robert Lake and Robert Lake. The parameters that exceeded the applicable water quality criteria and Site-specific background concentrations are summarized in **Table 4.11A** and **Table 4.11B**.

**Table 5.2 2022 Surface Water Compliance Exceedances – Little Robert Lake**

Monitoring Location	Exceedances of Applicable Water Quality Criteria (2022)	Exceedances also above Site-Specific Background Concentrations
Little Robert Lake	<ul style="list-style-type: none"> <li>- Chloride<sup>(IW-ST)</sup></li> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Aluminium<sup>(AW-ST, AW-LT, IW-ST)</sup></li> <li>- Arsenic<sup>(AW-ST)</sup></li> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Field Conductivity<sup>(IW-LT)</sup></li> <li>- Total Alkalinity (as CaCO<sub>3</sub>)<sup>(IW-LT)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Aluminium<sup>(AW-ST, AW-LT, IW-ST)</sup></li> <li>- Arsenic<sup>(AW-ST)</sup></li> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> </ul>
<p>Notes:                      AW-ST: BCWQG Aquatic Life Short-Term Maximum guideline.                      AW-LT: BCWQG Aquatic Life Long-Term Average guideline.                      IW-ST: BCWQG Irrigation Water Short-Term Maximum guideline.                      IW-LT: BCWQG Irrigation Water Long-Term Average guideline.</p>		

**Table 5.3 2022 Surface Water Compliance Exceedances –Robert Lake**

Monitoring Location	Exceedances of Applicable Water Quality Criteria (2022)	Exceedances also above Site-Specific Background Concentrations
Robert Lake	<ul style="list-style-type: none"> <li>- Chloride<sup>(IW-ST, AW-LT)</sup></li> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Ammonia<sup>(AW-ST)</sup></li> <li>- Aluminium<sup>(AW-ST, AW-LT)</sup></li> <li>- Arsenic<sup>(AW-ST)</sup></li> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Molybdenum<sup>(IW-ST, IW-LT)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Total Alkalinity (as CaCO<sub>3</sub>)<sup>(IW-LT)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> <li>- Field Conductivity<sup>(IW-LT)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Total Alkalinity (as CaCO<sub>3</sub>)<sup>(IW-LT)</sup></li> <li>- Aluminium<sup>(AW-ST, AW-LT)</sup></li> <li>- Arsenic<sup>(AW-ST)</sup></li> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Molybdenum<sup>(IW-ST, IW-LT)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> <li>- Field Conductivity<sup>(IW-LT)</sup></li> </ul>
<p>Notes:                      AW-ST: BCWQG Aquatic Life Short-Term Maximum guideline.                      AW-LT: BCWQG Aquatic Life Long-Term Average guideline.                      IW-ST: BCWQG Irrigation Water Short-Term Maximum guideline.                      IW-LT: BCWQG Irrigation Water Long-Term Average guideline.</p>		

As summarized above, there are a number of parameters within Little Robert Lake and Robert Lake that are confirmed exceedances following Protocol 9.

As described in the preceding sections, a large portion of the water quality impact in both Little Robert Lake and Robert Lake are likely due to the concentrative effect of seasonal evaporation. Over time, the effects of evaporation cycles cause concentrations in surface water to slowly increase over time. However, this effect does not explain the overall increasing trends in Lake Robert. The presence of landfill-related sulphate impacts in groundwater at the Site boundary suggests that increasing concentrations of sulphate in Robert Lake maybe related to the landfill. The



presence of artesian conditions in wells adjacent to Robert Lake provide additional evidence that landfill impacted groundwater may be influencing surface water quality.

In addition to impacted groundwater discharging to Robert Lake, impacts may be related to surface water flow into Little Robert Lake which occasionally overflows into Robert Lake.

Additional surface water monitoring is required to identify potential sources of impacts in Little Robert Lake and Robert Lake.

## 5.9 Geochemical Analysis – Piper Plots

A geochemical analysis of water quality data has been completed to support the interpretation of water quality presented in the preceding sections. This analysis includes an assessment of the major ion chemistry across the Site

This analysis builds upon the water quality results through the use of tri-linear Piper plots. Tri-linear Piper plot diagrams present the major ions as percentages which can be used to determine patterns in the geochemical character of water samples. Cations (positive ions) and anions (negative ions) are plotted in two triangles which are projected onto a central diamond. This central diamond presents the data from all major ions at once. Samples with similar geochemical characteristics (i.e., similar major ion percentages) will be located relatively close to one another.

Groundwater monitoring locations that plot in proximity to one another have similar major ion chemistry and thus groupings can be used to determine the likelihood of leachate impact or potentially alternate sources of water quality alterations. Water quality samples that plot in proximity to leachate samples indicate an increased likelihood of being impacted by the landfill. Groundwater monitoring locations that plot in closer proximity to non-impacted locations indicate a decreased likelihood of being impacted by landfill related sources.

**Appendix K** presents Piper plots prepared using the 2022 analytical results for the overburden and bedrock aquifers, as well as surface water monitoring locations.

The following conclusions can be drawn from an analysis of the Piper plots for the overburden monitoring locations (**Appendix K-1** and **Appendix K-2**):

- In general, water quality from the 2022 monitoring period plot in three clusters, one towards the top of the diamond, one in the central portion of the diamond, and one towards the bottom of the diamond.
- Background water quality samples plot in the central portion of the diamond. Waters in this area are classified as mixed type. Monitoring wells which plot with the central cluster have similar major ion chemistry to background and are unlikely to be impacted by leachate. This includes, GL-4-1, GL-4-2, GL-5-2, 09BH03, GL-35-3, and GL-42-2.
- Many of the wells in the landfill vicinity, compost area and downgradient overburden wells plot in the cluster towards the top of the diamond due to higher percentages of chloride, sulphate, calcium and magnesium and lower percentages of bicarbonate. This suggests that the major ion chemistry of these locations has been altered from background.
- Leachate water quality plots towards the bottom of the diamond due to increased percentages of sodium and potassium and alkalinity (as  $\text{CaCO}_2$ );
- The positioning of leachate monitoring results away from the two other primary clusters shows that the major ion chemistry differs between the leachate and groundwater. This provides a good line of evidence that overburden groundwater has not been impacted by leachate or at least has not been impacted to the point of altering the major ion chemistry.
  - However, it should be noted that the leachate quality originated from the collection system in the Phase 1 and Phase 2 areas of the Site. Leachate quality in the Phase 3, Slough, area is not available. Thus, alterations to the overburden groundwater chemistry shown by the Piper plots may be related to the Phase 3 area.
- GL-20-1 and GL-42-1 (both Till Unit wells) plot in the bottom portion of the diamond beyond the leachate samples. Typically, leachate impacted water quality plots between leachate and background.

- Alterations to the overburden groundwater chemistry at GL-20-1 and GL-42-1 may be related to the Phase 3 area or an alternate source (e.g. the Compost Facility).
- The sample collected from GL-42-1 has large charge balance (may be due to lab error or contribution from another ion that is not included in the Piper plot). The placement of this well on the Piper plot is likely unrepresentative.
- The results from GL-20-1 may represent a combination of leachate impacts plus an additional source.

The following conclusions can be drawn from an analysis of the Piper plots for the bedrock locations (**Appendix K-3**):

- The upgradient bedrock wells plot in the central portion of the diamond similar to overburden. Again, this water is classified as mixed type.
- The landfill vicinity monitor, GL-16-1, plots in the central cluster and has similar major ion chemistry to background.
- The fall sample collected from GL-29-1 has large charge balance (may be due to lab error or contribution from another ion that is not included in the Piper plot). The placement of this well on the Piper plot is likely unrepresentative.
- Monitoring wells GL-17-1 and GL-27-1, located immediately downgradient of the Slough, have distinct geochemical characteristics when plotted on a Piper plot. Water in these wells is characterized by a low percentage of chloride anions, higher percentage of bicarbonate alkalinity, and a high sodium and potassium percentage. Water quality in these well is geochemically similar to GL-20-1 and may represent a combination of landfill-derived impacts plus some other source.

The following conclusions can be drawn from an analysis of the Piper plots for surface water locations (**Appendix K-4**):

- Surface water quality plots in the central portion to the right corner of the diamond which is classified as mixed type water and sodium-chloride type water respectively. Background surface water quality from Bubna Slough is found in the central portion of the diamond while the Slough #2 is found towards the right corner of the diamond.
- The samples collected from the Slough and Robert Lake plot in a location similar to Slough #2 and thus have similar major ion chemistry that is different than the remaining surface water monitoring stations.
  - Slough #2 is located north of the Site, does not have a natural outlet (see **Figure 3.2**), and would be subject to evaporative conditions and concentrative effects. As discussed in the preceding section, landfill derived impacts are present in Slough. Similar major ion chemistry between Robert Lake, the Slough, and Slough #2 does not provide a clear indication or pattern that indicates landfill derived impacts in the Robert Lake. The similarities between the major ion chemistry at the three surface water bodies shows how evaporative conditions can mimic landfill derived impacts.
- Little Robert Lake is plotted slight right of the main cluster of surface water monitors due to a higher percentage of sulphate anions. This shows major ion chemistry in Little Robert Lake is dissimilar to Robert Lake and Slough #2 but also dissimilar to upstream location Bubna Slough and the on-Site ponds. This suggests less influence from evaporative conditions. If evaporative conditions influenced water quality in Little Robert Lake, ion percentages would be similar to Robert Lake and Slough #2. Differing major ion percentages from Bubna Slough and the on-Site ponds suggest an alternate source of impacts has influenced water quality in the Little Robert Lake.
- Bubna Slough and the stormwater management ponds surrounding the Site have similar major ion chemistry to one another and plot in the central portion of the diamond. This clustering shows that major ion chemistry is similar between background surface water quality and the three ponds (Bredin Pond, Tutt Pond and the NE Pond). Thus, any Site related impacts in the ponds are not significant enough to alter the major ion chemistry.

## 6. Conceptual Site Model

The Conceptual Site Model (CSM) was developed based on the existing dataset and may need to be updated when new Site information becomes available. Updates should be considered based on evolving water quality at the Site, additional geologic or hydrogeologic information, or changes in the Site operations. The CSM is presented visually on a North-South cross-section, presented on **Figure 6.1** and a West-East cross section, presented on **Figure 6.2**.

The CSM is intended to present a high-level summary of the hydrogeologic functioning of the Site which describes leachate migration in light of the Site's topography, overburden flow zones, bedrock flow zones and nearby receptors (i.e., surface water bodies).

The Site is situated within the Glenmore Valley which runs north-south, parallel to Lake Okanagan with topography on the north, east and west sloping towards the Site. The hydrostratigraphy at the Site is generally described as a glaciolacustrine Clay Unit which contains varying amounts of silt, overlying a discontinuous, glaciofluvial Sand and Gravel Unit, overlying a glacial Till Unit of varying composition. Bedrock beneath the Site has an undulating surface with a depression directly underlying the Slough area and mountains to the east and west of the Site. Bedrock across much of the Site consists of volcanic rock while sedimentary bedrock has been encountered in the south, west and northeast areas of the Site.

A portion of the precipitation falling on the Landfill Phase 1 and Phase 2 will infiltrate through the landfill cover and create leachate. Precipitation falling into Phase 3 (Slough) falls directly into waste and creates leachate. Portions of Phase 1 are completed with geosynthetic liners while the remaining Phase 1, Phase 2, and Phase 3 areas rely on a natural control layer (i.e., the Clay Unit) to limit downward migration of leachate into the subsurface. The Landfill is completed with leachate collection systems which collect and send leachate off-Site for treatment. The leachate management mechanisms will reduce potential for subsurface impacts; however, in areas where the natural control layer is thin or not present, downward migration of leachate into the underlying subsurface may occur which will impact the underlying groundwater flow zones.

The ridges and mountains surrounding the Landfill serve as local groundwater recharge zones in the vicinity of the Site. Precipitation that falls on the mountains and ridges infiltrates the ground surface and flow inwards to the Site. In addition to infiltration from the mountains and ridges, groundwater at the Site is recharged by upgradient flux from the north. A portion of surface water and overland flow will infiltrate the subsurface where the Clay Unit is thin or not present and will slowly infiltrate through the Clay Unit over time as it acts as a leaky aquitard.

Horizontal groundwater flow on Site is interpreted to occur primarily in the glaciofluvial Sand and Gravel Unit (Aquifer 469) and the underlying Bedrock Unit (Aquifer 470). Groundwater flow is interpreted to be controlled by the topography of the region and has a primary flow path from north to south, through the Landfill, the Slough, and the Compost Facility towards the mouth of the valley. Groundwater and surface water runoff from the surrounding mountains and valley walls to the east and west of the Site likely follow bedrock topography and flows towards the centre of the Site. Once flow reaches the centre of the Site, it joins the primary flow path to the south.

The Sand and Gravel Unit is discontinuous throughout the Site or is unsaturated in portions of the Site and there may be some localized differences in groundwater flow which reflect this. The Till Unit has a wide range of hydraulic conductivities and is inferred to vary in composition laterally across the Site. The Till Unit is considered a leaky aquitard, that partially separates the Sand and Gravel Unit from the Bedrock Unit below it. Flow within the Till Unit may be a combination of horizontal and vertical flow depending on the composition.

Groundwater flows to the south towards Little Robert Lake and Robert Lake. Little Robert Lake and Robert Lake are both located within 500 m of the south Site boundary and a comparison of groundwater elevations and lake elevations shows that Robert Lake is recharged by groundwater (Little Robert Lake may only become hydraulically connected to groundwater during flooding events) thus each lake represents a downgradient receiving water body. In addition to the lakes, any downgradient water users should be considered potential receptors.

Upgradient groundwater flowing onto the Site is generally of poor quality with elevated concentrations of several leachate indicator parameters.

Following Protocol 9, it was demonstrated that overburden groundwater concentrations at the south property boundary are higher than background concentrations and exceed the CSR DW standards for a number of analytes in the Sand and Gravel and Till Units. The Site impact assessment presented above shows that minor leachate impacts are likely present in the overburden, immediately downgradient of the Slough, within the Compost facility. Landfill related water quality impacts have resulted in compliance exceedances at the property boundary. The primary analyte of concern is sulphate.

Leachate indicator parameter concentrations at the 09BH06 well nest (located furthest downgradient, west of Robert Lake) are lower in concentration than the compliance wells, with reduced TDS, chloride, and sulphate concentrations. This suggests natural attenuation is occurring off-Site.

The current monitoring program does not include an upgradient well within the Clay Unit and thus a Protocol 9 assessment cannot be completed (90<sup>th</sup> percentile cannot be calculated). Concentrations of leachate indicator parameters reported in the Clay Unit at the downgradient Site boundary result in a number of compliance exceedances which may be Landfill related or may be due to natural variation in water quality.

The current monitoring well network does not include a downgradient/Site boundary well within the Bedrock Unit so a compliance assessment using Protocol 9 cannot be completed. Within bedrock, background groundwater quality is characterized by low concentrations of metals and ammonia with moderate concentrations of alkalinity, sulphate, and TDS. Bedrock groundwater within the Compost Facility appears to be impacted by the Landfill. Impact is less pronounced in bedrock than overburden and water quality is improving over time. No other impacts to bedrock groundwater are observed.

Surface water bodies in the region without inlets or outlets are subject to evaporative conditions which cause seasonal concentrative effects on water quality. During periods of low precipitation, concentrations are observed to increase (i.e., water quality worsens) and during periods of higher precipitation water quality appears improved. Overall, the evaporative effects result in generally poor surface water quality in the sloughs and lakes surrounding the Site. There is anecdotal evidence of long-term, 20-year cycles of evaporation and recharge which may contribute to apparent long-term worsening trends in water quality in surface water bodies in the region.

Site surface water, surface water run-on from the surrounding mountainous terrain, occasional discharge from the McKinley Reservoir, and run-on from areas north of the Site, is captured and managed by three constructed ponds: Northeast Pond (NE Pond), Bredin Pond and Tutt Pond. Surface water captured by the NE Pond flows to Bredin Pond, which flows into Tutt Pond. Water from Tutt Pond is typically allowed to evaporate and/or is pumped out for irrigation use on the farmlands located southwest of the Landfill. There is an overflow weir located between Tutt Pond and the Slough that allows for water to discharge from Tutt Pond to the Slough at high water levels. Tutt Pond is also equipped with an emergency by-pass system whereby water can be pumped from Tutt Pond, across the Compost Facility, and into the drainage system at the south end of the Site. From there water would flow into Little Robert Lake.

Utilizing Protocol 9 to assess surface water quality at the Site show that surface water quality in the on-Site stormwater management ponds is generally comparable to upstream or background surface water. Minor landfill-derived impacts are present in Tutt Pond. There are a number of parameters within Little Robert Lake and Robert Lake that are confirmed exceedances following Protocol 9.

It is unclear what portion, if any, the exceedances in Little Robert Lake or Robert Lake can be attributed to the Landfill. Some lines of evidence (groundwater flow direction, artesian conditions adjacent to Robert Lake, presence of landfill impacts at the Site boundary) suggest that impacts are landfill related. However, potential evaporative conditions or other non-Site related sources may be the cause.

GHD is unable to confirm the source of water quality impacts in Little Robert Lake and Robert Lake (the two downgradient surface water receptors) but is unable to rule out the landfill as a contributing factor. It's likely that a large portion of the impacts, particularly in Robert Lake, are related to evaporative conditions.

Data gaps exist in the current understanding of the Site's hydrologic and hydrogeologic functioning which make understanding potential downgradient impacts difficult. A number of additional monitoring points have been recommended to assist in future HHCR updates.

## 7. Conclusions

The following conclusions are summarized based on the findings of this report:

1. Based on the subsurface field activities, the interpretation of the geologic framework for the Site includes the following major geologic and hydrogeologic units. The hydrogeologic units are in brackets.
  - a. Glaciolacustrine silt and clay deposits (Clay Unit - acts as a leaky aquitard)
  - b. Glaciolacustrine silt and clay deposits (Clay Unit - acts as a leaky aquitard)
  - c. Glaciofluvial sand and gravel (Sand and Gravel Unit - Aquifer 469)
  - d. Glacial till (Till Unit - acts as a leaky aquitard)
  - e. Bedrock - (Bedrock Unit - Aquifer 470)
2. Single well response tests were not completed in wells screened in the Clay Unit. The hydraulic conductivity ranges for the remaining hydrogeologic units, include:
  - a. Sand and Gravel Unit ranges from  $1.5 \times 10^{-9}$  m/sec to  $9.6 \times 10^{-6}$  m/sec
  - b. Till Unit ranges from  $4.3 \times 10^{-10}$  m/sec to  $1.0 \times 10^{-3}$  m/sec
  - c. Bedrock Unit ranges from  $3.5 \times 10^{-9}$  m/sec to  $1.4 \times 10^{-6}$  m/sec.
3. Groundwater flows horizontally towards the centre of the Site from the walls of the valley following topography. Once groundwater reaches the vicinity of the Site, it flows from north to south towards the mouth of Glenmore Valley.
4. The Sand and Gravel Unit is discontinuous throughout the Site. The Till Unit has a varying geologic composition and hydraulic conductivity throughout the Site. For this reason, the Till Unit is considered a leaky aquitard; where the unit is more permeable downward flow to the underlying Bedrock Unit may occur.
5. Generally, groundwater is flowing upward in well nests near the ridge walls and within the Landfill vicinity. Downward groundwater flow occurs in the vicinity of the Slough. Artesian conditions were observed at the 09BH06 well nest (west of Robert Lake) during the March and June 2022 events.
6. Alkalinity, chloride, nitrate and/or ammonia, sulphate, TDS, boron, iron, and manganese were selected as leachate indicator parameters for the Site.
7. Upgradient groundwater is generally of poor quality with elevated concentrations of many leachate indicator parameters.
8. The majority of the wells in the Landfill vicinity and compost area overburden wells contain moderate to elevated concentrations of chloride, sulphate, and TDS.
9. Groundwater in the Sand and Gravel and Till Unit overburden compliance wells have elevated concentrations of sulphate, TDS, nitrate, lithium, and uranium that exceed the CSR DW or IW standards. These concentrations were compared against landfill leachate concentrations, to assess whether exceedances are likely landfill derived or not. Results indicate that sulphate exceedances are Landfill related. However, impacts are relatively minor.
10. The current monitoring network does not include an upgradient monitoring well in the Clay Unit or a Bedrock Unit monitoring well at the downgradient boundary. Thus, a compliance assessment cannot be completed following Protocol 9.
11. Upstream/background surface water is of poor quality with elevated concentrations of many leachate indicator parameters.

12. Some evidence for minor landfill derived impact is present in Tutt Pond. Concentrations are exceeding the IW standards and thus surface water should not be used to irrigate the adjacent farm field.
13. Several lines of evidence suggest that Little Robert Lake and Robert Lake have been impacted by the landfill; however, water quality in both water bodies shows influence from evaporative effects. It is unclear what portion of water quality impacts are related to the Site and what can be attributed to evaporative effects or other non-Landfill related sources. Additional monitoring has been recommended.

## 8. Recommendations

Based on the conclusions of the HHCR, the following recommendations can be made:

### Environmental Monitoring Program

1. Continue the EMP with the following changes:
  - a. Monitor Little Robert Lake and Robert Lake as part of the downgradient/compliance surface water monitoring network instead of background. The 2022 EMP (2022 City of Kelowna Annual Monitoring Report) includes Little Robert Lake and Robert Lake as part of the background surface water monitoring network. This change is recommended because it is unclear what portion of water quality issues is related to the Landfill.
    - i. The monitoring point within Robert Lake should be relocated to the north end of the lake closest to the Landfill.
    - ii. Two additional surface water monitoring points should be added to the EMP to identify potential surface water impacts originating from the ditching along John Hindle Drive and/or from the stormwater management system that services the administration buildings. There is limited surface water flow coming from both areas and thus, sampling/monitoring will need to be completed during or shortly after a precipitation event. One monitoring location should be added along the ditching just upstream of the Site. The second at the discharge point (culvert) which drains stormwater in the southeast corner of the Site.
  - b. An upgradient Clay Unit monitoring well should be added to the routine water quality monitoring program.
  - c. An additional Bedrock Unit monitoring well should be completed along the southern, downgradient Site boundary. This well should be added to the routine water quality monitoring program.
  - d. To better understand the spatial distribution of groundwater quality impacts south of the Site boundary, monitoring well nest 09BH05S/D and monitoring well 09BH04 should be added to the routine water quality monitoring program. GHD understands that well nest 09BH05S/D may not be accessible. The City should consider replacing the well nest with well to the east of Little Robert Lake.

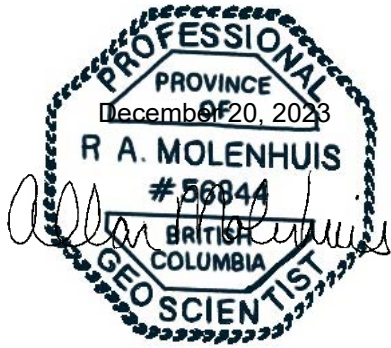
### Future HHCR and Water Quality Assessments

2. As per Section 3.2 of the OC, this HHCR should be submitted the ENV before December 31, 2024.
3. An updated HHCR should be submitted once every ten years (i.e. December 31, 2034).
4. Future annual monitoring reports should include a more detailed assessment of surface water and potential landfill related impacts in Little Robert Lake and Robert Lake. Assessments should incorporate the additional monitoring data recommended above. Future reports should also include an assessment of groundwater quality compliance following Protocol 9.

### Operations

5. Upgrade the Compost facility so runoff from the facility is directed to the Site leachate management system, instead of overland flowing into the Slough.

6. Continue to work towards installing a surface water bypass system to eliminate the need for Tutt Farm irrigation with Tutt Pond water.



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A handwritten signature in cursive script that reads 'Rose Marie Rocca'.

**Rose Marie Rocca, P.Ge**  
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# Tables

**Table 1**  
**Monitoring Well Details**  
**Hydrogeology and Hydrology Characterization Report**  
**Glenmore Landfill**  
**City of Kelowna**

City's Current Monitoring Well ID	Consultant Initial Monitoring Well ID	Monitoring Well		Geodetic Elevations				Screen Details				Drilling				
		UTM Zone 10 N Coordinates		Grade	Piezo	Top of screen	Bottom of Screen	Top of Screen	Bottom of Screen	Screen Length	Lithology	Method	Company	Consultant	Year	Current Status
		Northing	Easting	(m AMSL)	(m AMSL)	(m AMSL)	(m AMSL)	(m bgs)	(m bgs)	(m bgs)						
<b>North and North East of Phase 1</b>																
GL-41-1	GL-41-1	5537673.4	326191.3	449.7	450.6	440.6	439	9.1	10.7	1.6	volcanic bedrock, brown, hard	Sonic Core	VanMars	SNC Lavalin	2019	Active
GL-41-2	GL-41-2	5537673.3	326191.5	449.7	450.6	443.3	442.4	6.4	7.3	0.9	gravel and silt, trace clay (till)	Sonic Core	VanMars	SNC Lavalin	2019	Active
GL-41-3	GL-41-3	5537675.7	326192.7	449.7	450.6	447	445.5	2.7	4.2	1.5	silt, some clay followed by sand, trace silt	HSA	On the Mark	SNC Lavalin	2019	Active
GL-0-1	12-1A	5537338.6	326498.8	449.2	450	429.1	426	20.1	23.2	3.1	sandy clay (till) followed by bedrock	Sonic Core	MudBay	SLR	2012	Decomm in September 2020
GL-0-2	12-1B	5537338.6	326498.8	449	450	435	431.9	14	17.1	3.1	sandy silt, some gravel (suspect till) followed by sand and silt, some clay, trace gravel	Sonic Core	MudBay	SLR	2012	Decomm in September 2020
GL-0-3	12-1C	5537338.6	326498.8	449.42	450.49	439.9	436.9	9.5	12.5	3	trace silt and gravel	Sonic Core	MudBay	SLR	2012	Decomm in September 2020
GL-23-1	GL-23-1	5537307.3	326976.6	446	446.6	437.8	436.3	8.2	9.7	1.5	sand, compact	HSA	Beck	Golder	2007	Active
GL-24-1	GL-24-1	5537291.1	327107.7	446.8	447.6	443.6	441.6	3.2	5.2	2	sand, compact followed by silty sand (till)	HSA	Beck	Golder	2007	Active
GL-1-1	GL-1-1	5537230.4	327134.1	446.3	446.9	435.8	434.3	10.5	12	1.5	silt, some gravel (till)	HSA	-	Gartner Lee	1990	Active
GL-1-2	GL-1-2	5537230.4	327134.1	446.3	447	443.8	440.3	2.5	6	3.5	silty sand followed by sand	HSA	-	Gartner Lee	1990	Active
GL-22-1	GL-22-1	5537429.7	326934.5	449.4	450.3	438.2	436.6	11.2	12.8	1.6	sand, trace silt	HSA	Beck	Golder	2007	Decomm in Sept/Oct 2016
<b>Phase 1</b>																
GL-3-5	12-14	5537050.6	326414.3	457.1	457.4	435.5	433.9	21.6	23.2	1.6	sand and gravel followed by silty clay with sand	Sonic Core	MudBay	SLR	2012	Decomm in 2017
GL-3-1	GL-3-1	5537029.2	326492	-	-	-	-	?	46.9	-	volcanic bedrock	Air Rotary	-	Gartner Lee	1990	Decomm in May 2011
GL-3-2	GL-3-2	5537029.2	326492	-	-	-	-	16.8	18.5	1.7	silty sand some gravel (till)	HSA	-	Gartner Lee	1990	Decomm in May 2011
GL-3-3	GL-3-3	5537029.2	326492	-	-	-	-	0.5	3.5	3	fill followed by silty clay	HSA	-	Gartner Lee	1990	Decomm in May 2011
<b>Phase 2</b>																
GL-6-1 (2011)	GL-6-1 (2011)	5536528.3	326582.8	439.7	440.5	437.9	434.8	1.8	4.9	3.1	Interbedded clay and garbage (municipal solid waste)	Sonic Core	Beck	SLR	2011	Decomm in September 2021
GL-18-1	GL-18-1	5536537.1	326574.7	-	-	-	-	>24	-	-	bedrock	Sonic Core	Beck	SLR	2011	Decomm in May 2011
GL-18-2	GL-18-2	5536537.1	326574.7	442.6	442.9	426.4	423.4	16.2	19.2	3	silty sand	Mud Rotary	Foundex	Golder	2005	Decomm in January 2019
GL-18-3	GL-18-3	5536537.1	326574.7	442.9	442.8	437.5	434.6	5.4	8.3	2.9	landfill refusal	Mud Rotary	Foundex	Golder	2005	Decomm in January 2020
<b>West of Phase 2</b>																
GL-2-1	GL-2-1	5536880.9	326219.1	438.6	439	430.6	429.1	8	9.5	1.5	silty clay followed by silty sand	HSA	-	Gartner Lee	1990	Active
GL-2-2	GL-2-2	5536880.9	326219.1	438.9	439	436.4	432.9	2.5	6	3.5	silty clay	HSA	-	Gartner Lee	1990	Active
GL-5-1	GL-5-1	5536592.3	326175.4	439	440	421	420	18	19	1	crystalline bedrock	Air Rotary	-	Gartner Lee	1990	Active
GL-5-2	GL-5-2	5536592.3	326175.4	439.2	440.1	431.7	429.2	7.5	10	2.5	sand followed by gravelly silt (till)	HSA	-	Gartner Lee	1990	Active
GL-5-3	GL-5-3	5536592.3	326175.4	439.2	440.2	437.2	434.2	2	5	3	silty clay	HSA	-	Gartner Lee	1990	Active
<b>East of Phase 2</b>																
GL-4-1	GL-4-1	5536929.9	326887.8	441.1	441.4	433.4	432.4	7.7	8.7	1	silty gravel and sand	HSA	-	Gartner Lee	1990	Active
GL-4-2	GL-4-2	5536929.9	326887.8	441.1	441.4	439.4	435.9	1.7	5.2	3.5	silty clay	HSA	-	Gartner Lee	1990	Active

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		UTM Zone 10 N Coordinates		Grade	Piezo	Top of screen	Bottom of Screen	Top of Screen	Bottom of Screen	Screen Length	Lithology	Method	Company	Consultant	Year	Current Status
		Northing	Easting	(m AMSL)	(m AMSL)	(m AMSL)	(m AMSL)	(m bgs)	(m bgs)	(m bgs)						
<b>Phase 3 Slough</b>																
GL-34-1	11-26A	5536303.3	326445.5	439.2	440	433.2	431.7	6	7.5	1.5	fat clay (reworked soil, fill) with 7 cm sand lenses	Sonic Core	Beck	SLR	2011	Active
GL-34-2	11-26B	5536303.3	326445.5	439.2	439.7	428.5	427.6	10.7	11.6	0.9	lean clay, trace sand followed by fat clay, trace sand	Sonic Core	Beck	SLR	2011	Active
GL-34-3	11-26C	5536303.3	326445.5	439.3	440.1	425.7	424.8	13.6	14.5	0.9	fat clay (reworked soil, fill) with 10 cm sand lens	Sonic Core	Beck	SLR	2011	Active
GL-30-1	11-13A1	5536286	326746.8	439.2	440	432.6	431.1	6.6	8.1	1.5	0.9 silty sand followed by fat clay	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-30-2	11-13B	5536286	326746.8	439.4	440.7	427.5	426.6	11.9	12.8	0.9	0.9 fat clay	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-30-3	11-13C	5536286	326746.8	439.4	440.6	424.3	423.4	15.1	16	0.9	fat clay (reworked soil, fill) followed by lean clay (native)	Sonic Core	Beck	SLR	2011	Decomm in September 2021
GL-31-1	11-18A1	5536191.5	326639.6	439.4	440.3	432.5	431	6.9	8.4	1.5	0.9 lean clay followed by silt with sand	Sonic Core	Beck	SLR	2011	Active
GL-31-2	11-18B1	5536191.5	326639.6	439.2	440	428.6	427.7	10.6	11.5	0.9	1 silt some sand	Sonic Core	Beck	SLR	2011	Damaged 2020
GL-31-3	11-18C	5536191.5	326639.6	439.5	440.4	425.2	424.2	14.3	15.3	1	fat clay (native) with 1 cm sand lenses	Sonic Core	Beck	SLR	2011	Decomm in September 2021
GL-32-1	11-21A1	5536093.5	326735	438.2	439	433.6	432.1	4.6	6.1	1.5	lean clay with sand lenses followed by silty sand	Sonic Core	Beck	SLR	2011	Decomm in September 2021
GL-32-2	11-21B	5536093.5	326735	437.8	438.7	429.7	428.8	8.1	9	0.9	1 silty sand, trace clay	Sonic Core	Beck	SLR	2011	Decomm in September 2021
GL-32-3	11-21C1	5536093.5	326735	437.8	438.6	427.9	426.9	9.9	10.9	1	fat clay (reworked soil, fill) followed by silty sand with gravel (suspect till)	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-33-1	11-22A	5536202.4	326837.1	439.4	440	433.8	430.7	5.6	8.7	3.1	1.5 silty sand with gravel (suspect till)	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-33-2	11-22B	5536202.4	326837.1	439.5	440.1	430.5	429	9	10.5	1.5	1.5 followed by volcanic bedrock (weak)	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-33-3	11-22C	5536202.4	326837.1	439.5	440.2	427.7	426.2	11.8	13.3	1.5	fat clay (reworked soil, fill) followed by silty sand and lean clay	Sonic Core	Beck	SLR	2011	Active
GL-35-1	11-31A1	5536105.2	326411.2	438.1	439	432	430.5	6.1	7.6	1.5	1.6 lean clay	Sonic Core	Beck	SLR	2011	Active
GL-35-2	11-31B	5536105.2	326411.2	438.1	439	427.5	425.9	10.6	12.2	1.6	1.5 silty sand with gravel (till)	Sonic Core	Beck	SLR	2011	Active
GL-35-3	11-31C	5536105.2	326411.2	438.4	439.3	425.1	423.6	13.3	14.8	1.5	fat clay (reworked soil, fill) followed by fat clay (native) with cm sand	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-36-1	11-3A	5536496.4	326764.1	439.2	439.8	433.7	430.7	5.5	8.5	3	fat clay (native), trace sand followed by sandy silt	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-36-2	11-3B	5536496.4	326764.1	439.3	440	429.1	427.6	10.2	11.7	1.5	interbedded silt clay and garbage followed by clay, silty layers with wood chunks	Sonic Core	Beck	SLR	2011	Decomm in Oct 2019
GL-37	12-11	5536489.1	326646.4	439.3	440.1	437.5	431.4	1.8	7.9	6.1	interbedded silt clay and garbage followed by fat clay (reworked soil, fill). No recovery below 5 m.	Sonic Core	MudBay	SLR	2012	Decomm in 2017
GL-38	12-10	5536488.9	326634.4	439.3	440.1	437.5	431.5	1.8	7.8	6		Sonic Core	MudBay	SLR	2012	Decomm in 2017
<b>West of Phase 3 Slough</b>																
GL-8-1	GL-8-1	5535944.5	326391.9	438.8	439.7	431.3	429.8	7.5	9	1.5	sand, some gravel	HSA	-	Gartner Lee	1990	Active
GL-8-2	GL-8-2	5535944.5	326391.9	438.8	439.6	438.3	434.8	0.5	4	3.5	clay	HSA	-	Gartner Lee	1990	Active
GL-14-1	GL-14-1	5536265	326258.7	453.3	453.8			>8			bedrock	Mud Rotary	Foundex	Golder	2005	Decomm in 2016
<b>East of Phase 3 Slough</b>																
GL-7-1	GL-7-1	5536434.3	326891	439	439.7	436	435.5	3	3.5	0.5	weathered bedrock clayey silt followed by bedrock, some fractures	Air Rotary	-	Gartner Lee	1990	Active
GL-26-1	09-2-1	5535984.6	326863.3	440.9	441.4	435.8	434.3	5.1	6.6	1.5	clayey silt, trace sand and gravel	Odex	-	Golder	2009	Active
GL-26-2	09-2-2	5535984.6	326863.3	440.7	441.6	437	435.5	3.7	5.2	1.5	silty gravelly sand followed by layered clayey silt	HSA	-	Golder	2009	Active
GL-26-3	09-2-3	5535984.6	326863.3	440.7	441.5	438.6	437.3	2.1	3.4	1.3	3 bedrock	SSA	-	Golder	2009	Active
GL-26-4	09-2-4	5535984.6	326863.3	440.7	441.5	417.8	414.8	22.9	25.9	3	5.5 silty clay, some sand and gravel	Odex	-	Golder	2009	Active
GL-10-1	GL-10-1	5535933	326821.6	438.4	439.4	435.5	430	2.9	8.4	5.5	4.6 fat clay (reworked soil, fill)	HSA	-	Gartner Lee	1990	Active
12-16	12-16	5536514.5	326448.7	-	-	-	-	6.1	10.7	4.6	3 sand and gravel with silty clay (till)	HSA	On the Mark	SLR	2012	Decomm in 2012
GL-25-1	09-1-1	5536149	327105.1	458.3	459	443.7	440.7	14.6	17.6	3	1.5 interbedded clay and silty clay	Odex	-	Golder	2009	Decomm in 2016
GL-25-2	09-1-2	5536149	327105.1	458.3	459.108	456.5	455	1.8	3.3	1.5		SSA	-	Golder	2009	Decomm in 2016

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		UTM Zone 10 N Coordinates		Grade	Piezo	Top of screen	Bottom of Screen	Top of Screen	Bottom of Screen	Screen Length	Lithology	Method	Company	Consultant	Year	Current Status
		Northing	Easting	(m AMSL)	(m AMSL)	(m AMSL)	(m AMSL)	(m bgs)	(m bgs)	(m bgs)						
<b>Compost Facility - South of Phase 3 Slough</b>																
GL-27-1	09-3-1	5535841.1	326462.8	438.7	441.6	415.1	413.6	23.6	25.1	1.5	bedrock , some fractures silty clay, some sand and gravel	Odex	-	Golder	2009	Active
GL-27-2	09-3-2	5535841.1	326462.8	438.7	440.8	428.2	426.7	10.5	12	1.5	(till) layered clay followed by silty clay,	SSA	-	Golder	2009	Active
GL-27-3	09-3-3	5535841.1	326462.8	438.6	440.8	430.2	428.7	8.4	9.9	1.5	some sand and gravel (till)	HSA	-	Golder	2009	Active
GL-27-4	09-3-4	5535841.1	326462.8	438.7	440.6	437.9	436.9	0.8	1.8	1	sandy gravelly silt (fill)	SSA	-	Golder	2009	Active
GL-17-1	GL-17-1	5535791.4	326494.6	439.2	440.3	-	-	>18	-	-	bedrock	Mud Rotary	Foundex	Golder	2005	Active
GL-17-2	GL-17-2	5535791.4	326494.6	439.2	439.8	434.4	431.4	4.8	7.8	3	silty gravelly sand (till)	Mud Rotary	Foundex	Golder	2005	Active
GL-13-1	GL-13-1	5535791.4	326494.6	-	439.8	-	-	4.6	7.6	3	silty sand with gravel (till)	HSA	-	Gartner Lee	1998	Active
GL-12-1	GL-12-1	5535729.1	326538.3	441.3	442.3	435.2	432.2	6.1	9.1	3	silty sand (till)	HSA	-	Gartner Lee	1998	Active
GL-29-1	12-4A	5535749.3	326652.7	443.9	445.1	402.4	399.4	41.5	44.5	3	sand and silt followed by bedrock	Sonic Core	MudBay	SLR	2012	Active
GL-29-2	12-4B	5535749.3	326652.7	443.9	444.8	436	432.9	7.9	11	3.1	sand and silt (till)	Sonic Core	MudBay	SLR	2012	Active
<b>West of Compost Facility</b>																
GL-15-1	GL-15-1	5535905.1	326176.5	452	452.3	-	-	>12	-	-	bedrock	Mud Rotary	Foundex	Golder	2005	Active
GL-15-2	GL-15-2	5535905.1	326176.5	451.7	452	448.6	445.6	3.1	6.1	3	sandy silt and gravel (till)	Mud Rotary	Foundex	Golder	2005	Active
<b>East of Compost Facility</b>																
06BH02	06BH02	5535672.4	327122.8	445.6	445.4	437.6	434.6	8	11	3	clay followed by sand and gravel	HSA	Kamloops	EBA	2006	Active
<b>South Perimeter of Site</b>																
GL-39-1	GL-39-1	5535296.8	326790.4	439.5	440.4	430.7	429.5	8.8	10	1.2	silt, some sand, clay and gravel (till)	HSA	On the Mark	SNC Lavalin	2019	Active
GL-39-2	GL-39-2	5535297.6	326789.1	439.6	440.5	435.3	433.5	4.3	6.1	1.8	silty sand , trace gravel and clay	HSA	On the Mark	SNC Lavalin	2019	Active
GL-39-3	GL-39-3	5535298.3	326787.8	439.6	440.6	438.1	436.6	1.5	3	1.5	silty clay, some sand sand and gravel, trace clay and silt	HSA	On the Mark	SNC Lavalin	2019	Active
GL-40-1	GL-40-1	5535525.2	326465.2	449.7	450.5	446.7	445.1	3	4.6	1.6	(till)	HSA	On the Mark	SNC Lavalin	2019	Active
GL-40-2	GL-40-2	5535523.8	326466.4	449.6	450.4	435	433.4	14.6	16.2	1.6	volcanic bedrock, brown, hard clay and silt, some sand, trace	Sonic Core	VanMars	SNC Lavalin	2019	Decomm in September2021
GL-40-3	GL-40-3	5535523.7	326466.2	449.6	450.4	439.8	438	9.8	11.6	1.8	gravel (till)	Sonic Core	VanMars	SNC Lavalin	2019	Decomm in September2021
GL-42-1	GL-42-1	5535422.7	326636.2	447.6	448.4	429.3	427.7	18.3	19.9	1.6	sand and gravel, trace silt (till)	Sonic Core	VanMars	SNC Lavalin	2019	Active
GL-42-2	GL-42-2	5535422.6	326636.2	447.6	448.4	437.5	436	10.1	11.6	1.5	clayey silt	Sonic Core	VanMars	SNC Lavalin	2019	Active
GL-42-3	GL-42-3	5535423.9	326637.6	447.7	448.5	441	439.2	6.7	8.5	1.8	sand, gravel and cobbles (till)	Sonic Core	VanMars	SNC Lavalin	2019	Active
09BH01	09BH01	5535385.2	326712.8	-	-	-	-	-	-	-	-	SSA	Beck	SLR	2011	Decomm in Aug 2011
<b>South and South East of Site</b>																
09BH05-S	09BH05-S	5535090.7	326805.6	-	-	-	-	11.2	14.2	1.8	silty sand	HSA	Kel	EBA	2009	Inaccessible
09BH05-D	09BH05-D	5535090.7	326805.6	-	-	-	-	22	23	1.8	sand, some gravel, trace silt	HSA	Kel	EBA	2009	Inaccessible
09BH06-S	09BH06-S	5534457.6	326917.6	435.9	435.9	431.9	430.4	4	5.5	1.8	silty clay	HSA	Kel	EBA	2009	Active
09BH06-D	09BH06-D	5534457.6	326917.6	435.6	435.8	428.6	425.6	7	10	1.8	silty sand	HSA	Kel	EBA	2009	Active
09BH07	09BH07	5535293.6	327214.6	440.9	441	434.4	431.4	6.5	9.5	1.8	sand, trace silt	HSA	Kel	EBA	2009	Damaged 2020
09BH03	09BH03	5535064.2	327413.6	440.8	441	434.7	431.7	6.1	9.1	1.8	sand, trace silt	HSA	Kel	EBA	2009	Active
09BH04	09BH04	5535008.4	327178.2	436.2	436.4	425	422	11.2	14.2	1.8	sand and gravel, trace clay sand, some silt followed by gravel,	HSA	Kel	EBA	2009	Active
GL-28-1	09-4-1	5535273.8	326721.5	442.1	442.1	424.6	423.1	17.5	19	1.5	some sand, trace silt	Odex	-	Golder	2009	Active
GL-28-2	09-4-2	5535273.8	326721.5	441.4	441.8	435.9	434.4	5.5	7	1.5	silty sand	HSA	-	Golder	2009	Active
GL-28-3	09-4-3	5535273.8	326721.5	441.4	441.7	438.9	437.4	2.5	4	1.5	layered silty clay, some sand	SSA	-	Golder	2009	Active

Notes:  
Source: 2022 Annual Water Monitoring Report for Glenmore Landfill (Keltech Environmental, March 24, 2023)  
- - no data  
HSA - hollow stem auger  
SSA - solid stem auger

**Table 2**  
**Hydraulic Elevation Monitoring Results**  
**Hydrogeology and Hydrology Characterization Report**  
**Glenmore Landfill**  
**City of Kelowna**

Well ID	Monitoring Well UTM Zone 10 N Coordinates		Geodetic Elevations Grade (m AMSL)		Date																			
					Piezo (m AMSL)		3/17/2015	6/4/2015	8/27/2015	11/2/2015	3/22/2016	5/16/2016	9/16/2016	11/24/2016	3/21/2017	6/5/2017	8/16/2017	9/22/2017	11/14/2017	3/16/2018	5/25/2018	8/30/2018	11/16/2018	3/21/2019
					Northing	Easting	(m AMSL)	(m AMSL)																
GL-0-1	5537338.6	326498.8	449.20	450.00	444.11	444.20	444.21	444.21	444.36	444.69	444.91	444.93	444.93	445.45	445.62	445.63	445.66	445.62	446.34	446.86	446.73	446.51		
GL-0-2	5537338.6	326498.8	449.00	450.00	440.94	440.85	440.75	440.70	440.86	440.94	440.99	441.00	441.07	441.31	441.35	441.31	441.28	441.40	441.83	443.05	442.59	442.62		
GL-0-3	5537338.6	326498.8	449.42	450.49	440.90	440.79	440.69	440.64	440.80	440.88	440.92	440.93	441.01	441.24	441.29	441.24	441.22	441.35	441.58	443.06	442.58	442.59		
GL-1-1	5537230.4	327134.1	446.30	446.90	445.08	444.92	444.46	444.57	445.45	445.57	444.82	445.07	445.44	445.85	444.82	444.69	444.84	445.73	445.76	444.81	445.36	445.67		
GL-1-2	5537230.4	327134.1	446.30	447.00	444.99	444.84	444.39	444.54	445.35	445.51	444.74	444.99	445.37	445.67	444.74	444.61	444.81	445.69	445.65	444.73	445.25	445.58		
GL-2-1	5536880.9	326219.1	438.60	439.00	438.79	438.76	437.46	438.05	438.89	438.64	438.22	438.65	439.00	438.97	438.61	438.55	438.85	439.00	438.88	438.69	439.00	439.00		
GL-2-2	5536880.9	326219.1	438.90	439.00	438.59	438.58	437.72	437.95	438.76	438.38	437.76	438.41	438.56	438.84	438.19	438.24	438.69	438.87	438.61	438.48	438.81	436.59		
GL-3-5	5537050.6	326414.3	457.10	457.40	439.18	439.10	439.01	439.03	439.02	439.20	439.15	439.11	439.34	Decommisione	-	-	-	-	-	-	-	-		
GL-4-1	5536929.9	326887.8	441.10	441.40	440.06	440.21	439.99	440.04	440.25	440.25	440.07	440.07	440.34	440.23	440.08	440.07	440.16	440.55	440.44	439.82	439.99	440.15		
GL-4-2	5536929.9	326887.8	441.10	441.40	439.75	439.70	439.52	439.59	439.78	439.72	439.60	439.66	440.68	440.53	439.95	439.99	440.24	440.72	439.80	439.33	439.51	439.65		
GL-5-1	5536592.3	326175.4	439.00	440.00	438.59	438.62	437.51	437.49	438.67	438.53	437.93	438.43	438.59	438.96	438.49	438.41	438.69	438.99	438.87	438.56	438.84	438.91		
GL-5-2	5536592.3	326175.4	439.20	440.10	438.59	438.63	437.47	437.51	438.65	438.50	437.89	438.48	438.63	438.95	438.44	438.39	438.71	438.99	438.84	438.56	438.82	438.87		
GL-5-3	5536592.3	326175.4	439.20	440.20	438.57	438.61	437.34	437.33	438.61	438.43	437.81	438.44	438.58	438.89	438.38	438.35	438.70	438.94	438.81	438.53	438.81	438.86		
GL-6-1 (2011)	5536528.3	326582.8	439.70	440.50	437.89	437.87	437.56	437.56	437.93	437.89	437.70	437.82	438.16	438.40	438.07	437.90	437.90	438.43	438.52	437.54	437.97	438.36		
GL-7-1	5536434.3	326891	439.00	439.70	438.05	438.11	437.81	437.84	438.14	438.13	437.95	438.02	438.30	438.49	438.23	438.11	438.12	NM	NM	NM	438.21	438.46		
GL-8-1	5535944.5	326391.9	438.80	439.70	438.86	438.78	437.53	437.26	438.83	438.78	438.05	438.75	439.03	438.97	438.56	438.54	438.75	438.99	438.92	438.84	438.94	438.86		
GL-8-2	5535944.5	326391.9	438.80	439.60	438.14	438.14	437.29	437.09	438.19	438.02	437.68	438.04	438.48	438.49	437.93	437.89	438.16	438.73	438.47	438.12	438.34	438.72		
GL-9-1	-	-	-	-	439.50	439.50	439.41	439.39	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian		
GL-9-2	-	-	-	-	437.93	437.94	437.51	437.68	438.03	437.94	437.67	437.83	438.24	438.44	438.11	437.98	438.04	438.52	438.57	438.08	438.21	438.46		
GL-9-3	-	-	-	-	437.89	437.90	437.46	437.64	437.95	437.90	437.61	437.79	438.18	438.37	438.03	437.89	437.96	438.43	438.49	438.00	438.14	438.46		
GL-10-1	5535933	326821.6	438.40	439.40	437.90	438.15	437.37	437.94	438.03	437.91	437.60	438.01	438.26	438.42	438.01	437.88	438.19	438.48	438.52	437.95	438.21	438.48		
GL-12-1	5535729.1	326538.3	441.30	442.30	440.22	440.16	439.99	439.89	440.96	440.49	440.08	440.00	440.28	440.56	NM	440.31	440.10	NM	440.72	440.28	439.96	439.77		
GL-13-1	5535791.4	326494.6	-	439.80	439.14	439.10	438.96	438.90	439.27	439.31	439.24	439.32	439.41	439.51	439.51	439.47	439.32	439.61	439.67	439.40	439.25	439.33		
GL-15-1	5535905.1	326176.5	452.00	452.30	448.06	447.40	447.67	447.78	448.52	448.40	448.99	448.54	448.71	448.22	448.03	447.83	447.41	447.80	448.44	448.57	447.75	447.30		
GL-15-2	5535905.1	326176.5	451.70	452.00	448.60	448.00	448.25	448.33	449.11	448.85	449.50	449.08	449.32	447.76	448.42	448.29	448.00	448.71	448.99	448.95	448.23	447.92		
GL-16-1	-	-	-	-	438.87	438.78	437.57	437.28	438.89	438.78	437.57	438.05	439.03	438.58	438.55	438.77	439.01	438.94	438.85	438.96	438.83	-		
GL-17-1	5535791.4	326494.6	439.20	440.30	-	439.94	439.91	439.94	439.99	439.97	439.98	-	-	440.16	-	-	-	-	-	439.96	Artesian	440.25		
GL-17-2	5535791.4	326494.6	439.20	439.80	439.08	439.07	438.90	438.96	439.15	439.11	439.11	439.19	439.34	439.37	439.34	439.32	439.32	439.57	439.51	439.30	439.22	439.25		
GL-18-2	5536537.1	326574.7	442.60	442.90	439.09	439.50	439.38	439.59	439.74	439.78	439.67	439.66	439.69	439.74	439.62	439.65	439.76	440.10	440.30	440.00	440.02	Decommisione		
GL-18-3	5536537.1	326574.7	442.90	442.80	437.99	437.93	437.66	437.66	438.18	438.09	437.82	437.89	438.22	438.60	438.31	438.12	438.09	438.68	438.69	437.67	438.07	-		
GL-20-1	-	-	-	-	438.21	438.26	437.84	437.71	438.20	438.16	437.90	438.03	438.63	438.55	438.22	438.10	438.16	438.72	438.59	438.39	438.33	438.48		
GL-23-1	5537307.3	326976.6	446.00	446.60	444.58	444.48	444.13	444.14	445.01	444.90	444.22	444.65	445.27	445.19	444.40	444.35	444.47	445.23	445.35	444.43	444.64	445.15		
GL-24-1	5537291.1	327107.7	446.80	447.60	444.98	444.82	444.39	444.52	445.42	445.84	444.80	445.03	445.52	445.78	444.85	444.68	444.84	445.65	445.84	444.84	446.33	445.64		
06BH02	5535672.4	327122.8	445.60	445.40	444.10	444.27	444.13	444.35	444.80	445.23	445.20	445.33	-	-	445.26	445.17	445.11	-	-	-	-	445.37		
09BH03	5535064.2	327413.6	440.80	441.00	435.87	435.76	435.63	435.64	436.28	436.38	436.40	436.25	436.60	436.60	-	436.14	436.05	-	436.47	436.39	436.32	436.34		
09BH04	5535008.4	327178.2	436.20	436.40	436.06	435.94	435.77	435.88	-	436.32	-	-	-	-	-	-	436.17	-	-	-	-	436.35		
09BH06-D	5534457.6	326917.6	435.60	435.80	435.62	435.59	435.35	435.47	435.79	435.65	435.70	435.75	-	-	435.67	435.58	435.62	-	-	435.77	-	435.83		
09BH06-S	5534457.6	326917.6	435.90	435.90	435.42	435.43	435.07	435.31	435.52	435.40	435.36	435.49	435.60	435.53	435.31	435.35	435.43	-	435.57	435.56	435.57	435.69		
09BH07	5535293.6	327214.6	440.90	441.00	437.05	436.97	436.83	436.91	437.77	437.70	438.47	438.00	439.43	438.78	439.29	438.63	438.35	-	-	439.68	439.38	439.70		
GL-26-1	5535984.6	326863.3	440.90	441.40	440.60	440.59	440.45	440.45	440.92	440.92	440.78	440.82	441.07	441.31	441.16	441.09	441.02	441.31	-	441.23	441.17	441.17		
GL-26-2	5535984.6	326863.3	440.70	441.60	438.18	438.61	437.78	438.29	438.28	438.18	437.92	438.26	438.55	438.65	438.23	438.13	438.46	438.82	438.75	438.37	438.47	438.55		
GL-26-3	5535984.6	326863.3	440.70	441.50	438.26	438.57	437.80	438.25	438.35	438.20	437.95	438.34	438.63	438.72	438.23	438.12	438.45	438.89	438.78	438.43	438.51	438.57		
GL-26-4	5535984.6	326863.3	440.70	441.50	438.18	438.44	437.74	438.10	438.31	438.15	437.86	438.25	438.55	438.64	438.19	438.09	438.39	438.86	438.79	438.42	438.48	438.49		
GL-27-1	5535841.1	326462.8	438.70	441.60	439.97	439.62	439.58	439.59	439.83	439.85	439.79	440.03	-	-	-	-	-	-	-	-	440.19	441.30		
GL-27-2	5535841.1	326462.8	438.70	440.80	438.33	438.14	438.05	438.04	438.52	438.23	438.20	438.41	438.57	438.61	438.38	438.29	438.44	440.28	-	439.98	438.32	438.84		
GL-27-3	5535841.1	326462.8	438.60	440.80	438.41	438.30	438.00	438.02	438.54	438.35	438.18	438.41	438.78	438.71	438.40	438.35	438.50	-	439.93	438.53	439.19	-		
GL-27-4	5535841.1	326462.8	438.70	440.60	438.26	438.15	437.57	437.72	438.30	438.00	437.76	438.47	438.55	438.59	438.05	437.97								

**Table 2**  
**Hydraulic Elevation Monitoring Results**  
**Hydrogeology and Hydrology Characterization Report**  
**Glenmore Landfill**  
**City of Kelowna**

Well ID	Monitoring Well UTM Zone 10 N Coordinates		Geodetic Elevations Grade (m AMSL)		Date																	
					Piezo (m AMSL)	6/6/2019	7/12/2019	8/12/2019	8/13/2019	10/28/2019	3/21/2020	6/4/2020	9/15/2020	11/26/2020	3/29/2021	6/15/2021	9/29/2021	10/26/2021	3/29/2022	6/24/2022	9/29/2022	10/27/2022
GL-0-1	5537338.6	326498.8	449.20	450.00	446.40	446.30	446.22	-	446.00	445.87	-	Decommissione	-	-	-	-	-	-	-	-	-	
GL-0-2	5537338.6	326498.8	449.00	450.00	442.27	442.16	442.05	-	441.88	441.76	-	-	-	-	-	-	-	-	-	-	-	
GL-0-3	5537338.6	326498.8	449.42	450.49	442.25	442.14	442.02	-	441.84	441.72	-	-	-	-	-	-	-	-	-	-	-	
GL-1-1	5537230.4	327134.1	446.30	446.90	445.34	445.10	444.87	-	445.13	445.73	445.57	445.04	445.29	445.44	445.16	444.41	444.90	445.28	445.17	444.57	444.93	
GL-1-2	5537230.4	327134.1	446.30	447.00	445.23	445.00	444.77	-	445.03	445.61	445.45	444.95	445.20	445.34	445.08	444.33	444.83	445.20	445.09	444.49	444.87	
GL-2-1	5536880.9	326219.1	438.60	439.00	438.74	-	438.50	-	438.78	438.77	438.81	438.69	438.90	438.87	438.59	438.83	438.75	438.99	438.87	438.66	438.79	
GL-2-2	5536880.9	326219.1	438.90	439.00	438.55	-	438.12	-	438.61	438.99	438.40	438.52	438.64	438.64	438.18	438.65	438.30	438.58	438.48	438.35	438.49	
GL-3-5	5537050.6	326414.3	457.10	457.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-4-1	5536929.9	326887.8	441.10	441.40	439.90	439.88	439.81	-	439.89	440.25	440.32	439.90	439.90	440.10	439.86	439.69	439.77	440.18	440.08	439.73	439.78	
GL-4-2	5536929.9	326887.8	441.10	441.40	439.35	439.32	439.26	-	439.35	439.60	439.57	439.26	439.33	439.48	439.25	439.08	439.17	439.53	439.37	439.10	439.16	
GL-5-1	5536592.3	326175.4	439.00	440.00	438.62	438.55	438.29	-	438.62	438.82	438.57	438.59	438.71	438.72	438.33	438.51	438.47	438.62	438.58	438.32	438.49	
GL-5-2	5536592.3	326175.4	439.20	440.10	438.61	438.49	438.29	-	438.62	438.80	438.52	438.57	438.68	438.69	438.29	438.65	438.42	438.62	438.55	438.33	438.49	
GL-5-3	5536592.3	326175.4	439.20	440.20	438.58	438.45	438.22	-	438.62	438.78	438.48	438.55	438.66	438.67	438.22	438.79	438.36	438.58	438.51	438.31	438.47	
GL-6-1 (2011)	5536528.3	326582.8	439.70	440.50	438.14	437.84	437.02	-	437.54	438.20	438.16	437.86	437.51	438.21	438.11	Decommissione	-	-	-	-	-	
GL-7-1	5536434.3	326891	439.00	439.70	438.31	-	438.05	-	437.82	438.32	438.30	438.00	438.02	438.30	438.18	437.84	437.86	438.14	438.13	437.72	437.72	
GL-8-1	5535944.5	326391.9	438.80	439.70	438.63	438.70	438.59	-	438.67	438.88	438.69	438.86	439.03	438.67	438.90	438.74	438.41	438.74	438.83	438.60	438.69	
GL-8-2	5535944.5	326391.9	438.80	439.60	438.26	438.15	437.90	-	438.12	439.39	438.27	438.05	438.21	438.37	439.73	438.04	437.93	438.30	438.66	437.96	438.05	
GL-9-1	-	-	-	-	Artesian	439.57	-	-	439.57	439.54	439.52	439.52	439.54	439.54	439.53	439.57	439.57	-	-	-	-	
GL-9-2	-	-	-	-	438.29	438.16	438.03	-	437.93	438.31	438.28	437.95	438.08	438.33	438.16	Decommissione	-	-	-	-	-	
GL-9-3	-	-	-	-	438.21	438.09	437.97	-	437.87	438.26	438.21	437.89	439.04	438.29	438.11	-	-	-	-	-	-	
GL-10-1	5535933	326821.6	438.40	439.40	438.19	438.11	438.13	-	438.00	438.25	438.22	437.75	438.11	438.30	438.07	437.71	437.89	438.12	438.10	437.62	437.78	
GL-12-1	5535729.1	326538.3	441.30	442.30	439.75	439.68	439.68	-	439.65	440.06	440.06	440.06	439.95	439.99	439.84	439.69	439.66	440.19	440.20	439.98	439.95	
GL-13-1	5535791.4	326494.6	-	439.80	439.16	439.11	439.07	-	439.06	439.33	439.35	439.30	439.26	439.26	439.24	439.08	439.09	439.40	439.42	439.26	439.26	
GL-15-1	5535905.1	326176.5	452.00	452.30	446.87	448.30	448.61	-	447.22	447.45	448.93	449.00	448.82	448.04	448.87	447.25	447.50	447.66	447.97	448.47	447.75	
GL-15-2	5535905.1	326176.5	451.70	452.00	447.34	448.54	449.03	-	447.64	448.01	449.43	450.09	449.39	448.53	449.38	447.71	448.11	448.33	448.60	449.02	448.26	
GL-16-1	-	-	-	-	437.42	437.69	438.63	-	438.72	438.93	438.74	439.01	439.08	439.00	438.97	438.79	438.47	438.77	438.93	438.62	438.72	
GL-17-1	5535791.4	326494.6	439.20	440.30	440.25	440.25	440.23	-	440.05	440.21	440.23	440.24	440.18	440.17	440.19	440.19	440.13	440.17	440.15	440.20	440.10	
GL-17-2	5535791.4	326494.6	439.20	439.80	439.05	439.02	438.98	-	438.99	439.72	439.21	439.18	439.18	439.15	439.12	439.01	439.03	439.19	439.27	439.12	439.13	
GL-18-2	5536537.1	326574.7	442.60	442.90	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-18-3	5536537.1	326574.7	442.90	442.80	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-20-1	-	-	-	-	438.35	438.21	438.02	-	438.16	438.40	438.28	438.17	438.25	438.38	438.08	438.19	437.99	438.28	438.33	438.03	438.11	
GL-23-1	5537307.3	326976.6	446.00	446.60	445.02	444.86	444.58	-	444.80	445.37	445.36	444.35	444.95	445.26	444.94	443.80	444.73	444.78	445.00	444.39	444.48	
GL-24-1	5537291.1	327107.7	446.80	447.60	445.34	445.10	444.83	-	445.09	445.72	445.59	445.01	445.27	445.43	445.16	444.37	444.86	445.26	445.13	444.91	444.91	
06BH02	5535672.4	327122.8	445.60	445.40	445.37	-	-	445.37	445.37	-	Artesian	-	-	Artesian	CAN	CNL	CNL	Damaged	445.87	445.91	445.76	
09BH03	5535064.2	327413.6	440.80	441.00	435.99	-	437.52	-	436.74	-	437.08	436.84	436.58	436.42	436.97	436.97	436.80	436.94	437.12	Damaged	-	
09BH04	5535008.4	327178.2	436.20	436.40	436.35	-	Artesian	-	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	
09BH06-D	5534457.6	326917.6	435.60	435.80	435.83	-	Artesian	-	435.83	-	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	Artesian	
09BH06-S	5534457.6	326917.6	435.90	435.90	435.68	-	435.58	-	435.61	-	435.71	435.64	435.71	435.76	435.71	435.64	435.66	435.76	435.73	435.69	435.67	
09BH07	5535293.6	327214.6	440.90	441.00	439.64	-	439.70	-	439.05	-	439.18	-	-	436.11	Damaged	Damaged	Damaged	-	-	-	-	
GL-26-1	5535984.6	326863.3	440.90	441.40	441.21	441.16	441.12	-	441.03	441.43	441.28	441.19	441.16	441.29	441.24	441.01	441.02	440.98	441.15	441.03	441.02	
GL-26-2	5535984.6	326863.3	440.70	441.60	438.46	438.49	438.49	-	438.34	438.50	438.59	438.17	438.38	438.50	438.33	438.16	438.30	438.41	438.44	438.06	438.24	
GL-26-3	5535984.6	326863.3	440.70	441.50	438.40	438.60	438.85	-	438.39	438.49	438.61	438.14	438.41	438.45	438.32	438.21	438.39	438.49	438.53	438.19	438.42	
GL-26-4	5535984.6	326863.3	440.70	441.50	438.32	438.47	438.69	-	438.29	438.41	438.53	438.06	438.34	438.38	438.29	438.17	438.35	438.52	438.56	438.26	438.39	
GL-27-1	5535841.1	326462.8	438.70	441.60	440.24	440.23	440.24	-	440.11	440.10	440.25	440.16	440.16	440.15	440.17	440.00	440.09	440.18	440.19	440.14	440.15	
GL-27-2	5535841.1	326462.8	438.70	440.80	438.65	438.53	438.45	-	438.39	438.64	438.65	438.36	438.41	438.54	438.48	438.23	438.24	438.57	438.51	438.25	438.23	
GL-27-3	5535841.1	326462.8	438.60	440.80	438.46	438.36	438.25	-	438.33	438.61	438.56	438.33	438.48	438.62	438.41	438.20	438.23	438.59	438.63	438.27	438.32	
GL-27-4	5535841.1	326462.8	438.70	440.60	438.55	438.41	438.29	-	438.21	438.59	438.60	438.23	438.38	438.53	438.43	438.03	438.08	438.95	438.91	438.52	438.18	
GL-28-1	5535273.8	326721.5	442.10	442.10	436.60	436.79	436.79	-	436.68	-	436.89	437.06	436.79	436.71	437.25	436.78	436.71	436.82	436.80	436.78	436.71	
GL-28-2	5535273.8	326721.5	441.40	441.80	436.82	436.97	436.93	-	436.87	-	437.17	437.50	437.09	436.98	438.19	437.08	436.98	437.20	437.06	436.98	436.92	
GL-28-3	5535273.8	326721.5	441.40	441.70	436.82	436.96	436.93	-	436.86	-	436.16	437.49	437.08	436.98	438.21	437.08	436.98	437.20	437.06	436.98	436.93	
GL-29-1	5535749.3	326652.7	443.90	445.10	440.80	440.85	440.81	-	440.74	440.94	440.93	440.88	440.83	440.92	440.74	440.77	440.81	440.82	440.74	440.73	440.73	
GL-29-2	5535749.3	326652.7	443.90	444.80	441.24	441.28	441.38	-	441.12	441.56	441.73	441.40	441.37	441.33	441.23	440.90	440.79	441.60	441.82	441.27	441.00	
GL-30-1	5536																					

**Table 2**  
**Hydraulic Elevation Monitoring Results**  
**Hydrogeology and Hydrology Characterization Report**  
**Glenmore Landfill**  
**City of Kelowna**

Well ID	Monitoring Well		Geodetic Elevations		Date																		
	UTM Zone	10 N Coordinates	Grade	Piezo	3/17/2015	6/4/2015	8/27/2015	11/2/2015	3/22/2016	5/16/2016	9/16/2016	11/24/2016	3/21/2017	6/5/2017	8/16/2017	9/22/2017	11/14/2017	3/16/2018	5/25/2018	8/30/2018	11/16/2018	3/21/2019	
	Northing	Easting	(m AMSL)	(m AMSL)																			
GL-35-1	5536105.2	326411.2	438.10	439.00	438.17	438.17	437.02	436.75	438.12	438.01	437.52	437.95	438.29	-	438.03	437.98	438.13	-	-	438.15	438.32	-	
GL-35-2	5536105.2	326411.2	438.10	439.00	438.74	438.66	437.58	437.27	438.77	438.59	438.03	438.64	438.96	-	438.54	438.49	438.66	-	-	-	438.88	-	
GL-35-3	5536105.2	326411.2	438.40	439.30	438.73	438.65	437.73	437.27	438.69	438.58	438.04	438.63	438.94	439.06	438.54	438.49	438.66	438.87	-	438.79	438.86	-	
GL-36-1	5536496.4	326764.1	439.20	439.80	438.10	438.16	438.03	437.99	438.13	438.19	438.13	-	438.10	438.33	438.18	438.13	438.20	438.35	438.51	438.02	438.26	438.40	
GL-36-2	5536496.4	326764.1	439.30	440.00	438.39	438.44	438.24	438.28	438.47	438.52	438.44	438.49	438.60	438.73	438.55	438.48	438.53	438.88	439.00	438.56	438.62	438.83	
GL-36-3	-	-	-	-	438.46	438.49	438.29	438.34	438.59	438.58	438.50	438.53	438.67	438.77	438.56	438.48	438.53	438.79	438.88	438.53	438.60	438.81	
GL-37	5536489.1	326646.4	439.30	440.10	437.89	437.86	437.53	437.57	437.86	437.88	437.70	437.75	438.15	438.37	438.05	Decommission	-	-	-	-	-	-	
GL-38	5536488.9	326634.4	439.30	440.10	437.88	437.86	437.52	437.57	437.80	437.88	437.69	437.80	438.14	438.37	438.04	-	-	-	-	-	-	-	
GL-39-1	5535296.8	326790.4	439.50	440.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-39-2	5535297.6	326789.1	439.60	440.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-39-3	5535298.3	326787.8	439.60	440.60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-40-1	5535525.2	326465.2	449.70	450.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-40-2	5535523.8	326466.4	449.60	450.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-40-3	5535523.7	326466.2	449.60	450.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-41-1	5537673.4	326191.3	449.70	450.60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-41-2	5537673.3	326191.5	449.70	450.60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-41-3	5537675.7	326192.7	449.70	450.60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-42-1	5535422.7	326636.2	447.60	448.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-42-2	5535422.6	326636.2	447.60	448.40	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL-42-3	5535423.9	326637.6	447.70	448.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	

Notes:  
 Source: 2022 Annual Water Monitoring Report for Glenmore Landfill (Keltech Environmental, March 24, 2023)  
 - - no data (well not installed or data not available)  
 CNA - could not access  
 CNL - could not locate

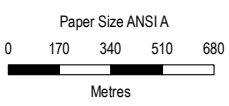
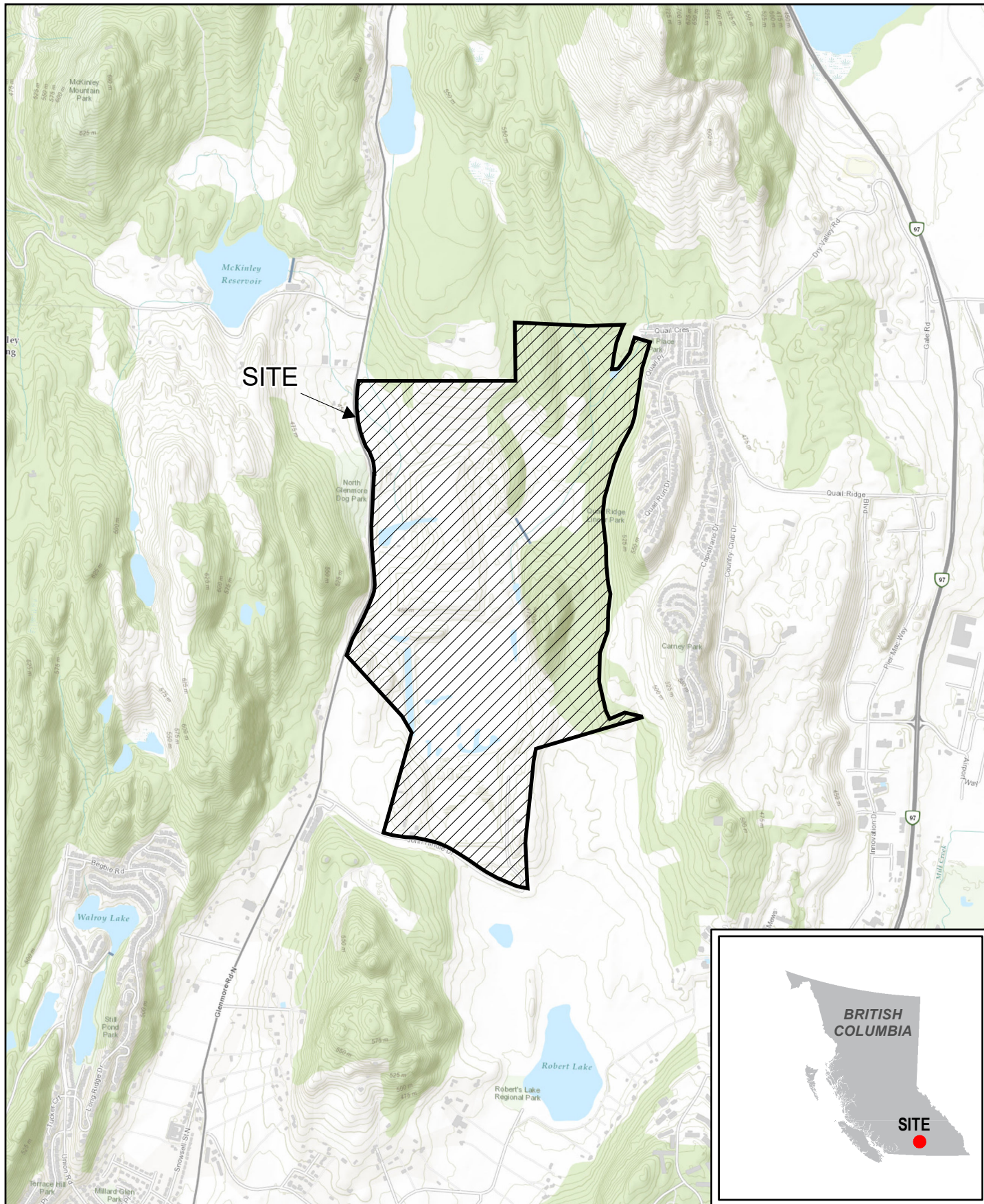


**Table 2**  
**Hydraulic Elevation Monitoring Results**  
**Hydrogeology and Hydrology Characterization Report**  
**Glenmore Landfill**  
**City of Kelowna**

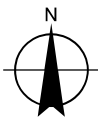
Well ID	Monitoring Well		Geodetic Elevations		Date																
	UTM Zone	10 N Coordinates	Grade (m AMSL)	Piezo (m AMSL)	6/6/2019	7/12/2019	8/12/2019	8/13/2019	10/28/2019	3/21/2020	6/4/2020	9/15/2020	11/26/2020	3/29/2021	6/15/2021	9/29/2021	10/26/2021	3/29/2022	6/24/2022	9/29/2022	10/27/2022
GL-35-1	5536105.2	326411.2	438.10	439.00	438.26	438.13	437.94	-	438.13	438.37	438.13	438.18	438.26	438.36	437.98	438.12	437.94	438.21	438.17	437.95	438.04
GL-35-2	5536105.2	326411.2	438.10	439.00	438.64	438.71	438.60	-	438.68	438.84	438.69	438.83	439.00	CNA	438.94	438.70	438.41	438.68	438.84	438.52	438.60
GL-35-3	5536105.2	326411.2	438.40	439.30	438.64	438.69	-	-	438.67	438.83	438.67	438.82	438.98	438.91	438.93	438.69	438.41	438.69	438.84	438.53	438.61
GL-36-1	5536496.4	326764.1	439.20	439.80	438.38	438.22	438.04	-	Decommission	-	-	-	-	-	-	-	-	-	-	-	-
GL-36-2	5536496.4	326764.1	439.30	440.00	438.72	438.59	438.47	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GL-36-3	-	-	-	-	438.69	438.56	438.45	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GL-37	5536489.1	326646.4	439.30	440.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GL-38	5536488.9	326634.4	439.30	440.10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GL-39-1	5535296.8	326790.4	439.50	440.40	-	-	-	-	-	437.09	437.14	437.43	437.13	437.02	437.20	437.04	437.04	437.19	437.15	437.21	437.07
GL-39-2	5535297.6	326789.1	439.60	440.50	-	-	-	-	-	437.13	437.23	437.51	437.20	437.06	437.51	437.09	437.08	437.25	437.19	437.24	437.12
GL-39-3	5535298.3	326787.8	439.60	440.60	-	-	-	-	-	437.19	437.21	437.63	437.28	437.14	437.49	437.12	437.05	437.43	437.23	437.15	437.15
GL-40-1	5535525.2	326465.2	449.70	450.50	-	-	-	-	-	-	-	-	-	Dry	Dry	Dry	Dry	445.35	Dry	Dry	Dry
GL-40-2	5535523.8	326466.4	449.60	450.40	-	-	-	-	-	443.50	443.27	443.08	441.58	442.91	440.62	Decommissione	-	-	-	-	-
GL-40-3	5535523.7	326466.2	449.60	450.40	-	-	-	-	-	443.55	443.29	443.12	441.61	442.96	440.58	-	-	-	-	-	-
GL-41-1	5537673.4	326191.3	449.70	450.60	-	-	-	-	-	448.39	448.13	447.76	447.41	448.23	447.91	447.86	447.86	448.07	448.18	448.06	448.08
GL-41-2	5537673.3	326191.5	449.70	450.60	-	-	-	-	-	448.33	448.15	447.65	447.36	448.18	447.86	447.80	447.81	448.04	448.15	448.04	448.06
GL-41-3	5537675.7	326192.7	449.70	450.60	-	-	-	-	-	448.36	448.16	447.66	447.38	448.20	447.87	447.82	447.82	448.09	448.20	448.09	448.11
GL-42-1	5535422.7	326636.2	447.60	448.40	-	-	-	-	-	440.04	440.05	449.37	440.04	439.99	439.96	439.90	439.82	438.01	Damaged	-	-
GL-42-2	5535422.6	326636.2	447.60	448.40	-	-	-	-	-	439.79	439.79	440.16	439.82	439.72	439.74	439.71	439.63	437.75	437.66	437.64	437.55
GL-42-3	5535423.9	326637.6	447.70	448.50	-	-	-	-	-	-	-	-	-	Dry	Dry	Dry	Dry	438.95	Damaged	-	-

Notes:  
 Source: 2022 Annual Water Monitoring Report for Glenmore Landfill (Keltech Environmental, March 2-  
 - - no data (well not installed or data not available)  
 CNA - could not access  
 CNL - could not locate

# Figures



Map Projection: Transverse Mercator  
 Horizontal Datum: North American 1983  
 Grid: NAD 1983 UTM Zone 11N



**CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT**

Project No. 12605725  
 Revision No. -  
 Date Oct 13, 2023

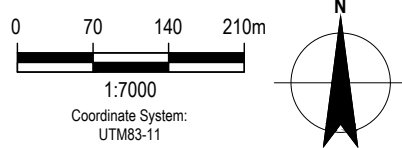
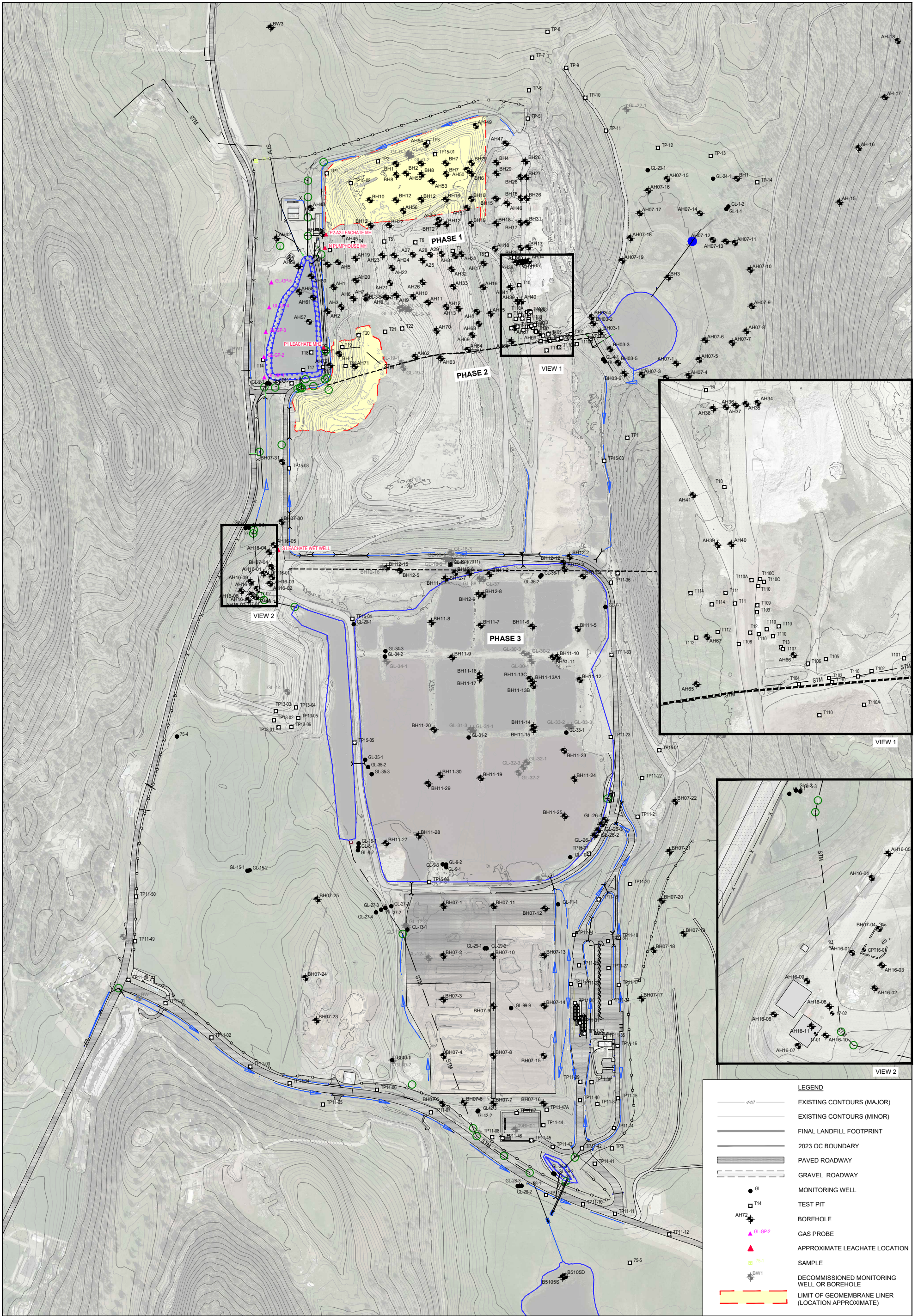
**SITE LOCATION MAP**

**FIGURE 1.1**









CITY OF KELOWNA  
**GLENMORE LANDFILL**  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT

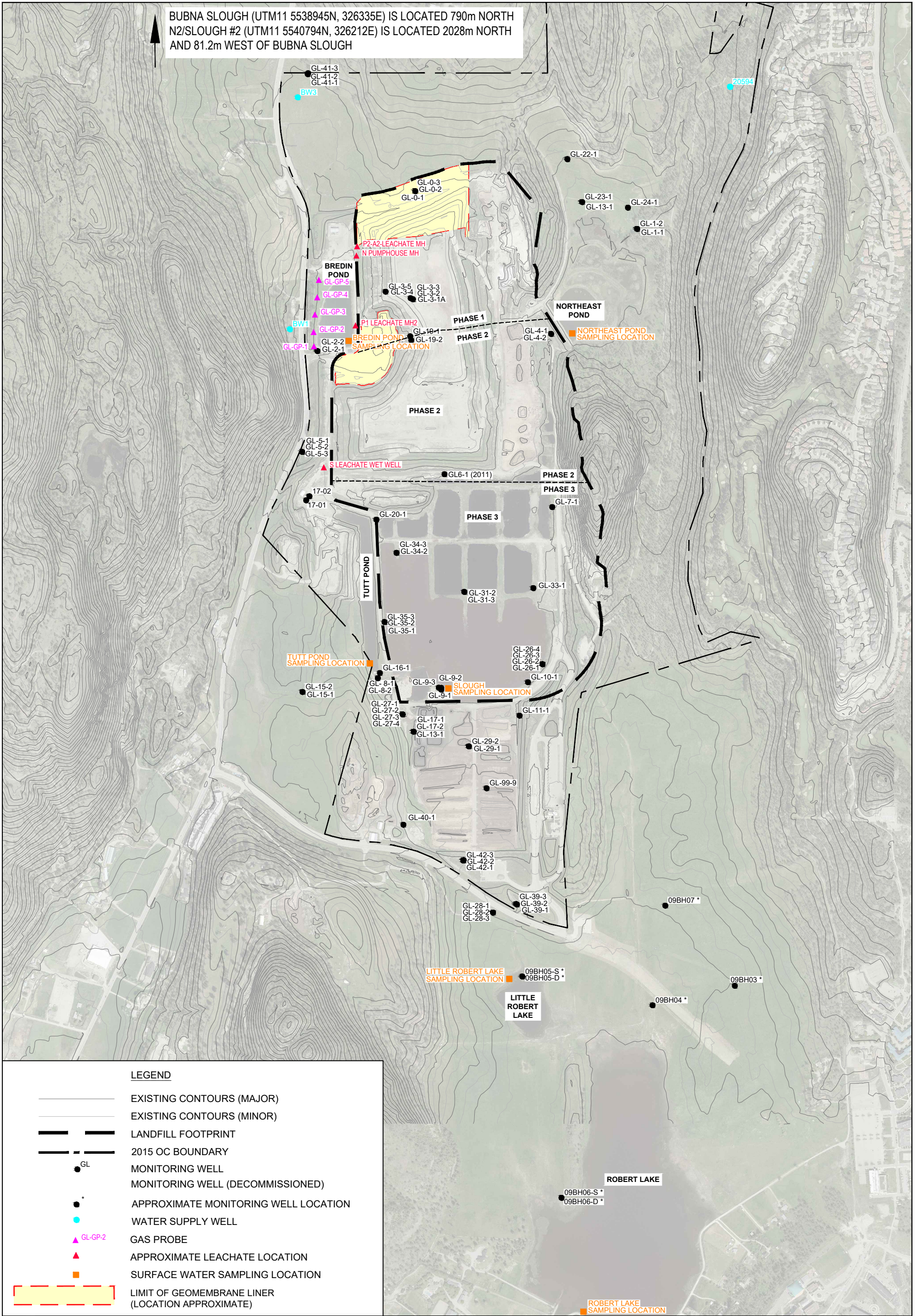
Project No. 12605725  
 Date December 2023

INVESTIGATIVE LOCATIONS





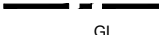







FIGURE 1.3

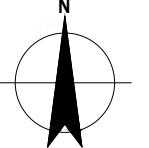
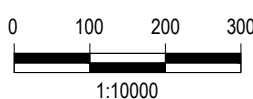


BUBNA SLOUGH (UTM11 5538945N, 326335E) IS LOCATED 790m NORTH N2/SLOUGH #2 (UTM11 5540794N, 326212E) IS LOCATED 2028m NORTH AND 81.2m WEST OF BUBNA SLOUGH



**LEGEND**

-  EXISTING CONTOURS (MAJOR)
-  EXISTING CONTOURS (MINOR)
-  LANDFILL FOOTPRINT
-  2015 OC BOUNDARY
-  MONITORING WELL
-  MONITORING WELL (DECOMMISSIONED)
-  APPROXIMATE MONITORING WELL LOCATION
-  WATER SUPPLY WELL
-  GAS PROBE
-  APPROXIMATE LEACHATE LOCATION
-  SURFACE WATER SAMPLING LOCATION
-  LIMIT OF GEOMEMBRANE LINER (LOCATION APPROXIMATE)



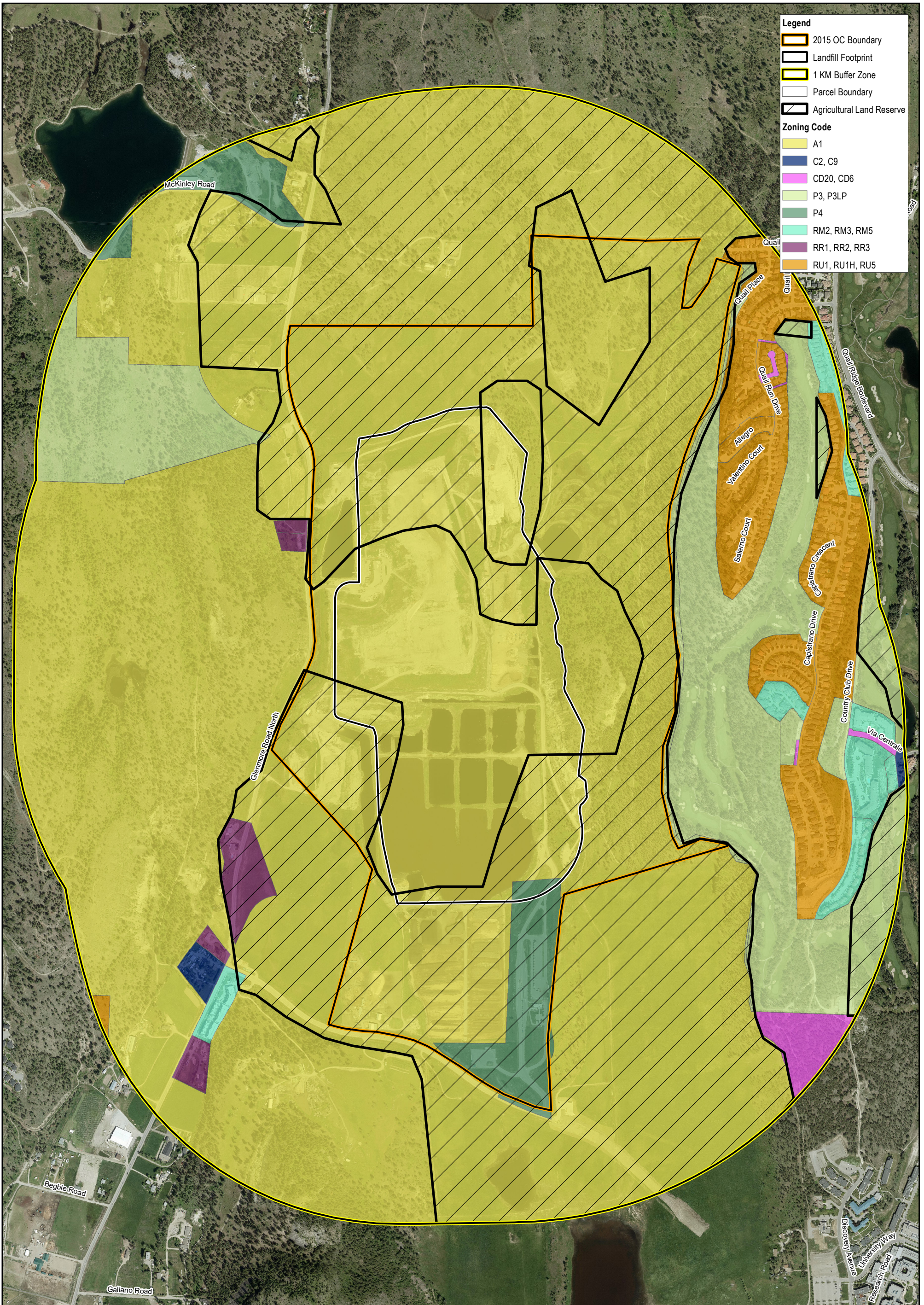
CITY OF KELOWNA - GLENMORE LANDFILL  
2023 DESIGN, OPERATIONS AND  
CLOSURE REPORT

Project No. 12605725  
Date December 2023

MONITORING NETWORK

FIGURE 1.4



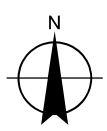
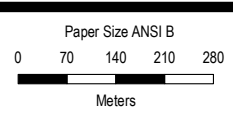


**Legend**

- 2015 OC Boundary
- Landfill Footprint
- 1 KM Buffer Zone
- Parcel Boundary
- Agricultural Land Reserve

**Zoning Code**

- A1
- C2, C9
- CD20, CD6
- P3, P3LP
- P4
- RM2, RM3, RM5
- RR1, RR2, RR3
- RU1, RU1H, RU5



Map Projection: Transverse Mercator  
 Horizontal Datum: North American 1983  
 Grid: NAD 1983 UTM Zone 11N

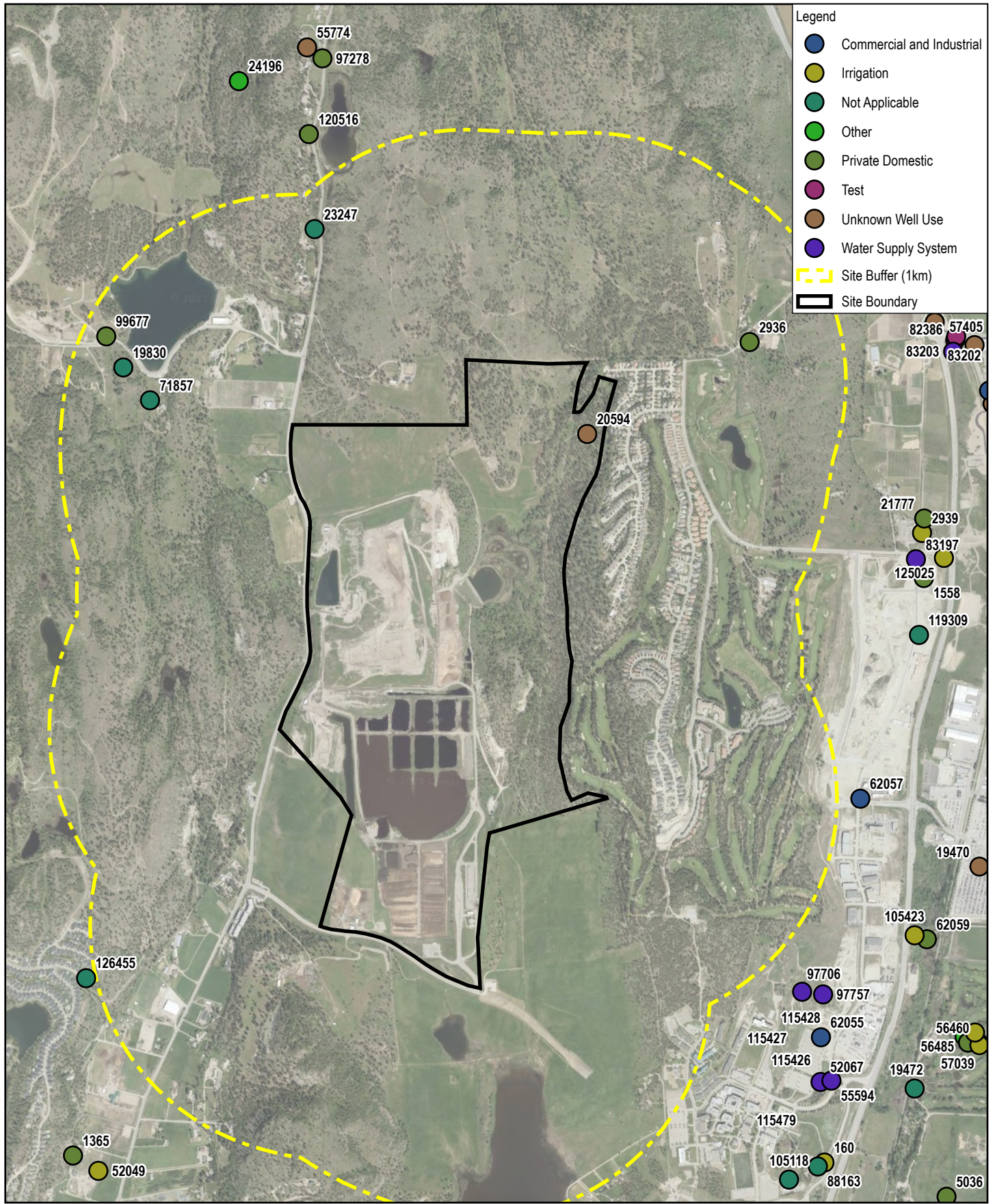
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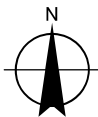
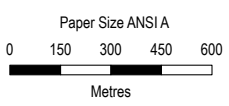
**ZONING AND LAND USE**

**FIGURE 2.1**





- Legend**
- Commercial and Industrial
  - Irrigation
  - Not Applicable
  - Other
  - Private Domestic
  - Test
  - Unknown Well Use
  - Water Supply System
  - Site Buffer (1km)
  - Site Boundary



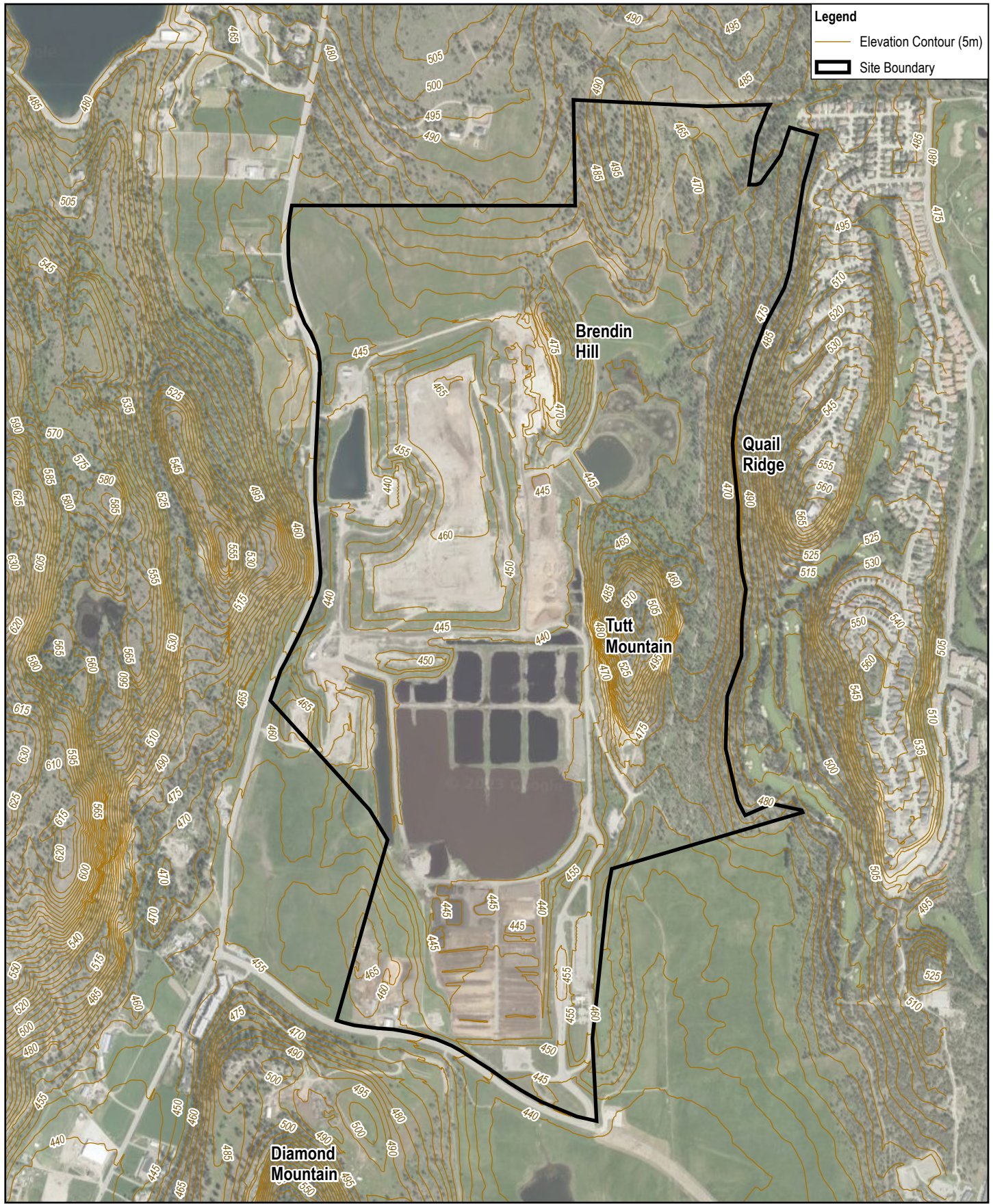
**CITY OF KELOWNA  
GLENMORE LANDFILL  
HYDROGEOLOGY AND HYDROLOGY  
CHARACTERIZATION REPORT**

**SITE HYDROLOGY  
AND DRAINAGE**

Project No. 12605725  
Revision No. -  
Date Oct 13, 2023

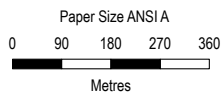
**FIGURE 2.2**



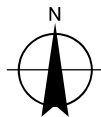


**Legend**

- Elevation Contour (5m)
- Site Boundary



Map Projection: Transverse Mercator  
 Horizontal Datum: North American 1983  
 Grid: NAD 1983 UTM Zone 11N



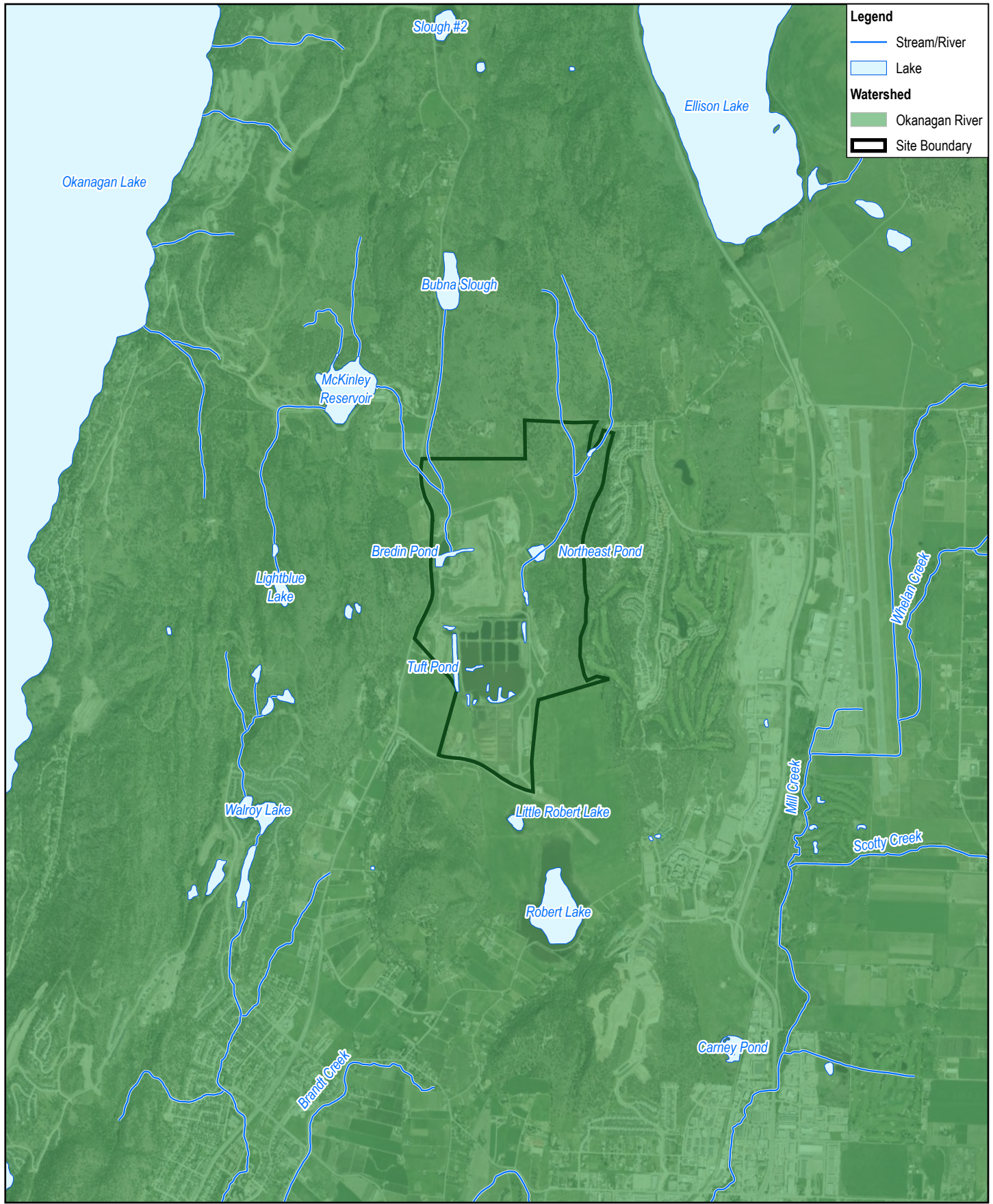
**CITY OF KELOWNA  
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 CHARACTERIZATION REPORT**

Project No. 12605725  
 Revision No. -  
 Date Nov 1, 2023

**SITE TOPOGRAPHY**

**FIGURE 3.1**



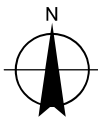
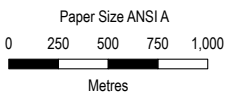


**Legend**

- Stream/River
- Lake

**Watershed**

- Okanagan River
- Site Boundary



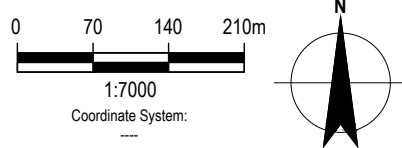
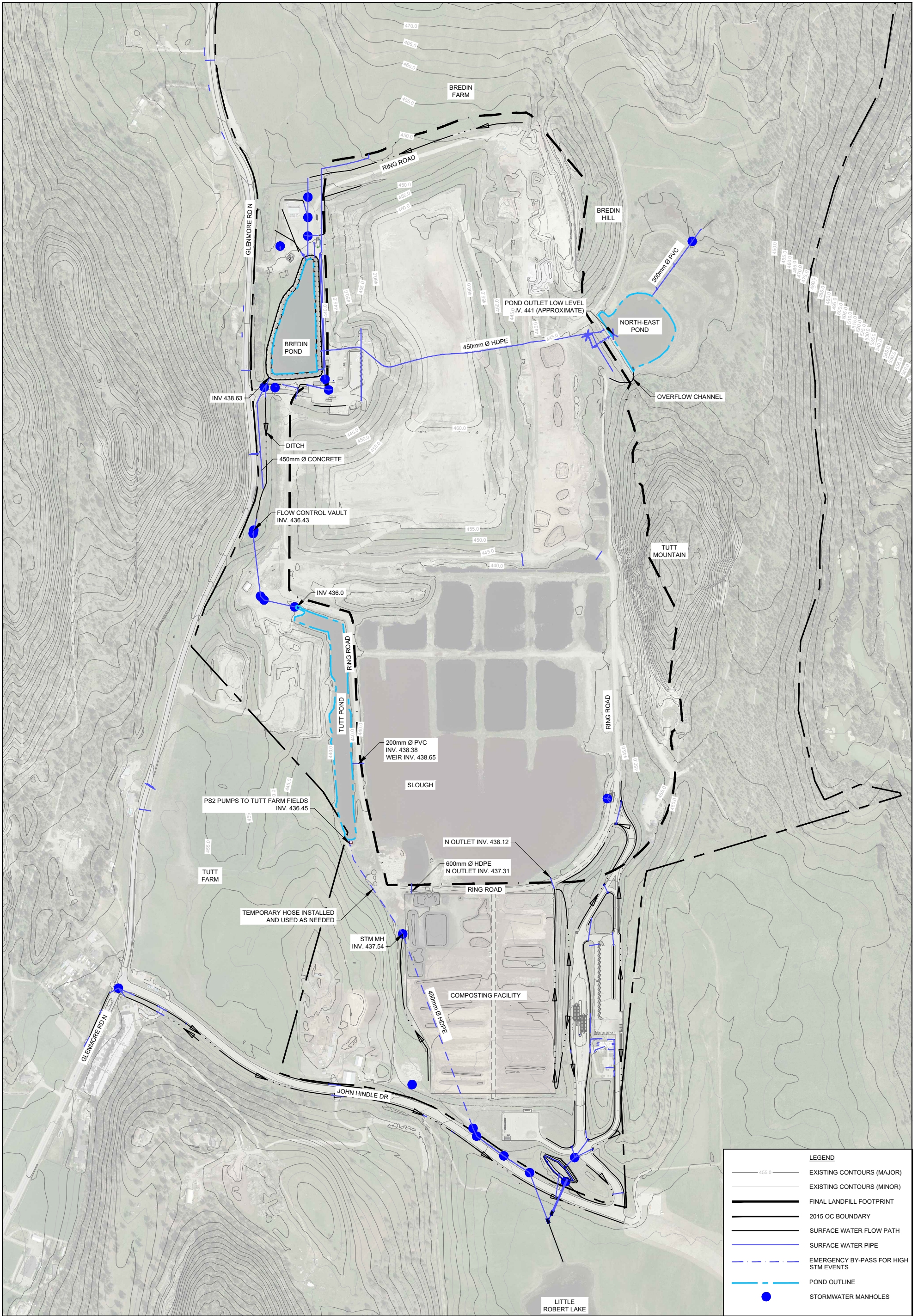
**CITY OF KELOWNA  
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HYDROGEOLOGY AND HYDROLOGY  
CHARACTERIZATION REPORT**

Project No. 12605725  
Revision No. -  
Date Oct 13, 2023

**REGIONAL HYDROLOGY  
AND DRAINAGE**

**FIGURE 3.2**



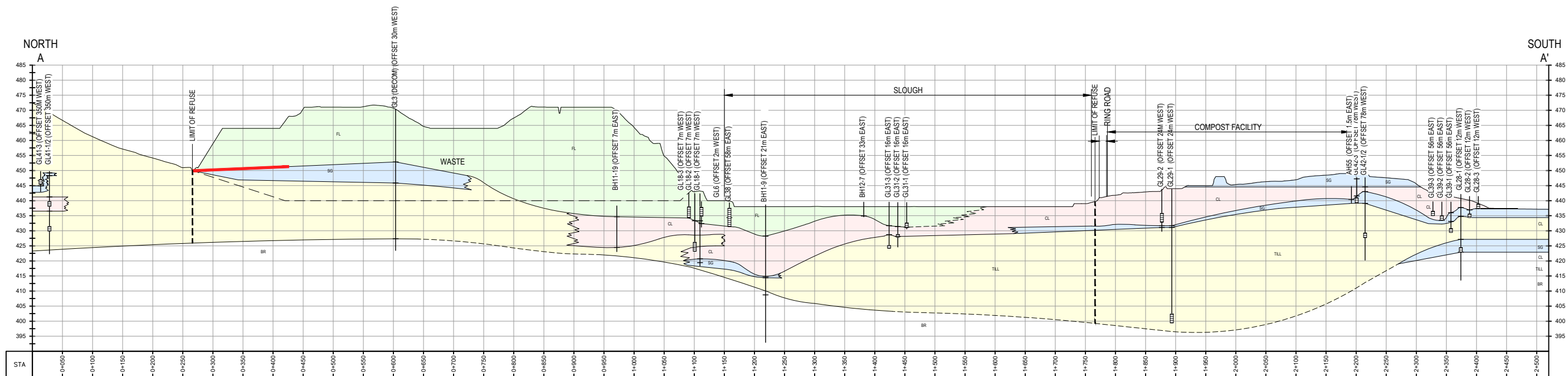


CITY OF KELOWNA  
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 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
**EXISTING CONDITIONS SURFACE WATER  
 WORKS**

Project No. 12605725  
 Date December 2023

**FIGURE 3.3**





SECTION A-A'  
 HOR. 1:3500  
 VER. 1:700  
 FIG. 3.4

- LEGEND
- FL - FILL
  - CL - CLAY
  - SG - SAND & GRAVEL
  - TL - TILL
  - SD - SAND
  - BR - BEDROCK
  - EXTENT OF GEOMEMBRANE LINER

NOTE:  
 \* BOREHOLE STRATIGRAPHY NOT USED IN CROSS-SECTION

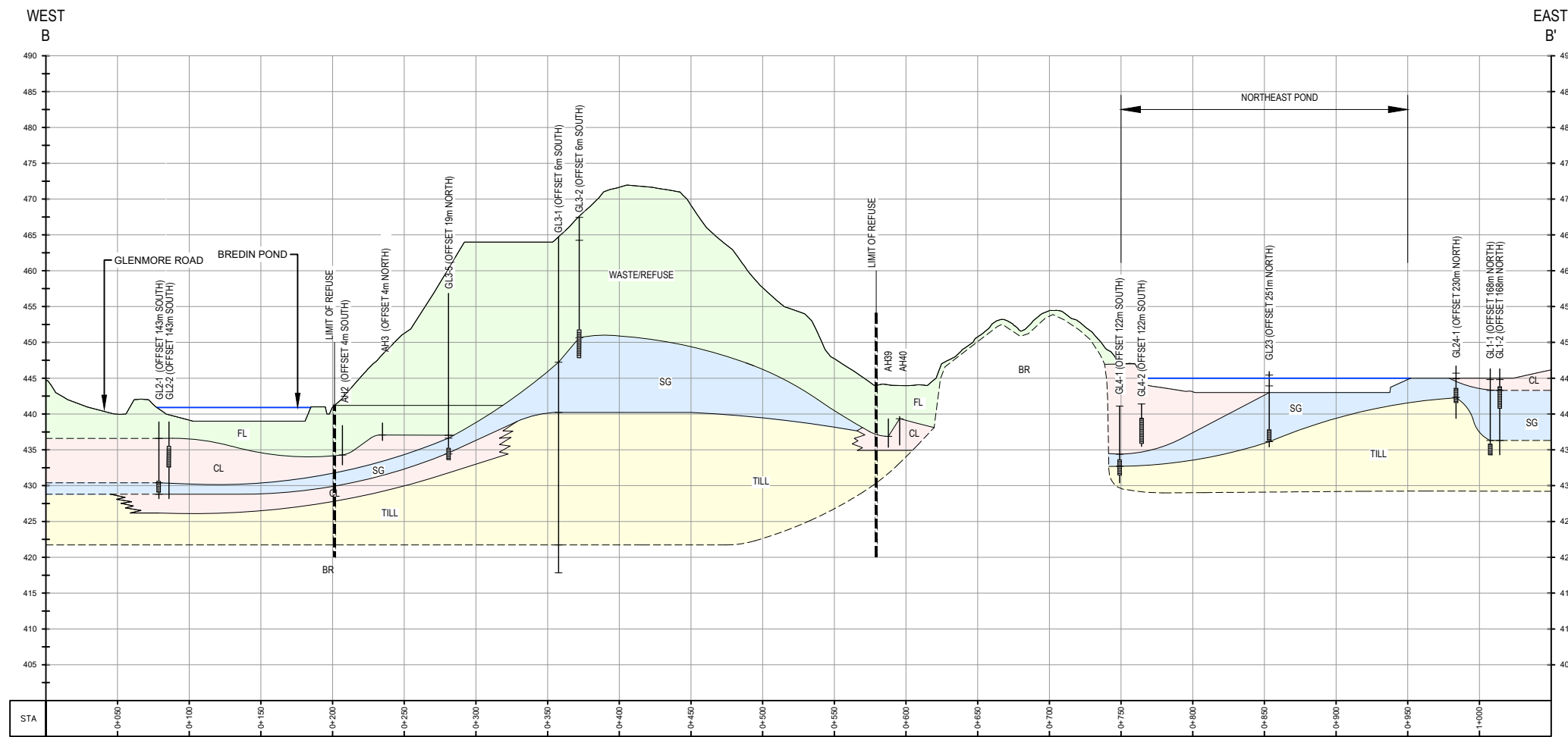


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 CHARACTERIZATION REPORT

Project No. 12605725  
 Date December 2023

SECTION A-A'

FIGURE 3.4A



SECTION B-B'  
HOR. 1:2000  
VER. 1:400  
CI-0101

- LEGEND
- FL - FILL
  - CL - CLAY
  - SG - SAND & GRAVEL
  - TL - TILL
  - SD - SAND
  - BR - BEDROCK

NOTE:  
\*BOREHOLE STRATIGRAPHY NOT USED IN CROSS-SECTION

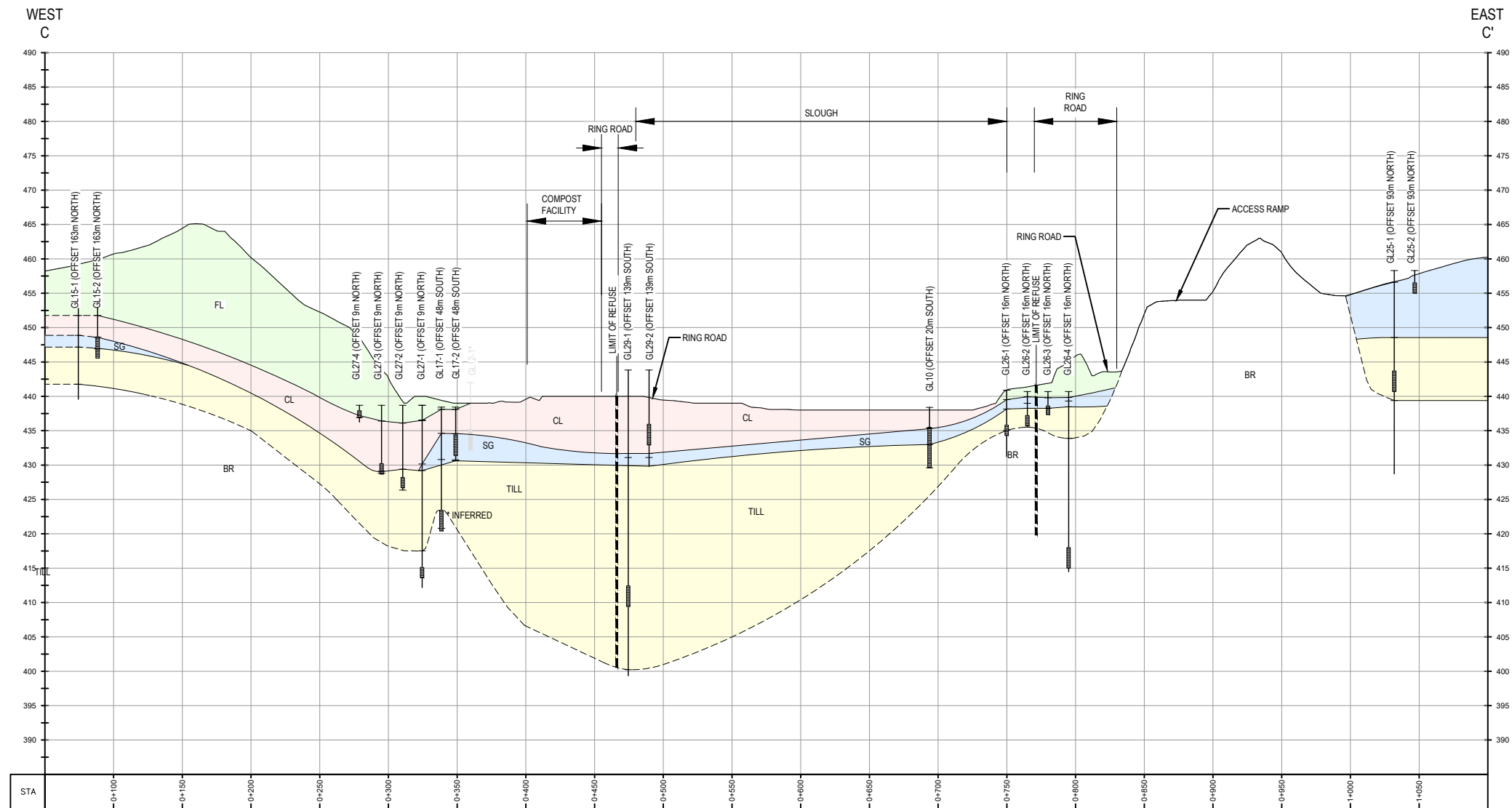


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CHARACTERIZATION REPORT

Project No. 12605725  
Date December 2023

SECTION B-B'

FIGURE 3.4B



SECTION C-C'  
HOR. 1:2000  
VER. 1:400  
CI-0101

- LEGEND
- FL - FILL
  - CL - CLAY
  - SG - SAND & GRAVEL
  - TL - TILL
  - SD - SAND
  - BR - BEDROCK

NOTE:  
\* BOREHOLE STRATIGRAPHY NOT USED IN CROSS-SECTION



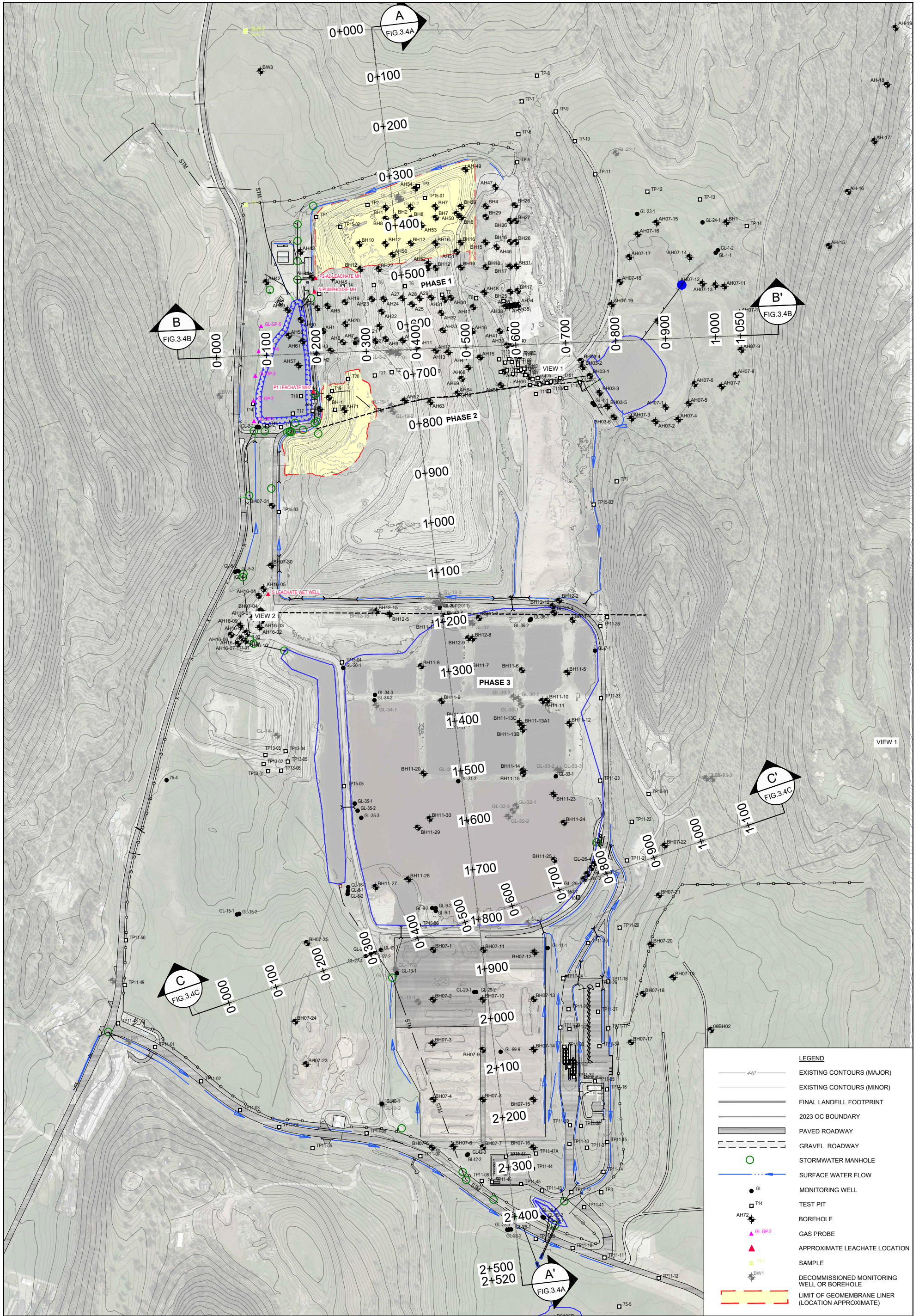
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HYDROGEOLOGY AND HYDROLOGY  
CHARACTERIZATION REPORT

Project No. 12605725  
Date December 2023

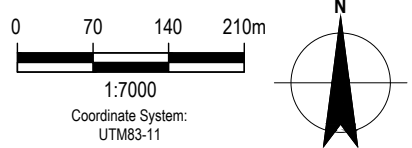
SECTION C-C'

FIGURE 3.4C





LEGEND	
	EXISTING CONTOURS (MAJOR)
	EXISTING CONTOURS (MINOR)
	FINAL LANDFILL FOOTPRINT
	2023 OC BOUNDARY
	PAVED ROADWAY
	GRAVEL ROADWAY
	STORMWATER MANHOLE
	SURFACE WATER FLOW
	MONITORING WELL
	TEST PIT
	BOREHOLE
	GAS PROBE
	APPROXIMATE LEACHATE LOCATION
	SAMPLE
	DECOMMISSIONED MONITORING WELL OR BOREHOLE
	LIMIT OF GEOMEMBRANE LINER (LOCATION APPROXIMATE)



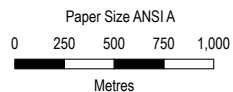
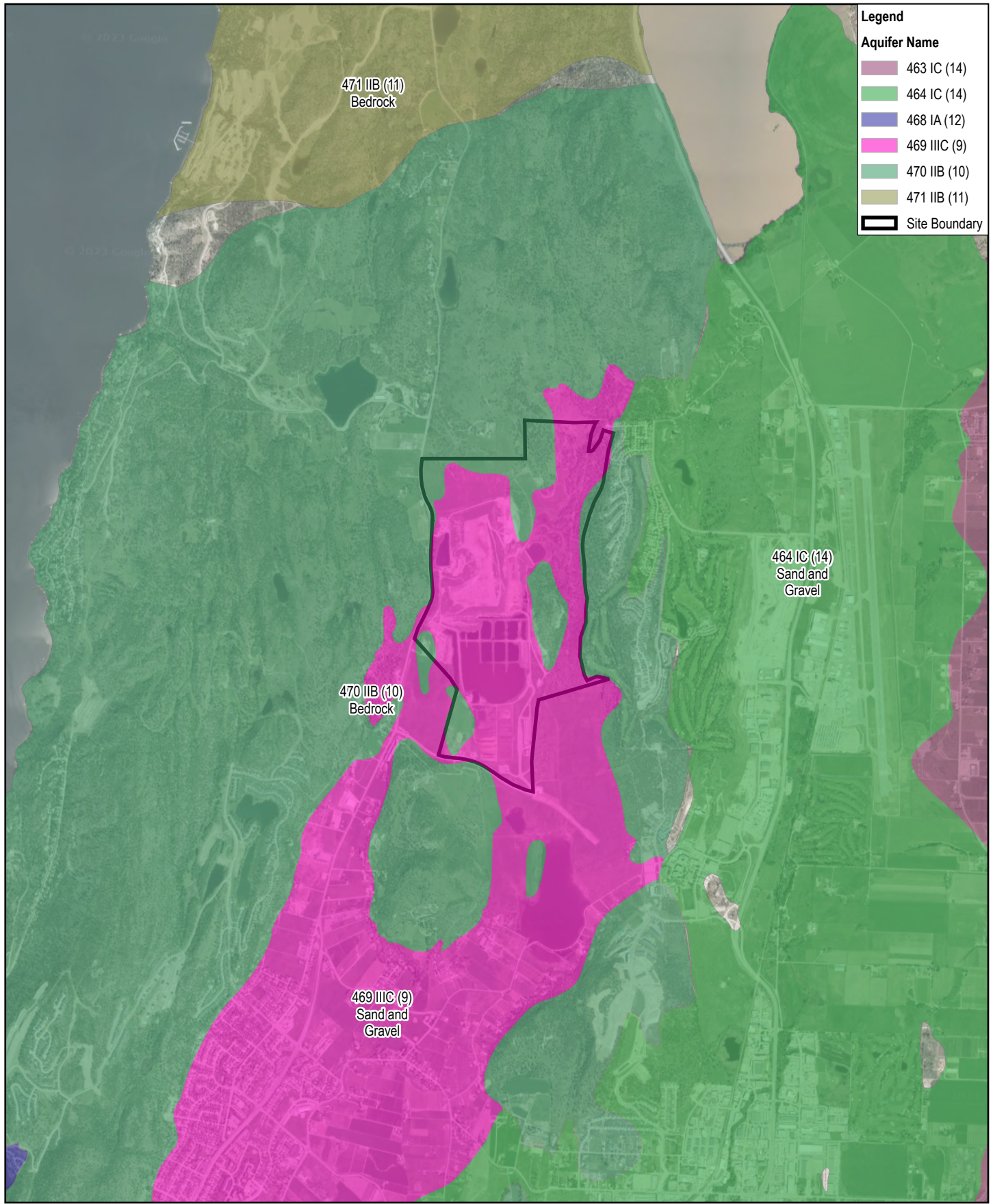
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CHARACTERIZATION REPORT

Project No. 12605725  
Date December 2023

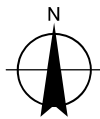
CROSS-SECTION MAP

FIGURE 3.4





Map Projection: Transverse Mercator  
Horizontal Datum: North American 1983  
Grid: NAD 1983 UTM Zone 11N



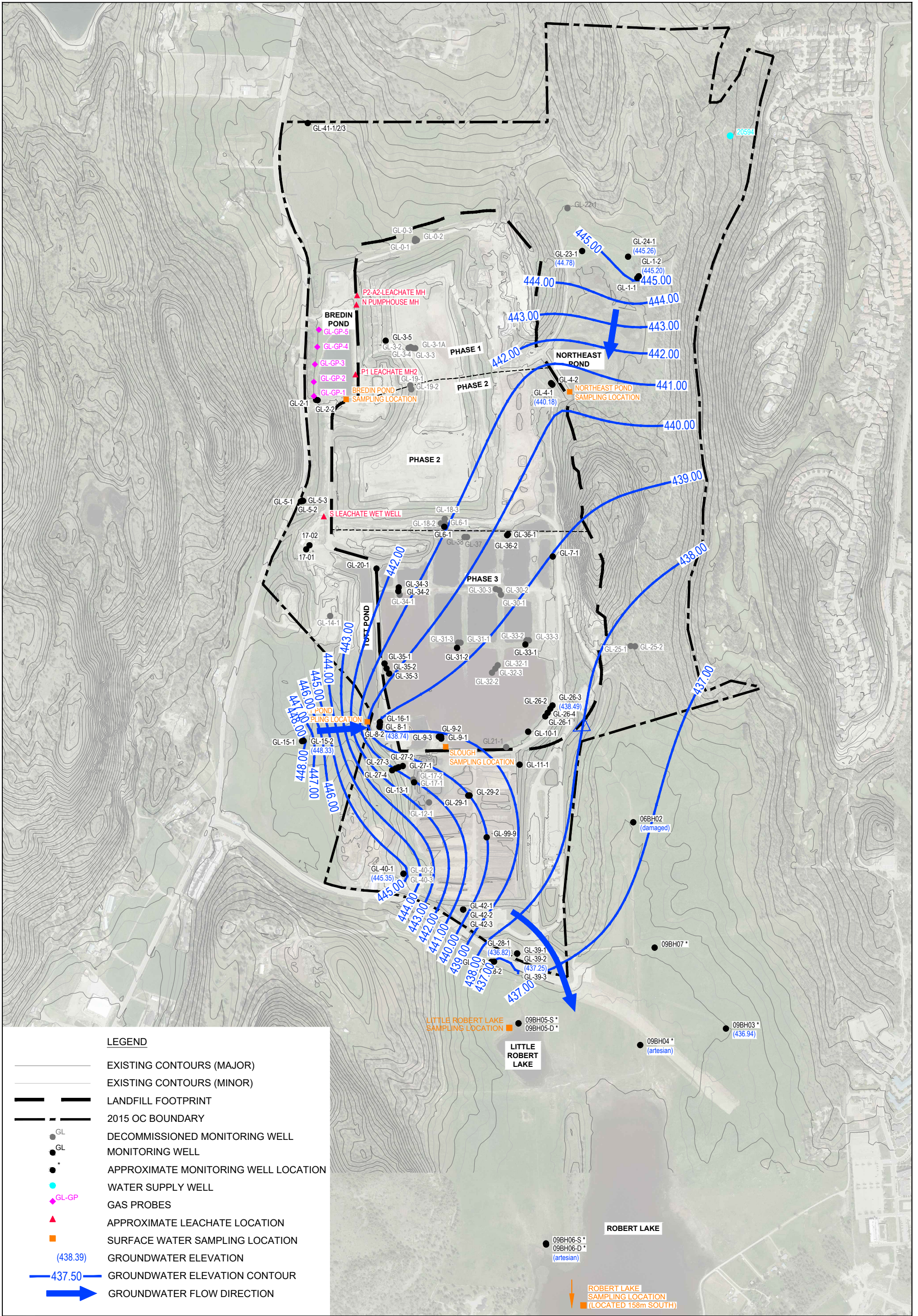
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CHARACTERIZATION REPORT**

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Revision No. -  
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**REGIONAL AQUIFER MAP**

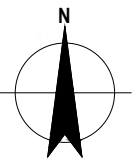
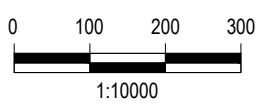
**FIGURE 3.5**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- GL  
● GL  
● APPROXIMATE MONITORING WELL LOCATION
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39)  
— GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION

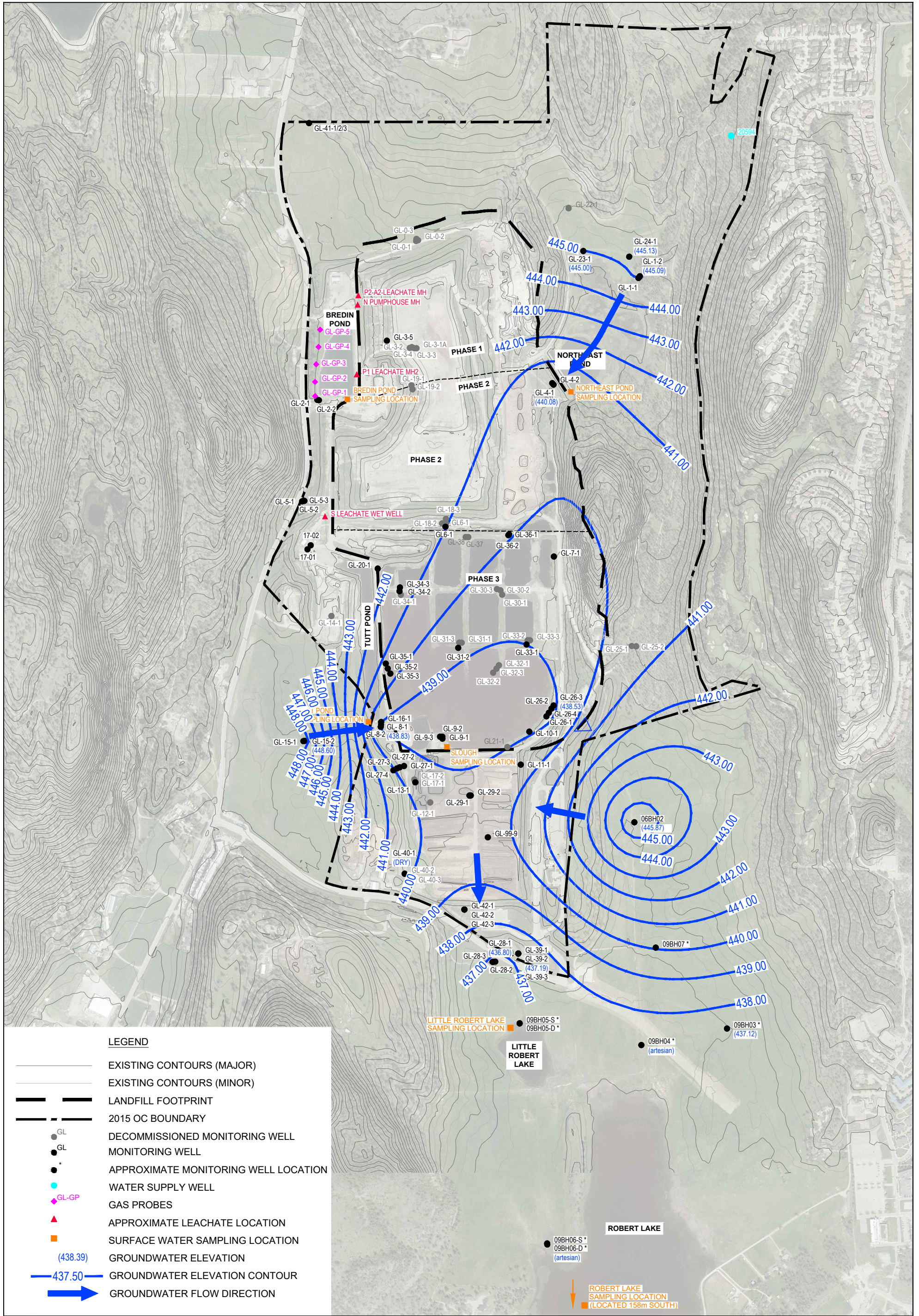


**CITY OF KELOWNA**  
**GLENMORE LANDFILL**  
**HYDROGEOLOGY AND HYDROLOGY**  
**CHARACTERIZATION REPORT**  
**SAND AND GRAVEL UNIT GROUNDWATER**  
**ELEVATION CONTOURS (MARCH 2022)**

Project No. 12605725  
 Date December 2023

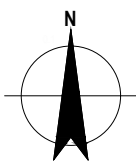
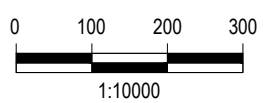
**FIGURE 3.6A**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- GL  
● GL  
● APPROXIMATE MONITORING WELL LOCATION
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39)  
— GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION

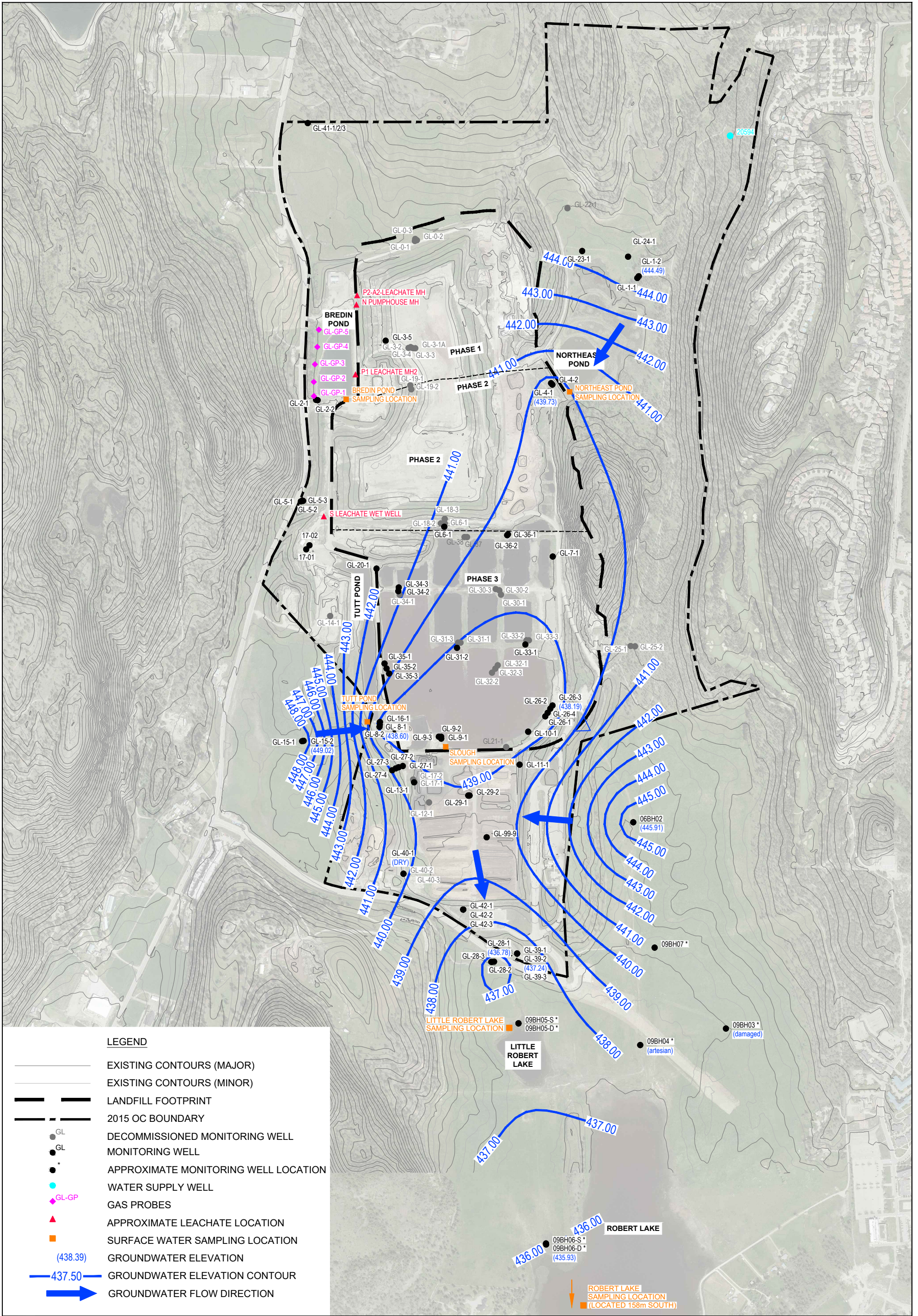


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 CHARACTERIZATION REPORT  
**SAND AND GRAVEL UNIT GROUNDWATER  
 ELEVATION CONTOURS (JUNE 2022)**

Project No. 12605725  
 Date December 2023

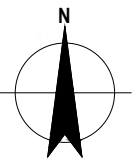
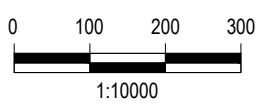
**FIGURE 3.6B**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- - - 2015 OC BOUNDARY
- GL  
● GL  
● DECOMMISSIONED MONITORING WELL
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39) GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION

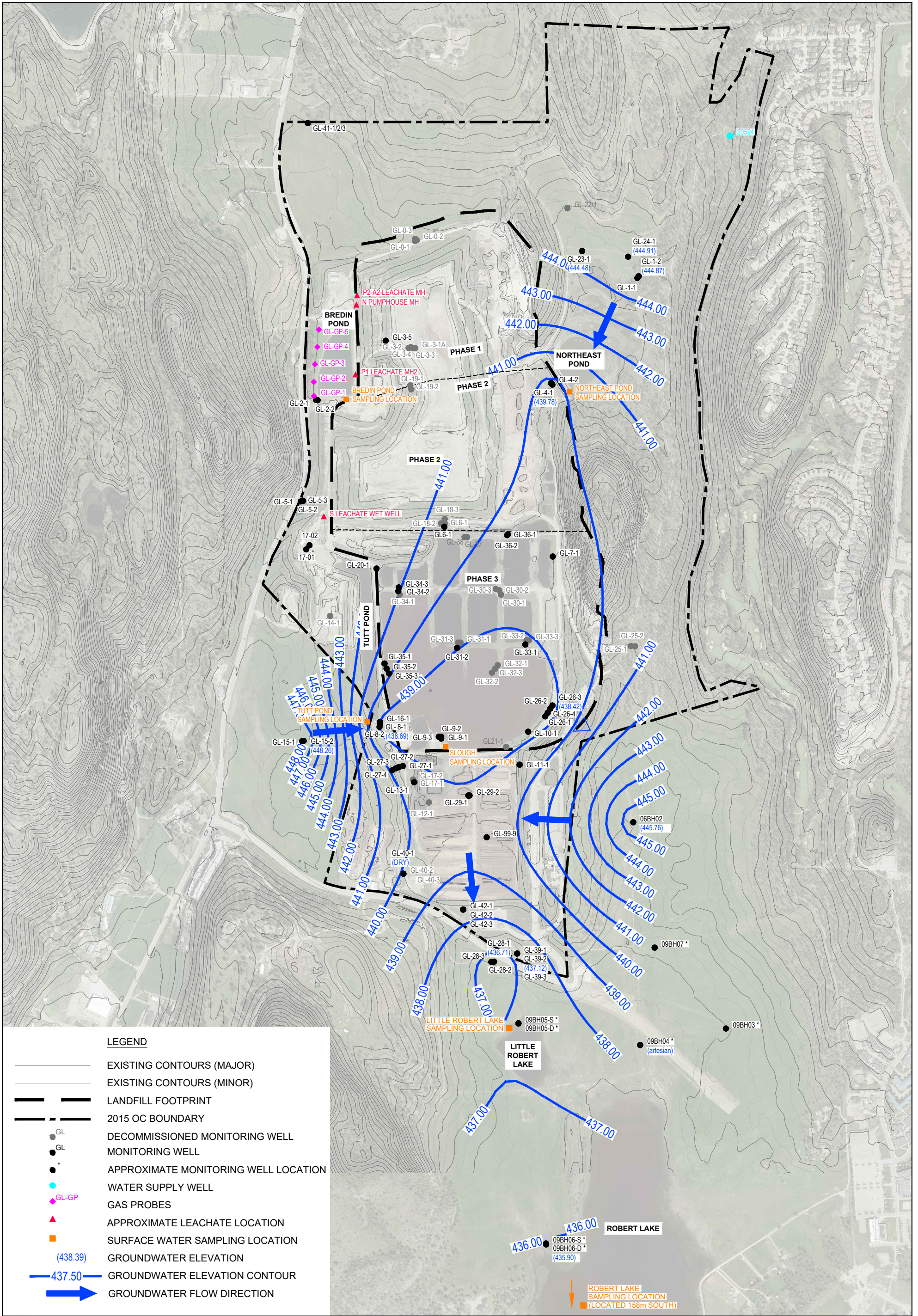


CITY OF KELOWNA  
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 CHARACTERIZATION REPORT  
**SAND AND GRAVEL UNIT GROUNDWATER  
 ELEVATION CONTOURS (AUGUST 2022)**

Project No. 12605725  
 Date December 2023

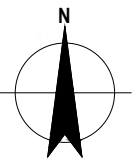
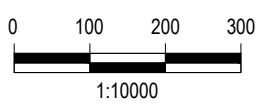
**FIGURE 3.6C**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- GL  
● GL  
● APPROXIMATE MONITORING WELL LOCATION
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39)  
— GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION



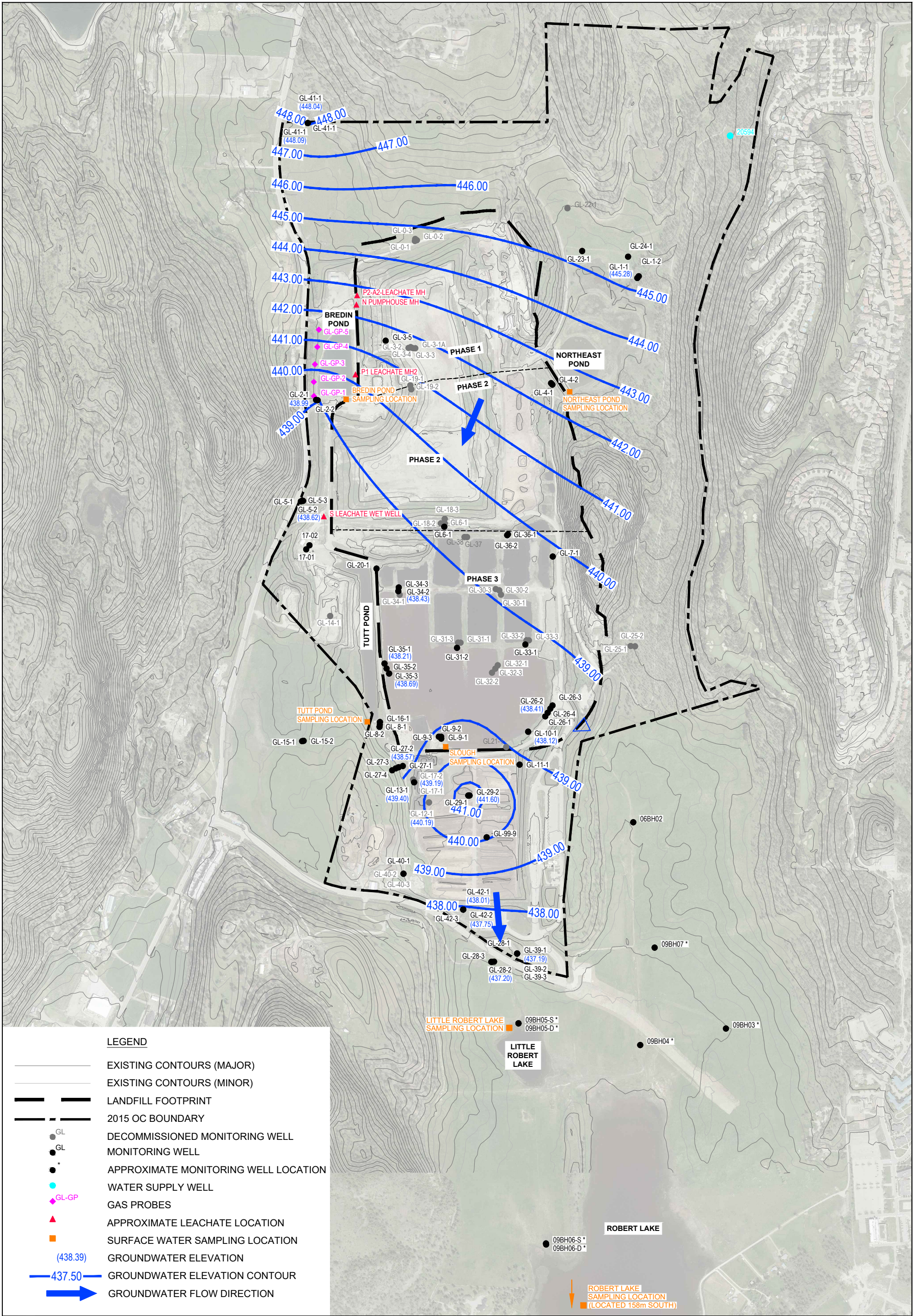
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 CHARACTERIZATION REPORT  
**SAND AND GRAVEL UNIT GROUNDWATER  
 ELEVATION CONTOURS (OCTOBER 2022)**

Project No. 12605725  
 Date December 2023

**FIGURE 3.6D**

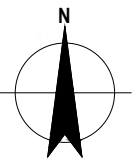
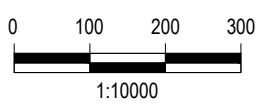
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 Plot Date: 05 December 2023 1:19 AM





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- GL  
● GL  
● APPROXIMATE MONITORING WELL LOCATION
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39) GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION

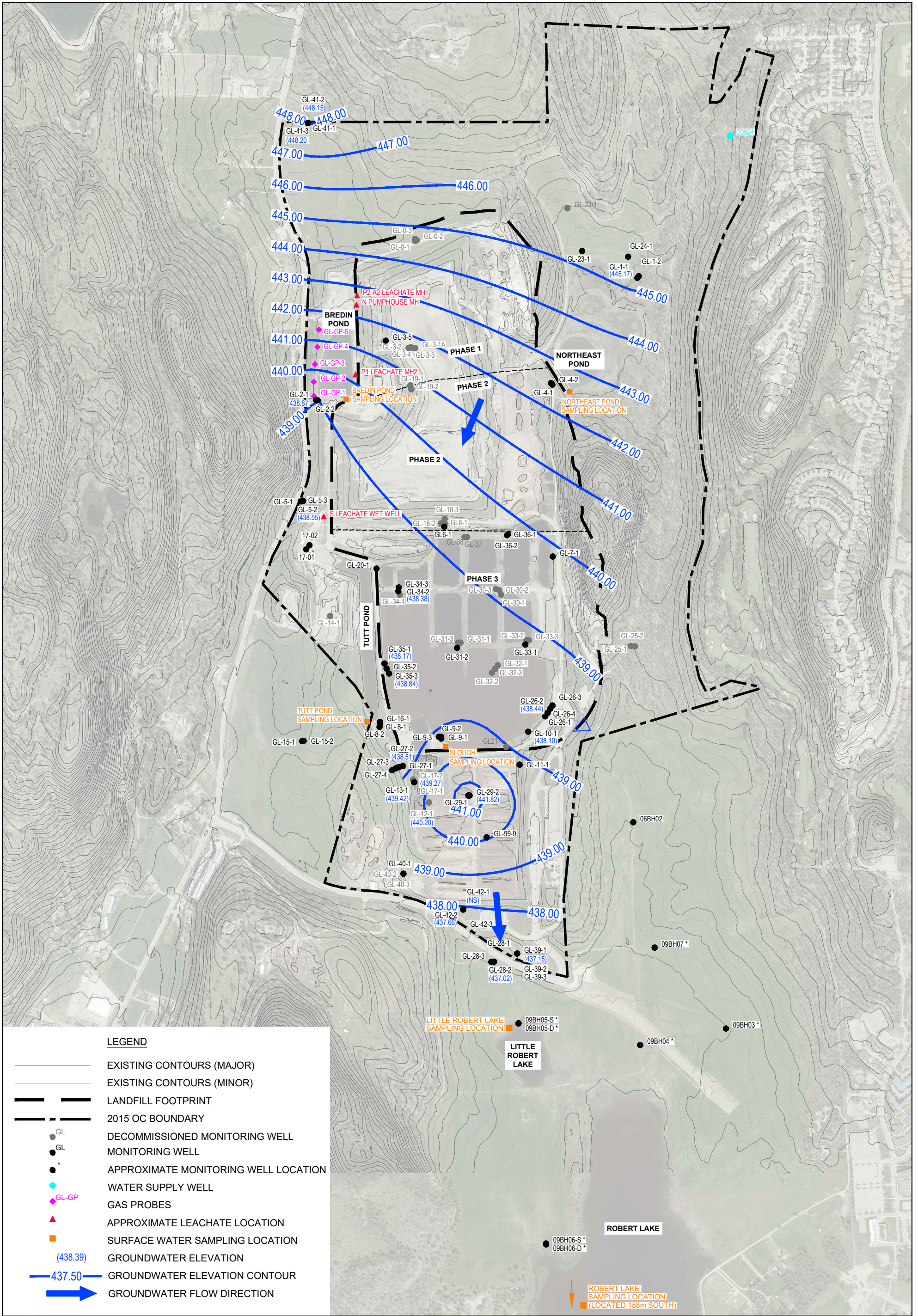


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 CHARACTERIZATION REPORT  
**TILL UNIT GROUNDWATER ELEVATION  
 CONTOURS (MARCH 2022)**

Project No. 12605725  
 Date December 2023

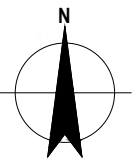
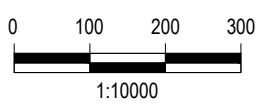
**FIGURE 3.7A**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- - - 2015 OC BOUNDARY
- GL  
● GL  
● APPROXIMATE MONITORING WELL LOCATION
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39) GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- ➔ GROUNDWATER FLOW DIRECTION

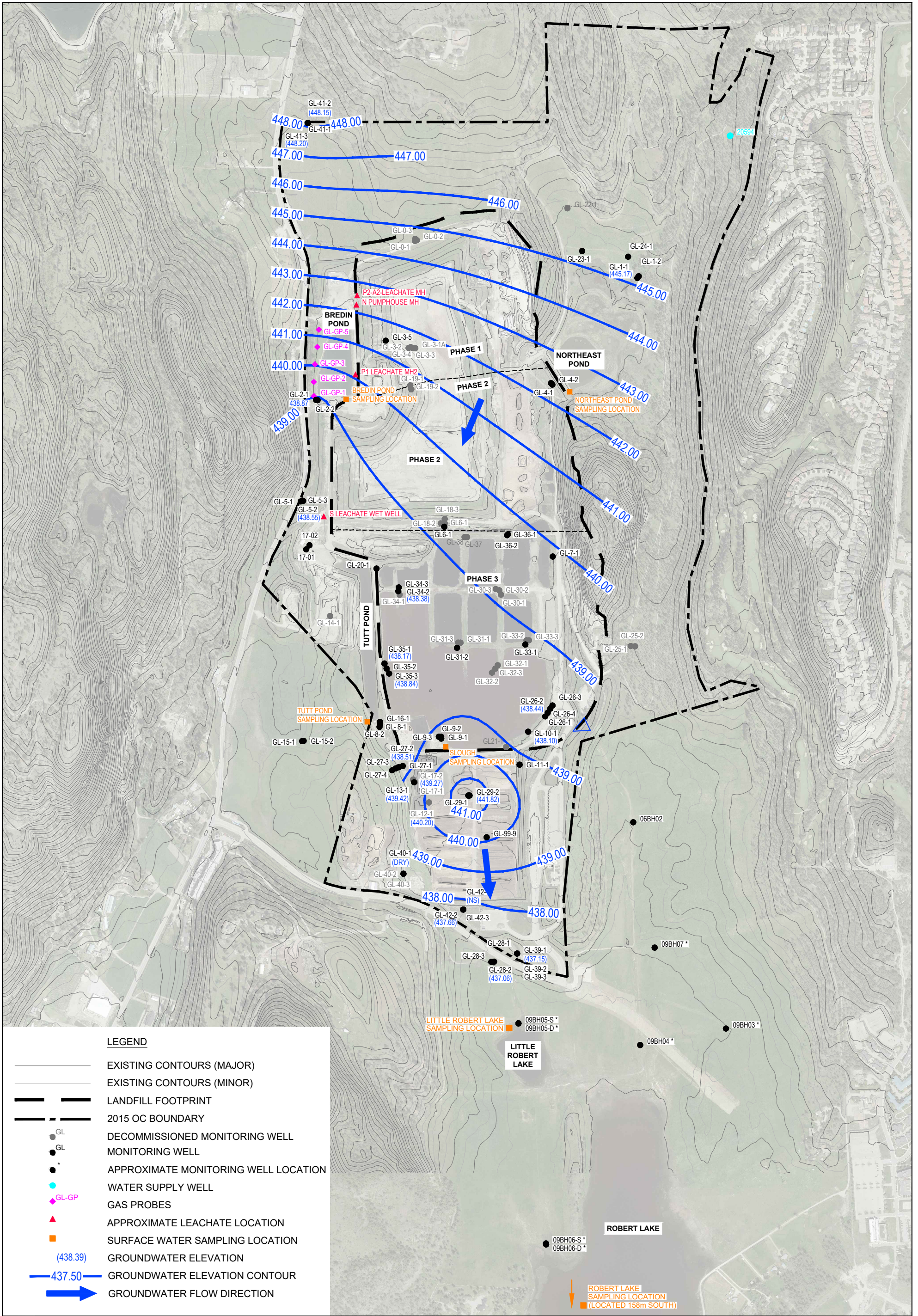


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 CHARACTERIZATION REPORT  
**TILL UNIT GROUNDWATER ELEVATION  
 CONTOURS (JUNE 2022)**

Project No. 12605725  
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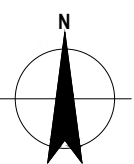
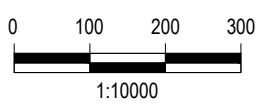
**FIGURE 3.7B**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- - - 2015 OC BOUNDARY
- GL  
● GL  
● DECOMMISSIONED MONITORING WELL
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39) GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION

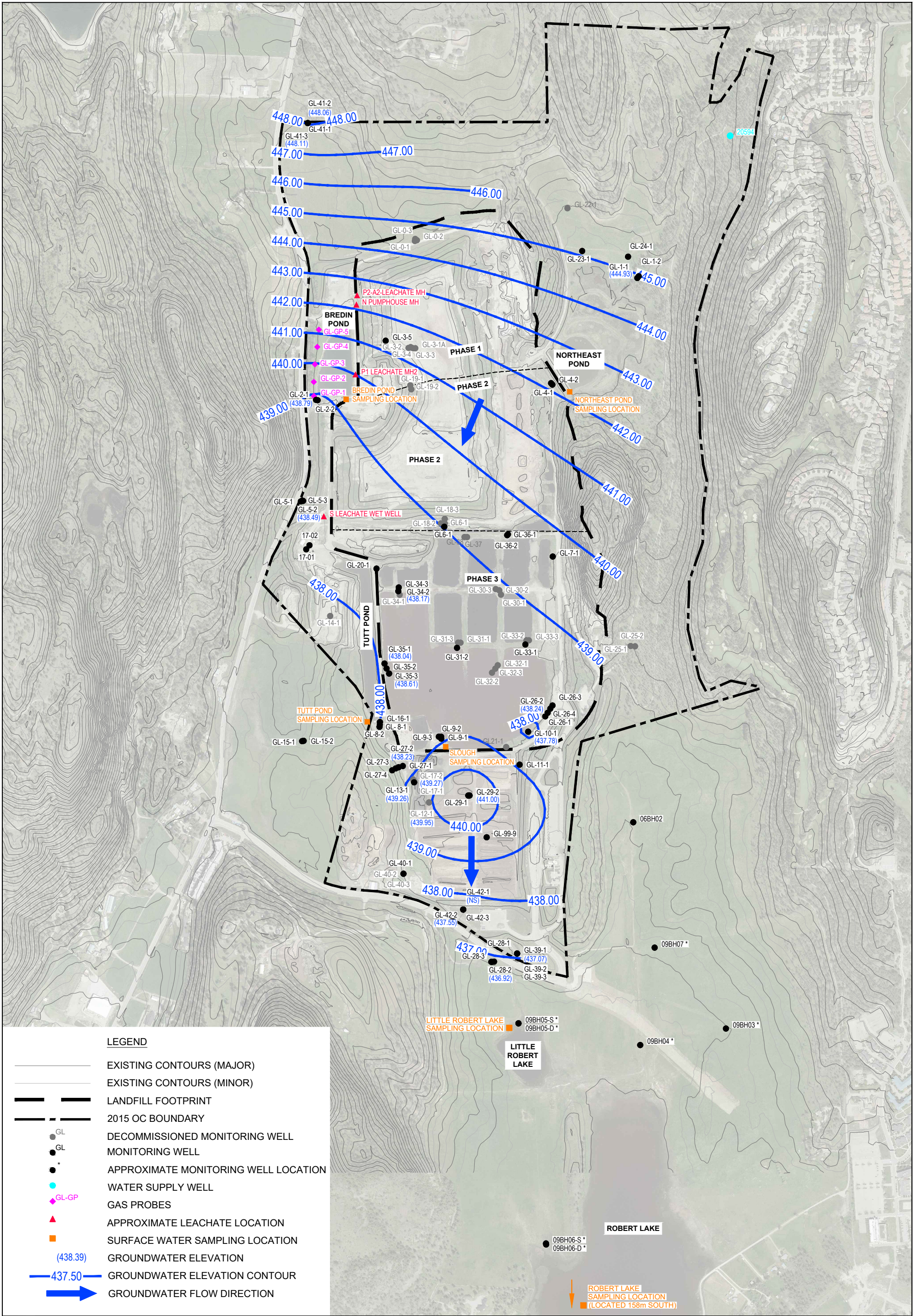


CITY OF KELOWNA  
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 CHARACTERIZATION REPORT  
**TILL UNIT GROUNDWATER ELEVATION  
 CONTOURS (AUGUST 2022)**

Project No. 12605725  
 Date December 2023

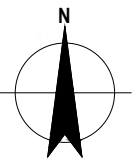
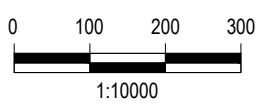
**FIGURE 3.7C**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- GL  
● GL  
● APPROXIMATE MONITORING WELL LOCATION
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- ◆ GL-GP  
◆ GAS PROBES
- ▲ APPROXIMATE LEACHATE LOCATION
- SURFACE WATER SAMPLING LOCATION
- (438.39)  
— GROUNDWATER ELEVATION
- 437.50— GROUNDWATER ELEVATION CONTOUR
- GROUNDWATER FLOW DIRECTION



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**TILL UNIT GROUNDWATER ELEVATION  
 CONTOURS (OCTOBER 2022)**

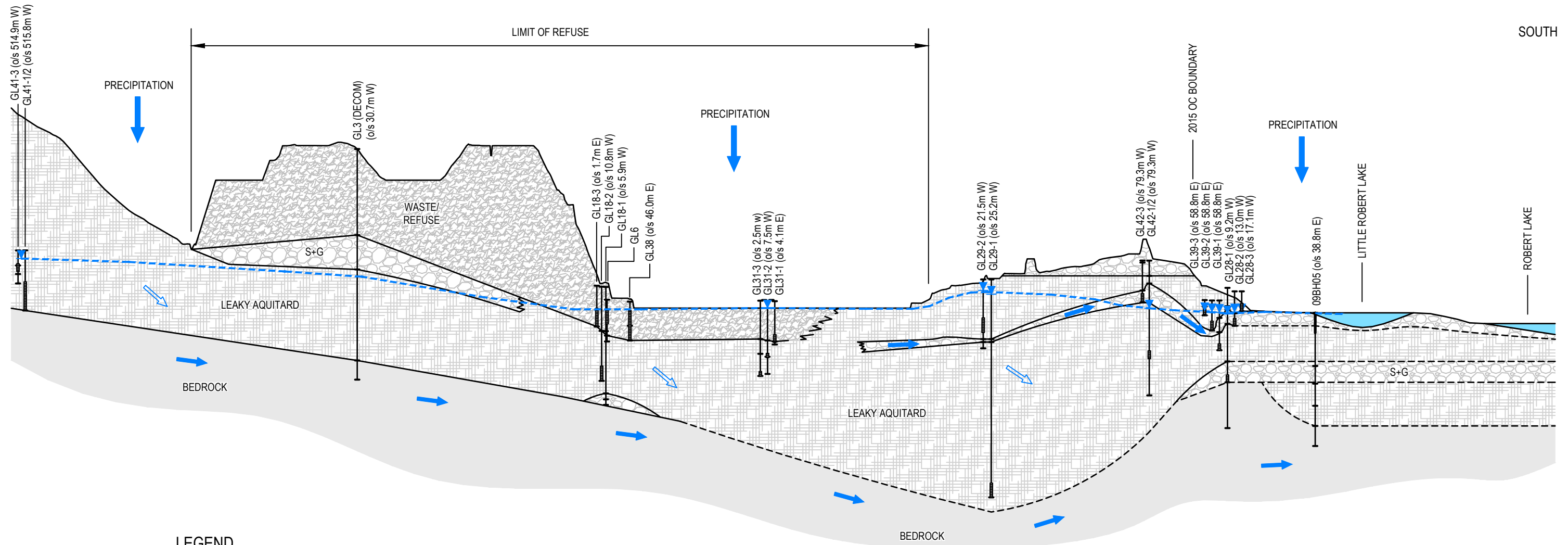
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 Date December 2023

**FIGURE 3.7D**











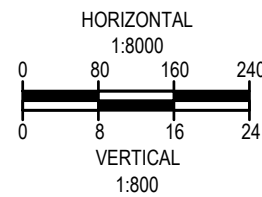
NORTH

SOUTH



**LEGEND**

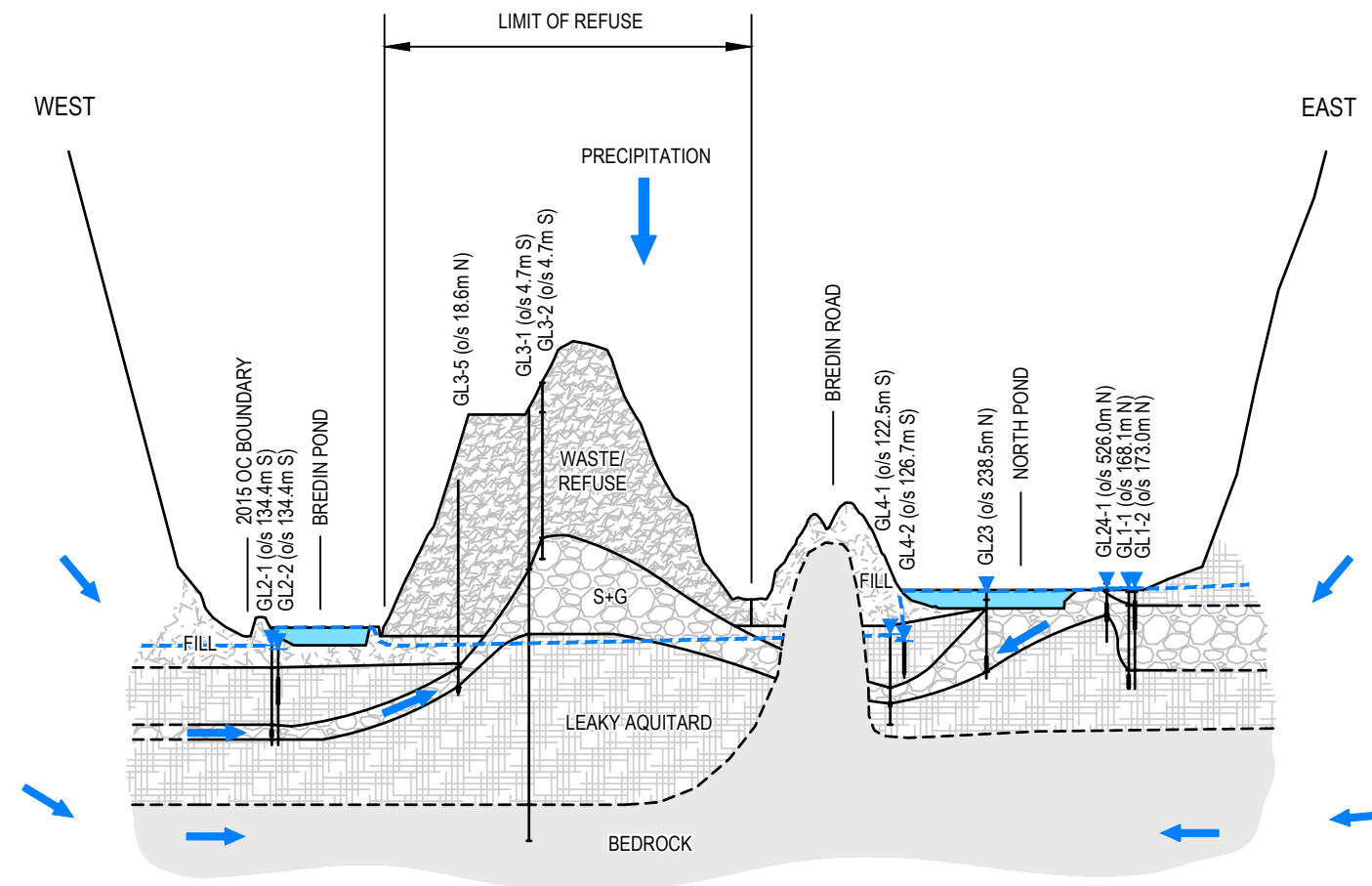
-  WASTE/REFUSE
-  FILL
-  SAND & GRAVEL
-  SAND
-  LEAKY AQUITARD
-  BEDROCK
-  GROUNDWATER ELEVATION (mASL) (MARCH 29, 2023)
-  GROUNDWATER FLOW DIRECTION











CITY OF KELOWNA  
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 CHARACTERIZATION REPORT  
 CONCEPTUAL FLOW MODEL -  
 SCHEMATIC CROSS-SECTION  
 NORTH - SOUTH

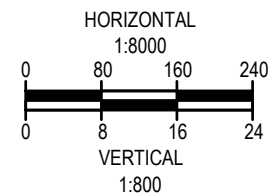
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 Date November 2023

**FIGURE 3.8**



**LEGEND**

-  WASTE/REFUSE
-  FILL
-  SAND & GRAVEL
-  SAND
-  LEAKY AQUITARD
-  BEDROCK
-  GROUNDWATER ELEVATION (mASL) (MARCH 29, 2023)
-  GROUNDWATER FLOW DIRECTION



NOTE:  
 PRIMARY FLOW PATHWAY FOR THE WEST-EAST  
 CROSS-SECTION IS TOWARDS THE READER.  
 ARROWS ILLUSTRATE SECONDARY FLOW PATHWAYS.



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 CHARACTERIZATION REPORT  
 CONCEPTUAL FLOW MODEL -  
 SCHEMATIC CROSS-SECTION  
 WEST - EAST

Project No. 12605725  
 Date October 2023

**FIGURE 3.9**

# Appendices

# **Appendix A**

## **Operational Certificate**



May 30, 2023

Tracking Number: 384004

Authorization Number: 12218

**REGISTERED MAIL**

CITY OF KELOWNA  
City Hall  
1435 Water Street  
Kelowna BC V1Y 1J4

Dear Operational Certificate Holder:

Enclosed is Amended Operational Certificate 12218 issued under the provisions of the *Environmental Management Act*. Your attention is respectfully directed to the terms and conditions outlined in the operational certificate. An annual fee will be determined according to the Permit Fees Regulation.

This operational certificate does not authorize entry upon, crossing over, or use for any purpose of private or Crown lands or works, unless and except as authorized by the owner of such lands or works. The responsibility for obtaining such authority rests with the operational certificate holder. It is also the responsibility of the operational certificate holder to ensure that all activities conducted under this authorization are carried out with regard to the rights of third parties, and comply with other applicable legislation that may be in force.

Requirements may also be specified by the *Environmental Management Act* and regulations including, but not limited to, the Contaminated Sites Regulation, Environmental Data Quality Assurance Regulation, Hazardous Waste Regulation, Landfill Gas Management Regulation, Organic Matter Recycling Regulation, Ozone Depleting Substances and Other Halocarbons Regulation, Recycling Regulation, Spill Reporting Regulation, Storage of Recyclable Material Regulation, Waste Discharge Regulation and Codes of Practice.

When a spill occurs, or there is an imminent risk of one occurring, the responsible person must ensure that it is reported in accordance with the Spill Reporting Regulation. Additional information on spill reporting requirements is available at [gov.bc.ca/reportaspill](http://gov.bc.ca/reportaspill).

This decision may be appealed to the Environmental Appeal Board in accordance with Part 8 of the *Environmental Management Act*. An appeal must be delivered within 30 days from the date that notice of this decision is given. For further information, please contact the Environmental Appeal Board at (250) 387-3464.

Administration of this operational certificate will be carried out by staff from the Environmental Protection Division's Regional Operations Branch. Documents pertinent to the operational certificate are to be submitted by email or electronic transfer to the director, in accordance with the ministry Data & Report Submissions website at: <http://www2.gov.bc.ca/gov/content/environment/waste-management/waste-discharge-authorization/data-and-report-submissions>, or as further instructed.

For more information about how the Ministry will assess compliance with your operational certificate please refer to [gov.bc.ca/environmentalcompliance](http://gov.bc.ca/environmentalcompliance).

For more information about how to make changes to your operational certificate and to access waste discharge amendment forms and guidance, please refer to [gov.bc.ca/wastedischarge-authorizations](http://gov.bc.ca/wastedischarge-authorizations).

Yours truly,



Carol Danyluk, P.Eng.  
for Director, *Environmental Management Act*  
Authorizations - South Region



**MINISTRY OF ENVIRONMENT  
AND CLIMATE CHANGE  
STRATEGY**

**OPERATIONAL CERTIFICATE**

12218

*Under the Provisions of the Environmental Management Act*

**CITY OF KELOWNA**

**City Hall  
1435 Water Street  
Kelowna BC V1Y 1J4**

is authorized to manage waste and recyclable material from the Regional District of Central Okanagan and environs (including Reserve Land), and also the Big White area, at the Glenmore Landfill located 9 kilometres north-east of the Kelowna city centre, British Columbia, subject to the conditions listed below. Contravention of any of these conditions is a violation of the *Environmental Management Act* and may result in prosecution.

This Operational Certificate supersedes all previous versions of Operational Certificate 12218 issued under the authority of the *Environmental Management Act*.

**Glossary**

Capitalized terms referred to in this authorization are defined below. Other terms used in this authorization have the same meaning as those defined in the *Environmental Management Act*, applicable regulations, and the Landfill Criteria;

"Contaminated Soil" means soil in which the concentration of a substance is greater than or equal to the lowest applicable industrial land use standard under the Contaminated Sites Regulation, and below any applicable standards that classify the soil as Hazardous Waste under the Hazardous Waste Regulation;

"Facility" means the Landfill including all facilities and works on the Facility Site including the Landfill, Leachate Management Works, Stormwater Management Works, and Facility Entrance;

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“Facility Entrance” means the authorized works in section 1.4.1 of this operational certificate;

“Facility Site” means the location of the Facility in section 1.5.1 of this operational certificate;

“Facility Site Boundary” means the perimeter boundary of the Facility Site;

“International Waste” means International waste as defined in the latest amended version of the Government of Canada International Waste Directive TAHD-DSAT-IE-2002-17-6, October 15, 2012;

“Landfill” means the authorized works in section 1.1.5 of this operational certificate;

“Landfill Criteria” means the Landfill Criteria for Municipal Solid Waste Second Edition June 2016, as amended or replaced from time to time;

“Leachate Management Works” means the authorized works in section 1.2.3 of this operational certificate;

“Province” means His Majesty the King in right of British Columbia;

“Regulatory Document” means any document that the operational certificate holder is required to cause to be prepared or submit to the director or the Province, pursuant to: (i) this authorization; (ii) any regulation made under the *Environmental Management Act* that regulates the Facility described in this authorization or the discharge of waste from that Facility; or (iii) any order issued under the *Environmental Management Act* directed against the operational certificate holder that is related to the Facility described in this authorization or the discharge of waste from that Facility;

“Significant Works” means the Landfill, Leachate Management Works, Stormwater Management Works;

“Stormwater Management Works” means the authorized works in section 1.3.1 of this operational certificate;

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## 1. AUTHORIZED DISCHARGES AND WORKS

### 1.1 Landfill

This section applies to the discharge of waste to the Landfill. The site reference number for this discharge is E104956.

- 1.1.1 The maximum authorized rate of waste discharge is:
- (a) 200,000 tonnes per calendar year of municipal solid waste;
  - (b) 30,000 tonnes per calendar year of Contaminated Soil;
  - (c) 1,000 tonnes per calendar year of International Waste.

- 1.1.2 The characteristics of the waste discharge to the Landfill must be:
- (a) municipal solid waste;
  - (b) soil;
  - (c) other waste as authorized in writing by the director,
  - (d) waste asbestos as per Section 40 of the Hazardous Waste Regulation(HWR) under the *Environmental Management Act*.

The following types of wastes must not be discharged:

- (1) Hazardous wastes, other than those specifically approved for disposal to authorized landfills, as defined in the Hazardous Waste Regulation (HWR) under the *Environmental Management Act*.
- (2) Anatomical, pathological, and untreated biomedical wastes as defined in the *Guidelines for the Management of Biomedical Wastes in Canada* (Canadian Council of Ministers of the Environment, February 1992) with exception of the limited biomedical wastes described within the City of Kelowna "Solid Waste Management Regulation Bylaw No. 10106, revised October 25, 2021".
- (3) Bulk liquids and semi-solid wastes, which contain free liquids, as determined by US EPA Method 9095A Paint Filter Liquids Test, Test Methods for Evaluating Solid Wastes-Physical/Chemical Methods (EPA Publication No. Sw-846).
- (4) Hog fuel, log yard debris and chipped wood waste. The reuse of these materials for temporary roads, dust control or a component of alternative daily cover is permitted.
- (5) Recyclable materials, including automobiles, white goods, other large metallic objects and tires

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- (6) Animal carcasses, with the exception of those of a domestic nature, those resulting from animal road kills, or those resulting from animal control activities of the Ministry of Environment's Conservation Officer Service (COS).
  - (7) Mortalities from agricultural operations, with the exception of carcasses that cannot be disposed of in accordance with the Code of Practice for Agricultural Environmental Management under the Environmental Management Act.
- 1.1.3 Composting of yard waste must be in accordance with the Organic Matter Recycling Regulation under the *Environmental Management Act*.
- 1.1.4 The discharged waste must originate from within the Regional District of Central Okanagan including Reserve Lands, and the Big White area, subject to the following:
- (a) Waste discharged to this landfill must satisfy the requirements of the Regional District of Central Okanagan Solid Waste Management Plan.
  - (b) Waste discharged to this landfill must not contravene the Regional Solid Waste Management Plan of the Regional District from which the waste originated.
- 1.1.5 The works authorized are a landfill with an area of 81 ha, and related appurtenances as specified in the most recent Design, Operations, and Closure Plan (DOCP) under Section 3.1.
- At a minimum, active landfill cells must include an impermeable base liner.
- 1.1.6 The waste discharge is authorized to the Landfill approximately located as shown on Site Plan A.
- 1.1.7 The operational certificate holder must ensure that the authorized works, excluding final cover in active landfilling areas, are complete and fully operational as per the most recent DOCP, under Section 3.1.

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## 1.2 Leachate Management

This section applies to the management of leachate from the Landfill.

- 1.2.1 The operational certificate holder must collect and convey the leachate from the Landfill prior to discharge.
- 1.2.2 The treated leachate effluent is authorized to be discharged to the City of Kelowna municipal sewage collection system.
- 1.2.3 The authorized works are leachate collection, conveyance, treatment and discharge works, and related appurtenances approximately located as shown on Site Plan A.
- 1.2.4 The operational certificate holder must ensure that the Leachate Management Works are complete and fully operational as per the most recent DOCP, under Section 3.1.

## 1.3 Stormwater Management

This section applies to the management of stormwater from the Landfill.

- 1.3.1 The authorized Stormwater Management works are specified in the most recent DOCP required under Section 3.1. The Stormwater Management works include use of Bredin Pond, Tutt Pond, Northeast Pond, conveyance systems (ditches, pipes, culverts), pump houses, irrigation systems and an overflow to the Slough. Stormwater that has been diverted to the Slough must be managed as leachate.
- 1.3.2 The operational certificate holder must ensure that the Stormwater Management Works are complete and fully operational as per the most recent DOCP, under Section 3.1.

## 1.4 Facility Entrance

This section applies to the Facility Entrance.

- 1.4.1 The authorized works are sign(s), gate, fence, weigh scale, attendant hut, waste and recyclable material drop-off and storage facilities, and related appurtenances approximately located as shown on Site Plan A.

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- 1.4.2 The operational certificate holder must ensure that the authorized works are complete and fully operational, as per the most recent DOCP, under Section 3.1.

1.5 **Location of Facility**

This section applies to the location of the Facility.

- 1.5.1 The location of the Facility is: (per Parcel Identification [PID])  
PID 024-353-281, Part of PID 024-353-302, PID 024-353-329,  
PID 024-353-752, PID 011-843-322, PID 011-843-331,  
PID 011-843-357, PID 011-843-365, PID 011-843-373,  
PID 011-845-163, PID 011-843-381, Part of PID 029-954-444,  
PID 029-954-398, PID 011-843-071, PID 011-843-187,  
PID 011-843-195, PID 011-843-209, PID 011-843-217, and  
PID 011-843-390

Approximately located as shown on Site Plan A

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## 2. GENERAL REQUIREMENTS

### 2.1 General Provisions

Where this Authorization provides that the director may require an action to be carried out, the operational certificate holder must carry out the action in accordance with the requirements of the director.

### 2.2 Use of Qualified Professional(s)

The operational certificate holder must cause a Qualified Professional to:

(a) Design and inspect the construction of the Significant Works, and,

(b) Certify documents related to the Significant Works including plans, specifications, drawings, construction reports, assessments, reviews, investigations, studies, surveys, programs, reports and as-built record drawings.

(c) Submit a completed Declaration of Competency and a Conflict of Interest Disclosure Statement with each document.

### 2.3 Regulatory Documents

(a) The operational certificate holder must retain all Regulatory Documents for a period of at least 7 years after they are made.

(b) If requested by a director or an officer, the operational certificate holder must submit the requested Regulatory Documents to the director or officer within 14 days of the request.

### 2.4 Construction Report(s)

(a) The operational certificate holder must cause a Qualified Professional to:

(i) carry out inspections before and during the construction or modification of Significant Works, and,

(ii) certify construction report(s) and submit them to the director as part of the Annual Report.

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(b) The construction report(s) must demonstrate that the Significant Works have been constructed in accordance with this operational certificate and the most recent DOCP, describe any technical changes that arose from the inspections and testing and how they were addressed, and include as-built record drawings of the constructed Significant Works, all the inspection and testing reports and results including geologic inspection report, quality control and quality assurance testing, soil test data including field and laboratory data, as described in the Landfill Criteria section 10.2 Construction Report(s).

## 2.5 **Buffer Zone**

The operational certificate holder must ensure that the footprint of the Landfill is located a minimum of 50 m from the Facility Site Boundary.

2.5.1 A berm of suitable material must be maintained to limit visibility of the active waste discharge area where practical for travelers using the Glenmore Road and John Hindle Drive.

## 2.6 **Additional Requirements**

The director may require the operational certificate holder to:

(a) Cause a Qualified Professional to certify and submit to the director additional, amended or improved documents of the Facility including plans, specifications, drawings, construction reports, assessments, reviews, investigations, studies, surveys, programs, reports and as-built record drawings.

(b) Carry out actions in accordance with the additional, amended or improved documents submitted, and additional actions as specified.

(c) Repair, alter, remove, improve or add to existing facilities and works, or construct new facilities and works, at the Facility.

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### **3. OPERATING AND PERFORMANCE REQUIREMENTS**

#### **3.1 Design, Operations, and Closure Plan (DOCP)**

(a) The following DOCP has been certified by a Qualified Professional and submitted by the operational certificate holder to the director on March 26, 2019; 2018 Design, Operations and Closure Plan – Glenmore Landfill – GHD Ltd.

(b) The operational certificate holder must cause a Qualified Professional to certify and submit an updated DOCP to the director, as necessary to keep the DOCP up to date, at least once every five years.

(c) The operational certificate holder must carry out the most recent DOCP and design, construct, operate, inspect, maintain, monitor, and close the Facility, in compliance with most recent DOCP.

(d) The DOCP must comply with the requirements of this operational certificate, include the information specified in all the relevant items listed in the Landfill Criteria Section 10.3 Design, Operations and Closure Plan, and, if a Landfill Criteria Upgrading Plan is required pursuant to Section 3.2 of this operational certificate, conform with the Landfill Criteria Upgrading Plan.

#### **3.2 Hydrogeology and Hydrology Characterization Report (HHCR)**

(a) The operational certificate holder must cause a Qualified Professional to certify and submit an up-to-date HHCR, to the director, on or before December 31, 2024.

(b) The HHCR must include the information specified in all the items listed in the Landfill Criteria, Section 10.1 Hydrogeology and Hydrology Characterization Report.

(c) The operational certificate holder must cause a Qualified Professional to certify and submit an updated HHCR to the director, at least once every ten years after the date specified in the preceding (a).

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3.3 **Multiple and/or Spare Works and Auxiliary Power Facilities**

The operational certificate holder must provide and install multiple and/or spare works and auxiliary power facilities to ensure that the Significant Works are operational as specified in this operational certificate, including during maintenance, breakdowns and electrical power outages.

3.4 **Maintenance of the Facility**

(a) The operational certificate holder must cause persons that are qualified and trained, to operate, regularly inspect, and maintain the Facility, in good working order.

(b) The operational certificate holder must prepare documents of the qualification and training of the persons operating, inspecting and maintaining the Facility, and of Facility inspections, operation and maintenance.

3.5 **Facility Manager and Operator Certification**

(a) The operational certificate holder must ensure that at least one person responsible for the management of the Facility is certified, and maintains certification by The Solid Waste Association of North America (SWANA) as a Manager of Landfill Operations, and at least one person responsible for the operation of the Facility is certified, and maintains certification by SWANA as a Landfill Operator.

(b) The operational certificate holder must prepare documents of the SWANA certification and training of the person(s) responsible for the management and operation of the Facility.

3.6 **Stormwater Quality**

(a) The operational certificate holder must ensure that the Facility does not cause the concentration of any substance in the stormwater flowing from the Facility Site Boundary, to be of worse quality than:

(i) the applicable long-term average, short-term maximum, maximum allowable concentration, maximum acceptable concentration, and/or aesthetic objective, specified in the British Columbia Approved and Working Water Quality Guidelines, for the applicable water use(s), for that substance,

or,

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(ii) if the local background concentration of any substance is of worse quality than (i), the local background concentration of that substance.

(b) The operational certificate holder must cause a Qualified Professional to determine the applicable water use(s) and the applicable long-term average, short-term maximum, maximum allowable concentration, maximum acceptable concentration, and/or aesthetic objective, specified in the British Columbia Approved and Working Water Quality Guidelines, for the applicable water use(s), for substances, and, if the preceding (a)(ii) is being used, the local background concentration of substance(s), and include such determinations in the Annual Operations and Monitoring Report.

### 3.7 Groundwater Quality

(a) The operational certificate holder must ensure that the Facility does not cause the concentration of any substance in groundwater flowing from the Facility Site Boundary to be greater than:

(i) the lowest of the Contaminated Sites Regulation Generic Numerical Water Standards, for the applicable water use(s), for that substance.

or,

(ii) if the local background concentration of any substance is greater than (i), the local background concentration of that substance.

(b) The operational certificate holder must cause a Qualified Professional to determine the applicable water use(s) in accordance with the latest approved version of Protocol 21 for Contaminated Sites, Water Use Determination, and, if the preceding (a)(ii) is being used, the local background concentration of substance(s) in accordance with the latest approved version of Protocol 9 for Contaminated Sites, Determining Background Groundwater Quality or another method recommended by a Qualified Professional, and include such determinations in the Annual Operations and Monitoring Report.

### 3.8 Complaints

The operational certificate holder must prepare documents of complaints with regard to matters relevant to this operational certificate, including environmental, bear, and nuisance complaints. These documents must include the source and nature of the complaint, actions, responses, and corresponding dates and times.

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### 3.9 Soil

All soil discharged at the Landfill site must be beneficially reused as cover, berms, and/or roads within the waste cells.

Soil containing contaminants in concentrations that are less than the threshold to be characterized as Contaminated Soil does not contribute to the annual discharge limit in Section 1.1.1(b).

Contaminated Soil must not be used as final cover or deposited within 1.2 meters of the seasonal high groundwater level.

## 4. MONITORING

### 4.1 Monitoring and Sampling Facilities

The operational certificate holder must maintain measurement, monitoring and sampling facilities for waste, leachate, treated leachate effluent, stormwater, groundwater, and landfill gas, in compliance with, and including at locations specified in, the most recent DOCP under Section 3.1.

### 4.2 Monitoring and Sampling

The operational certificate holder must carry out measurement, monitoring and sampling of waste, leachate, treated leachate effluent, stormwater, groundwater, and landfill gas, in compliance with, and including at frequencies and for substances specified in, the most recent DOCP under Section 3.1.

### 4.3 Sampling Procedures

The operational certificate holder must carry out sampling in accordance with the procedures described in the "British Columbia Field Sampling Manual for Continuous Monitoring and the Collection of Air, Air-Emission, Water, Wastewater, Soil, Sediment, and Biological Samples, 2013 Edition (Permittee)" or most recent edition, or by alternative procedures as authorized by the director. A copy of the above manual is available on the Ministry web page at

<https://www2.gov.bc.ca/gov/content/environment/research-monitoring-reporting/monitoring/laboratory-standards-quality-assurance>.

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#### 4.4 **Analytical Procedures**

The operational certificate holder must carry out analyses in accordance with procedures described in the "British Columbia Laboratory Manual (2015 Permittee Edition)", or the most recent edition or by alternative procedures as authorized by the director. A copy of the above manual is available on the Ministry web page at <https://www2.gov.bc.ca/gov/content/environment/research-monitoring-reporting/monitoring/laboratory-standards-quality-assurance>.

#### 4.5 **Quality Assurance**

(a) The operational certificate holder must obtain from the analytical laboratory(ies) their precision, accuracy and blank data for each sample set submitted by the operational certificate holder and an evaluation of the data acceptability, based on criteria set by such laboratory.

(b) The operational certificate holder must collect, prepare and submit for analysis by the analytical laboratory(ies) quality control (QC) samples for each parameter. As a minimum,  
-The number of QC samples should be 20% of all samples collected (environmental + QC samples) within 48 hours of each other, and,  
-Include duplicate, field and trip blank samples for each parameter.

(c) The operational certificate holder must submit samples to analytical laboratory(ies) that meet the definition of a qualified laboratory under the Environmental Data Quality Assurance Regulation.

#### 4.6 **Data Uploading**

The operational certificate holder must cause the analytical laboratory(ies) to upload monitoring and analytical data required by this operational certificate, to the Ministry's Environmental Monitoring System (EMS) database, on or before 30 days after the data is available, or as further instructed by the director.

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## 5. **REPORTING**

### 5.1 **Electronic Reporting**

The operational certificate holder must submit all data required to be submitted under this section by email to the Ministry's Routine Environmental Reporting Submission Mailbox (RERSM) at [Envauthorizationsreporting@gov.bc.ca](mailto:Envauthorizationsreporting@gov.bc.ca) or as otherwise instructed by the director. For guidelines on how to properly name the files and email subject lines or for more information visit the Ministry website:

<https://www2.gov.bc.ca/gov/content/environment/waste-management/waste-discharge-authorization/data-and-report-submissions/routine-environmental-reporting-submission-mailbox>.

### 5.2 **Non-compliance Notification**

The operational certificate holder must immediately notify the director by email at [EnvironmentalCompliance@gov.bc.ca](mailto:EnvironmentalCompliance@gov.bc.ca), or as otherwise instructed by the director of any non-compliance with the requirements of this Authorization and must immediately take remedial action to remedy any effects of such non-compliance.

### 5.3 **Non-compliance Reporting**

The operational certificate holder must, within 30 days of any non-compliance event, submit to the director a written report that includes, but is not necessarily limited to, the following:

- (a) all relevant test results obtained by the operational certificate holder related to the non-compliance,
- (b) an explanation of the most probable cause(s) of the non-compliance, and
- (c) a description of remedial action planned and/or taken by the operational certificate holder to prevent similar non-compliance(s) in the future.

The operational certificate holder must submit all non-compliance reporting required to be submitted under this section by email to the Ministry's Compliance Reporting Submission Mailbox (CRSM) at

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[EnvironmentalCompliance@gov.bc.ca](mailto:EnvironmentalCompliance@gov.bc.ca) or as otherwise instructed by the director. For guidelines on how to report a non-compliance or for more information visit the Ministry website:  
<http://www2.gov.bc.ca/gov/content/environment/waste-management/waste-discharge-authorization/data-and-report-submissions/non-compliance-reporting-mailbox>.

#### 5.4 **Annual Operations and Monitoring Report**

(a) The operational certificate holder must cause a Qualified Professional to certify and submit an Annual Operations and Monitoring Report, for the preceding calendar year, to the director on or before March 31 of each year.

(b) The Annual Operations and Monitoring Report must include the following information:

Operations Report:

- (i) Tonnages and categories of waste and recyclable material received at the Facility, and how they were managed,
- (ii) Tonnages and categories of waste discharged to the Landfill,
- (iii) Leachate volume collected and conveyed to municipal sewer system, and leachate quality;
- (iv) Remaining volume and life of the Landfill;
- (v) Summary of DOCP implementation;
- (vi) Summary of screening/revegetation efforts;
- (vii) Summary of construction report(s);
- (viii) Summary of complaints;
- (ix) Summary of non-compliance notifications and reporting;
- (x) For the next calendar year, summary of planned DOCP implementation and construction of Significant Works,

Environmental Monitoring Plan Report:

- (xi) Site plan(s), sampling locations, stormwater and surface water flow paths, groundwater elevations, gradients and flow directions;
- (xii) Measurement, monitoring and sampling facilities, locations, frequencies, substances, sampling and analytical procedures, quality assurance and quality control;
- (xiii) Data including laboratory analysis and quality assurance and quality control results;
- (xiv) Data tabulation, trend analysis, graphs, diagrams, and interpretation;

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- (xv) Discussion and determinations required by section 3.5 of this operational certificate,
- (xvi) Discussion and determination of compliance with section 3.6 of this operational certificate,
- (xvii) Discussion and determination of compliance with section 3.7 of this operational certificate,
- (xviii) Results, conclusions, recommendations and changes to the environmental monitoring plan.

## 5.5 **Publication of Documents**

The Ministry of Environment and Climate Change Strategy publishes Regulatory Documents on its website for the purpose of research, public education and to provide transparency in the administration of environmental laws. The operational certificate holder acknowledges that the Province may publish any Regulatory Documents submitted by the operational certificate holder, excluding information that would be exempted from disclosure if the document was disclosed pursuant to a request under section 5 of the *Freedom of Information and Protection of Privacy Act*, and the operational certificate holder consents to such publication by the Province.

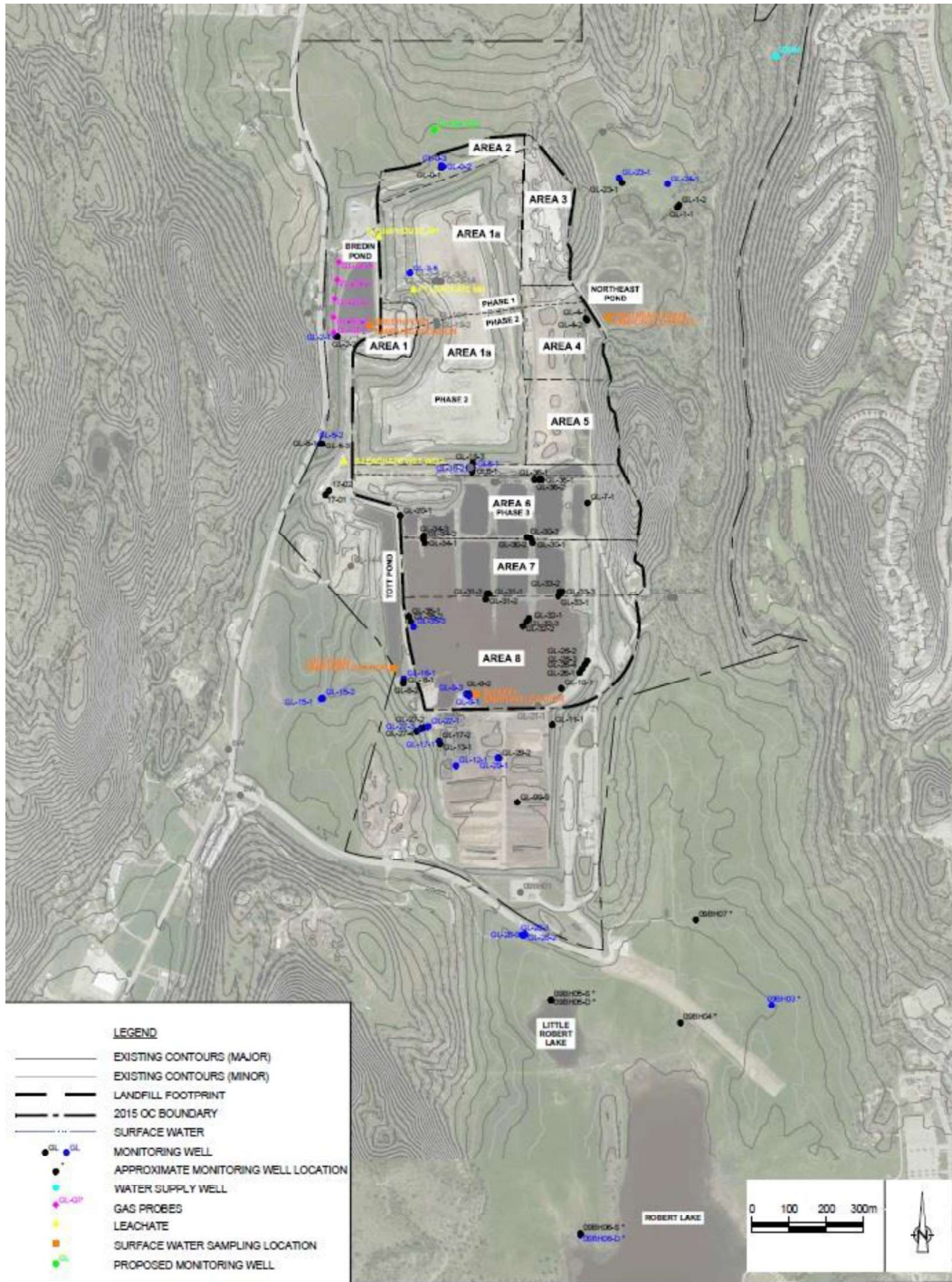
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SITE PLAN



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# **Appendix B**

**Land and Water Use Information**



## Well Summary

**Well Tag Number:** 2936  
**Well Identification Plate Number:**  
**Owner Name:** BAKER  
**Intended Water Use:** Private Domestic  
**Artesian Condition:** No

**Well Status:** New  
**Well Class:** Water Supply  
**Well Subclass:**  
**Aquifer Number:**  
**Technical Report:** N/A

**Observation Well Number:**  
**Observation Well Status:**  
**Environmental Monitoring System (EMS) ID:**  
**Alternative specs submitted:** No  
**Drinking Water Area Indicator:** No

## Licensing Information

**Licensed Status:** Unlicensed

**Licence Number:**

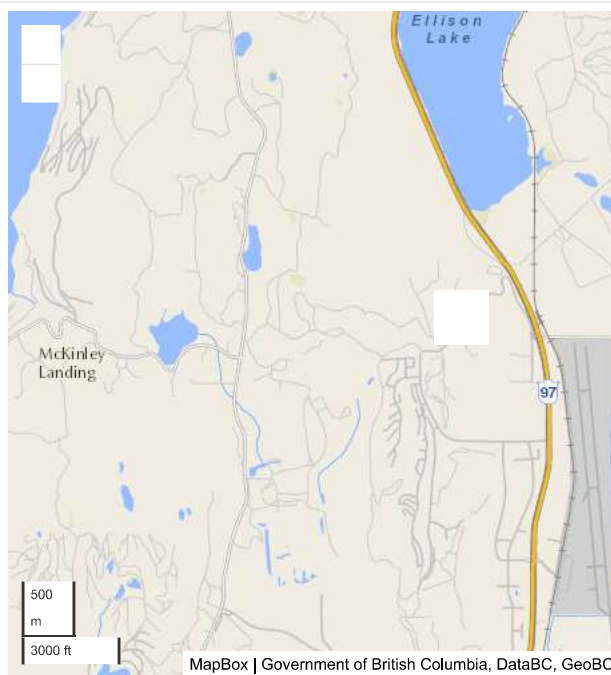
## Location Information

**Street Address:** DRY VALLEY RD  
**Town/City:** KELOWNA

### Legal Description:

Lot	8
Plan	1453
District Lot	
Block	
Section	23
Township	23
Range	
Land District	41
Property Identification Description (PID)	

### Description of Well Location:



### Geographic Coordinates - North American Datum of 1983 (NAD 83)

**Latitude:** 49.96988      **Longitude:** -119.39714  
**UTM Easting:** 328105      **UTM Northing:** 5538036  
**Zone:** 11      **Coordinate Acquisition Code:** (20 m accuracy) Digitized from 1:5,000 mapping

## Well Activity

Activity	Work Start Date	Work End Date	Drilling Company	Date Entered
Legacy record	1948-01-01	1948-01-01	Unknown	August 13th 2003 at 5:38 AM

## Well Work Dates

Start Date of Construction	End Date of Construction	Start Date of Alteration	End Date of Alteration	Start Date of Decommission	End Date of Decommission
1948-01-01	1948-01-01				

## Well Completion Data

Total Depth Drilled:  
 Finished Well Depth: 30 ft bgl  
 Final Casing Stick Up:  
 Depth to Bedrock:  
 Ground elevation:

Estimated Well Yield: 0 USgpm  
 Well Cap:  
 Well Disinfected Status: Not Disinfected  
 Drilling Method: Excavating  
 Method of determining elevation: Unknown

Static Water Level (BTOC): 23 feet btoc  
 Artesian Flow:  
 Artesian Pressure (head):  
 Artesian Pressure (PSI):  
 Orientation of Well: VERTICAL

## Lithology

From (ft bgl)	To (ft bgl)	Raw Data	Description	Moisture	Colour	Hardness	Observations	Water Bearing Flow Estimate (USGPM)
There are no records to show								

## Casing Details

From (ft bgl)	To (ft bgl)	Casing Type	Casing Material	Diameter (in)	Wall Thickness (in)	Drive Shoe
There are no records to show						

## Surface Seal and Backfill Details

Surface Seal Material:  
 Surface Seal Installation Method:  
 Surface Seal Thickness:  
 Surface Seal Depth:

Backfill Material Above Surface Seal:  
 Backfill Depth:

## Liner Details

Liner Material:  
 Liner Diameter:  
 Liner from:

Liner Thickness:  
 Liner to:

### Liner perforations

From (ft bgl)	To (ft bgl)
There are no records to show	

## Screen Details

Intake Method:  
 Type:  
 Material:  
 Opening:  
 Bottom:

### Installed Screens

From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size
There are no records to show				

## Well Development

Developed by:

Development Total Duration:

## Well Yield

Estimation Method:  
 Static Water Level Before Test:  
 Hydrofracturing Performed: No

Estimation Rate:  
 Drawdown:  
 Increase in Yield Due to Hydrofracturing:

Estimation Duration:

## Well Decommission Information

Reason for Decommission:  
 Sealant Material:  
 Decommission Details:

Method of Decommission:  
 Backfill Material:

## Pumping Test Information and Aquifer Parameters

Start Date	Pumping Test Description	Test Duration (min)	Boundary Effect	Transmissivity Storativity (m <sup>2</sup> /day)	Hydraulic Conductivity (m/day)	Specific Yield	Specific Capacity (L/s/m)	Analysis Method	Comments
There are no records to show									

## Comments

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NO LOG GIVEN. NO LITHOLOGIC INFORMATION AVAILABLE. T.D. 30'

## Documents

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- [WTN 2936 Well Record.pdf](#)

## Disclaimer

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# Groundwater Wells and Aquifers

## Well Summary

<b>Well Tag Number:</b> 19830	<b>Well Status:</b> New	<b>Observation Well Number:</b>
<b>Well Identification Plate Number:</b>	<b>Well Class:</b> Unknown	<b>Observation Well Status:</b>
<b>Owner Name:</b> C STEPHENS	<b>Well Subclass:</b>	<b>Environmental Monitoring System (EMS) ID:</b>
<b>Intended Water Use:</b> Not Applicable	<b>Aquifer Number:</b> <u>1191</u>	<b>Alternative specs submitted:</b> No
<b>Artesian Condition:</b> No	<b>Technical Report:</b> N/A	<b>Drinking Water Area Indicator:</b> No

## Licensing Information

**Licensed Status:** Unlicensed      **Licence Number:**

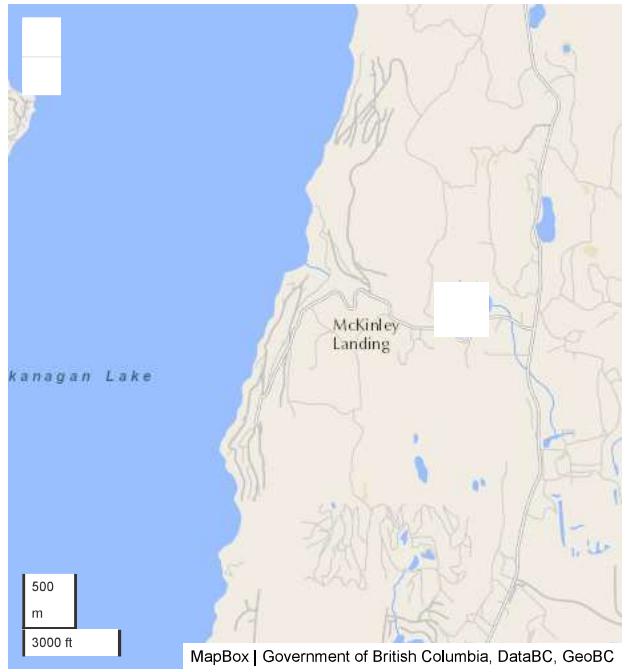
## Location Information

**Street Address:**  
**Town/City:** KELOWNA

**Legal Description:**

Lot	
Plan	
District Lot	
Block	
Section	21
Township	23
Range	
Land District	41
Property Identification Description (PID)	

**Description of Well Location:**



**Geographic Coordinates - North American Datum of 1983 (NAD 83)**

**Latitude:** 49.96811      **Longitude:** -119.435  
**UTM Easting:** 325384      **UTM Northing:** 5537927  
**Zone:** 11      **Coordinate Acquisition Code:** (100 m accuracy) Digitized from old Dept. of Lands, Forests and Water Resources maps

## Well Activity

Activity	Work Start Date	Work End Date	Drilling Company	Date Entered
Legacy record	1966-02-01	1966-02-01	Art Moore & Son	August 13th 2003 at 3:04 AM

## Well Work Dates

Start Date of Construction	End Date of Construction	Start Date of Alteration	End Date of Alteration	Start Date of Decommission	End Date of Decommission
1966-02-01	1966-02-01				

## Well Completion Data

**Total Depth Drilled:**  
**Finished Well Depth:** 25 ft bgl  
**Final Casing Stick Up:**  
**Depth to Bedrock:** 25 feet bgl  
**Ground elevation:**

**Estimated Well Yield:** 0 USgpm  
**Well Cap:**  
**Well Disinfected Status:** Not Disinfected  
**Drilling Method:** Other  
**Method of determining elevation:** Unknown

**Static Water Level (BTOC):**  
**Artesian Flow:**  
**Artesian Pressure (head):**  
**Artesian Pressure (PSI):**  
**Orientation of Well:** VERTICAL

## Lithology

From (ft bgl)	To (ft bgl)	Raw Data	Description	Moisture	Colour	Hardness	Observations	Water Bearing Flow Estimate (USGPM)
0	1	topsoil						
1	4	gravel sand and clay						
4	6.6	cemented gravel						
6.6	14	clay with some sand						
14	18	clay and gravel (w.b.)						
18	23	clay and rocks						
23	24	light brown clay						
24	25	yellow clay						
25	25	bedrock						

## Casing Details

From (ft bgl)	To (ft bgl)	Casing Type	Casing Material	Diameter (in)	Wall Thickness (in)	Drive Shoe
There are no records to show						

## Surface Seal and Backfill Details

**Surface Seal Material:**  
**Surface Seal Installation Method:**  
**Surface Seal Thickness:**  
**Surface Seal Depth:**

**Backfill Material Above Surface Seal:**  
**Backfill Depth:**

## Liner Details

**Liner Material:**  
**Liner Diameter:**  
**Liner from:**

**Liner Thickness:**  
**Liner to:**

### Liner perforations

From (ft bgl)	To (ft bgl)
There are no records to show	

## Screen Details

**Intake Method:**  
**Type:**  
**Material:**  
**Opening:**  
**Bottom:**

### Installed Screens

From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size
There are no records to show				

## Well Development

**Developed by:**

**Development Total Duration:**

## Well Yield

**Estimation Method:**  
**Static Water Level Before Test:**  
**Hydrofracturing Performed:** No

**Estimation Rate:**  
**Drawdown:**  
**Increase in Yield Due to Hydrofracturing:**

**Estimation Duration:**

## Well Decommission Information

**Reason for Decommission:**  
**Sealant Material:**  
**Decommission Details:**

**Method of Decommission:**  
**Backfill Material:**

## Pumping Test Information and Aquifer Parameters

Start Date	Pumping Test	Test	Boundary	Transmissivity	Hydraulic	Specific	Specific	Analysis	
Pumping Test	Description	Duration (min)	Effect	Storativity (m <sup>2</sup> /day)	Conductivity (m/day)	Yield	Capacity (L/s/m)	Method	Comments
There are no records to show									

### Comments

METHOD OF DRILLING = DRILLED

### Documents

- [WTN 19830 Well Record.pdf](#)

### Disclaimer

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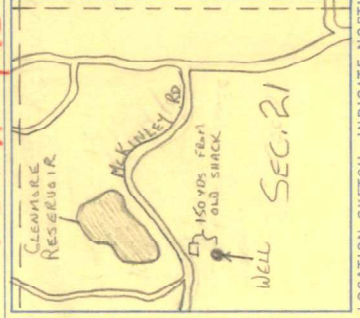
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 88 F. 093  
 42.3  
 514-S 1/2

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 MERIDIAN  
 UNITS TENS 2 1 7 4 2 1  
 RANGE  
 UNITS TENS 2 1 7 4 2 1  
 SECTION  
 UNITS TENS 2 1 7 4 2 1  
 QUARTER  
 UNITS TENS 2 1 7 4 2 1  
 LAND DISTRICT  
 UNITS TENS 2 1 7 4 2 1

GROUND — WATER DIVISION, WATER INVESTIGATIONS BRANCH, DEPT. OF LANDS, FORESTS, and WATER RESOURCES, VICTORIA, B.C.  
 LOCATION (COMPLETE LEGAL DESCRIPTION)  
 OWNER'S NAME M.R. & MRS. C. STEPHENS ADDRESS Box 13 Winfield DATE OF COMPLETION Feb/66  
 DRILLER'S NAME Moore & Son ADDRESS Box 13 Winfield  
 DEPTH 25' ELEVATION OF COLLAR (163) CASING DIAM. 6" LENGTH \_\_\_\_\_ TYPE \_\_\_\_\_  
 METHOD OF DIGGING DRILLED SCREEN  SIZE \_\_\_\_\_ LENGTH \_\_\_\_\_ TYPE \_\_\_\_\_

LOCATION OF SCREEN \_\_\_\_\_ DEVELOPED  DESCRIBE \_\_\_\_\_  
 PERFORATED CASING  LENGTH 3' 6" LOCATION OF PERFORATIONS \_\_\_\_\_  
 GRAVEL PACK  LENGTH \_\_\_\_\_ DIAM. \_\_\_\_\_ SIZE GRAVEL, ETC. \_\_\_\_\_  
 PUMP  TYPE \_\_\_\_\_ POWER \_\_\_\_\_  
 CAPACITY \_\_\_\_\_ OTHER DATA \_\_\_\_\_  
 COSTS WELL \_\_\_\_\_ PUMP \_\_\_\_\_ PUMP HOUSE, ETC. \_\_\_\_\_  
 MAINTENANCE \_\_\_\_\_  
 DISTANCE TO WATER FROM TOP OF CASING  ESTIMATED  MEASURED ELEVATION \_\_\_\_\_ FLUCTUATION \_\_\_\_\_  
 HIGH WATER \_\_\_\_\_ MONTH \_\_\_\_\_ LOW WATER \_\_\_\_\_ MONTH \_\_\_\_\_ OBSERVATION DATA  FILE NO. \_\_\_\_\_  
 WATER USE NO SUITABLE FORMATION FOR A WELL. WATER SEEPED THROUGH AN OPEN HOLE.  
 MAX. RATE WITHDRAWAL  ESTIMATED  MEASURED \_\_\_\_\_  
 TEMPERATURE \_\_\_\_\_ PUMPS SAND  \_\_\_\_\_  
 CLOGS SCREEN  TYPE DEPOSIT \_\_\_\_\_ AQUIFER DATA \_\_\_\_\_

LICENSE No. \_\_\_\_\_ DATE LICENSE \_\_\_\_\_ AMOUNT \_\_\_\_\_  
 DATE APPLICATION \_\_\_\_\_ USE \_\_\_\_\_  
 LOCATION SKETCH—INDICATE NORTH



DRY HOLE \_\_\_\_\_  
 INADEQUATE QUANTITY \_\_\_\_\_  
 PUMPING TEST \_\_\_\_\_  
 CAPACITY GPD. \_\_\_\_\_  
 901 \_\_\_\_\_

SYSTEMS EQUIPMENT LIMITED, VICTORIA-CANADA 0 2231-65

SYSTEMSORT	SUPPLY AQUIFER		OTHER AQUIFER PRESENT		OTHER AQUIFER PRESENT		OTHER AQUIFER PRESENT					
	TENS	UNITS	TENS	UNITS	TENS	UNITS	TENS	UNITS				
7	4	2	1	7	4	2	1	7	4	2	1	
4	7	4	2	1	7	4	2	1	7	4	2	1
1	7	4	2	1	7	4	2	1	7	4	2	1
2	7	4	2	1	7	4	2	1	7	4	2	1
4	7	4	2	1	7	4	2	1	7	4	2	1
7	7	4	2	1	7	4	2	1	7	4	2	1

CHARACTER OF SUPPLY AQUIFER: SAND, GRAVEL, TILL, DOMESTIC, GARDEN, STOCK, COOLING, IRRIGATION, INDUSTRIAL, WATERWORKS

WATER USE: \_\_\_\_\_

RELIABILITY OF DATA: 1008

ROCK: \_\_\_\_\_

SPRING: \_\_\_\_\_

APPROX. 700' SOUTH OF THE GLENMORE RESERVOIR.  
 100 YDS SOUTH OF THE FLINTAKE RANCHO GATE.  
 NORTH OF SHEET 1.

WTN 19830

North of APPROX.  
 82E/4 49S

1









# Groundwater Wells and Aquifers

## Well Summary

<b>Well Tag Number:</b> 20594	<b>Well Status:</b> New	<b>Observation Well Number:</b>
<b>Well Identification Plate Number:</b>	<b>Well Class:</b> Unknown	<b>Observation Well Status:</b>
<b>Owner Name:</b> WILFRED WERGER	<b>Well Subclass:</b>	<b>Environmental Monitoring System (EMS) ID:</b>
<b>Intended Water Use:</b> Unknown Well Use	<b>Aquifer Number:</b> <u>469</u>	<b>Alternative specs submitted:</b> No
<b>Artesian Condition:</b> No	<b>Technical Report:</b> N/A	<b>Drinking Water Area Indicator:</b> No

## Licensing Information

**Licensed Status:** Unlicensed      **Licence Number:**

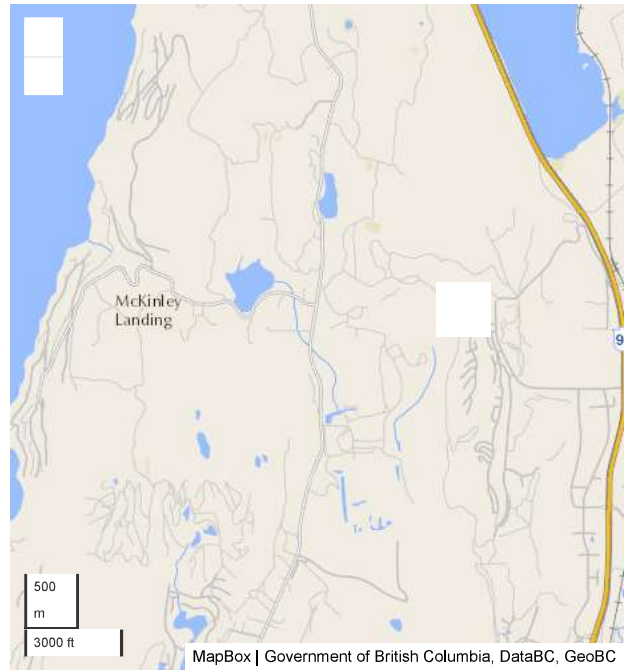
## Location Information

**Street Address:** GLENMORE RD  
**Town/City:** KELOWNA

### Legal Description:

Lot	2
Plan	16293
District Lot	
Block	
Section	16
Township	23
Range	
Land District	41
Property Identification Description (PID)	

### Description of Well Location:



### Geographic Coordinates - North American Datum of 1983 (NAD 83)

**Latitude:** 49.966091      **Longitude:** -119.406788  
**UTM Easting:** 327400      **UTM Northing:** 5537637  
**Zone:** 11      **Coordinate Acquisition Code:** (100 m accuracy) Digitized from old Dept. of Lands, Forests and Water Resources maps

## Well Activity

Activity	Work Start Date	Work End Date	Drilling Company	Date Entered
Legacy record	1967-04-01	1967-04-01	Okanagan Rotary Well Drilling	August 13th 2003 at 8:01 AM

## Well Work Dates

Start Date of Construction	End Date of Construction	Start Date of Alteration	End Date of Alteration	Start Date of Decommission	End Date of Decommission
1967-04-01	1967-04-01				

### Well Completion Data

<b>Total Depth Drilled:</b>	<b>Estimated Well Yield:</b> 5 USgpm	<b>Static Water Level (BTOC):</b> 35 feet btoc
<b>Finished Well Depth:</b> 105 ft bgl	<b>Well Cap:</b>	<b>Artesian Flow:</b>
<b>Final Casing Stick Up:</b>	<b>Well Disinfected Status:</b> Not Disinfected	<b>Artesian Pressure (head):</b>
<b>Depth to Bedrock:</b>	<b>Drilling Method:</b> Other	<b>Artesian Pressure (PSI):</b>
<b>Ground elevation:</b>	<b>Method of determining elevation:</b> Unknown	<b>Orientation of Well:</b> VERTICAL

### Lithology

From (ft bgl)	To (ft bgl)	Raw Data	Description	Moisture	Colour	Hardness	Observations	Water Bearing Flow Estimate (USGPM)
0	10	brown clay, sand and rocks						
10	42	hard clay -yellowish- then light brown						
42	64	hard grey clay						
64	86	slate, white and black rock w.b.						
86	105	hard clay and white lime						

### Casing Details

From (ft bgl)	To (ft bgl)	Casing Type	Casing Material	Diameter (in)	Wall Thickness (in)	Drive Shoe
There are no records to show						

### Surface Seal and Backfill Details

<b>Surface Seal Material:</b>	<b>Backfill Material Above Surface Seal:</b>
<b>Surface Seal Installation Method:</b>	<b>Backfill Depth:</b>
<b>Surface Seal Thickness:</b>	
<b>Surface Seal Depth:</b>	

### Liner Details

<b>Liner Material:</b>		<b>Liner perforations</b>				
<b>Liner Diameter:</b>	<b>Liner Thickness:</b>	<table border="1"> <thead> <tr> <th>From (ft bgl)</th> <th>To (ft bgl)</th> </tr> </thead> <tbody> <tr> <td colspan="2" style="text-align: center;">There are no records to show</td> </tr> </tbody> </table>	From (ft bgl)	To (ft bgl)	There are no records to show	
From (ft bgl)	To (ft bgl)					
There are no records to show						
<b>Liner from:</b>	<b>Liner to:</b>					

### Screen Details

<b>Intake Method:</b>	<b>Installed Screens</b>										
<b>Type:</b>	<table border="1"> <thead> <tr> <th>From (ft bgl)</th> <th>To (ft bgl)</th> <th>Diameter (in)</th> <th>Assembly Type</th> <th>Slot Size</th> </tr> </thead> <tbody> <tr> <td colspan="5" style="text-align: center;">There are no records to show</td> </tr> </tbody> </table>	From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size	There are no records to show				
From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size							
There are no records to show											
<b>Material:</b>											
<b>Opening:</b>											
<b>Bottom:</b>											

### Well Development

<b>Developed by:</b>	<b>Development Total Duration:</b>
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### Well Yield

<b>Estimation Method:</b>	<b>Estimation Rate:</b>	<b>Estimation Duration:</b>
<b>Static Water Level Before Test:</b>	<b>Drawdown:</b>	
<b>Hydrofracturing Performed:</b> No	<b>Increase in Yield Due to Hydrofracturing:</b>	

### Well Decommission Information

<b>Reason for Decommission:</b>	<b>Method of Decommission:</b>
<b>Sealant Material:</b>	<b>Backfill Material:</b>
<b>Decommission Details:</b>	



## Pumping Test Information and Aquifer Parameters

Start Date	Pumping Test	Test	Boundary	Transmissivity	Hydraulic	Specific	Specific	Analysis	
Pumping Test	Description	Duration (min)	Effect	Storativity (m <sup>2</sup> /day)	Conductivity (m/day)	Yield	Capacity (L/s/m)	Method	Comments
There are no records to show									

## Comments

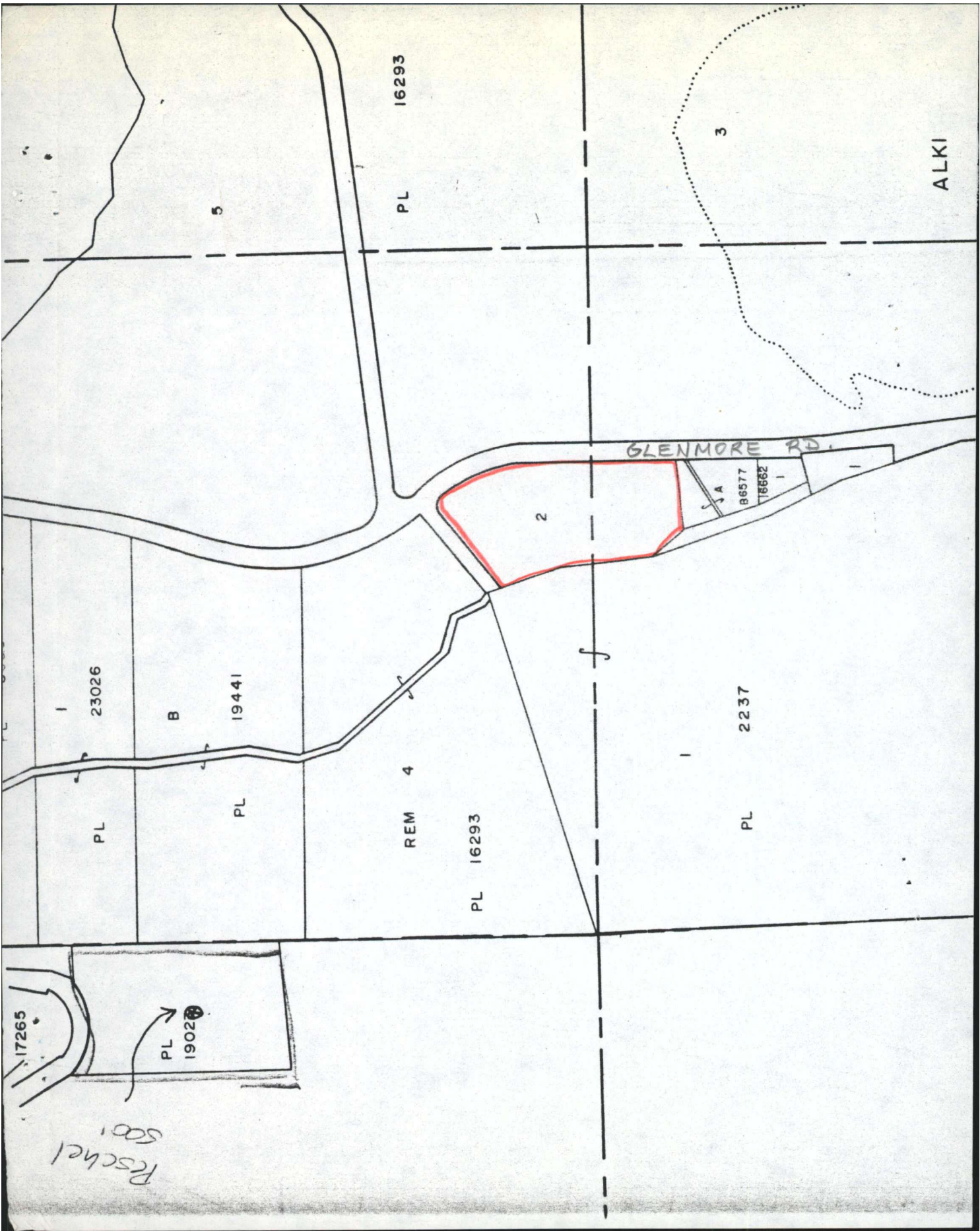
METHOD OF DRILLING = DRILLED

## Documents

- [WTN 20594 Well Record.pdf](#)

## Disclaimer

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82E.093.4.2.4

GROUND - WATER DIVISION, WATER INVESTIGATIONS BRANCH, DEPT. OF LANDS, FORESTS, and WATER RESOURCES, VICTORIA, B.C. 0501005 Dist

LOCATION Lot 2 Plain 16293 GLENMORE RD KELOWNA SEC. 16+21 TP 23 No Mapping

OWNER'S NAME Wilfred Wenger ADDRESS R.R.1 Glenmore (Kelowna city) WTA20594

DRILLER'S NAME Okanagan Rotary Water Wells ADDRESS DATE OF COMPLETION Apr 1/67

DEPTH 105' ELEVATION OF COLLAR 105' CASING DIAM. 6 1/4" LENGTH TYPE

METHOD OF DIGGING drilled

LOCATION OF SCREEN DEVELOPED DESCRIBE

PERFORATED CASING LENGTH LOCATION OF PERFORATIONS

GRAVEL PACK LENGTH DIAM. SIZE GRAVEL, ETC.

PUMP TYPE PUMP POWER

CAPACITY OTHER DATA

COSTS WELL PUMP PUMP HOUSE, ETC.

MAINTENANCE

DISTANCE TO WATER FROM TOP OF CASING 35' ESTIMATED MEASURED ELEVATION FLUCTUATION

HIGH WATER MONTH LOW WATER MONTH OBSERVATION DATA FILE NO.

WATER USE

MAX. RATE WITHDRAWAL ESTIMATED MEASURED

TEMPERATURE PUMPS SAND PUMPS DEPOSIT AQUIFER DATA

CLOGS SCREEN TYPE DEPOSIT DATE LICENSE AMOUNT USE

LICENSE NO. DATE LICENSE AMOUNT USE

DATE APPLICATION USE

LOCATION SKETCH-INDICATE NORTH

WATER USE

CHARACTER OF SUPPLY

RELIABILITY OF DATA

ROCK

SPRING

PART CONFINED

GOOD FAIR POOR

992

WATERWORKS

INDUSTRIAL

IRRIGATION

COOLING

STOCK

GARDEN

DOMESTIC

TILL

GRAVEL

SAND

12708

OTHER AQUIFER PRESENT

TENS UNITS

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## Well Summary

Well Tag Number: 23247  
 Well Identification Plate Number:  
 Owner Name: CHARLES PROKES  
 Intended Water Use: Not Applicable  
 Artesian Condition: No

Well Status: New  
 Well Class: Unknown  
 Well Subclass:  
 Aquifer Number: 464  
 Technical Report: N/A

Observation Well Number:  
 Observation Well Status:  
 Environmental Monitoring System (EMS) ID:  
 Alternative specs submitted: No  
 Drinking Water Area Indicator: No

## Licensing Information

Licensed Status: Unlicensed

Licence Number:

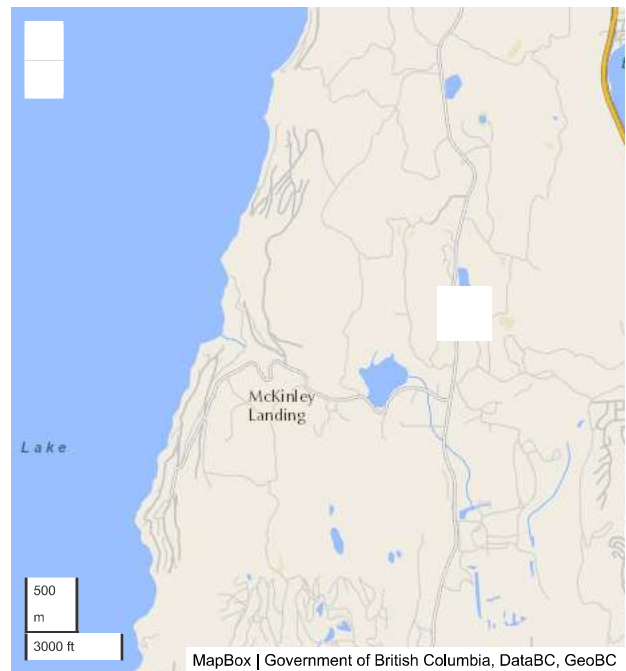
## Location Information

Street Address: GLENMORE RD  
 Town/City: KELOWNA

### Legal Description:

Lot	A
Plan	22105
District Lot	
Block	
Section	21
Township	23
Range	
Land District	41
Property Identification Description (PID)	

### Description of Well Location:



### Geographic Coordinates - North American Datum of 1983 (NAD 83)

Latitude: 49.97374

Longitude: -119.4237

UTM Easting: 326215

UTM Northing: 5538526

Zone: 11

Coordinate Acquisition Code: (100 m accuracy) Digitized from old Dept. of Lands, Forests and Water Resources maps

## Well Activity

Activity	Work Start Date	Work End Date	Drilling Company	Date Entered
Legacy record	1970-01-26	1970-01-26	Oasis Drilling	August 13th 2003 at 11:01 AM

## Well Work Dates

Start Date of Construction	End Date of Construction	Start Date of Alteration	End Date of Alteration	Start Date of Decommission	End Date of Decommission
1970-01-26	1970-01-26				

## Well Completion Data

Total Depth Drilled:  
 Finished Well Depth: 37 ft bgl  
 Final Casing Stick Up:  
 Depth to Bedrock: 34 feet bgl  
 Ground elevation:

Estimated Well Yield: 9 USgpm  
 Well Cap:  
 Well Disinfected Status: Not Disinfected  
 Drilling Method: Other  
 Method of determining elevation: Unknown

Static Water Level (BTOC): 8 feet btoc  
 Artesian Flow:  
 Artesian Pressure (head):  
 Artesian Pressure (PSI):  
 Orientation of Well: VERTICAL

## Lithology

From (ft bgl)	To (ft bgl)	Raw Data	Description	Moisture	Colour	Hardness	Observations	Water Bearing Flow Estimate (USGPM)
0	1	topsoil						
1	7	oxidized till						
7	9	oxidized sand						
9	16	clay and boulders						
16	34	gravel (med. - coarse)					W.B.	
34	37	bedrock						

## Casing Details

From (ft bgl)	To (ft bgl)	Casing Type	Casing Material	Diameter (in)	Wall Thickness (in)	Drive Shoe
There are no records to show						

## Surface Seal and Backfill Details

Surface Seal Material:  
 Surface Seal Installation Method:  
 Surface Seal Thickness:  
 Surface Seal Depth:

Backfill Material Above Surface Seal:  
 Backfill Depth:

## Liner Details

Liner Material:  
 Liner Diameter:  
 Liner from:  
 Liner Thickness:  
 Liner to:

### Liner perforations

From (ft bgl)	To (ft bgl)
There are no records to show	

## Screen Details

Intake Method:  
 Type:  
 Material:  
 Opening:  
 Bottom:

### Installed Screens

From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size
There are no records to show				

## Well Development

Developed by:

Development Total Duration:

## Well Yield

Estimation Method:  
 Static Water Level Before Test:  
 Hydrofracturing Performed: No

Estimation Rate:  
 Drawdown:  
 Increase in Yield Due to Hydrofracturing:

Estimation Duration:

## Well Decommission Information

Reason for Decommission:  
 Sealant Material:  
 Decommission Details:

Method of Decommission:  
 Backfill Material:



## Pumping Test Information and Aquifer Parameters

Start Date Pumping Test	Pumping Test Description	Test Duration (min)	Boundary Effect	Transmissivity Storativity (m <sup>2</sup> /day)	Hydraulic Conductivity (m/day)	Specific Yield	Specific Capacity (L/s/m)	Analysis Method	Comments
There are no records to show									

### Comments

METHOD OF DRILLING = DRILLED. ESTIMATED YIELD: 9 GALS/MIN. SLOTTED PIPE.

### Documents

- [WTN 23247 Well Record.pdf](#)

### Disclaimer

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# Groundwater Wells and Aquifers

## Well Summary

<b>Well Tag Number:</b> 71857	<b>Well Status:</b> New	<b>Observation Well Number:</b>
<b>Well Identification Plate Number:</b>	<b>Well Class:</b> Unknown	<b>Observation Well Status:</b>
<b>Owner Name:</b> PESCHEL OTTO	<b>Well Subclass:</b>	<b>Environmental Monitoring System (EMS) ID:</b>
<b>Intended Water Use:</b> Not Applicable	<b>Aquifer Number:</b>	<b>Alternative specs submitted:</b> No
<b>Artesian Condition:</b> No	<b>Technical Report:</b> N/A	<b>Drinking Water Area Indicator:</b> No

## Licensing Information

**Licensed Status:** Unlicensed      **Licence Number:**

## Location Information

**Street Address:** MCKINLEY RESERVOIR  
**Town/City:** WINFIELD

### Legal Description:

Lot	A
Plan	19023
District Lot	
Block	
Section	21
Township	23
Range	
Land District	41
Property Identification Description (PID)	

**Description of Well Location:** MCKINLEY RESERVOIR



### Geographic Coordinates - North American Datum of 1983 (NAD 83)

**Latitude:** 49.966851      **Longitude:** -119.433309  
**UTM Easting:** 325501      **UTM Northing:** 5537783  
**Zone:** 11  
**Coordinate Acquisition Code:**  
 (unknown, accuracy based on parcel size) No ICF cadastre, poor or no location sketch; site located in center of primary parcel

## Well Activity

Activity	Work Start Date	Work End Date	Drilling Company	Date Entered
Legacy record	1979-06-19		Okanagan Water Well Drilling	August 13th 2003 at 9:05 AM

## Well Work Dates

Start Date of Construction	End Date of Construction	Start Date of Alteration	End Date of Alteration	Start Date of Decommission	End Date of Decommission
1979-06-19					



## Well Completion Data

<b>Total Depth Drilled:</b>	<b>Estimated Well Yield:</b>	<b>Static Water Level (BTOC):</b>
<b>Finished Well Depth:</b> 500 ft bgl	<b>Well Cap:</b>	<b>Artesian Flow:</b>
<b>Final Casing Stick Up:</b>	<b>Well Disinfected Status:</b> Not Disinfected	<b>Artesian Pressure (head):</b>
<b>Depth to Bedrock:</b>	<b>Drilling Method:</b> Other	<b>Artesian Pressure (PSI):</b>
<b>Ground elevation:</b>	<b>Method of determining elevation:</b> Unknown	<b>Orientation of Well:</b> VERTICAL

## Lithology

From (ft bgl)	To (ft bgl)	Raw Data	Description	Moisture	Colour	Hardness	Observations	Water Bearing Flow Estimate (USGPM)
0	500	ROCK HOLE	0 nothing entered		0 nothing entered			

## Casing Details

From (ft bgl)	To (ft bgl)	Casing Type	Casing Material	Diameter (in)	Wall Thickness (in)	Drive Shoe
There are no records to show						

## Surface Seal and Backfill Details

<b>Surface Seal Material:</b> Other	<b>Backfill Material Above Surface Seal:</b>
<b>Surface Seal Installation Method:</b>	<b>Backfill Depth:</b>
<b>Surface Seal Thickness:</b>	
<b>Surface Seal Depth:</b>	

## Liner Details

<b>Liner Material:</b>		<b>Liner perforations</b>				
<b>Liner Diameter:</b>	<b>Liner Thickness:</b>	<table border="1"> <thead> <tr> <th>From (ft bgl)</th> <th>To (ft bgl)</th> </tr> </thead> <tbody> <tr> <td colspan="2" style="text-align: center;">There are no records to show</td> </tr> </tbody> </table>	From (ft bgl)	To (ft bgl)	There are no records to show	
From (ft bgl)	To (ft bgl)					
There are no records to show						
<b>Liner from:</b>	<b>Liner to:</b>					

## Screen Details

<b>Intake Method:</b>	<b>Installed Screens</b>										
<b>Type:</b>	<table border="1"> <thead> <tr> <th>From (ft bgl)</th> <th>To (ft bgl)</th> <th>Diameter (in)</th> <th>Assembly Type</th> <th>Slot Size</th> </tr> </thead> <tbody> <tr> <td colspan="5" style="text-align: center;">There are no records to show</td> </tr> </tbody> </table>	From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size	There are no records to show				
From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size							
There are no records to show											
<b>Material:</b> Other											
<b>Opening:</b>											
<b>Bottom:</b>											

## Well Development

<b>Developed by:</b>	<b>Development Total Duration:</b>
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## Well Yield

<b>Estimation Method:</b>	<b>Estimation Rate:</b>	<b>Estimation Duration:</b>
<b>Static Water Level Before Test:</b>	<b>Drawdown:</b>	
<b>Hydrofracturing Performed:</b> No	<b>Increase in Yield Due to Hydrofracturing:</b>	

## Well Decommission Information

<b>Reason for Decommission:</b>	<b>Method of Decommission:</b>
<b>Sealant Material:</b>	<b>Backfill Material:</b>
<b>Decommission Details:</b>	

## Pumping Test Information and Aquifer Parameters

Start Date	Pumping Test	Test Duration	Boundary	Transmissivity	Hydraulic Conductivity	Specific Capacity	Specific Yield	Analysis Method	Comments
Pumping Test	Description	(min)	Effect	Storativity (m <sup>2</sup> /day)	(m/day)	(L/s/m)			
There are no records to show									

## Comments

NOT CASSED. VERY LITTLE H2O. METHOD OF DRILLING = DRILLED

## Documents

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- [WTN 71857 Well Record.pdf](#)

## Disclaimer

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# Okanagan Water Well Drilling Ltd.

3706 - 24th AVENUE • VERNON, B.C. V1T 1L9 • PHONE 542-7827

Date June 19 1979

TO: Otto Reschel Phone \_\_\_\_\_  
 ADDRESS: P.O. B. 1114 Kelowna

Lot H B7 for 21 Sep 23  
Plan M0237A 41 O.D.V.D.

DESCRIPTION	PRICE PER	AMOUNT
<u>rock hole charge for 500' hole to be paid for by Otto Reschel</u>	<u>\$13.50</u>	<u>\$3,325.00</u>
<u>John O. Fickett</u>		
<u>Drilled at the Winfield water reservoir</u>		
PAID IN GOOD ORDER		TAX
		TOTAL <u>\$3375.00</u>
ORDER NO.	CASH	CHEQUE

TERMS: DEPOSIT OF 20% ON COMPLETION



PL B3562

PL B 3562

RESERVOIR

18402

4

5

MCKINLEY

D

C

PL

17265

21

E

PL

17265

PL

3

*Reschel  
500'*

PL

1902

PL

I

23026

B

PL

19441

REM 4

PL 16293

PL

2237









## Well Summary

**Well Tag Number:** 99677  
**Well Identification Plate Number:**  
**Owner Name:** D G FLINTOFT  
**Intended Water Use:** Private Domestic  
**Artesian Condition:** No

**Well Status:** Closure  
**Well Class:** Water Supply  
**Well Subclass:** Not Applicable  
**Aquifer Number:** 467  
**Technical Report:** N/A

**Observation Well Number:**  
**Observation Well Status:**  
**Environmental Monitoring System (EMS) ID:**  
**Alternative specs submitted:** No  
**Drinking Water Area Indicator:** No

## Licensing Information

**Licensed Status:** Unlicensed

**Licence Number:**

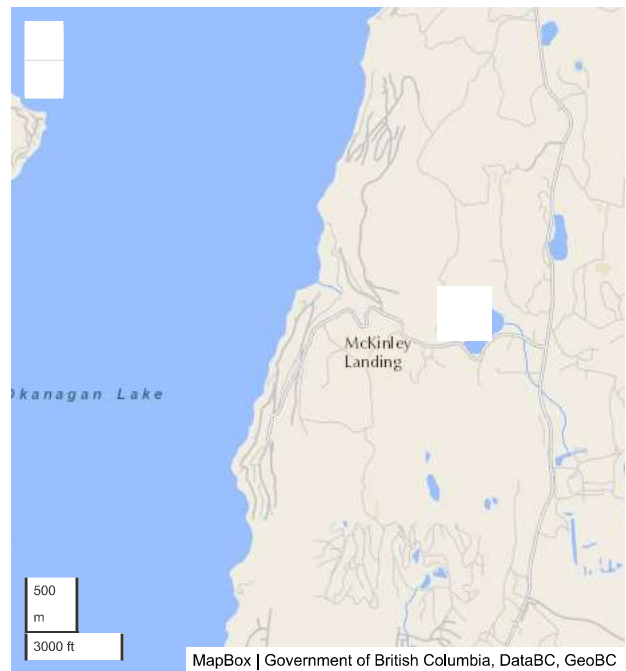
## Location Information

**Street Address:** 2010 MCKINLEY ROAD  
**Town/City:** KELOWNA

### Legal Description:

Lot	A
Plan	18402
District Lot	
Block	
Section	21
Township	23
Range	
Land District	41
Property Identification Description (PID)	008249334

**Description of Well Location:** SW CORNER OF LOT



### Geographic Coordinates - North American Datum of 1983 (NAD 83)

**Latitude:** 49.9693      **Longitude:** -119.4361  
**UTM Easting:** 325310      **UTM Northing:** 5538062  
**Zone:** 11      **Coordinate Acquisition Code:** (10 m accuracy) Handheld GPS with accuracy of +/- 10 metres

## Well Activity

Activity	Work Start Date	Work End Date	Drilling Company	Date Entered
Decommission report	2018-10-10	2018-10-10		February 21st 2020 at 1:35 PM
Legacy record	2005-08-15	2005-08-15		February 22nd 2010 at 8:07 AM

## Well Work Dates

Start Date of Construction	End Date of Construction	Start Date of Alteration	End Date of Alteration	Start Date of Decommission	End Date of Decommission
2005-08-15	2005-08-15			2018-10-10	2018-10-10

## Well Completion Data

**Total Depth Drilled:** 13.5 ft bgl  
**Finished Well Depth:** 13.5 ft bgl  
**Final Casing Stick Up:** 18 inches  
**Depth to Bedrock:**  
**Ground elevation:** 489.4 feet

**Estimated Well Yield:**  
**Well Cap:** WOOD FRAME ON CONCRETE LID  
**Well Disinfected Status:** Not Disinfected  
**Drilling Method:**  
**Method of determining elevation:** GPS

**Static Water Level (BTOC):** 7 feet btoc  
**Artesian Flow:**  
**Artesian Pressure (head):**  
**Artesian Pressure (PSI):**  
**Orientation of Well:** VERTICAL

## Lithology

From (ft bgl)	To (ft bgl)	Raw Data	Description	Moisture	Colour	Hardness	Observations	Water Bearing Flow Estimate (USGPM)
0	2	SILT, TILL						
2	13	SAND, SILT, GRAVEL						
13	13.5	HARDPAN LAYER						

## Casing Details

From (ft bgl)	To (ft bgl)	Casing Type	Casing Material	Diameter (in)	Wall Thickness (in)	Drive Shoe
0	13.5		Open hole	36		Not Installed

## Surface Seal and Backfill Details

**Surface Seal Material:**  
**Surface Seal Installation Method:**  
**Surface Seal Thickness:**  
**Surface Seal Depth:**

**Backfill Material Above Surface Seal:**  
**Backfill Depth:**

## Liner Details

**Liner Material:**  
**Liner Diameter:**  
**Liner from:**

**Liner Thickness:**  
**Liner to:**

### Liner perforations

From (ft bgl)	To (ft bgl)
There are no records to show	

## Screen Details

**Intake Method:**  
**Type:**  
**Material:**  
**Opening:**  
**Bottom:**

### Installed Screens

From (ft bgl)	To (ft bgl)	Diameter (in)	Assembly Type	Slot Size
There are no records to show				

## Well Development

**Developed by:** Pumping

**Development Total Duration:**

## Well Yield

**Estimation Method:**  
**Static Water Level Before Test:**  
**Hydrofracturing Performed:** No

**Estimation Rate:**  
**Drawdown:**  
**Increase in Yield Due to Hydrofracturing:**

**Estimation Duration:**

## Well Decommission Information

**Reason for Decommission:** HOOKED TO GEID DOMESTIC  
**Sealant Material:** BENTONITE  
**Decommission Details:** CONCRETE RINGS LEFT IN PLACE

**Method of Decommission:** POURED  
**Backfill Material:** RIVER ROCK

## Pumping Test Information and Aquifer Parameters

Start Date	Pumping Test Description	Test Duration (min)	Boundary Effect	Storativity	Transmissivity (m <sup>2</sup> /day)	Hydraulic Conductivity (m/day)	Specific Yield	Specific Capacity (L/s/m)	Analysis Method	Comments
There are no records to show										

## Comments

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MEASUREMENTS FROM GROUND LEVEL. RECOMMENDED PUMP TYPE: JET PUMP. METHOD OF DRILLING: BACK HOE. WELL DEVELOPED IN 1969 WHEN HOUSE WAS BUILT. NO RECORD OF THESE WORKS. WELL HAS BEEN IN USE SINCE 1969. FLUCT RATES WITH LOW WATER YEARS BUT HAS NEVER RUN DRY.

## Documents

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- [WTN 99677 Well Decommission.PNG](#)
- [WTN 99677 Well Decommission.pdf](#)

## Disclaimer

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Province of British Columbia  
*Water Act*

---

ORDER

Section 39 of the  
*Water Act* of British Columbia  
RSBC 1996, Chap. 483

File Numbers: 0254102, 0281437 & 0370025

IN THE MATTER OF Conditional Water Licence No. 029197, Conditional Water Licence No. 034631 and Conditional Water Licence No. 061861 held by the Glenmore-Ellison Improvement District (herein referred to as GEID), which authorizes the storage behind the McKinley Reservoir Dam from Kelowna Creek.

WHEREAS the GEID plans the following construction for the McKinley Dam Headworks Upgrade Project which can be categorized as:

1. Construction of a new intake structure including concrete work, inlet pipe fittings, and trashrack,
2. Excavation through existing dam at high elevation for pipe installation,
3. Construction of an intake valve chamber,
4. Installation of a 900 mm diameter Ductile Iron intake pipe along the upstream face of the dam, through the dam, and along the downstream dam face, including required earthwork, trenching and backfilling, and
5. Construction of a valve chamber at downstream toe of dam.

WHEREAS the GEID requests authorization to proceed with the McKinley Dam Headworks Upgrade Project; and

WHEREAS the GEID has submitted the following design documents of the proposed work:

1. McKinley Reservoir Dam Improvements, Predesign Report, dated May 2003, by Ker Wood Leidal Associates Ltd. (herein referred to as KWL),
2. McKinley Reservoir Dam Improvements, Technical Memorandum (Predesign Report Update), dated September 22, 2003, by KWL,
3. Preliminary Design Plans, Drawing Set No. 2028-008, revision 0, dated September 2003, by KWL, and
4. Contract No. 2028-008A documents, technical specifications and supervision plan., dated September 2003, by KWL..

WHEREAS a Senior Dam Safety Officer from the Dam Safety Section has reviewed and approved the plans for the upgrade.

NOW THEREFORE pursuant to Section 39 of the *Water Act* of British Columbia, RSBC 1996, Chap. 483, and pursuant to the Dam Safety Regulation, BC Reg. 44/2000, OIC 131/2000, I, Glen Davidson, P.Eng., Deputy Comptroller of Water Rights, hereby order that Glenmore-Ellison Irrigation District has authorization to proceed with the McKinley Dam Headworks Upgrade subject to the following conditions:

1. Signed Final Design Plans, KWL Drawing Set No. 2028-008, are to be submitted to the Dam Safety Officer for authorization to proceed,
2. Existing McKinley Dam and Balancing Reservoir Operation, Maintenance and Surveillance Manual and Emergency Preparedness Plan is to be upgraded following completion of the McKinley Dam Headworks Upgrade Project,
3. Changes, of a minor nature, may be made to the design provided that they are signed off by the Project Engineer, and
4. Drawings of record are to be produced on completion of the project and kept with the records of the dam and an electronic (pdf) copy of the drawing of record sent to the Dam Safety Officer for our files.

THIS ORDER does not relieve you of obtaining all other permits and approvals from all other agencies.

THIS ORDER is dated at Victoria, British Columbia this 7th day of October, 2003.



Glen Davidson, P.Eng  
Deputy Comptroller of Water Rights

THE PROVINCE OF BRITISH COLUMBIA—WATER ACT  
**CONDITIONAL WATER LICENCE**

**Glenmore Irrigation District** of **1481 Water Street,**  
**Kelowna, B. C.**

is/are hereby authorized to **store** water as follows:—

(a) The source(s) of the water-supply is/are **Kelowna Creek and storage in Glenmore balancing reservoir.**

(b) The point(s) of **storage** is/are located as shown on the attached plan.

(c) The date from which this licence shall have precedence is **17th July, 1968.**

(d) The purpose for which the water is to be used is **as set out in Conditional Water Licence No. 15908.**

(e) The maximum quantity of water which may be **stored is 35 acre feet per annum,**

and such additional quantity as the Engineer may from time to time determine should be allowed for losses.

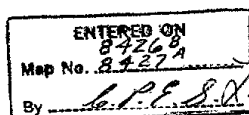
(f) The period of the year during which the water may be **stored is 1st October to 15th June.**

(g) The land upon which the water is to be used and to which this licence is appurtenant is **as set out in Conditional Water Licence No. 15908.**

(h) The works authorized to be constructed are **ditch, flume and dam,**

and they shall be located approximately as shown on the attached plan.

(i) The construction of the said works **has been completed and the water shall be beneficially used on or before the 31st day of December, 1971.**



*[Signature]*

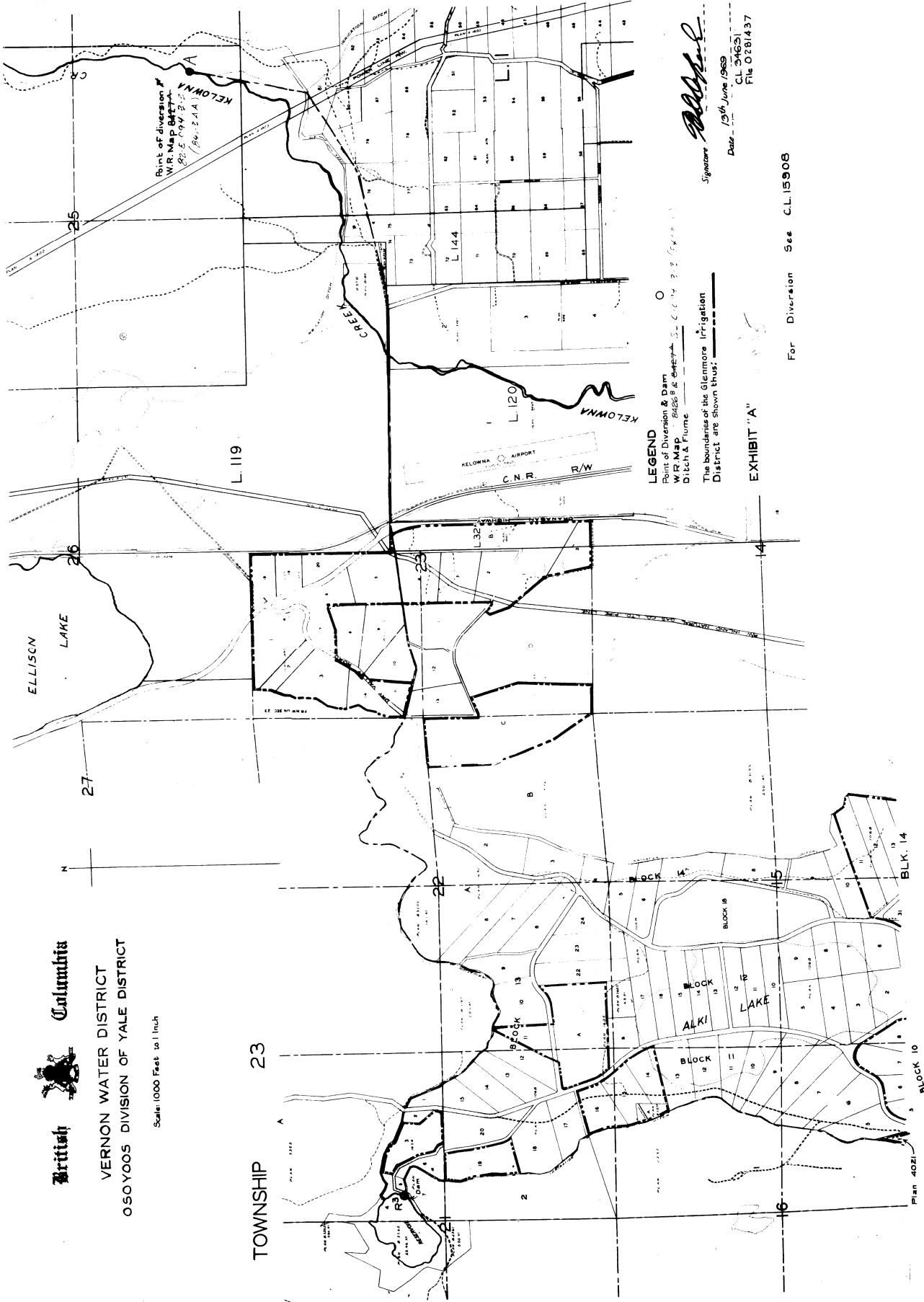
**H. D. DeBeck,**  
Comptroller of Water Rights.





VERNON WATER DISTRICT  
OSOYOOS DIVISION OF YALE DISTRICT

Scale: 1000 Feet to 1 Inch



Point of diversion of  
W.R. Map Safety  
25-5-1949  
(84-244)

LEGEND

- O Point of Diversion & Dam
- W.R. Map Side of Center
- Ditch & Flume
- The boundaries of the Glenmore Irrigation District are shown thus: ————

Signature *[Handwritten Signature]*

Date: 13th June 1969  
CL 34651  
File 0281437

EXHIBIT "A"

For Diversion See C.L. 15908

Plan 4021



# Province of British Columbia

## *Water Act*

---

### ORDER

Section 39 of the  
*Water Act* of British Columbia  
RSBC 1996, Chap. 483

File Numbers: 0254102, 0281437 & 0370025

IN THE MATTER OF Conditional Water Licence No. 029197, Conditional Water Licence No. 034631 and Conditional Water Licence No. 061861 held by the Glenmore-Ellison Improvement District (herein referred to as GEID), which authorizes the storage behind the McKinley Reservoir Dam from Kelowna Creek.

WHEREAS the GEID plans the following construction for the McKinley Dam Headworks Upgrade Project which can be categorized as:

1. Construction of a new intake structure including concrete work, inlet pipe fittings, and trashrack,
2. Excavation through existing dam at high elevation for pipe installation,
3. Construction of an intake valve chamber,
4. Installation of a 900 mm diameter Ductile Iron intake pipe along the upstream face of the dam, through the dam, and along the downstream dam face, including required earthwork, trenching and backfilling, and
5. Construction of a valve chamber at downstream toe of dam.

WHEREAS the GEID requests authorization to proceed with the McKinley Dam Headworks Upgrade Project; and

WHEREAS the GEID has submitted the following design documents of the proposed work:

1. McKinley Reservoir Dam Improvements, Predesign Report, dated May 2003, by Ker Wood Leidal Associates Ltd. (herein referred to as KWL),
2. McKinley Reservoir Dam Improvements, Technical Memorandum (Predesign Report Update), dated September 22, 2003, by KWL,
3. Preliminary Design Plans, Drawing Set No. 2028-008, revision 0, dated September 2003, by KWL, and
4. Contract No. 2028-008A documents, technical specifications and supervision plan., dated September 2003, by KWL..

WHEREAS a Senior Dam Safety Officer from the Dam Safety Section has reviewed and approved the plans for the upgrade.

NOW THEREFORE pursuant to Section 39 of the *Water Act* of British Columbia, RSBC 1996, Chap. 483, and pursuant to the Dam Safety Regulation, BC Reg. 44/2000, OIC 131/2000, I, Glen Davidson, P.Eng., Deputy Comptroller of Water Rights, hereby order that Glenmore-Ellison Irrigation District has authorization to proceed with the McKinley Dam Headworks Upgrade subject to the following conditions:

1. Signed Final Design Plans, KWL Drawing Set No. 2028-008, are to be submitted to the Dam Safety Officer for authorization to proceed,
2. Existing McKinley Dam and Balancing Reservoir Operation, Maintenance and Surveillance Manual and Emergency Preparedness Plan is to be upgraded following completion of the McKinley Dam Headworks Upgrade Project,
3. Changes, of a minor nature, may be made to the design provided that they are signed off by the Project Engineer, and
4. Drawings of record are to be produced on completion of the project and kept with the records of the dam and an electronic (pdf) copy of the drawing of record sent to the Dam Safety Officer for our files.

THIS ORDER does not relieve you of obtaining all other permits and approvals from all other agencies.

THIS ORDER is dated at Victoria, British Columbia this 7th day of October, 2003.



Glen Davidson, P.Eng  
Deputy Comptroller of Water Rights



THE PROVINCE OF BRITISH COLUMBIA—WATER ACT  
CONDITIONAL WATER LICENCE

Glenmore Irrigation District of R. R. #1, Glenmore Road, Kelowna, B. C. V1Y 7P9

is hereby authorized to divert and store water as follows:

- (a) The stream on which the rights are granted is Kelowna Creek and the reservoir is McKinley Reservoir.
- (b) The point of storage is located as shown on the attached plan.
- (c) The date from which this licence shall have precedence is 5th March, 1982.
- (d) The purpose for which this licence is issued is as set out in Conditional Water Licence 61860.
- (e) The maximum quantity of water which may be diverted into storage is 182 acre feet per annum.
- (f) The period of the year during which the water may be stored is 1st October to 30th June.
- (g) The land upon which the water is to be used and to which this licence is appurtenant is as set out in Conditional Water Licence.
- (h) The works authorized to be constructed are dam and reservoir, which shall be located approximately as shown on the attached plan.
- (i) The construction of the said works shall be completed and the water beneficially used prior to the 31st day of December, 1990. Thereafter, the licensee shall continue to make a regular beneficial use of water in the manner authorized herein.
- (j) Construction of the dam authorized under clause (h) hereof shall not be commenced until plans of same have been submitted to and approved by the Comptroller of Water Rights.
- (k) The reservoir area shall be cleared and the debris disposed of in such a manner and extent as directed by the Comptroller of Water Rights.



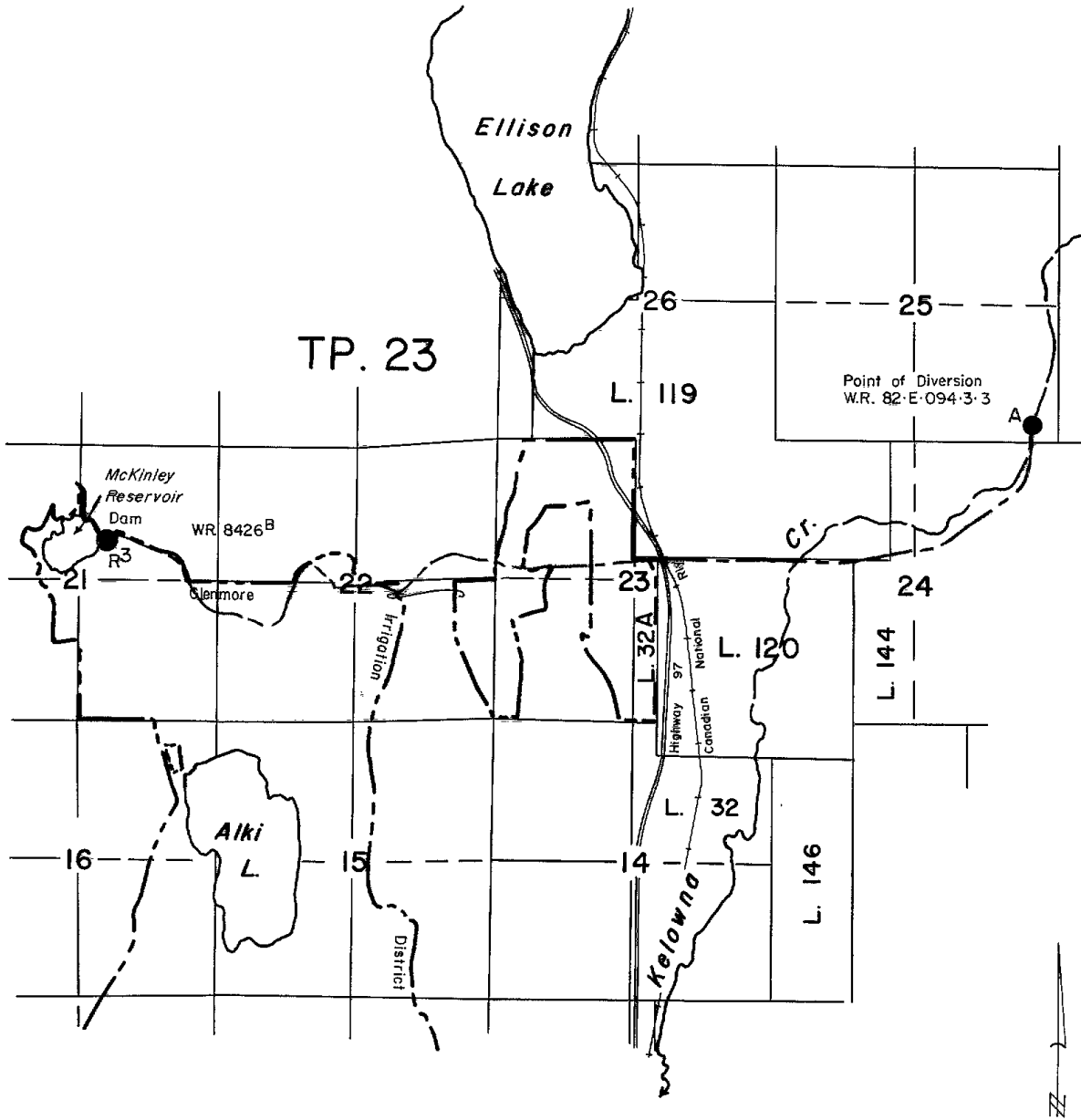
J. E. Farrell

Deputy Comptroller of Water Rights

File No. 0370025 Date issued: 30th January, 1987 CONDITIONAL LICENCE 61861



Province of British Columbia



WATER DISTRICT : VERNON  
PRECINCT : KELOWNA  
LAND DISTRICT : OSOYOOS DIVISION OF YALE

LEGEND

Scale : 40 Chains to 1 Inch  
Point of Diversion, Dam : ●  
Map Number : WR 82·E·094·3·3, WR. 8426<sup>B</sup>  
Pipe : ————

Signature: *Paul Swell*  
Date: *January 30, 1997*

C.L. 61861  
File 0370025  
For Diversion See C.L.61860



**Province of British Columbia**  
*Water Act*

---

**ORDER**

Section 39 of the  
*Water Act* of British Columbia  
RSBC 1996, Chap. 483

File Numbers: 0254102, 0281437 & 0370025

IN THE MATTER OF Conditional Water Licence No. 029197, Conditional Water Licence No. 034631 and Conditional Water Licence No. 061861 held by the Glenmore-Ellison Improvement District (herein referred to as GEID), which authorizes the storage behind the McKinley Reservoir Dam from Kelowna Creek.

WHEREAS the GEID plans the following construction for the McKinley Dam Headworks Upgrade Project which can be categorized as:

1. Construction of a new intake structure including concrete work, inlet pipe fittings, and trashrack,
2. Excavation through existing dam at high elevation for pipe installation,
3. Construction of an intake valve chamber,
4. Installation of a 900 mm diameter Ductile Iron intake pipe along the upstream face of the dam, through the dam, and along the downstream dam face, including required earthwork, trenching and backfilling, and
5. Construction of a valve chamber at downstream toe of dam.

WHEREAS the GEID requests authorization to proceed with the McKinley Dam Headworks Upgrade Project; and

WHEREAS the GEID has submitted the following design documents of the proposed work:

1. McKinley Reservoir Dam Improvements, Predesign Report, dated May 2003, by Ker Wood Leidal Associates Ltd. (herein referred to as KWL),
2. McKinley Reservoir Dam Improvements, Technical Memorandum (Predesign Report Update), dated September 22, 2003, by KWL,
3. Preliminary Design Plans, Drawing Set No. 2028-008, revision 0, dated September 2003, by KWL, and
4. Contract No. 2028-008A documents, technical specifications and supervision plan., dated September 2003, by KWL..

WHEREAS a Senior Dam Safety Officer from the Dam Safety Section has reviewed and approved the plans for the upgrade.



NOW THEREFORE pursuant to Section 39 of the *Water Act* of British Columbia, RSBC 1996, Chap. 483, and pursuant to the Dam Safety Regulation, BC Reg. 44/2000, OIC 131/2000, I, Glen Davidson, P.Eng., Deputy Comptroller of Water Rights, hereby order that Glenmore-Ellison Irrigation District has authorization to proceed with the McKinley Dam Headworks Upgrade subject to the following conditions:

1. Signed Final Design Plans, KWL Drawing Set No. 2028-008, are to be submitted to the Dam Safety Officer for authorization to proceed,
2. Existing McKinley Dam and Balancing Reservoir Operation, Maintenance and Surveillance Manual and Emergency Preparedness Plan is to be upgraded following completion of the McKinley Dam Headworks Upgrade Project,
3. Changes, of a minor nature, may be made to the design provided that they are signed off by the Project Engineer, and
4. Drawings of record are to be produced on completion of the project and kept with the records of the dam and an electronic (pdf) copy of the drawing of record sent to the Dam Safety Officer for our files.

THIS ORDER does not relieve you of obtaining all other permits and approvals from all other agencies.

THIS ORDER is dated at Victoria, British Columbia this 7th day of October, 2003.



Glen Davidson, P.Eng  
Deputy Comptroller of Water Rights

THE PROVINCE OF BRITISH COLUMBIA—WATER ACT

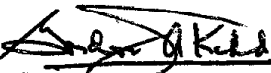
CONDITIONAL WATER LICENCE

Glenmore Irrigation District of 1481 Water Street, Kelowna, B.C.

is/are hereby authorized to store water as follows:—

- (a) The source(s) of the water-supply is/are Kelowna Creek and the reservoir is the Glenmore Balancing Reservoir.
- (b) The point(s) of storage is/are located as shown on the attached plan.
- (c) The date from which this licence shall have precedence is 11th December, 1963.
- (d) The purpose for which the water is to be used is as set out in Conditional Water Licence No. 15908.
- (e) The maximum quantity of water which may be stored is 772 acre feet per annum, and such additional quantity as the Engineer may from time to time determine should be allowed for losses.
- (f) The period of the year during which the water may be stored is 1st October to 15th June.
- (g) ~~The land upon which the water is to be used and to which this licence is appurtenant is to the Irrigation Undertaking of the Glenmore Irrigation District.~~
- (h) The works authorized to be constructed are earth fill dam, and they shall be located approximately as shown on the attached plan.
- (i) The construction of the said works has been commenced, and shall be completed and the water beneficially used on or before the 31st day of December, 1966.

REGISTERED ON
Map 8401
R.M. E.B.

  
Gordon J.A. Kidd,

Comptroller of Water Rights.

FILE No. 0254102 Date issued: 1 September 1964

CONDITIONAL LICENCE No. 29197



# Province of British Columbia

## *Water Sustainability Act*

### CONDITIONAL WATER LICENCE

The owner of the undertaking to which this licence is appurtenant is hereby authorized to divert, use, and store water as follows:

- a) The stream on which the rights are granted is Avocet Creek, and the reservoir is on the creek.
- b) The point of diversion is located as shown on the attached plan.
- c) The date from which this licence shall have precedence is March 10, 2008.
- d) The purpose for which this licence is issued is land improvement.
- e) The maximum quantity of water which may be diverted is 123,348 cubic metres per year.
- f) The period of the year during which the water may be used is January 1 to December 31.
- g) The undertaking upon which the water is to be used and to which this licence is appurtenant is the land improvement project of the licensee under Operation Certificate MR 12218 (Glenmore Landfill).
- h) The authorized works are dam, pumphouse, pond, and pipe which shall be located approximately as shown on the attached plan.
- i) The construction of the said works has been completed and the water is being beneficially used. The licensee shall continue to make regular beneficial use of the water in a manner authorized herein.
- j) This Licence is issued in substitution of Conditional Water Licence C123789.
- k) The dam authorized under clause (h) is subject to the Dam Safety Regulation and shall be designed, constructed and maintained to the satisfaction of a Dam Safety Officer under the *Water Sustainability Act* and in accordance with the Canadian Dam Association Guidelines.
- l) This licence is issued under the *Water Sustainability Act* (the Act). The exercise of rights under the licence is subject to the Act and its regulations, the terms and conditions of the



licence, orders under the Act and the rights of licensees whose rights have precedence on the stream or on an aquifer. The licensee must comply with all such requirements, as well as the provisions of all other applicable enactments. In exercising rights under the licence, the licensee must exercise reasonable care to avoid damaging land, works, trees or other property, and must make full compensation to the owners for damage or loss resulting from construction, maintenance, use, operation or failure of the works.

- m) During all phases of construction and maintenance of the licenced works and related activities, the holder of this licence is subject to the habitat protection requirements, described in the document entitled "*Terms and Conditions for Construction and Maintenance of Licensed Works*" (dated March 1, 2017). Those habitat protection requirements are hereby incorporated into this licence as if written herein as licence conditions, which requirements must be implemented by the licensee in conjunction with any guidance provided by a Water Manager or Habitat Officer.



Michael Epp  
Assistant Water Manager



# Province of British Columbia

## *Water Sustainability Act*

### CONDITIONAL WATER LICENCE

The owner of the undertaking to which this licence is appurtenant is hereby authorized to divert, use, and store water as follows:

- a) The stream on which the rights are granted is Avocet Creek, and the reservoir is on the creek.
- b) The point of diversion is located as shown on the attached plan.
- c) The date from which this licence shall have precedence is March 10, 2008.
- d) The purpose for which this licence is issued is land improvement.
- e) The maximum quantity of water which may be diverted is 123,348 cubic metres per year.
- f) The period of the year during which the water may be used is January 1 to December 31.
- g) The undertaking upon which the water is to be used and to which this licence is appurtenant is the land improvement project of the licensee under Operation Certificate MR 12218 (Glenmore Landfill).
- h) The authorized works are dam, pumphouse, pond, and pipe which shall be located approximately as shown on the attached plan.
- i) The construction of the said works has been completed and the water is being beneficially used. The licensee shall continue to make regular beneficial use of the water in a manner authorized herein.
- j) This Licence is issued in substitution of Conditional Water Licence C123789.
- k) The dam authorized under clause (h) is subject to the Dam Safety Regulation and shall be designed, constructed and maintained to the satisfaction of a Dam Safety Officer under the *Water Sustainability Act* and in accordance with the Canadian Dam Association Guidelines.
- l) This licence is issued under the *Water Sustainability Act* (the Act). The exercise of rights under the licence is subject to the Act and its regulations, the terms and conditions of the

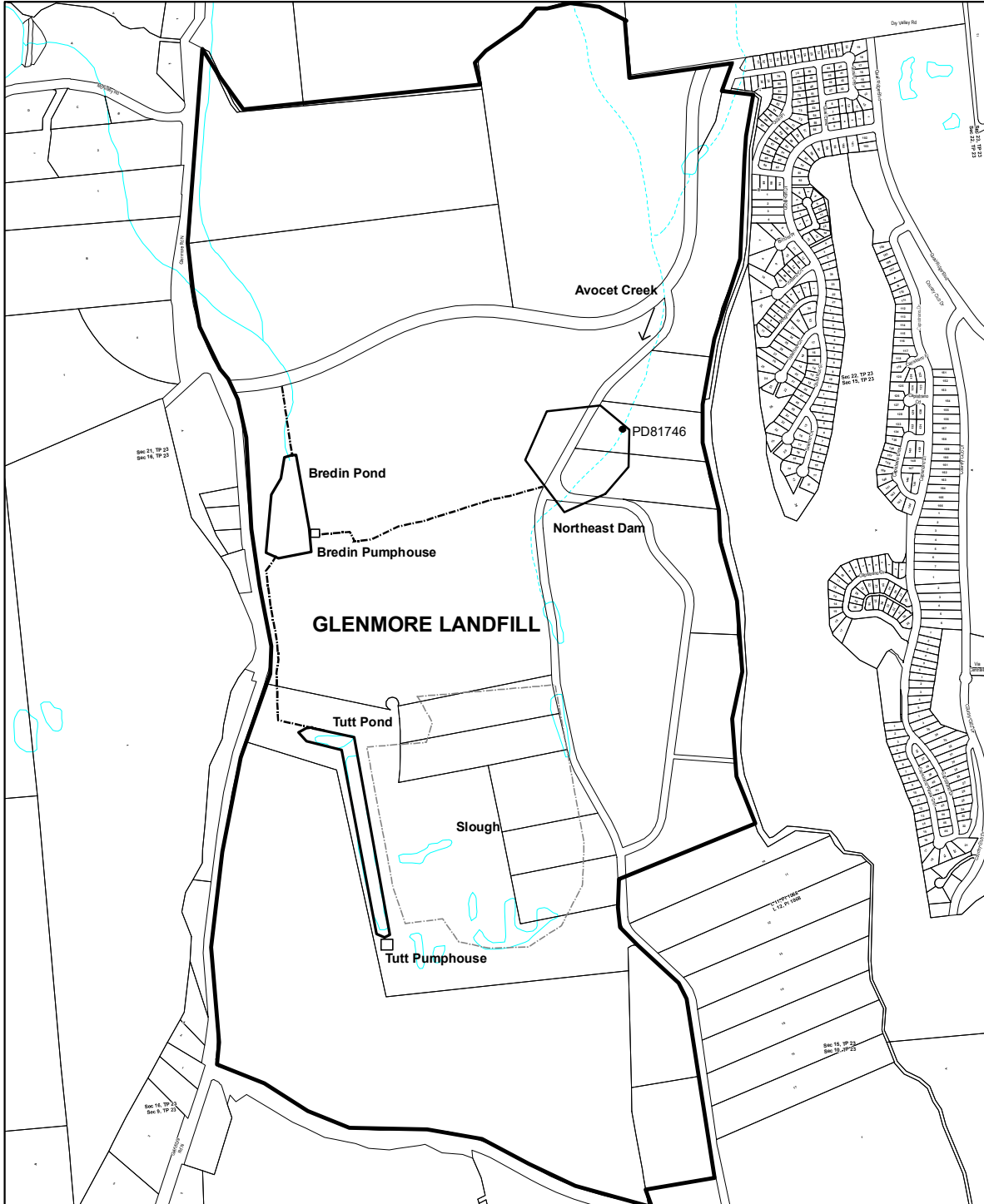
licence, orders under the Act and the rights of licensees whose rights have precedence on the stream or on an aquifer. The licensee must comply with all such requirements, as well as the provisions of all other applicable enactments. In exercising rights under the licence, the licensee must exercise reasonable care to avoid damaging land, works, trees or other property, and must make full compensation to the owners for damage or loss resulting from construction, maintenance, use, operation or failure of the works.

- m) During all phases of construction and maintenance of the licenced works and related activities, the holder of this licence is subject to the habitat protection requirements, described in the document entitled "*Terms and Conditions for Construction and Maintenance of Licensed Works*" (dated March 1, 2017). Those habitat protection requirements are hereby incorporated into this licence as if written herein as licence conditions, which requirements must be implemented by the licensee in conjunction with any guidance provided by a Water Manager or Habitat Officer.




Michael Epp  
Assistant Water Manager





Water District: Vernon  
Precinct: Kelowna  
Land District: ODYD  
Map Number: 082.E.096  
Scale: 1:12,000

Signature:   
Date: July 31, 2018  
Licence: C134394  
File: 8002781

**LEGEND:**

Point of Diversion: ●  
Pipe: - - - - -

The boundaries of this land to which this licence is appurtenant are shown thus: 

# **Appendix C**

## **Stratigraphy**

# **Appendix C.1**

**Stratigraphic and Instrumentation Logs**





PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH2

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		438.38						
	Topsoil (FILL).		0.00						
			438.08						
			0.30						
	Brown clayey SILT and silty CLAY cover (FILL).								
1			437.31						
			1.07						
2	Municipal Solid Waste (FILL).								
								436.88	
3									
4			434.27						
	Soft to Firm brown silty CLAY.		4.11						
			433.81						
			4.57						
5	Soft to firm brown clayey SILT, some sand layers.								
			432.89						
			5.49						
6	END OF HOLE								
7									
8									
9									
10									

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH3

SHEET: 1 OF 1



PROJECT LOCATION: Glenmore Dump

BORING DATE: Sept 9, 1992

DATUM: Geodetic


PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.

DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp  -----  W	
0	Ground Surface		438.75							
	Topsoil (FILL).		0.00							
			438.45							
	Brown clayey SILT and silty CLAY cover (FILL).		0.30							
			438.14							
			0.61							
1	Municipal Solid Waste (FILL).									
			437.07							
			1.68							
2	Soft to Firm brown clayey SILT, some sand.									
			436.31							
			2.44							
	END OF HOLE									
3										
4										
5										
6										
7										
8										
9										
10										

  
 Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH4

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m	PIEZOMETER OR STANDPIPE INSTALLATION										
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE			BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp   W   Wl						
0	Ground Surface		438.86															
	Topsoil (FILL).		0.00															
			438.56	0.30														
1	Brown clayey SILT and silty CLAY cover (FILL).																	
			437.64	1.22														
2	Municipal Solid Waste (FILL).																	
			435.81	3.05														
3	Soft to Firm brown to grey silty CLAY.																	
			434.90	3.96														
4	END OF HOLE																	
5																		
6																		
7																		
8																		
9																		
10																		

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH5

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT		
			DEPTH						Wp		Wi
0	Ground Surface		439.39								
	Topsoil (FILL).		0.00								
			439.09								
			0.30								
	Brown clayey SILT cover (FILL).										
1			438.53								
			0.86								
	Municipal Solid Waste (FILL).										
			437.87								
			1.52								
2											
	Firm brown silty CLAY and clayey SILT.										
			436.95								
			2.44								
	END OF HOLE										
3											
4											
5											
6											
7											
8											
9											
10											

Augerhole  
dry upon  
completion  
of drilling

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH6

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT				
			DEPTH						Wp	W	Wl		
0	Ground Surface		438.75										
	Topsoil (FILL).		0.00										
			438.45										
	Brown clayey SILT cover (FILL).		0.30										
1			437.84										
	Municipal Solid Waste (FILL).		0.91										
			437.07										
2			1.68										
	Firm brown to grey clayey SILT.												
			436.31										
	END OF HOLE		2.44										
3													
4													
5													
6													
7													
8													
9													
10													

Augerhole  
dry upon  
completion  
of drilling

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH7

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT			
			DEPTH						Wp	W <sub>L</sub>	W <sub>I</sub>	
0	Ground Surface		438.89									
	Topsoil (FILL).		0.00									
			438.59									
			0.30									
1	Brown silty CLAY and clayey SILT cover (FILL).		437.82									
			1.07									
2	Municipal Solid Waste (FILL).											
3												
			435.23									
			3.66									
4	Firm brown to grey silty CLAY.											
5												
			433.71									
			5.18									
6	END OF HOLE											
7												
8												
9												
10												

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH8

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		OTHER TESTS
0	Ground Surface		438.64	0.00						
	Topsoil (FILL).		438.34	0.30						
	Brown silty CLAY cover (FILL).		438.03	0.61						
1	Municipal Solid Waste (FILL).		436.20	2.44						
2										
3	Firm to stiff brown silty CLAY.				1	AS				
4	END OF HOLE		434.68	3.96						
5										
6										
7										
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH9

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT		
								Wp	Wl	
	ELEV DEPTH									
0	Ground Surface	438.60								
	Topsoil (FILL).	0.00								
		438.30								
		0.30								
1										
2										
3	Municipal Solid Waste (FILL).									
4										
5										
6		432.81								
		5.79								
	Soft to Firm brown to grey silty CLAY.									
7		431.59								
		7.01								
	END OF HOLE									
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH10

SHEET: 1 OF 1



PROJECT LOCATION: Glenmore Dump

BORING DATE: Sept 9, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.

DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		438.83						
	Topsoil (FILL).		0.00						
			438.53						
			0.30						
	Brown clayey SILT cover (FILL).								
1			437.76						
			1.07						
	Municipal Solid Waste (FILL).								
2									
			435.93						
			2.90						
	Firm to stiff brown to grey silty CLAY.								
3									
			434.87						
			3.96						
4	END OF HOLE								
5									
6									
7									
8									
9									
10									

Sept 9, 1992  
Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
DRILLING CONTRACTOR: Sandwell  
DRILLER: Ray/Rick

LOGGED: BLJM  
CHECKED: BLJM  
DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH11

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		438.38	0.00						
	Topsoil (FILL).		438.08	0.30						
	Brown silty CLAY cover (FILL).		437.47	0.91						
1										
2										
3	Municipal Solid Waste (FILL).									
4										
5	Soft to Firm brown silty CLAY.		433.81	4.57						
6	END OF HOLE		432.89	5.49						
7										
8										
9										
10										

▽  
 Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH12

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT		
									Wp		Wl
0	Ground Surface		438.85								
	Topsoil (FILL).		0.00 438.55								
			0.30								
1	Brown silty CLAY cover (FILL).										
			437.63								
			1.22								
2	Municipal Solid Waste (FILL).										
			436.11								
			2.74								
3	Soft to Firm brown silty CLAY.										
			434.89								
			3.96								
4	END OF HOLE										
5											
6											
7											
8											
9											
10											

▽  
 Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH13

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		OTHER TESTS
0	Ground Surface		438.53							
	Topsoil (FILL).		0.00							
			438.23	0.30						
1	Brown silty CLAY cover (FILL).									
			437.31	1.22						
2										
3	Municipal Solid Waste (FILL).									
4										
5			433.35	5.18						
6	Soft to Firm brown to grey silty CLAY.				1	AS				
7	END OF HOLE		431.52	7.01						
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH14

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp   W		
0	Ground Surface		438.91								
	Topsoil (FILL).		0.00								
			438.61								
			0.30								
	Brown silty CLAY cover (FILL).										
			438.00								
1			0.91								
	Municipal Solid Waste (FILL).										
			436.47								
			2.44								
3											
	Soft to Firm brown silty CLAY.										
			434.95								
4			3.96								
	END OF HOLE										
5											
6											
7											
8											
9											
10											

▽  
 Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH15

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	
0	Ground Surface		439.15						
	Topsoil (FILL).		0.00 438.85						
			0.30						
1	Brown silty CLAY and clayey SILT cover (FILL).								
			437.78						
			1.37						
2	Municipal Solid Waste (FILL).								
			435.04						
			4.11						
5	Soft to Firm brown silty CLAY.								
			433.66						
			5.49						
	END OF HOLE								
6									
7									
8									
9									
10									

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH16

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		RECI/ATT
0	Ground Surface		438.40	0.00						
	Topsoil (FILL).		438.10	0.30						
1	Brown silty CLAY cover (FILL).		437.33	1.07						
2										
3	Municipal Solid Waste (FILL).									
4										
5										
6	Soft to Firm grey silty CLAY.		432.91	5.49						
7	END OF HOLE		431.39	7.01						
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH17

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	
0	Ground Surface		438.66						
	Topsoil (FILL).		0.00						
			438.36	0.30					
1	Brown silty CLAY and clayey SILT cover (FILL).								
			437.44	1.22					
2	Municipal Solid Waste (FILL).								
			434.55	4.11					
5	Firm to stiff brown silty CLAY.								
			433.17	5.49					
	END OF HOLE								

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

# RECORD OF BOREHOLE AH18

SHEET: 1 OF 1



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger

DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	RECI/ATT	WATER CONTENT, PERCENT Wp ——— Wl	
0	Ground Surface	[Symbol]	439.19							
	Topsoil.	[Symbol]	0.00							
		[Symbol]	438.89							
		[Symbol]	0.30							
1		[Symbol]								
2	Firm to stiff brown silty CLAY and clayey SILT.	[Symbol]								
3		[Symbol]								
4		[Symbol]								
5	END OF HOLE	[Symbol]	434.62							
		[Symbol]	4.57							
6		[Symbol]								
7		[Symbol]								
8		[Symbol]								
9		[Symbol]								
10		[Symbol]								

Augerhole dry upon completion of drilling

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH19

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	
0	Ground Surface		438.84	0.00						
	Topsoil (FILL).		438.54	0.30						
	Brown silty CLAY cover (FILL).									
1			437.77	1.07						
	Municipal Solid Waste (FILL).									
2			435.49	3.35						
	Firm brown silty CLAY.									
4			434.88	3.96						
	END OF HOLE									
5										
6										
7										
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH20

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	
0	Ground Surface		438.63							
	Topsoil (FILL).		0.00							
			438.33	0.30						
1	Brown silty CLAY and clayey SILT cover (FILL).									
			437.11	1.52						
2										
3	Municipal Solid Waste (FILL).									
4			434.36	4.27						
5	Soft to firm brown silty CLAY.									
			433.14	5.49						
	END OF HOLE									
6										
7										
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH21

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	
0	Ground Surface		438.45							
	Topsoil (FILL).		0.00							
			438.15	0.30						
	Brown silty CLAY cover (FILL).									
			437.69	0.76						
1										
2										
3	Municipal Solid Waste (FILL).									
4			434.03	4.42						
5	Soft to firm brown to grey silty CLAY.									
			432.96	5.49						
	END OF HOLE									
6										
7										
8										
9										
10										

▽  
 Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH22

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	WATER CONTENT, PERCENT Wp — W — Wt	
0	Ground Surface		438.76							
	Topsoil (FILL).		0.00							
			438.46							
			0.30							
1	Brown to grey silty CLAY and clayey SILT cover (FILL).		437.54							
			1.22							
2										
3	Municipal Solid Waste (FILL).									
4										
			434.34							
			4.42							
5	Soft to firm brown silty CLAY.			1	AS					
			433.27							
			5.49							
6	END OF HOLE									
7										
8										
9										
10										

▽  
 Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH23

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	RECI/ATT	
0	Ground Surface		439.48							
	Topsoil (FILL).		0.00							
			439.16							
	Brown silty CLAY and clayey SILT cover (FILL).		0.30							
1			438.55							
			0.91							
2										
	Municipal Solid Waste (FILL).									
3										
4										
			435.04							
			4.42							
5	Soft to firm brown silty CLAY.									
			433.97							
			5.49							
6	END OF HOLE									
7										
8										
9										
10										

▽  
 Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH24

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	WATER CONTENT, PERCENT Wp ———— W	
0	Ground Surface		439.41							
	Topsoil (FILL).		0.00							
			439.11							
	Brown silty CLAY and clayey SILT cover (FILL).		0.30							
			438.80							
			0.61							
1	Municipal Solid Waste (FILL).									
			437.89							
			1.52							
2	Soft to firm brown silty CLAY.									
3										
4	END OF HOLE		435.45							
			3.96							
5										
6										
7										
8										
9										
10										

Augerhole dry upon completion of drilling

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH25

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	RECI/T	
0	Ground Surface		438.65							
	Topsoil (FILL).		0.00							
			438.35							
	Brown silty CLAY and clayey SILT cover (FILL).		0.30							
			438.04							
			0.61							
1	Municipal Solid Waste (FILL).									
2										
3										
4										
			434.38							
			4.27							
5	Soft to firm brown to grey silty CLAY.									
			433.16							
			5.49							
6	END OF HOLE									
7										
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH26

BORING DATE: Sept 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	WATER CONTENT, PERCENT Wp — W — Wl	
0	Ground Surface		438.88							
	Topsoil (FILL).		0.00							
			438.38							
			0.30							
	Brown silty CLAY and clayey SILT cover (FILL).		437.77							
1			0.91							
2										
3	Municipal Solid Waste (FILL).									
4										
5			433.96							
	Soft brown silty CLAY.		4.72							
			433.19							
	END OF HOLE		5.49							
6										
7										
8										
9										
10										

Sept 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH27

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		RECI/TT
0	Ground Surface		439.34							
	Topsoil (FILL).		0.00							
			439.09							
			0.25							
1	Municipal Solid Waste (FILL).									
			437.51							
			1.83							
2	Soft to firm brown silty CLAY.									
3										
4	END OF HOLE		435.38							
			3.96							
5										
6										
7										
8										
9										
10										

Augerhole dry upon completion of drilling

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH28

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	
0	Ground Surface		438.79						
	Topsoil (FILL).		0.00						
			438.49	0.30					
1	Brown silty CLAY and clayey SILT cover (FILL).		437.72	1.07					
2	Municipal Solid Waste (FILL).								
3			435.59	3.20					
4	Soft to firm brown to grey silty CLAY.		434.83	3.96	1	AS			
4	END OF HOLE								
5									
6									
7									
8									
9									
10									

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH29

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	
0	Ground Surface		438.83							
	Topsoil (FILL).		0.00							
			438.53	0.30						
1	Brown to grey silty CLAY and clayey SILT cover (FILL).									
			437.61	1.22						
2										
3	Municipal Solid Waste (FILL).									
4			434.72	4.11						
5	Soft to firm brown to grey silty CLAY.									
			433.34	5.49						
6	END OF HOLE									
7										
8										
9										
10										

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH30

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	WATER CONTENT, PERCENT				
			DEPTH						Wp	w	wi		
0	Ground Surface		438.69										
	Topsoil.		0.00										
			438.39										
			0.30										
1	Brown silty CLAY and clayey SILT.												Augerhole dry upon completion of drilling
2													
	END OF HOLE		436.25										
			2.44										
3													
4													
5													
6													
7													
8													
9													
10													

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH31

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	
0	Ground Surface		438.68							
	Topsoil (FILL).		438.38	0.30						
1	Brown to grey silty CLAY cover (FILL).		437.16	1.52						
2	Municipal Solid Waste (FILL).		434.72	3.96						
3	Soft to firm brown to grey silty CLAY.		433.19	5.49						
4	END OF HOLE									
5										
6										
7										
8										
9										
10										

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH32

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	WATER CONTENT, PERCENT Wp  -----  W	
0	Ground Surface		438.71							
	Topsoil (FILL).		0.00							
			438.41							
			0.30							
1	Brown to grey silty CLAY and clayey SILT cover (FILL).		436.88							
			1.83							
2	Municipal Solid Waste (FILL).		434.75							
			3.96							
4	Soft to firm brown silty CLAY.		433.22							
			3.49							
5	END OF HOLE									
6										
7										
8										
9										
10										

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH33

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	WATER CONTENT, PERCENT Wp — W — W		
0	Ground Surface		438.55								
	Topsoil (FILL).		0.00								
			438.25								
			0.30								
1	Brown to grey silty CLAY and clayey SILT cover (FILL).		437.48								
			1.07								
2											
3											
4	Municipal Solid Waste (FILL).										
5											
6			432.76								
			5.79								
7	Soft to firm grey silty CLAY.		431.54								
			7.01								
7	END OF HOLE										
8											
9											
10											

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992



PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH34

SHEET: 1 OF 1



PROJECT LOCATION: Glenmore Dump

BORING DATE: Sept 10, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.

DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp   W   Wl	
0	Ground Surface		440.35							
	Topsoil.		0.00							
			440.05							
	Brown silty CLAY.		0.30							
1			439.44							
			0.91							
2										
	Loose brown SAND and GRAVEL.									
3										
4										
	END OF HOLE (Refusal)		436.08							
			4.27							
5										
6										
7										
8										
9										
10										

Sept 10, 1992  
Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
DRILLING CONTRACTOR: Sandwell  
DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
CHECKED: BLJM  
DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

### RECORD OF BOREHOLE AH35

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRAATA PLOT	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT		
								Wp		Wl
0	Ground Surface									
	Topsoil.									
		439.91								
		0.00								
		439.61								
		0.30								
1	Brown clayey SILT.									
		438.08								
		1.83								
2										
3										
4	Loose brown medium to coarse SAND, trace gravel.									
5		434.73								
		5.18								
	Compact to dense grey silty SAND, some gravel (TILL).	434.42								
		5.49								
	END OF HOLE									
6										
7										
8										
9										
10										

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH36

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		OTHER TESTS
0	Ground Surface		439.64	0.00						
	Topsoil.		439.34	0.30						
	Brown clayey SILT.									
1			438.57	1.07						
	Brown silty CLAY.									
2										
3										
4			435.68	3.96						
	Loose to compact brown gravelly medium SAND.									
5			434.15	5.49						
	END OF HOLE									
6										
7										
8										
9										
10										

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH37

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	
0	Ground Surface		439.55						
	Topsoil.		0.00						
			439.25	0.30					
	Brown clayey SILT.								
1			438.48	1.07					
2									
3	Firm to stiff brown and grey silty CLAY.								
4									
5									
6	Loose brown SAND, trace to some gravel.		433.91	5.64					
7	END OF HOLE		432.54	7.01					
8									
9									
10									

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH38

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT			
			DEPTH						Wp	W		Wl
0	Ground Surface		439.40									
	Topsoil (FILL).		0.00									
			439.10									
	Brown clayey SILT cover (FILL).		0.30									
1			438.49									
	Municipal Solid Waste (FILL).		0.91									
2			437.57									
	Firm to stiff brown silty CLAY.		1.83									
3												
4	END OF HOLE		435.74									
			3.66									
5												
6												
7												
8												
9												
10												

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH39

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT				
			DEPTH						Wp	W	WI		
0	Ground Surface		439.32										
	Topsoil (FILL).		0.00										
			439.02										
	Brown clayey SILT cover (FILL).		0.30										
			438.56										
			0.76										
1	Municipal Solid Waste (FILL).												
2													
			436.88										
			2.44										
3	Soft to firm brown silty CLAY.												
4													
			435.36										
			3.96										
4	END OF HOLE												
5													
6													
7													
8													
9													
10													

Sept 10, 1992  
 Water level  
 based on  
 observations  
 made at  
 time of  
 drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH40

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (M)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp — W — Wt	
0	Ground Surface		439.64							
	Topsoil (FILL).		0.00							
			439.34							
	Brown clayey SILT.		0.30							
			439.03							
			0.61							
1										
2	Soft to firm brown silty CLAY.									
3										
4	END OF HOLE		435.68							
			3.96							
5										
6										
7										
8										
9										
10										

Augerhole dry upon completion of drilling

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH41

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	REC/ATT	
0	Ground Surface		439.21							
	Topsoil (FILL).		0.00							
			438.91							
			0.30							
1	Brown silty CLAY and clayey SILT cover (FILL).		438.14							
			1.07							
2	Municipal Solid Waste (FILL).									
3										
4										
			434.64							
			4.57							
5	Soft to firm brown silty CLAY.									
			433.72							
			5.49							
6	END OF HOLE									
7										
8										
9										
10										

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH42

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		OTHER TESTS
										Wp  -----  W  -----  Wl 20  -----  40  -----  60  -----  80
0	Ground Surface		440.81							
	TOPSOIL.		0.00							
			440.51	0.30						
	Brown dessicated clayey SILT.									
			439.90	0.91						
1										
2					1	AS				
3										
4	Firm to stiff brown silty CLAY, occasional pockets and thin seams of sand.				2	AS				
5										
6			435.02	5.78	3	AS				
7	Soft to firm brown silty CLAY, occasional seams of fine sand, some gravel.				4	AS				
	END OF HOLE		433.80	7.01						
8										
9										
10										

Sept 10, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992



PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH43

SHEET: 1 OF 1



PROJECT LOCATION: Glenmore Dump

BORING DATE: Sept 10, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.

DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m				PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT					
			DEPTH						Wp	W	Wl	80		
0	Ground Surface		442.13											
	TOPSOIL		0.00											
			441.83											
	Brown dessicated clayey SILT.		0.30											
			441.37											
			0.76											
1	Soft to firm brown silty CLAY.		440.91											
			1.22											
	Loose brown fine to medium SAND.		440.45											
			1.68											
2	Firm to stiff brown silty CLAY.			1	AS									
3	Firm to stiff brown silty CLAY.													
4	Loose brown silty fine SAND.			2	AS									
			438.02											
			4.11											
5	Loose brown medium to coarse SAND, some gravel.													
			437.25											
			4.88											
	END OF HOLE			3	AS									
			436.64											
			5.49											
6														
7														
8														
9														
10														

Sept 10, 1992  
Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
DRILLING CONTRACTOR: Sandwell  
DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
CHECKED: BLJM  
DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH44

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	
0	Ground Surface		440.15						
	TOPSOIL		0.00						
			439.85						
	Brown dessicated clayey SILT.		0.30						
1			439.24						
			0.91						
2	Firm to stiff brown silty CLAY.				1	AS			H
3	Loose brown silty fine SAND.		437.25						
			2.90						
			437.00						
			3.15						
4	Soft brown silty CLAY.				2	AS			
5	Soft brown clayey SILT, occasional pockets of medium sand.		434.97						
			5.18						
6	Compact to dense brown silty SAND, some gravel, trace cobbles (TILL-LIKE).		434.36						
			5.79						
7	END OF HOLE		433.14						
			7.01		4	AS			

Backfilled with cuttings.  
 Sept 14, 1992



DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

### RECORD OF BOREHOLE AH45

BORING DATE: Sept 10, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRAATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		439.78						
	TOPSOIL.		0.00						
			439.48						
	Brown dessicated clayey SILT.		0.30						
			439.18						
			0.60						
1	Firm to stiff brown silty CLAY.								
2				1	AS				
			437.19						
	Loose brown medium SAND.		2.59						
			2.74						
3	Soft brown silty CLAY.								
4				2	AS				
			435.06						
	Soft brown clayey SILT, occasional seams of sand, trace gravel.		4.72						
5			434.60						
	Loose brown SAND and GRAVEL.		5.18						
			434.29						
	END OF HOLE		5.49						
6									
7									
8									
9									
10									

Sept 10, 1992  
 Water level  
 based on  
 observa-  
 tions made  
 at time of  
 drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Sept 10, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH46

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		441.98 0.00						
	TOPSOIL		441.53 0.45						
1									
2	Firm to stiff brown silty CLAY. (upper 0.9m dessicated)								
3									
4			437.88 4.10						
5	Loose to compact brown to grey silty SAND and GRAVEL with some clay and occasional cobbles.								
			436.48 5.50						
6	END OF HOLE								
7									
8									
9									
10									

▽  
 Nov 5, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH47

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	
0	Ground Surface		448.25	0.00					
	TOPSOIL		447.80	0.45					
1	Firm to stiff brown silty CLAY. (upper 0.6m dessicated)		445.35	2.90					
2			445.05	3.20					
3	Loose to compact light brown SILT with a trace of clay and some sand.		444.45	3.80					
4	Compact brown SAND with some silt.		442.75	5.50					
5	Compact to dense brown silty SAND and GRAVEL with a trace of clay and occasional cobbles. (TILL)								
6	END OF HOLE								
7									
8									
9									
10									

Augerhole dry upon completion.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH48

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp ———— W	
0	Ground Surface		454.05 0.00							
	TOPSOIL		453.60 0.45							
1	Loose to compact brown SILT with a trace to some clay and some sand.		452.85 1.20							
2	Compact to dense brown silty SAND and GRAVEL with occasional cobbles. (TILL)		451.60 2.45							Augerhole dry upon completion.
	END OF HOLE									
3										
4										
5										
6										
7										
8										
9										
10										

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH49

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT		
		ELEV DEPTH						Wp	Wl	
0	Ground Surface		452.06							
	TOPSOIL		0.00							
			451.61							
1	Loose brown sandy SILT with a trace to some gravel.		0.45							
			450.56							
2	Loose brown SAND with a trace to some gravel.		1.50							
3			448.06							
4	END OF HOLE		4.00							
5										
6										
7										
8										
9										
10										

Augerhole dry upon completion.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH50

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION		
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT				
									Wp	W		Wl	
0	Ground Surface		446.75										
	TOPSOIL		0.00										
			446.30										
	Firm to stiff brown desiccated silty CLAY.		0.45										
1			445.55										
	Stiff brown clayey SILT with some sand and some gravel.		1.20										
			445.05										
			1.70										
2	Compact to dense brown silty SAND and GRAVEL with occasional cobbles.		444.30										
			2.45										
	END OF HOLE												
3													
4													
5													
6													
7													
8													
9													
10													

Augerhole dry upon completion.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH51

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

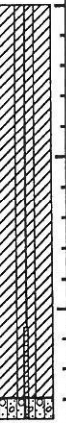
SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT				
			DEPTH						W <sub>p</sub>	W	W <sub>L</sub>		
0	Ground Surface		441.36										
	TOPSOIL		0.00										
			440.91										
			0.45										
1	Firm to stiff brown silty CLAY. (upper 0.6m dessicated)												
2			1	AS									
			438.76										
			2.60										
3	Loose brown gravelly SAND with a trace of silt.												
			437.66										
			3.70										
4	Compact grey sandy SILT with some gravel and some clay. (TILL)												
			437.36										
			4.00										
	END OF HOLE												
5													
6													
7													
8													
9													
10													

Backfilled  
with auger  
cuttings.

Augerhole  
Dry  
Nov 9, 1992



DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH52

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m				PIEZOMETER OR STANDPIPE INSTALLATION		
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT					
			DEPTH						Wp	W	Wi		80	
0	Ground Surface		439.83											
	TOPSOIL		0.00											
			439.38											
			0.45											
1	Firm to stiff brown silty CLAY. (upper 0.9m dessicated)													
2														
3			1	AS										
4	Loose to compact brown silty SAND with some gravel and occasional seams of coarse sand.		435.73											
5			4.10											
6	END OF HOLE		434.33											
7			5.50											
8														
9														
10														

▽  
 Nov 5, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH53

SHEET: 1 OF 1



PROJECT LOCATION: Glenmore Dump

BORING DATE: November 5, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.

DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	
0	Ground Surface		443.91	0.00					
	TOPSOIL		443.61	0.30					
	Firm to stiff brown dessicated clayey SILT.		443.01	0.90					
1	Firm to stiff brown silty CLAY. (upper 0.3m dessicated)		441.61	2.30					Augerhole dry upon completion.
2	Loose brown fine silty SAND.		441.31	2.60					
3	Compact to dense brown gravelly silty SAND with occasional cobbles. (TILL)		439.91	4.00					
4	END OF HOLE								
5									
6									
7									
8									
9									
10									

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH54

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp — W — Wi	
			DEPTH							
0	Ground Surface		448.47							
	TOPSOIL		0.00							
			448.02							
	Firm brown dessicated clayey SILT.		0.45							
1			447.37							Augerhole dry upon completion.
			1.10							
2	Compact to dense brown gravelly silty SAND.									
3			445.37							
			3.10							
4	Dense brown gravelly silty SAND with occasional cobbles. (TILL)									
			444.47							
	END OF HOLE		4.00							
5										
6										
7										
8										
9										
10										

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH55

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT			
			DEPTH						W <sub>p</sub>	W		W <sub>L</sub>
0	Ground Surface		444.71									
	TOPSOIL		0.00									
			444.26									
	Firm to stiff brown dessicated clayey SILT.		0.45									
1			443.51									
			1.20									
2												
	Firm to stiff brown silty CLAY.											
3												
				1	AS							
4			440.41									
			4.30									
5	Compact to dense brown gravelly silty SAND. (TILL)											
			439.21									
			5.50									
6	END OF HOLE											
7												
8												
9												
10												

Augerhole dry upon completion.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH56

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		441.42						
	TOPSOIL		0.00						
			440.97						
1	Firm to stiff brown desiccated clayey SILT with a trace of sand.		0.45						Augerhole dry upon completion.
			439.92						
2	Loose to compact brown gravelly SAND with some silt.		1.50						
			438.82						
			2.60						
3	Compact to dense brown gravelly silty SAND with occasional cobbles. (TILL)								
			437.42						
4	END OF HOLE		4.00						
5									
6									
7									
8									
9									
10									

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH57

SHEET: 1 OF 1



PROJECT LOCATION: Glenmore Dump

BORING DATE: November 5, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.

DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		OTHER TESTS
0	Ground Surface		438.28							
	TOPSOIL		0.00							
			437.98	0.30						
1	Firm brown silty CLAY, some gravel, organics (FILL).									
			436.76	1.52						
2										
3	Firm to stiff brown silty CLAY, occasional thin seams of sand.									
4			433.56	4.72						
5	Firm brown clayey SILT, occasional thin seams of sand.									
6			432.18	6.10						
7	Firm to soft grey silty CLAY.									
			431.12	7.16						
8	Soft grey sandy clayey SILT.									
			429.75	8.53						
9	END OF HOLE									
10										

Nov 5, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH58

SHEET: 1 OF 1



PROJECT LOCATION: Glenmore Dump

BORING DATE: November 5, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.

DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT				
								Wp	W	Wl		
0	Ground Surface	438.45										
	TOPSOIL	0.00										
		438.00										
		0.45										
1												
2												
3	Firm to stiff brown silty CLAY (upper 0.6m dessicated), occasional pockets and thin seams of sand.											
4			1	AS								
		433.88										
		4.57										
5			2	AS								
6	Firm grey clayey SILT, occasional pockets and thin seams of sand.											
7	END OF HOLE	431.44										
		7.01										
8												
9												
10												

▽  
Nov 9, 1992

Backfilled with auger cuttings.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH59

BORING DATE: November 5, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT	
			DEPTH							
0	Ground Surface		439.04							
	TOPSOIL		0.00							
			438.59							
			0.45							
1	Firm to stiff brown silty CLAY, occasional thin sand seams.									
2										
3										
4				1	AS					
			434.77							
			4.27							
5	Firm brown to grey clayey SILT, some thin sand seams.									
6										
7			432.03	2	AS					
			7.01							
	END OF HOLE									
8										
9										
10										

Hole caved - no water detected to 4.57m depth

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992



PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH60

SHEET: 1 OF 1

PROJECT LOCATION: Glenmore Dump

BORING DATE: November 5, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m	PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N		
			DEPTH					WATER CONTENT, PERCENT	
0	Ground Surface		438.57						
	TOPSOIL		0.00						
			438.12						
	Firm brown clayey SILT, some sand.		0.45						
1			437.50						
			1.07						
2				1	AS				
3	Firm to stiff brown silty CLAY (upper 0.3m dessicated), occasional pockets and thin seams of sand.			2	AS			H	
4			433.85						
			4.72						
5	Firm grey clayey SILT, some seams of sand.		433.08						
			5.49						
6	END OF HOLE								
7									
8									
9									
10									

Nov 9, 1992

Backfilled with auger cuttings.

DRILL RIG: Mobil P70  
DRILLING CONTRACTOR: Sandwell  
DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
CHECKED: BLJM  
DATE: Nov 5, 1992

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH61

SHEET: 1 OF 1

PROJECT LOCATION: Glenmore Dump

BORING DATE: November 5, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT			
								Wp	W		Wi
0	Ground Surface										
	TOPSOIL										
		438.36 0.00 438.06 0.30									
1											
2	Firm to stiff brown silty CLAY (upper 0.9m dessicated), occasional pockets and thin seams of sand.										
3			1	AS							
4		434.25 4.11									
5	Stiff brown to grey clayey SILT, occasional pockets and thin seams of sand.										
6											
7	END OF HOLE	431.35 7.01									
8											
9											
10											

▽

Nov 6, 1992

Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 5, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH62

BORING DATE: November 6, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		OTHER TESTS
0	Ground Surface		441.39							
	Brown Clayey SILT, some organics, cover (FILL).		0.00							
			441.09	0.30						
1										
2	Municipal Solid Waste (FILL).									
3										
4			437.58	3.81						
5	Firm to stiff grey to brown silty CLAY.									
6			435.90	5.49						
7	END OF HOLE									
8										
9										
10										

Nov 6, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 6, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH63

BORING DATE: November 6, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT			
			DEPTH						Wp	W		Wi
0	Ground Surface		442.43									
	Brown Sandy Clayey SILT, some gravel, cover (FILL).		0.00									
			0.15									
1												
2												
3	Municipal Solid Waste (FILL).											
4												
5												
			436.94									
			5.49									
6												
7	Firm grey to brown silty CLAY.											
8												
			433.90									
	END OF HOLE		8.53									
9												
10												

▽  
 Nov 6, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 6, 1992



PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH64

SHEET: 1 OF 1

PROJECT LOCATION: Glenmore Dump

BORING DATE: November 6, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		442.88						
	SILT, organics and wood chips, cover (FILL).		0.00						
			0.30						
1									
2									
3	Municipal Solid Waste (FILL).								
4									
5									
			437.24						
			5.64						
6	Firm grey to brown silty CLAY.								
7	END OF HOLE		435.87						
			7.01						
8									
9									
10									

▽

Nov 6, 1992

Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 6, 1992

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH65

SHEET: 1 OF 2

PROJECT LOCATION: Glenmore Dump

BORING DATE: November 6, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
0	Ground Surface		443.42						
	SAND and GRAVEL, some silt, cover (FILL).		0.00						
			0.15						
1									
2									
3									
4									
5	Municipal Solid Waste (FILL).								
6									
7									
8									
9									
10			433.67						
			9.75						

CONTINUED ON NEXT PAGE

Water level based on observations made at time of drilling.



Nov 6, 1992

DRILL RIG: Mobil P70  
DRILLING CONTRACTOR: Sandwell  
DRILLER: Ray/Rick

LOGGED: BLJM  
CHECKED: BLJM  
DATE: Nov 6, 1992

**Golder Associates**

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH65

SHEET: 2 OF 2

PROJECT LOCATION: Glenmore Dump

BORING DATE: November 6, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	
10	CONTINUED FROM PREVIOUS PAGE								
11	Soft to firm grey silty CLAY.								
12	END OF HOLE		431.84 11.58						
13									
14									
15									
16									
17									
18									
19									
20									

DRILL RIG: Mobil P70  
DRILLING CONTRACTOR: Sandwell  
DRILLER: Ray/Rick

LOGGED: BLJM  
CHECKED: BLJM  
DATE: Nov 6, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH66

BORING DATE: November 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp 20 — W — Wl 80	
			DEPTH							
0	Ground Surface		444.31 0.00							
1	Loose Brown Sandy SILT, some clay, some gravel, some pieces of plastic, some cobbles (FILL).									
2										
3										
4	Compact to dense Black Organic Matter (FILL).		440.65 3.66							
5										
6	Compact to dense dark grey Gravelly Sandy SILT, some clay (TILL-LIKE).									
7										
8										
9	END OF HOLE		437.30 7.01							
10										
			434.25 10.06	2	AS					

▽  
 Nov 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 9, 1992



PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH67

BORING DATE: November 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp   $\frac{w}{w}$   Wl	
			DEPTH							
0	Ground Surface		440.38							
	Topsoil (FILL).		0.00							
			440.08							
			0.30							
1	Municipal Solid Waste (FILL).									
2										
3										
4										
5										
6	Firm to stiff brown silty CLAY.		434.74							
			5.64							
7	END OF HOLE		433.37							
			7.01							
8										
9										
10										

Nov 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH68

BORING DATE: November 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N		OTHER TESTS
0	Ground Surface		439.44							
	Topsoil (FILL).		0.00							
			0.15							
1	Municipal Solid Waste (FILL).									
2										
3										
			436.09							
			3.35							
	Firm to stiff brown silty CLAY.									
4			435.48							
	END OF HOLE		3.96							
5										
6										
7										
8										
9										
10										

▽  
 Nov 9, 1992

Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 9, 1992

PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH69

SHEET: 1 OF 1

PROJECT LOCATION: Glenmore Dump

BORING DATE: November 9, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172


BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	ELEV	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT			
			DEPTH						Wp	W		Wi
0	Ground Surface		442.50									
	Brown Sandy Clayey SILT, trace gravel cover (FILL)		0.00									
			0.15									
1												
2												
3	Municipal Solid Waste (FILL).											
4												
5												
			437.17									
			5.33									
6	Firm to stiff brown silty CLAY.											
7	END OF HOLE		435.49									
			7.01									
8												
9												
10												

  
 Nov 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH70

BORING DATE: November 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m		PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp — W — Wi	
0	Ground Surface		441.74							
	Brown Sandy Clayey SILT, trace gravel cover (FILL)		0.00 0.10							
1										
2										
3										
4	Municipal Solid Waste (FILL).									
5										
6										
7										
8	Firm to stiff brown silty CLAY.		434.12 7.62							
9	END OF HOLE		433.21 8.53							
10										

▽  
 Nov 9, 1992

Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

Golder Associates

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 9, 1992



PROJECT: Pond Relocation

# RECORD OF BOREHOLE AH71

SHEET: 1 OF 1

PROJECT LOCATION: Glenmore Dump

BORING DATE: November 9, 1992

DATUM: Geodetic

PROJECT NUMBER: 922-4172

BORING LOCATION: See Figure 1

BOREHOLE TYPE: 140 mm Auger

Sampler Hammer: 63.5 kg., Drop 0.76m.



DEPTH SCALE (m)	SOIL PROFILE		SAMPLES					PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION	
	DESCRIPTION	STRATA PLOT	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT				
								Wp	W	Wi		
0	Ground Surface											
	Sand and Gravel (FILL).											
	Brown Sandy Clayey SILT cover (FILL).											
1	Municipal Solid Waste (FILL).											
2												
3	Firm to stiff grey to brown silty CLAY.											
4												
5	END OF HOLE											
6												
7												
8												
9												
10												

▽

Nov 9, 1992

Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 9, 1992

PROJECT: Pond Relocation  
 PROJECT LOCATION: Glenmore Dump  
 PROJECT NUMBER: 922-4172  
 Sampler Hammer: 63.5 kg., Drop 0.76m.

# RECORD OF BOREHOLE AH72

BORING DATE: November 9, 1992  
 BORING LOCATION: See Figure 1

SHEET: 1 OF 1  
 DATUM: Geodetic  
 BOREHOLE TYPE: 140 mm Auger



DEPTH SCALE (m)	SOIL PROFILE			SAMPLES				PENETRATION RESISTANCE BLOWS/0.3m			PIEZOMETER OR STANDPIPE INSTALLATION
	DESCRIPTION	STRATA PLOT	ELEV DEPTH	NUMBER	TYPE	BLOWS / 0.15m.	N	OTHER TESTS	WATER CONTENT, PERCENT Wp  -----  W		
0	Ground Surface		439.02								
	Sand and Gravel (FILL).		0.00								
	Brown Clayey SILT cover (FILL).		0.10								
			0.30								
1	Municipal Solid Waste (FILL).										
2			436.73								
			2.29								
3	Firm to stiff grey to brown silty CLAY.										
4	END OF HOLE		435.06								
			3.96								
5											
6											
7											
8											
9											
10											

▽  
 Nov 9, 1992  
 Water level based on observations made at time of drilling.

DRILL RIG: Mobil P70  
 DRILLING CONTRACTOR: Sandwell  
 DRILLER: Ray/Rick

**Golder Associates**

LOGGED: BLJM  
 CHECKED: BLJM  
 DATE: Nov 9, 1992

**RECORD OF TEST PITS**

November 10, 1992

922-4172

TEST PIT NO.	DEPTH (m)	SOIL DESCRIPTION
T1 (west end)	0.0 - 0.45 0.45 - 2.44	<p><b>TOPSOIL.</b></p> <p>Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.7m), trace sand.</p> <p>Standing groundwater at 1.83m below existing ground surface in open test pit.</p>
T1 (east end)	0.0 - 0.30 0.30 - 0.91 0.91 - 1.83	<p><b>TOPSOIL (FILL).</b></p> <p>Brown clayey <b>SILT</b> cover (<b>FILL</b>).</p> <p><b>MUNICIPAL SOLID WASTE (FILL).</b></p>
T2 (west end)	0.0 - 0.30 0.30 - 2.44	<p><b>TOPSOIL.</b></p> <p>Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.7m), trace to some sand.</p> <p>Standing groundwater at 1.83m below existing ground surface in open test pit.</p>
T2 (east end)	0.0 - 0.30 0.30 - 0.76 0.76 - 1.83	<p><b>TOPSOIL (FILL).</b></p> <p>Brown clayey <b>SILT</b> cover (<b>FILL</b>).</p> <p><b>MUNICIPAL SOLID WASTE (FILL).</b></p>

438.4  
 - 1.8  
 -----  
 436.6

**RECORD OF TEST PITS**

November 10, 1992

922-4172

T3 (north end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 2.59	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.6m), trace sand.  Standing groundwater at 2.13m below existing ground surface in open test pit.
T3 (south end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.91	Brown clayey <b>SILT</b> cover ( <b>FILL</b> ).
	0.91 - 1.68	<b>MUNICIPAL SOLID WASTE (FILL).</b>
T4 (north end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 2.74	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.6m), trace sand.  Standing groundwater at 1.98m below existing ground surface in open test pit.
T4 (south end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.76	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	0.76 - 1.83	<b>MUNICIPAL SOLID WASTE (FILL).</b>



**RECORD OF TEST PITS**

November 10, 1992

922-4172

T5 (north end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 2.43	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.7m), trace to some sand.  Standing groundwater at 1.98m below existing ground surface in open test pit.
T5 (south end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.91	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	0.91 - 1.83	<b>MUNICIPAL SOLID WASTE (FILL).</b>
T6 (north end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 2.43	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.9m), trace sand.  Standing groundwater at 1.83m below existing ground surface in open test pit.
T6 (south end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.76	Brown clayey <b>SILT</b> cover ( <b>FILL</b> ).
	0.76 - 1.68	<b>MUNICIPAL SOLID WASTE (FILL).</b>

**RECORD OF TEST PITS**

**November 10, 1992**

**922-4172**

T7 (north end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 2.13	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.9m), trace sand.  Standing groundwater at 1.68m below existing ground surface in open test pit.
T7 (south end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.91	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	0.91 - 1.68	<b>MUNICIPAL SOLID WASTE (FILL).</b>
T8 (north end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 1.98	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.6m), trace to some sand.  Standing groundwater at 1.68m below existing ground surface in open test pit.
T8 (south end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 1.07	Brown clayey <b>SILT</b> cover ( <b>FILL</b> ).
	1.07 - 1.68	<b>MUNICIPAL SOLID WASTE (FILL).</b>

**RECORD OF TEST PITS**

November 10, 1992

922-4172

T9 (north end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 2.13	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.9m), trace to some sand.  Standing groundwater at 1.68m below existing ground surface in open test pit.
T9 (south end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.91	Brown clayey <b>SILT</b> cover ( <b>FILL</b> ).
	0.91 - 1.68	<b>MUNICIPAL SOLID WASTE (FILL).</b>
T10 (east end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 2.13	Firm to stiff brown clayey <b>SILT</b> and silty <b>CLAY</b> (desiccated in upper 0.6m), trace to some sand.  Standing groundwater at 1.98m below existing ground surface in open test pit.
T10 (west end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 1.07	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	1.07 - 1.83	<b>MUNICIPAL SOLID WASTE (FILL).</b>

**RECORD OF TEST PITS**

November 10, 1992

922-4172

T11 (west end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.91	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	0.91 - 1.83	<b>MUNICIPAL SOLID WASTE (FILL).</b>  Standing groundwater at 1.83m depth.
T11 (east end)	0.0 - 0.30	<b>TOPSOIL.</b>
	0.30 - 1.83	Firm to stiff brown fissured silty <b>CLAY</b> , trace sand, dark brown staining from 1.22 to 1.83m depth.  Test pit dry at east end.
T12 (west end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.91	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	0.91 - 1.83	<b>MUNICIPAL SOLID WASTE (FILL).</b>  Test pit dry at west end.
T12 (east end)	0.0 - 0.30	<b>TOPSOIL (FILL).</b>
	0.30 - 0.91	Brown silty <b>CLAY</b> , some sand ( <b>FILL</b> ).
	0.91 - 1.52	Firm to stiff brown silty <b>CLAY</b> .  Test pit dry at east end.



**RECORD OF TEST PITS**

**November 10, 1992**

**922-4172**

<p align="center">T13 (north end)</p>	<p>0.0 - 1.52</p>	<p>Loose to compact brown silty <b>SAND</b> and <b>COBBLES</b>, some gravel (<b>FILL</b>).</p> <p>Test pit dry at north end.</p>
<p align="center">T13 (south end)</p>	<p>0.0 - 0.61 0.61 - 0.91 0.91 - 1.52</p>	<p>Brown clayey <b>SILT</b>, some sand cover (<b>FILL</b>).</p> <p><b>MUNICIPAL SOLID WASTE (FILL)</b>.</p> <p>Brown silty <b>SAND</b> and <b>COBBLES</b>, some gravel (<b>FILL</b>).</p> <p>Test pit dry at south end.</p>
<p align="center">T14</p>	<p>0.0 - 0.30 0.30 - 0.91 0.91 - 2.44 2.44 - 3.05</p>	<p><b>TOPSOIL (FILL)</b>.</p> <p>Brown silty <b>CLAY</b> cover (<b>FILL</b>).</p> <p>Construction debris (pieces of wood, metal, concrete and brick) (<b>FILL</b>).</p> <p>Stiff brown silty <b>CLAY</b>.</p> <p>Standing groundwater at 1.52m below existing ground surface in open test pit.</p>
<p align="center">T15</p>	<p>0.0 - 0.15 0.15 - 1.37 1.37 - 1.52</p>	<p><b>TOPSOIL (FILL)</b>.</p> <p>Brown silty <b>CLAY</b> cover (<b>FILL</b>).</p> <p>Construction debris (pieces of wood and concrete).</p> <p>Standing groundwater at 0.91m below existing ground surface in open test pit.</p>

**RECORD OF TEST PITS**

November 10, 1992

922-4172

T16	0.0 - 0.15	<b>TOPSOIL.</b>
	0.15 - 1.52	Firm to stiff brown fissured silty <b>CLAY.</b>  Standing groundwater at 0.91m below existing ground surface in open test pit.
T17	0.0 - 0.15	<b>TOPSOIL.</b>
	0.15 - 0.61	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	0.61 - 0.76	<b>MUNICIPAL SOLID WASTE (FILL).</b>
	0.76 - 1.68	Stiff to firm brown silty <b>CLAY.</b>  Standing groundwater at 1.4m below existing ground surface in open test pit.
T18	0.0 - 0.15	<b>TOPSOIL.</b>
	0.15 - 1.22	Firm to stiff brown desiccated silty <b>CLAY.</b>
	1.22 - 2.74	Firm to stiff brown fissured silty <b>CLAY.</b>  Test pit dry.
T19	0.0 - 0.15	<b>TOPSOIL.</b>
	0.15 - 1.52	Brown silty <b>CLAY</b> cover ( <b>FILL</b> ).
	1.52 - 1.83	Construction debris (pieces of wood and concrete).  Standing groundwater at 1.52m below existing ground surface in open test pit.

**RECORD OF TEST PITS**

November 10, 1992

922-4172

T20	0.0 - 0.15	<b>TOPSOIL.</b>
	0.15 - 0.91	Firm to stiff brown desiccated silty <b>CLAY.</b>
	0.91 - 1.83	Firm to stiff brown fissured silty <b>CLAY.</b>
Standing groundwater at 1.52m below existing ground surface in open test pit.		
T21	0.0 - 0.08	Wood mulch ( <b>FILL</b> ).
	0.08 - 1.68	Firm to stiff brown fissured silty <b>CLAY.</b>
Standing groundwater at 1.52m below existing ground surface in open test pit.		
T22	0.0 - 0.15	<b>TOPSOIL.</b>
	0.15 - 0.91	Firm to stiff brown desiccated silty <b>CLAY.</b>
	0.91 - 1.83	Firm to stiff brown fissured silty <b>CLAY.</b>
Standing groundwater at 1.52m below existing ground surface in open test pit.		
T23	0.0 - 0.30	Brown silty <b>CLAY</b> , some sand and gravel cover ( <b>FILL</b> ).
	0.30 - 1.37	<b>MUNICIPAL SOLID WASTE (FILL).</b>
Standing groundwater at 1.22m below existing ground surface in open test pit.		

RECORD OF TEST PITS

November 10, 1992

922-4172

T24	0.0 - 0.15	TOPSOIL.
	0.15 - 0.76	Brown silty CLAY cover (FILL).
	0.76 - 1.22	MUNICIPAL SOLID WASTE (FILL).
Standing groundwater at 0.91m below existing ground surface in open test pit.		



2011/2012 Monitoring Wells - Naming Convention

Consultant Monitoring Well ID      City Monitoring Well ID  
Revised

BH11-3A	GL 36-1
BH11-3B	GL 36-2
BH11-3C	GL 36-3
BH11-13A1	GL 30-1
BH11-13B	GL 30-2
BH11-13C	GL 30-3
BH11-18A1	GL 31-1
BH11-18B1	GL 31-2
BH11-18C	GL 31-3
BH11-21A1	GL 32-1
BH11-21B	GL 32-2
BH11-21C1	GL 32-3
BH11-22A	GL 33-1
BH11-22B	GL 33-2
BH11-22C	GL 33-3
BH11-26A	GL 34-1
BH11-26B	GL 34-2
BH11-26C	GL 34-3
BH11-31A	GL 35-1
BH11-31B	GL 35-2
BH11-31C	GL 35-3
BH12-1A	GL 0-1
BH12-1B	GL 0-2
BH12-1C	GL 0-3
BH12-4A	GL29-1
BH12-4B	GL29-2
BH12-10	GL38
BH12-11	GL37
BH12-14	GL 3-5 (2012)
GL6-1 (2011)	GL6-1 (2011)

Bedrock wells

GL 0-1      GL 33-3 <sup>bed</sup>/<sub>sand</sub>

GL 3-1 (dash)

GL 5-1

GL 7-1

GL 9-1

GL 14-1?

GL 15-1?

GL 16-1

GL 17-1

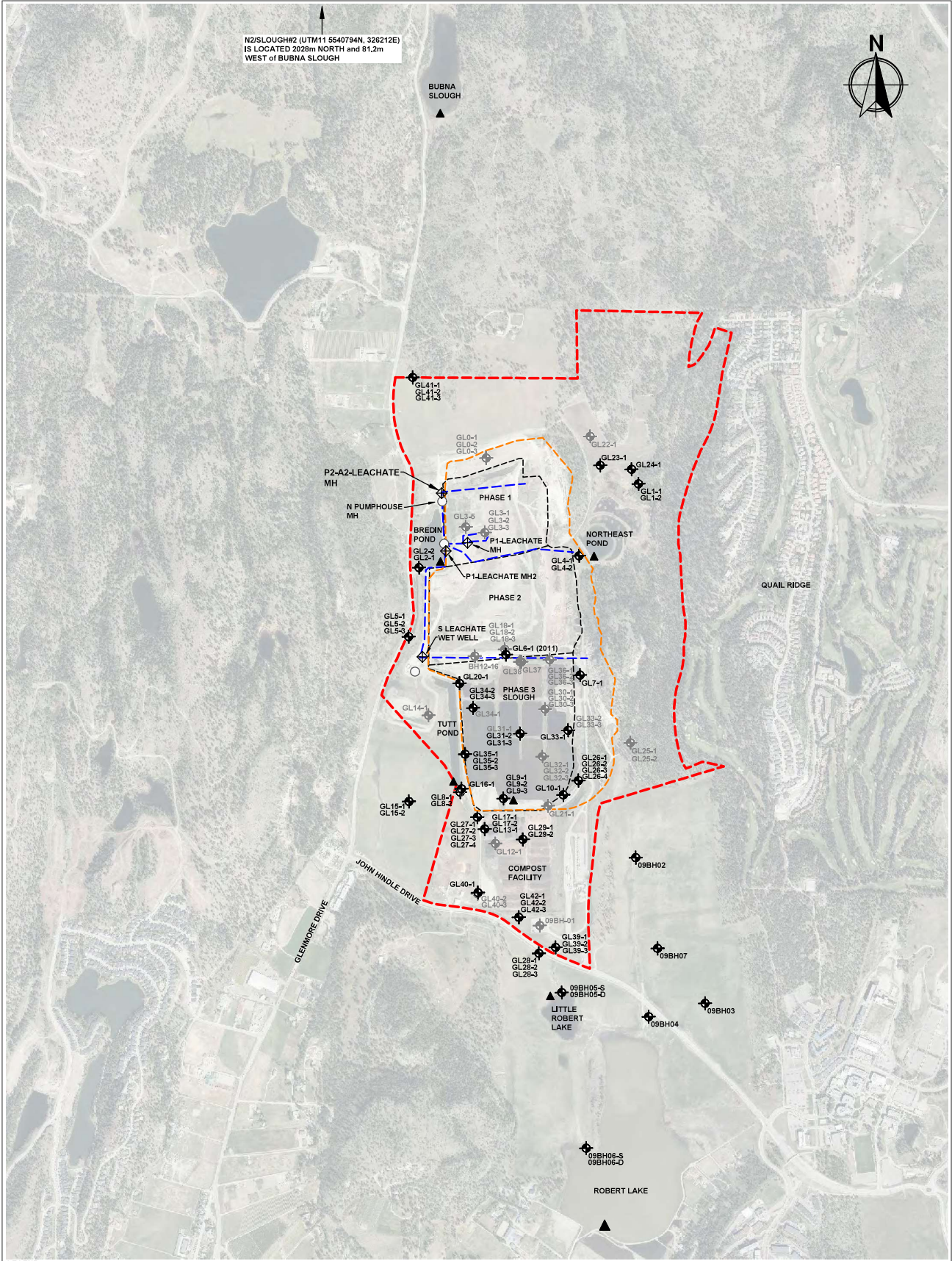
GL 18-1 -dash

GL 26-1 (bedrock/clay)

GL 26-4

GL 27-1

GL 29-1 bedrock/silt/sand

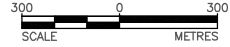


N2/SLOUGH#2 (UTM11 5640794N, 326212E)  
IS LOCATED 2028m NORTH and 81.2m  
WEST of BUBNA SLOUGH



**LEGEND**

- APPROXIMATE SITE BOUNDARY (REPORTING ONLY)
- APPROXIMATE EXTENTS OF LANDFILL (BASED ON ACTIVE AND/OR HISTORICAL LANDFILLING ACTIVITIES)
- LEACHATE COLLECTION SYSTEM
- LIMITS OF FOOTPRINT
- MONITORING WELL LOCATION
- MONITORING WELL (DECOMMISSIONED)
- APPROXIMATE MANHOLE LOCATION
- APPROXIMATE LEACHATE SAMPLING LOCATION
- APPROXIMATE SURFACE WATER SAMPLING LOCATION



PROJECT 2022 ANNUAL WATER MONITORING REPORT FOR GLENMORE LANDFILL 2720 JOHN HINDLE DRIVE, KELOWNA, BC			
TITLE SITE PLAN			
CLIENT CITY OF KELOWNA			
CONSULTANT	PROJECT No.	FIGURE	
	2022-059	<b>2</b>	
	REVISION		00
	DATE		03-03-2023
CADD	AR		
CHECK	GCS		

**REFERENCES**

- 1.) COORDINATE REFERENCE: UTM ZONE 11n, NAD83
- 2.) MAP REFERENCES: KELOWNA ONLINE MAPPING SERVICE

GL 0-1

SLR

MISSING  
GL 19-1, 19-2  
GL 19-3

Kelowna, BC

**BOREHOLE LOG**

BOREHOLE NO: **BH12-1A**

SURFACE ELEVATION: 449.04 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
					ORGANIC VAPOUR LEVEL (ppmv)								
					1	10	100	1000	10000				
0					Ground Surface								449
0 - 1		BH12-1A-1		sandy SILT medium sand, some clay, firm, brown, dry									448
1 - 3				silty LEAN CLAY trace to some fine sand, medium plasticity, firm, brown, moist									446
3 - 4				- gypsum crystals in sand laminations at 3.7 and 4.3 m									445
4 - 5		BH12-1A-2											444
5 - 6				SAND AND GRAVEL some clay, some silt, compact, brown, moist - some cobbly green/white granite at 5.3 m									443
6 - 7													442
7 - 8		BH12-1A-3											441
8 - 9													440
9 - 10													439
10 - 11		BH12-1A-4		SAND medium, trace gravel, trace fines, loose, brown, moist									438
11 - 12				sandy CLAY (till) some silt, some gravel, firm, brown, moist									437
12 - 13				- grey, dry at 13.1									436
13 - 14		BH12-1A-5		- coarse fraction increasing, very hard at 13.7 m - cobbles encountered at 14 m									435
14 - 15				- wet between 15.2 and 15.8 m									434
15 - 16													433
16 - 17		BH12-1A-6		- fractured green rock between 16.2 and 19.5 m									432
17 - 18				- moist at 19.5 m									431

GW = 6.32 mbg  
(October 3, 2012)

bentonite chips to 18.9 m

stickup, jplug

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/14/13

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: September 25, 2011 LOGGED BY: JN  
DRILLER NAME: Mud Bay

GLO-1

SLR		CLIENT: City of Kelowna PROJECT: Glenmore Landfill ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG											
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH12-1A SURFACE ELEVATION: 449.04 m											
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)		
						ORGANIC VAPOUR LEVEL (ppmv)										
						1	10	100	1000	10000						
20		BH12-1A-7														
21																
22																
23		BH12-1A-8			<b>BEROCK</b> orange rusty colour on rock fragments, some volcanic ash, dense, light green, dry											
					End of borehole at 23.2 m											
					Well Completion Details: Screened interval from 20.1 m to 23.2 m below surface Elevation at top of casing (TOC) = 449.991 m											
					Groundwater Information: Depth to groundwater from TOC = 7.27 m (October 3, 2012)											
					(1) - Water added during drilling from surface to 23.2 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste											
					GSA %: BH12-1A-1: 13.9 Gravel, 23.8 Sand, 23.6 Silt, 38.6 Clay BH12-1A-2: <0.10 Gravel, 2.59 Sand, 17.5 Silt, 79.9 Clay BH 12-1A-3: 36.3 Gravel, 25.6 Sand, 30.3 Silt, 7.79 Clay BH 12-1A-4: 21.5 Gravel, 69.3 Sand, 5.01 Silt, 4.24 Clay											

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/14/13



RL 0-2



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-1B**  
 SURFACE ELEVATION: **448.95 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)	
						ORGANIC VAPOUR LEVEL (ppmv)									
						1	10	100	1000	10000					
0					Ground Surface									stickup, jplug	449
0.5		BH12-1B-1			<b>sandy SILT</b> fine to medium sand, some clay, hard, brown, dry										448
2.4					- dark brown to black organic layer from 2.4 to 2.7 m										
3.0					<b>silty LEAN CLAY</b> trace fine sand, medium plasticity, laminated, firm to hard, brown, dry										446
4.0		BH12-1B-2													445
6.0					<b>SAND AND GRAVEL</b> medium to coarse sand, some silt, loose, brown, dry to moist										443
6.4					- gypsum crystals at 6.4 m										
7.0					- coarse fraction increasing at 7.0 m										
7.5					- cobbles, very dense, grey at 7.5 m										
8.2					- increasing silt from 8.2 to 8.5 m										
8.8					- silty, soft, grey from 8.8 to 9.1 m										
9.4					- dry, grey from 9.4 and 10.1 m										
10.0		BH12-1B-4													439
11.9					- increased fine sand, moist to wet from 11.9 to 12.5 m										
12.5															
14.0		BH12-1B-5			<b>sandy SILT</b> fine to medium sand with 2 mm seams fine sand, trace to some clay, firm to hard, dark grey, dry to moist										435
14.2					<b>sandy CLAY</b> some silt, some gravel, occasional cobble, very dense (suspect TILL), dark grey, moist - 4 cm sand seams at 14.2 m - granite cobbles at 14.3 m										434
14.3		BH12-1B-6													433
16.0					<b>SAND AND SILT</b> some clay, trace gravel, compact, grey, moist to wet										432
17.1		BH12-1B-7			End of borehole at 17.1 m										
Well Completion Details: Screened interval from 14.0 m to 17.1 m below surface Elevation at top of casing (TOC) = 449.945 m															

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/14/13

DRILLING METHOD: Core Sample  
 DRILL DATE: September 25, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

Notes:  SONIC CORE SAMPLE

FL 0-2



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-1B**  
 SURFACE ELEVATION: **448.95 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
					Groundwater Information: Depth to groundwater from TOC = 9.01 m (October 3, 2012)  (1) - Water added during drilling from surface to 17.1 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste  GSA %: BH12-B-6: 9.7 Gravel, 38.9 Sand, 37.8 Silt, 13.6 Clay									

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/14/13

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: September 25, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

GL0-3

SLR		CLIENT: City of Kelowna PROJECT: Glenmore Landfill ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR CONSULTING (CANADA) LTD. SLR JOB NO: 219.05164			BOREHOLE LOG											
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH12-1C SURFACE ELEVATION: 449.32 m											
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)		
						ORGANIC VAPOUR LEVEL (ppmv)										
						1	10	100	1000	10000						
0					Ground Surface										450	
0					<b>sandy SILT</b> medium sand, some clay, firm to hard, brown, dry										449	
1															448	
2															447	
3					- organic layer between 2.4 and 2.7 m										446	
3					<b>silty CLAY</b> trace fine grained sand, medium plasticity, laminations, very firm to hard, brown, moist										445	
4															444	
5															443	
6					<b>SAND AND GRAVEL</b> trace to some some silt, loose, brown, moist										442	
7															441	
8															440	
9															439	
10					<b>SAND</b> fine to coarse, trace gravel, trace silt, loose, brown, moist to wet										438	
11					- medium to coarse from 10.4 m										437	
12					- layer gravel from 11 to 11.3 m; gravel increasing with depth										437	
					End of borehole at 12.5 m											
					Well Completion Details: Screened interval from 9.5 m to 12.5 m below surface Elevation at top of casing (TOC) = 450.531 m											
					Groundwater Information: Depth to groundwater from TOC = 9.66 m (October 3, 2012)											
					(1) - Water added during drilling from surface to 12.5 m											
					GSA - grain size analysis											
					M - moisture content											
					Att - Atterberg limits											
					MSW - Municipal solid waste											
DRILLING METHOD: Core Sample					Notes:											
DRILL DATE: September 25, 2012					LOGGED BY: JN DRILLER NAME: Mud Bay											

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/14/13





# BOREHOLE NO. GL2-1

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 28/11/90  
 BOREHOLE TYPE 0.20 m Hollow Stem Auger with 0.05 m GEOLOGIST SBS  
 GROUND ELEVATION 98.47 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS /0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	Wp
0.76	GREENISH BROWN CLAY TOPSOIL			1	SS	8				
	FILL MATERIAL			2	SS	7				
				3	SS	7				
2.3				4	SS	17				
	GREENISH GREY SILT CLAY with grey weathered, vertical microfractures and varved silt layers			5	SS	16				
				6	SS	-				-grain size -no blow-count
				7	SS	10				
5				8	SS	8				
6.1				9	SS	5				
	GREY SILT CLAY with varved silt layers			10	SS	2				-grain size
				11	SS	-				-spoon sank under own weight
8.5				12	SS	6				
	GREY SILTY FINE SAND			13	SS	4				-grain size
10				14	SS	-				-spoon sank under own weight
	GREY SILT CLAY with varved silt layers			15	SS	-				
10.7		EOH	GL 2-2 GL 2-1							
15										
20										

# BOREHOLE NO. GL3-1 *decsm*

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 28/11/90  
 BOREHOLE TYPE 0.15 m Steel Casing with Air Rotary Rig GEOLOGIST SBS  
 GROUND ELEVATION 98.90 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS/0.3m	WATER CONTENT %		
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	Wp	Wl
5	GREY CLAY			1	C						
				2	C						
				3	C						
10	5.2 VARVED CLAYEY SILT			4	C						
				5	C						
				6	C						
				7	C						
				8	C						
				9	C						
				10	C						
				11	C						
				12	C						
				13	C						
20	17.5 GRAVEL										
25	24.5 GREY CLAY with some gravel										

**BOREHOLE NO.** GL3-1 *delcom*

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 28/11/90  
 BOREHOLE TYPE 0.15 m Steel Casing with Air Rotary Rig GEOLOGIST SBS  
 GROUND ELEVATION 98.90 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS/0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	Wp
30	GREY CLAY with some gravel 25.9									
	GREY GRAVEL with some clay 27.4			14	C					
	GREY CLAYEY SILT with some gravel			15	C					
35	34.7 GREY SILTY GRAVEL			16	C					
	36.6 GREY SILT CLAY			17	C					
	39.5 GREY CLAY with some sand			18	C					
40	41.5 GREY CLAY GRAVEL			19	C					
	43.0 DARK GREY VOLCANIC BEDROCK			20	C					
	46.9 EOH			21	C					
45				22	C					
				23	C					
				24	C					
50										



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-1 (Decom)**  
 SURFACE ELEVATION: **454.70 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)			
							Laboratory Analyses								
1						Monitoring well decommissioned May 27, 2011			[Hatched pattern]		concrete to 0.9 m	454			
2															453
3															452
4															451
5															450
6															449
7															448
8															447
9															446
10															445
11															444
12															443
13															442
14															441
15															440
16															439
17															438
18															437
19															436
												435			

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Core Sample**  
 DRILL DATE: **May 27, 2011**  
 LOGGED BY: **JN**  
 DRILLER NAME: **Beck**

Notes:





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-1 (Decom)**  
 SURFACE ELEVATION: **454.70 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses				
21										434
22									grout from 0.9 to 42.7 m	433
23										432
24										431
25										430
26										429
27										428
28										427
29										426
30										425
31										424
32										423
33										422
34										421
35										420
36										419
37										418
38										417
39										416
										415

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 27, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-1 (Decom)**

SURFACE ELEVATION: 454.70 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
41											414
42											413
					End of borehole at 42.7 m						412
					GL3-1 was a 150 mm diameter steel water well. Decommissioning was completed by grouting the inside of the well, as it could not be drilled out.						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 27, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:

**BOREHOLE NO.** GL3-2 *GL3-2*

**PROJECT NAME** GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
**CLIENT** CITY OF KELOWNA **DATE** 28/11/90  
**BOREHOLE TYPE** 0.20 m Hollow Stem Auger with 0.05 m split spoon **GEOLOGIST** SBS  
**GROUND ELEVATION** 98.91 m.a.s.l. **PROJECT NO.** 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS /0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		WP	WL
	SILTY CLAY TOPSOIL			1		11				
	0.76			2		19				
	FILL MATERIAL			3		10				
				4		14				
	3.2			5		16				
	GREENISH BROWN SILT CLAY with grey weathered microfractures			6		11				
				7		8				
5	5.3			8		-			-spoon sank under own weight	
	GREY CLAY			9		2				
				10		-				
				11		-			-spoon sank under own weight	
	8.5			12		3			-grain size	
	9.1 GREY SILT CLAY with some sand			13		-				
10	GREY SANDY SILT			14		-			-spoon sank under own weight	
				15		22			-spoon sank under own weight	
				16		28				
	12.2			17		11			-grain size	
	GREY SILTY CLAY			18		2				
				19		-			-spoon sank under own weight	
15				20		4				
				21		3				
				22		1				
	16.8			23		25				
	GREY SILTY MEDIUM SAND			24		99				
	18.0			25		73+			-grain size	
	GREY SILT TILL with some gravel			26		90+				
20	19.1	EOH								
			GL 3-3							
			GL 3-2							



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-2/GL3-3 (Decom)**  
 SURFACE ELEVATION:

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)		
							Laboratory Analyses							
1						Monitoring well decommissioned August 25 and 26, 2011					concrete to 0.3 m	1.0		
2														2.0
3														3.0
4														4.0
5														5.0
6														6.0
7														7.0
8														8.0
9														9.0
10														10.0
11														11.0
12														12.0
13														13.0
14														14.0
15													grout from 0.3 to 30.2 m	15.0
16														16.0
17														17.0
18														18.0
19														19.0

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Mud Rotary Drilling** Notes:

DRILL DATE: **August 26, 2011** LOGGED BY: **EM**  
 DRILLER NAME: **Beck**

Sheet 1 of 2





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-2/GL3-3 (Decom)**  
 SURFACE ELEVATION:

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)
						Laboratory Analyses					
21											21.0
22											22.0
23											23.0
24											24.0
25											25.0
26											26.0
27											27.0
28											28.0
29											29.0
30											30.0
					End of borehole at 30.2 m						
					Wells GL3-2 and GL3-3 were housed within one steel monument that was too long to be pulled out completely. Approximately 5 m of the monument were pulled out when it broke off. The overlying 5 m of MSW and fill were excavated to provide access for the drill rig. Mud rotary drilling technology was used to drill down inside the monument to decommission the wells.						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Mud Rotary Drilling**  
 DRILL DATE: **August 26, 2011**  
 LOGGED BY: **EM**  
 DRILLER NAME: **Beck**

Notes:

GL 3-2

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GL 3-2 (2005)

SHEET 1 OF 2

LOCATION: See Figure 1

BORING DATE: Mar 2 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION  GL 3-2(2005)	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH Cu, kPa				WATER CONTENT PERCENT					
								20	40	60	80	nat V. + rem V. ⊕	Q - ● U - ○	10 <sup>-5</sup>			10 <sup>-5</sup>
0		GROUND SURFACE		0.00													
2																Filler sand	
4																Bentonite seal	
8		LANDFILL REFUSE (Paper, plastic, wood etc. and soil) (FILL)															
10																	
12																	
16				15.85												Grout and bentonite	
18		Refer to Gartner Lee Soil Stratigraphy (GL 3-2) Nov 28, 1990															
20																	

CONTINUED NEXT PAGE

BOREHOLE BOREHOLES.GPJ\_GLDR\_CAN.GDT 10/1/06

DEPTH SCALE

1 : 100



LOGGED: RR

CHECKED: GTI

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GL 3-2 (2005)

SHEET 2 OF 2

LOCATION: See Figure 1

BORING DATE: Mar 2 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION  GL 3-2(2005)	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20 40 60 80		10 <sup>-6</sup> 10 <sup>-5</sup> 10 <sup>-4</sup> 10 <sup>-3</sup>		nat V. + Q - ●		rem V. ⊕ U - ○			W <sub>p</sub>  -----  W  -----  W <sub>L</sub>
20	Foundex Explorations Bomaster Simco 2800 120 mm dia. Mud Rotary	Refer to Gartner Lee Soil Stratigraphy (GL 3-2) Nov 28, 1990 (continued)	[Strata Plot]	27.43											Grout and bentonite		
22																50 mm dia. PVC Screen	
24																	Filter sand
26	Bentonite seal																
28		Filter sand															
30			End of BOREHOLE.														
32	30.78																
34																	
36																	
38																	
40																	

BOREHOLE BOREHOLES.GPJ\_GLDR\_CAN.GDT 10/1/06

DEPTH SCALE  
1 : 100



LOGGED: RR  
CHECKED: GTI



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-2 (2005) (Decom)**  
 SURFACE ELEVATION:

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)	
							Laboratory Analyses						
1						Monitoring well decommissioned May 27, 2011					concrete to 0.9 m	1.0	
2													2.0
3													3.0
4													4.0
5													5.0
6													6.0
7													7.0
8													8.0
9													9.0
10													10.0
11													11.0
12													12.0
13													13.0
14												grout from 0.9 to 27.4 m	14.0
15													15.0
16													16.0
17													17.0
18													18.0
19													19.0

DRILLING METHOD: Core Sample

Notes:

DRILL DATE: May 27, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-2 (2005) (Decom)**  
 SURFACE ELEVATION:

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)
						Laboratory Analyses					
21											21.0
22											22.0
23											23.0
24											24.0
25											25.0
26											26.0
27											27.0
					End of borehole at 27.4 m						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Core Sample**  
 DRILL DATE: **May 27, 2011**  
 LOGGED BY: **JN**  
 DRILLER NAME: **Beck**

Notes:



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-4 (Decom)**  
 SURFACE ELEVATION: **454.21 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
						Monitoring well decommissioned May 28, 2011				concrete to 0.9 m	454
1											453
2											452
3											451
4											450
5											449
6											448
7											447
8										grout from 0.9 to 14.6 m	446
9											445
10											444
11											443
12											442
13											441
14											440
15											439
16											438
17											437
18											436
19											435

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Core Sample**  
 DRILL DATE: **May 28, 2011**  
 LOGGED BY: **JN**  
 DRILLER NAME: **Beck**

Notes:



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL3-4 (Decom)**  
 SURFACE ELEVATION: **454.21 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
21											434
22											433
23											432
24											431
25											430
26											429
27											428
28											427
29											426
30											425
31											424
32											423
33											422
34											421
35											420
36											419
					End of borehole at 36.6 m						418

bentonite from  
14.6 m to 36.6 m

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 28, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:





GL3-5  
(2012)



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-14**

SURFACE ELEVATION: 456.83 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
20		BH12-14-1			CLAY with SILT AND SAND (native) firm, laminations, brown, moist								bentonite pellets to 21 m	437
21		BH12-14-2			SAND AND GRAVEL some silt, trace clay, loose to compact, dark grey, wet - organics throughout (small sticks, trace wood chips)								silica sand	436
22					- wood chips at 22.1 m silty CLAY with SAND laminations, high plasticity, firm, brown, moist									435
23					End of borehole at 23.2 m									434
<p>Well Completion Details:          Screened interval from 21.6 m to 23.2 m below surface          Elevation at top of casing (TOC) = 457.981 m</p> <p>(1) - Water added during drilling from surface to 23.2 m          GSA - grain size analysis          M - moisture content          Att - Atterberg limits          MSW - Municipal solid waste</p> <p>GSA %:          BH12-14-1: 1.5 Gravel, 4.1 Sand, 21.5 Silt, 72.9 Clay          BH12-14-2: 6.4 Gravel, 38.5 Sand, 34.3 Silt, 20.7 Clay</p>														

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/14/13

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: September 28, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

**BOREHOLE NO.** GL4-1

**PROJECT NAME** GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION

**CLIENT** CITY OF KELOWNA **DATE** 28/11/90

**BOREHOLE TYPE** 0.20 m Hollow Stem Auger with 0.05 m Split Spoon **GEOLOGIST** SBS

**GROUND ELEVATION** 100.56 m.a.s.l. **PROJECT NO.** 90-732

DEPTH	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS /0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	Wp
44.7										
440.6	RAINAGE TILE @ DAM									
0.8 mb TPC										
3.8	GREENISH BROWN SILT CLAY with grey weathered microfractures		439.8	1	SS	13				
				2	SS	9				
				3	SS	13				
				4	SS	15				
				5	SS	14				-grain size
5	GREENISH BROWN CLAY with grey weathered microfractures		435.8	6	SS	6				
				7	SS	5				
6.7				8	SS	-				
				9	SS	-				-spoon sank under own weight
	GREY MEDIUM SAND		437.4	10	SS	-				-grain size
8.4				11	SS	23				
	GREY GRAVELLY SILT TILL with some sand and pebbles		432.4	12	SS	60+				
				13		55+				
10				14	SS	58+				
				15	SS	88+				-grain size
	EOH									
15	EOH 4-1 - 9.6m 4-2 5.9m		GL4-2 GL4-1							
20										







Decom

**BOREHOLE NO.** GL6-1

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 11/28/90  
 BOREHOLE TYPE 0.20 m Hollow Stem Auger with 0.05 m Split Spcon GEOLOGIST SBS  
 GROUND ELEVATION 100.81 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS /0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	Wp
0 - 8.5	FILL MATERIAL		▽							
8.5 - 10.7	GREY SILTY CLAY				1					
10.7 - 15		EOH	GL6-1						grain size spoon sank under own weight	



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL6-1 (Decom)**  
 SURFACE ELEVATION: **442.20 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1										concrete to 0.9 m	442
2											441
3											440
4											439
5											438
6										grout from 0.9 to 8.8 m	437
7											436
8											435
9											434
10											433
11										bentonite from 8.8 m to 11.4 m	432
											431
End of borehole at 11.4 m											

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL\_GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Core Sample**  
 DRILL DATE: **May 28, 2011**  
 LOGGED BY: **JN**  
 DRILLER NAME: **Beck**

Notes:



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL6-1 (2011)**

SURFACE ELEVATION: 439.66 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	440
1			1 40	CLAY	some silt, some sand, some gravel, trace organic matter (roots, grass, wood debris), trace garbage (plastic), soft, laminated, brown, moist					bentonite seal	439
2				Interbedded CLAY AND GARBAGE (MSW)	Clay is firm, laminated, odour, grey, moist					GW = 1.83 mbg (June 15, 2011)	438
3					- black from 3.3 to 3.6 m - Garbage (foam, wood, plastic) from 3.3 to 4.0 m					silica sand	437
4			2 100		- 5 cm thick medium sand lens at 4.6 m						436
5				FAT CLAY (reworked soil, fill)	firm, laminated, brown, moist - gypsum crystals from 4.9 to 6.7 m						435
6											434
7			3 100	LEAN CLAY (native)	soft to very soft, grey, moist - wet from 7.6 to 8.5 m						433
8					- 5 cm thick medium sand lens at 8.4 m End of borehole at 8.5 m						432

Well Completion Details:  
 Screened interval from 1.8 m to 4.9 m below surface  
 Elevation at top of casing (TOC) = 440.521 m

Groundwater Information:  
 Depth to groundwater from TOC = 2.69 m (June 15, 2011)

(1) - Water added during drilling from surface to 8.5 m

GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

SLR CANADA V5.2. 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

DRILL DATE: May 27, 2011

LOGGED BY: JN

DRILLER NAME: Beck

Notes:

**BOREHOLE NO.** BH7-1

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 28/11/90  
 BOREHOLE TYPE 0.15 m Steel Casing with Air Rotary GEOLOGIST SBS  
 GROUND ELEVATION 98.96 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS /0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	
	FILL MATERIAL FROM BORROW									
1.2	LIGHT BROWN/GREY WEATHERED BEDROCK		GL7-1	1	C					
3.0	LIGHT GREY/GREEN FRACTURED BEDROCK		GL7-1	2	C					
5			GL7-1	3	C					
6.1		EOH	GL7-1	4	C					
10										
15										





**BOREHOLE NO. GL8-2**

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 28/11/90  
 BOREHOLE TYPE 0.20 m Hollow Stem Auger with 0.05 m Split Spoon GEOLOGIST SBS  
 GROUND ELEVATION 98.89 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION *	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS/0.3m	WATER CONTENT	
				NO.	TYPE	'N' VALUE	% WATER		%	COMMENT
1.0	LIGHT GREY CLAY		S 							
1.6	DARK BROWN CLAY									
	GREENISH GREY CLAY									
5.6	GREY MEDIUM SAND with some gravel									
9.9	BEDROCK?	EOH								
15										
20										

\* taken from GL 8-1

**BOREHOLE NO.** GL9-1

**PROJECT NAME** GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
**CLIENT** CITY OF KELOWNA **DATE** 11/28/90  
**BOREHOLE TYPE** 0.15 m Steel Casing with Air Rotary **GEOLOGIST** SBS  
**GROUND ELEVATION** 98.74 m.a.s.l. **PROJECT NO.** 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS/0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	WP
5	BROWNISH GREY CLAY		▽							
	5.2			1	C					
				2	C					
10	GRAVEL with some coarse sand and silt				3	C				
	9.1			4	C					
				5	C					
15	GREY SILT TILL with some sand and gravel				6	C				
				7	C					
				8	C					
				9	C					
				10	C					
				11	C					
				12	C					
				13	C					
				14	C					
				15	C					
			16	C						
20										
25										

## BOREHOLE NO. GL9-1

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 11/28/90  
 BOREHOLE TYPE 0.15.m Steel Casing with Air Rotary Rig GEOLOGIST SBS  
 GROUND ELEVATION 98.74 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS/0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	Wp
30	GREY SILT TILL with some sand and gravel		GL9-1	17	C					
	28.7			18	C					
	GRAVEL AND COARSE SAND with some weathered bedrock			19	C					
	30.5			20	C					
	WEATHERED BEDROCK			21	C					
35	33.2									
	GREEN/GREY SOFT BEDROCK									
40										
45										





# BOREHOLE NO. GL9-3

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 28/11/90  
 BOREHOLE TYPE 0.20 m Hollow Stem Auger with 0.05 m Split Spoon GEOLOGIST SBS  
 GROUND ELEVATION 98.73 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS /0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	WP
5	no samples taken above 20' 6.1 (see GL9-2)		V							
	6.9 POORLY SORTED SAND with trace gravel			1	SS	43				
	DARK GREY GRAVELLY SILT TILL			2	SS	76				
	8.4 FINE SILTY SAND			3	SS	60+				-grain size
	8.7 DARK GREY GRAVELLY SILT TILL with occasional silty sand lenses			4	SS	127				-grain size
10				5	SS	60+				
				6	SS	90+				
				7	SS	60+				
				8	SS	83				
	12.2	EOH								
15			GL9-3							
20										

# BOREHOLE NO. GL10-1

PROJECT NAME GLENMORE LANDFILL HYDROGEOLOGICAL INVESTIGATION  
 CLIENT CITY OF KELOWNA DATE 28/11/90  
 BOREHOLE TYPE 0.20 Hollow Stem Auger with 2" Split Spoon GEOLOGIST SBS  
 GROUND ELEVATION 98.42 m.a.s.l. PROJECT NO. 90-732

DEPTH (m)	STRATIGRAPHIC DESCRIPTION	STRATIGRAPHY	MONITOR DETAILS AND NUMBER	SAMPLE				PENETRATION RESISTANCE BLOWS /0.3m	WATER CONTENT %	
				NO.	TYPE	'N' VALUE	% WATER		COMMENT	
								Wp	WL	
	GREEN/BROWN CLAY		12	1	SS	22				
				2	SS	18				
				3	SS	6				
3.0				4	SS	7				
	GREEN/BROWN SILT with some sand and gravel			5	SS	31				
5				6	SS	41				
5.3				7	SS	28				
	GREY SILTY CLAY with some sand and gravel			8	SS	55				
				9	SS	43				
				10	SS	55				
8.4				11	SS	60				
	GREY SILTY CLAY TILL with some sand and gravel		GL10-1	12	SS	66+				
10										
15										
20										

\*decommissioned in 2007

<b>BOREHOLE LOG</b>	<b>PROJECT:</b> 98-771	<b>BOREHOLE:</b> GL11-1 1 of 1
Monitoring Well Installation Glenmore Landfill <b>FOR:</b> City of Kelowna		<b>DATE:</b> 5 November 1998 <b>GEOLOGIST:</b> RCD <b>ELEVATION:</b> 445.6 m ASL

DEPTH (m)	STRATIGRAPHY	STRATIGRAPHIC DESCRIPTION	MONITOR DETAILS & NUMBER	SAMPLE					COMMENTS		
				NUMBER	INTERVAL	TYPE	N VALUE	% WATER		% REC	% RQD
0.3		Dark brown, Silty TOPSOIL with organics.									
1		Brown, Silty CLAY, Laminated, DTPL to APL, very stiff.			SS		20				Grain size analysis.
2.5					SS		30				
3		Greenish brown, Silty SAND TILL with gravel and some clay. Very stiff to dense. APL to WTPL.			SS		30				
4					SS		30				
5					SS		48				
6		Slow and difficult drilling at 6 m.			SS		41				
7					SS		34				Grain size analysis.
8					SS		31				
9					SS		25				
10					SS		30				
11		Slow and difficult drilling at 11 m.			SS		22				Grain size analysis.
12											
13											
14											
15.2		Borehole completed at 15.2 m in silty SAND TILL, monitor dry on completion. NOTES: 1. Borehole advanced using hollow stem auger drilling equipment. 2. Monitor construction: Schedule 40 PVC standpipe (51mm dia.) with 1.5 m slotted (#10 size) screen. Waterra standard flow tubing and foot-valve installed. 3. Surface completed with concrete seal. 4. Monitor provided with lockable protective steel housing. 5. Ground water not present, monitor dry, 6 Nov 98. 6. PVC monitor stick-up above grade 0.20 m.									



<b>BOREHOLE LOG</b>	<b>PROJECT:</b> 98-771	<b>BOREHOLE:</b> GL12-1 1 of 1
Monitoring Well Installation Glenmore Landfill <b>FOR:</b> City of Kelowna	<b>DATE:</b> 6 November 1998 <b>GEOLOGIST</b> RCD <b>ELEVATION</b> 442.0 m ASL	

DEPTH (m)	STRATIGRAPHY	STRATIGRAPHIC DESCRIPTION	MONITOR DETAILS & NUMBER	SAMPLE						COMMENTS	
				NUMBER	INTERVAL	TYPE	N VALUE	% WATER	% REC		% RQD
0.3		Dark brown. Silty TOPSOIL with organics.									
1		Brown. Silty CLAY. Laminated. APL.									
1.8		Greenish brown. Silty SAND Till with gravel. Very dense. Moist.									Grain size analysis.
2		Gravel content increasing and colour change to reddish brown and black.									
3											
4											
5		Thin grey clay layer within till, saturated.									Grain size analysis.
6		Till colour becomes dark grey. WTPL.									
7											
8											
9.1		Borehole completed at 9.1 m in silty SAND TILL.									Grain size analysis.
9		NOTES: 1. Borehole advanced using hollow stem auger drilling equipment. 2. Monitor construction: Schedule 40 PVC standpipe (51mm dia.) with 1.5 m slotted (#10 size) screen. Waterra standard flow tubing and foot-valve installed. 3. Surface completed with concrete seal. 4. Monitor provided with lockable protective steel housing. 5. Water level measured on 6 Nov 98 at 3.68 m depth (from top of PVC pipe). 6. PVC monitor stick-up above grade 0.18m.									

<b>BOREHOLE LOG</b>	<b>PROJECT:</b> 98-771	<b>BOREHOLE:</b> GL13-1 1 of 1
Monitoring Well Installation Glenmore Landfill <b>FOR:</b> City of Kelowna		<b>DATE:</b> 5 November 1998 <b>GEOLOGIST:</b> RCD <b>ELEVATION:</b> 438.6 m ASL

DEPTH (m)	STRATIGRAPHY	STRATIGRAPHIC DESCRIPTION	MONITOR DETAILS & NUMBER	SAMPLE						COMMENTS	
				NUMBER	INTERVAL	TYPE	N VALUE	% WATER	% REC		% RQD
0.3		Dark brown. Silty TOPSOIL with organics.									
1		Brown. CLAY. Increasing pebble content with depth. Rootlets present in upper 2 m, possibly fill. Past infilling of area reported by farmer.									
2					SS	11					Grain size analysis.
3					SS	5					
4					SS	11					
4.6				SS	10						
5		Brown. Silty SAND TILL with gravel. Wet, very dense, possible sand and gravel layers. Poor sample recovery due to gravel content.									
6					SS	8					Grain size analysis.
7		Weathered rock at 7.6 m.									
7.9					SS	>30					Grain size analysis.
		Refusal on cobble or bedrock at 7.9 m. Pink granite-like rock fragments in split spoon. NOTES: 1. Borehole advanced using hollow stem auger drilling equipment. 2. Monitor construction: Schedule 40 PVC standpipe (51mm dia.) with 1.5 m slotted (#10 size) screen, Waterra standard flow tubing and foot-valve installed. 3. Surface completed with concrete seal. 4. Monitor provided with lockable protective steel housing. 5. Water level measured on 6 Nov 98 at 1.65 m depth (from top of PVC pipe). 6. PVC monitor stick-up above grade 0.17m.									

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 14-1

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Feb 22 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION  GA 14-1	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. + rem V. $\oplus$ $\ominus$		Wp		W			
0		GROUND SURFACE		453.10													
		Loose dark brown organic SILT, some clay.		452.85												Steel Well Protector in Concrete	
				0.25	1	DO	N/R										
2		Very dense grey brown SILT, some sand, trace to some gravel. (GLACIAL TILL)			2	DO	>100										
4				449.29													
				3.81		DO	>100										
6		Very dense light grey silty GRAVEL, trace sand grading to very dense light grey GRAVEL, some silt, trace sand. (WEATHERED BEDROCK)				DO	>100										
8				444.87		DO	>100									Grout and bentonite	
		Bedrock Encountered. Refer to ROCK LOG for continuation of rock description.														Screen?	

BOREHOLE BOREHOLES.GPJ GLDR CAN.GDT 10/1/06

DEPTH SCALE  
1 : 100



LOGGED: RR  
CHECKED: GTI

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 15-1

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Feb 23,24 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GA 15-1</b>	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20 40 60 80		nat V. + Q - rem V. ⊕ U - ⊙		10 <sup>-5</sup> 10 <sup>-5</sup> 10 <sup>-4</sup> 10 <sup>-3</sup>		Wp   W			
0		GROUND SURFACE		451.77													
		Loose dark brown organic SILT, some clay with roots at the surface.		0.16												Steel Well Protector in Concrete	
		Firm grey brown CLAY, some silt occasional root fibres grading to clayey SILT.			1	DO	6										
2				449.33													
		Loose light brown SILT, trace fine sand.		2.44	2	DO	6										
				448.87													
				2.90													
		Compact brown gravelly SAND, some silt with cobbles.			3	DO	20										
4				447.19													
				4.57													
		Dense to very dense brown sandy SILT and GRAVEL with cobbles. (GLACIAL TILL)			4	DO	>100										
6				444.68													
				7.09													
		Very dense grey brown SILT, some gravel, trace sand. (GLACIAL TILL)			6	DO	>100										
8				441.88													
				9.91													
		Very dense light grey silty GRAVEL, trace sand. (WEATHERED BEDROCK)				DO	>100										
12				439.57													
		Bedrock Encountered. Refer to ROCK LOG for continuation of rock description.														Grout and bentonite	
14																	
16																	
18																	
20																	

BOREHOLE BOREHOLES.GPJ GLDR\_CAN.GDT 10/1/06

DEPTH SCALE  
1 : 100



LOGGED: RR  
CHECKED: GTI



PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 15-2

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Feb 23,24 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH Cu, kPa				WATER CONTENT PERCENT					
								20	40	60	80	nat V. + rem V. ⊕	Q - U - ⊙	10 <sup>-6</sup>			10 <sup>-5</sup>
0		GROUND SURFACE		451.48													
		Loose dark brown organic SILT, some clay with roots at the surface.		0.15												Steel Well Protector in Concrete	
		Firm grey brown CLAY, some silt occasional root fibres grading to clayey SILT.			1	DO	6									Bentonite seal	
		Loose light brown SILT, trace fine sand.		449.04													
				2.44	2	DO	6										
				448.58													
				2.90													
		Compact brown gravelly SAND, some silt with cobbles.			3	DO	20									5/04/05	
				446.91												50 mm dia. PVC Screen	
				4.57													
		Dense to very dense brown sandy SILT and GRAVEL with cobbles. (GLACIAL TILL)			4	DO	>100										
				445.38													
6		End of BOREHOLE.		6.10													

BOREHOLE BOREHOLES.GPJ GLDR\_CAN.GDT 10/1/06

DEPTH SCALE

1 : 100



LOGGED: RR

CHECKED: GTI

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 16-1

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Feb 24, 25 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION  GA 16-1	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20 40 60 80		nat V. + Q - rem V. ⊕ U - ⊙		10 <sup>-6</sup> 10 <sup>-5</sup> 10 <sup>-4</sup> 10 <sup>-3</sup>		Wp         W         Wp			
0		GROUND SURFACE		438.78													
		Loose to compact SILT, CLAY and SAND with miscellaneous debris. (FILL)		0.15	1	DO	6									Steel Well Protective Concrete	
2		Firm grey brown thinly layered CLAY, some silt.			2	DO	7										
4		Soft grey brown thinly layered CLAY, trace to some silt.		435.25 3.51	3	DO	2										
6		Loose brown SAND, some gravel, trace to some silt.		433.11 5.64	4	DO	5									Grout and bentonite	
8		Dense grey SAND and GRAVEL, trace to some silt grading to very dense grey SAND and GRAVEL.		431.44 7.32	5	DO	25										
10		Very dense brown SILT grading to laminated SILT (WEATHERED BEDROCK)		429.69 9.07	6	DO	62									Filter sand Bentonite seal	
12		Bedrock Encountered. Refer to ROCK LOG for continuation of rock description.		427.78												SCREEN?	

BOREHOLE BOREHOLES.GPJ GLDR\_CAN.GDT 10/1/06

DEPTH SCALE

1 : 100



LOGGED: RR

CHECKED: GTI

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 17-1

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Feb 25, 26 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION GA 17-1		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. + rem V.		Q - U				Wp	
0		GROUND SURFACE		438.42													
		Loose dark brown clayey organic SILT. (reworked native)		438.11 0.30											Steel Well Protector in Concrete 5/04/05		
2		Stiff brown thinly layered CLAY, trace to some silt occasional gravel inclusions.		436.28 2.13	1	DO	11										
		Soft grey brown thinly layered CLAY, trace to some silt, occasional gravel.		434.61 3.81	2	DO	2										
4		Loose brown SILT, some gravel.		433.16 5.26	3	DO	11										
6		Very dense brown silty gravelly SAND with cobbles.		432.02 6.40	4	DO	101										
8		Very dense brown grey silty SAND and GRAVEL with cobbles.		430.80 7.62	5	DO	68										
10		Very dense brown grey SILT and GRAVEL, some sand with cobbles grading to dark grey sandy SILT and GRAVEL with cobbles. (GLACIAL TILL)		426.99 11.43	6	DO	70										
12					7	DO	87										
14		Dense dark grey sandy SILT, some gravel with cobbles. (GLACIAL TILL)		422.72 15.70	8	DO	45										
16		Compact dark grey SILT, some clay and fine gravel, trace sand with cobbles. (GLACIAL TILL)		421.35 17.07	9	DO	38										
18		Very dense grey layered GRAVEL with dark brown organic clayey SILT. (WEATHERED BEDROCK)		420.74	10	DO	16										
		Soft dark brown organic clayey SILT					DO-100								Filter sand		
20		Bedrock Encountered. Refer to ROCK LOG for continuation of rock description.															

BOREHOLE BOREHOLES.GPJ GLDR CAN.GDT 10/1/06

DEPTH SCALE  
1 : 100



LOGGED: RR  
CHECKED: GTI

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 17-2

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Feb 26 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GA 17-2</b>		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V. + Q - U - O		Wp				W	
0		GROUND SURFACE		438.38													
		Loose dark brown clayey oraganic SILT. (reworked native)		438.08											Steel V. 4/05 Protector in Concrete		
				0.30													
		Stiff brown thinly layered CLAY, trace to some silt occasional gravel inclusions.			1	DO	11								Bentonite		
2				436.25													
				2.13													
		Soft grey brown thinly layered CLAY, trace to some silt occasional gravel.			2	DO	2								Filter sand		
				434.57											Bentonite seal		
				3.81													
4		Loose brown SILT, some gravel.			3	DO	11								Filter sand		
				433.12													
				5.26													
		Very dense brown silty gravelly SAND with cobbles.			4	DO	101										
6				431.98													
				6.40													
		Very dense brown grey silty SAND and GRAVEL with cobbles.															
				430.76													
				430.46													
8		Very dense brown grey SILT and GRAVEL, some sand with cobbles grading to dark grey sandy SILT and GRAVEL with cobbles. (GLACIAL TILL)			5	DO	68								50 mm dia. PVC Screen		
				7.92													
		End of BOREHOLE.															

BOREHOLE BOREHOLES.GPJ GLDR CAN.GDT 10/1/06

DEPTH SCALE

1 : 100



LOGGED: RR

CHECKED: GTI



DECOM

PROJECT No.: Glenmore Landfill

**RECORD OF BOREHOLE: GA 18-1**

SHEET 1 OF 2

LOCATION: See Figure 1

BORING DATE: Feb 28 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GA 18-1</b>	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		Q, kPa		Wp		W			
0		GROUND SURFACE		442.31 0.00													
0.91		Loose mixed brown SILT, CLAY and SAND, trace gravel. (FILL)		441.40 0.91												Steel Well Protector in Concrete Grout and bentonite	
2		LANDFILL REFUSE (Paper, plastic, wood etc. and soil) (FILL)			1	DO	7										
4				2	DO	21											
6				3	DO	4											
8				4	DO	8											
8.99		Very soft grey brown thinly layered CLAY grading to very soft grey thinly layered CLAY, some silt with occasional grey clayey silt layers.		433.32 8.99	5	DO	1										
10				6	DO	wh											
12				7	DO	wh											
14				8	DO	wh											
16.15		Loose grey silty fine SAND.		426.16 16.15	9	DO	5										
18																	
18.59		Very soft grey thinly layered CLAY, some silt.		423.72 18.59	10	DO	wh										
20																	

Foundex Explorations  
Bonsadier Simco 2800 120 mm dia. Mud Rotary

5/04/05  
▽

Bentonite seal

Grout and bentonite

CONTINUED NEXT PAGE

BOREHOLE BOREHOLES.GPJ GLDR CAN.GDT 10/1/06

DEPTH SCALE  
1 : 100



LOGGED: RR  
CHECKED: GTI

at DeLeon

PROJECT No.: Glenmore Landfill

**RECORD OF BOREHOLE: GA 18-1**

SHEET 2 OF 2

LOCATION: See Figure 1

BORING DATE: Feb 28 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m		HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GA 18-1</b>	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH Cu, kPa		WATER CONTENT PERCENT					
								20	40	60	80	10 <sup>-6</sup>			10 <sup>-5</sup>
20	Foundex Explorations Borehole Simeco 2800 120 mm dia. Mud Rotary	Very soft grey thinly layered CLAY, some silt. (continued)	[Hatched]	420.67 21.64										Grout and bentonite	
22		Compact light grey silty gravelly SAND.	[Dotted]	419.45 22.86	11	DO	16								
24		Very dense light grey silty SAND, some gravel grading to very dense light grey laminated silty SAND, trace gravel. (WEATHERED BEDROCK)	[Dotted]	418.33											
24		Bedrock Encountered. Refer to ROCK LOG for continuation of rock description.	[Blank]												
26															
28															
30															
32															
34															
36															
38															
40															

BOREHOLE BOREHOLES.GPJ GLDR\_CAN.GDT 10/1/06

DEPTH SCALE

1 : 100



LOGGED: RR

CHECKED: GTI



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL18-1 (Decom)**  
 SURFACE ELEVATION: **442.46 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1					Monitoring well decommissioned May 30, 2011					concrete to 0.9 m	442
2											441
3											440
4											439
5											438
6											437
7											436
8											435
9											434
10											433
11											432
12											431
13											430
14											429
15											428
16											427
17											426
18											425
19											424
											423

SLR CANADA V6.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 30, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **GL18-1 (Decom)**  
 SURFACE ELEVATION: **442.46 m**

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
21											422
22											421
23											420
24					End of borehole at 24.1 m						419

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Core Sample**  
 DRILL DATE: **May 30, 2011**  
 LOGGED BY: **JN**  
 DRILLER NAME: **Beck**

Notes:



PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 18-2

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Mar 1 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GA 18-2</b>	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. + rem V. $\oplus$ $\ominus$		10 <sup>-6</sup> 10 <sup>-5</sup> 10 <sup>-4</sup> 10 <sup>-3</sup>		Wp			W
0		GROUND SURFACE		442.35													
		Loose mixed brown SILT, CLAY and SAND, trace gravel. (FILL)		441.44 0.91												Steel Well Protector in Concrete Filter sand	
2		LANDFILL REFUSE (Paper, plastic, wood etc. and soil) (FILL)			1	DO	7									Bentonite seal	
4				2	DO	21											
6				3	DO	4											
8				4	DO	8											
10				5	DO	1										Grout	
12		Very soft grey brown thinly layered CLAY grading to very soft grey thinly layered CLAY, some silt with occasional grey clayey silt layers.		433.36 8.99	6	DO	wh										
14				7	DO	wh											
16				8	DO	wh											
18		Loose grey silty fine SAND.		426.20 16.15	9	DO	5									50 mm dia. PVC Screen Filter sand	
20					423.76 18.59												
		Very soft grey thinly layered CLAY, some silt.		423.20													
		End of BOREHOLE.		19.15													

BOREHOLE BOREHOLES.GPJ GLDR\_CAN.GDT 10/1/06

DEPTH SCALE  
1 : 100



LOGGED: RR  
CHECKED: GTI

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: GA 18-3

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: Mar 1 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GA 18-3</b>		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20    40		60    80		10 <sup>-6</sup> 10 <sup>-5</sup> 10 <sup>-4</sup> 10 <sup>-3</sup>				Wp	
0		GROUND SURFACE		442.55 0.00											Steel Well Protector in Concrete		
		Loose mixed brown SILT, CLAY and SAND, trace gravel. (FILL)	[Hatched Pattern]	441.63 0.91											Bentonite Seal		
2		LANDFILL REFUSE (Paper, plastic, wood etc. and soil) (FILL)	[Hatched Pattern]												Filler sand		
4															13/04/05		
6																150 mm dia. PVC Screen	
8		End of BOREHOLE.		434.24 8.31													
10																	
12																	
14																	
16																	
18																	
20																	

BOREHOLE BOREHOLES.GPJ GLDR. CAN.GDT 10/1/06

DEPTH SCALE

1 : 100



LOGGED: RR

CHECKED: GTI

PROJECT No.: 05-1440-252

# RECORD OF MONITORING WELL: MW07-2 (GL-20)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: May 16, 2007

DATUM: Local

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20		40		60		80			10 <sup>-6</sup>
0		Ground Surface		0.00												Concrete Riser	
0.5		Very soft to soft dark brown/grey SILTY CLAY, occasional black rocks and organics, some fine sand intermixed with brown silty sand, some gravel. (FILL)		1.52	1	DO	14									Cuttings	
1.5				2	DO	36											Bentonite Seal
2.5				3	DO	32											Slotted Section Filler Sand
3.35		End of MONITORING WELL.														Filter Sand	

BOREHOLE 05-1440252\_1000.LOGS.GPJ GLDR\_CAN.GDT 19/3/09

DEPTH SCALE  
1 : 50



LOGGED: AR  
CHECKED: **DRAFT**

PROJECT No.: 05-1440-252

# RECORD OF MONITORING WELL: MW07-3 (GL-21)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: May 16, 2007

DATUM: Local

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20 40 60 80		nat V. + Q - rem V. ⊕ U - ○		20 40 60 80				Wp	
0		Ground Surface		0.00											Concrete Riser		
1	Beck Drilling & Environmental Services Hollow Stem Auger	Loose/soft SILT, CLAY and SAND, some gravel, trace refuse with angular cobbles and boulders. (FILL)													Bentonite Seal		
2																	
3				1	DO	4											Slotted Section Filter Sand
4		Very soft to firm greyish-brown CLAY, trace to some thin silt seams, occasional rootlets.		2.95													
5	2			DO	1												
6																	
7		Compact greyish brown silty SAND, some gravel and clay. (TILL)		5.03											Slough		
8	3			DO	8												
9		5.18															
10		End of MONITORING WELL.															

BOREHOLE 051440252\_1000\_LOGS.GPJ\_GLDR\_CAN.GDT 19/3/09

DEPTH SCALE  
1 : 50



LOGGED: AR  
CHECKED: **DRAFT**



PROJECT No.: NE Pond

# RECORD OF AUGERHOLE: GL22-1

SHEET 1 OF 2

LOCATION: See Figure

BORING DATE: Oct. 31/07

DATUM: Geodetic

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION GL22-1	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.		+		Q -			Wp
0		GROUND SURFACE		449.54												Concreted in stick up steel well protector.           Bentonite seal.   Nov 9/07 ▽  Sieve   Sieve   Filter sand.	
		Organic WOOD MULCH, some silt and fine sand.		0.00													
		Firm to stiff grey dessicated layered CLAY, some light brown silt seams and inclusions, trace brown fine sand lenses.		449.24													
				0.30													
1		Stiff grey layered CLAY, some light brown silt seams and inclusions, trace to some brown fine sand, some silt seams and lenses.		448.63	1	AS											
				0.91													
2		Firm to stiff grey-brown laminated silty CLAY, some silt, trace clay layers and seams, trace to some fine sand lenses, and occasional decomposed root fibres.		447.72													
				1.83													
				446.78	2	DO	22										
				2.77													
3		Dense grey fine SAND, some fine to medium sand, occasional fine gravel layers.															
					3	DO	34										
4																	
5	Beck Drilling Hollow Stem Auger			444.36													
				5.18													
6		Compact grey fine SAND, some brownish-grey clayey silt seams.			4	DO	13										
7				442.38													
				7.16	5	DO	40										
8		Dense grey fine SAND, occasional fine to medium sand layers, and occasional grey clayey silt seams.															
9				440.65	6	DO											
				8.89													
10		Dense grey fine SAND, trace silt with slight rust brown oxidation.															

CONTINUED NEXT PAGE

BOREHOLE 2007 BOREHOLES.GPJ GLDR\_CAN.GDT 11/16/07

DEPTH SCALE

1 : 50



LOGGED: AR

CHECKED:

PROJECT No.: NE Pond

# RECORD OF AUGERHOLE: GL22-1

SHEET 2 OF 2

LOCATION: See Figure

BORING DATE: Oct. 31/07

DATUM: Geodetic

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GL22-1</b>	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. + Q - ● rem V. ⊕ U - ○		Wp		W			
10	Beck Drilling Hollow Stem Auger	Dense grey fine SAND, trace silt with slight rust brown oxidation (continued)		436.74	7	DO	39										Filter sand.  50 mm dia. PVC well screen.
11				12.80													
12		Dense grey fine SAND with cobbles, some medium to coarse sand and gravel (GLACIAL TILL).		435.83													
13	End of AUGERHOLE.		13.72														
14																	
15																	
16																	
17																	
18																	
19																	
20																	

BOREHOLE 2007 BOREHOLES.GPJ GLDR\_CAN.GDT 11/16/07

DEPTH SCALE  
1 : 50



LOGGED: AR  
CHECKED:

PROJECT No.: NE Pond  
 LOCATION: See Figure

# RECORD OF AUGERHOLE: GL23-1

BORING DATE: Nov. 5/07

SHEET 1 OF 2

DATUM: Geodetic

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION GL23-1	
		DESCRIPTION	STRATA PLOT ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
							Cu, kPa		nat V. rem V.		+ ⊕ - ⊙		Wp			W
0		GROUND SURFACE	445.93													
		Very loose brown organic WOOD MULCH, intermixed with some silt and sand.	0.00 445.72 0.20												Concrete in stick up steel well protector.	
		Compact brownish-grey SILT and SAND, some gravel (FILL).	445.37 0.56												Bentonite seal.	
		Stiff grey dessicated CLAY, some light brown silt seams.	445.01 0.91	1	AS											
1		Stiff grey layered CLAY, some light brown silt seams and brown fine sand, some silt lenses.	443.94 1.98													
2				2	DO	19										
3															Nov 9/07 ▽	
4				3	DO	13										
5	Beck Drilling Hollow Stem Auger															
6		Compact to dense brown fine SAND.													Native slough.	
7																
8				4	DO											
9																
10		Dense grey silty SAND, some gravel (GLACIAL TILL).	436.17 9.75	5	DO										50 mm dia. PVC well screen.  Native slough.	

CONTINUED NEXT PAGE

BOREHOLE 2007 BOREHOLES.GPJ GLDR CAN.GDT 11/16/07

DEPTH SCALE  
1 : 50



LOGGED: AR  
CHECKED:

PROJECT No.: NE Pond

# RECORD OF AUGERHOLE: GL23-1

SHEET 2 OF 2

LOCATION: See Figure

BORING DATE: Nov. 5/07

DATUM: Geodetic

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GL23-1</b>	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.		+ Q. U. -		Wp			W
10	Back Drilling	Dense grey silty SAND, some gravel (GLACIAL TILL). (continued)		435.41 10.52	5	DO										Native slough.	
11		End of AUGERHOLE.															
12																	
13																	
14																	
15																	
16																	
17																	
18																	
19																	
20																	

BOREHOLE 2007 BOREHOLES.GPJ GLDR\_CAN.GDT 11/16/07

DEPTH SCALE

1 : 50



LOGGED: AR

CHECKED:



PROJECT No.: NE Pond

# RECORD OF AUGERHOLE: GL24-1

SHEET 1 OF 1

LOCATION: See Figure

BORING DATE: Nov. 5 and 6/07

DATUM: Geodetic

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION <b>GL24-1</b>	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	SHEAR STRENGTH		WATER CONTENT PERCENT							
							Cu, kPa	nat V. rem V. $\oplus$ $\ominus$	U - O	Wp	W					
0		GROUND SURFACE		446.71												
		Very loose dark brown organic SILT and fine SAND with roots (TOPSOIL).		0.00 446.48 0.23											Concreted in stick up steel well protector.	
		Compact greyish-brown silty fine SAND.		446.02												
		Stiff grey dessicated CLAY, some light brown silt seams and lenses, and trace brown silt and fine sand lenses.		0.69 445.69 1.02											Bentonite seal.	
1		Stiff grey layered CLAY, trace to some light brown silt seams and lenses, trace brown fine sand lenses and occasional root fibres.		444.88	1	AS										
2				1.83												
3		Compact brown fine SAND, occasional coarse sand, and grey clay, some silt seams.			2	DO 10										
4	Beck Drilling Hollow Stem Auger															
5				442.26	3	DO 20									Nov 8/07 ▽ 50 mm dia. PVC well screen. Filter sand.	
6				4.44	4	DO 44										
7		Dense brownish-grey gravelly SAND with cobbles, some silt to silty (GLACIAL TILL).			5	DO									Native slough.	
8				439.39	6	DO										
9		End of AUGERHOLE.		7.32												
10																

BOREHOLE 2007 BOREHOLES.GPJ GLDR\_CAN.GDT 11/16/07

DEPTH SCALE  
1 : 50



LOGGED: AR  
CHECKED:

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL25-1 (MW09-1-1)

SHEET 1 OF 2

LOCATION: See Figure 1

BORING DATE: June 11/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, $k_v$ cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH $C_u$ , kPa				WATER CONTENT PERCENT					
							20	40	60	80	10 <sup>-6</sup>	10 <sup>-5</sup>	10 <sup>-4</sup>			10 <sup>-3</sup>
0		Ground Surface													Stickup= 0.753m	
0.05		Loose dark brown organic silt (forest cover)														
0.76		Loose to compact light brown sandy SILT with rootlets.														
1.68		Loose to compact light brown fine SAND, trace silt.		1	CS											
2		Stiff to very stiff interlayered CLAY and SILTY CLAY fissured with organic root matter infilling with occasional fine sand and silt partings.		2	DO	8										
1.68				4/5	DO	8										
4		Very dense light brown silty SAND and GRAVEL with occasional very stiff brown silty clay layers, contains cobbles.		6	DO	50 for 3.5"										
3.96				7	DO	50 for 5.5"										
8		Very dense light brown SAND, some silt and gravel.		8	DO	50 for 2.5"										
7.77		Very dense light brown silty SAND and GRAVEL with occasional very stiff brown silty clay layers, contains cobbles.		9	DO	50 for 6"										
9.75				10	CS											
10		Very dense grey and brown SAND and GRAVEL with silty clay, contains cobbles (Glacial Till).		11	DO	78										
12				12	DO	50 for 6"										
13				13	DO											
14		Very dense grey and brown SAND and GRAVEL with silty clay, contains cobbles (Glacial Till).		14	DO	76										
16				15	CS											
18.90				16	DO	51										
18		Fresh medium strong to strong light grey BEDROCK.		17	CS											
20																

CONTINUED NEXT PAGE

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE

1 : 100



LOGGED: BS

CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL25-1 (MW09-1-1)

SHEET 2 OF 2

LOCATION: See Figure 1

BORING DATE: June 11/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH Cu, kPa				WATER CONTENT PERCENT					
								20	40	60	80	nat V. rem V.	+ ⊕	- ⊙			Wp
20	Odeix B61	Fresh medium strong to strong light grey BEDROCK. (continued)		21.95	17	CS											
22		Fresh medium strong to strong dark grey BEDROCK.		22.56	18	CS											
24		Fresh strong to very strong light grey BEDROCK.			19	CS											
26																	
28																	
30		End of MONITORING WELL.		29.57													
32																	
34																	
36																	
38																	
40																	

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL25-2 (MW09-1-2)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 2/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.		+ ⊕				Q - ⊙	
0	6" OD Solid Stem Augers R-59 (B53)	Ground Surface													Stickup= 0.95m  Bentonite  Slotted Section Filter Sand		
0.05		Loose dark brown organic silt (forest cover). Loose to compact light brown sandy SILT with rootlets.															
1.22		Loose to compact light brown fine SAND, trace silt.															
1.83		Stiff to very stiff interlayered CLAY and SILTY CLAY fissured with organic root matter infilling with occasional fine sand and silt partings.															
3.35		End of MONITORING WELL.															
4																	
6																	
8																	
10																	
12																	
14																	
16																	
18																	
20																	

BOREHOLE: 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA



PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL26-1 (MW09-2-1)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 3/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V.	rem V.	+	Q -			U -	Wp
0		Ground Surface		0.00											Stickup= 0.735m		
1.37		Loose light brown sandy SILT, trace to some clay and gravel contains rootlets and wood debris. (FILL)															
2		Dense light brown silty SAND and GRAVEL, contains cobbles.		1.37	1	DO	38								June 12/09		
2.74				2.74	2	DO	54								Bentonite		
4		Very stiff to hard light brown layered CLAYEY SILT trace to little sand and gravel occasional fine sand partings.			3	DO	41										
5.84		Fresh, medium strong to strong, light grey BEDROCK, some fractures.		5.84		DO	>100								Slotted Section Filter Sand		
6.61				6.61											Sand		
8		Fresh, strong, light grey BEDROCK.			5	CS									Bentonite		
9.65		End of MONITORING WELL.		9.65													

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE

1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL26-2 (MW09-2-2)

SHEET 1 OF 1

LOCATION: See Figure 1

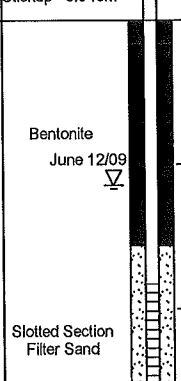
BORING DATE: June 3/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.	+ ⊕	Q - U	⊙			Wp	W
0		Ground Surface													Stickup= 0.946m		
0.76		Loose light brown sandy SILT, trace to some gravel, contains rootlets and wood debris. (FILL)		0.00													
1.71		Stiff brown desiccated CLAY, contains root matter.		0.76													
2.44		Dense light brown silty SAND and GRAVEL.		1.71													
5.18		Very stiff to hard light brown layered CLAYEY SILT, trace to little sand and gravel, occasional fine sand partings.		2.44													
5.18		End of MONITORING WELL.		5.18													
6																	
8																	
10																	
12																	
14																	
16																	
18																	
20																	



BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE

1 : 100



LOGGED: BS

CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL26-3 (MW09-2-3)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 3/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.	+ ⊕	Q - U	○			Wp	W
0	6" OD Solid Stem R-59 (B53)	Ground Surface		0.00											Stickup= 0.856m		
		Loose light brown sandy SILT, trace to some gravel, contains rootlets and wood debris. (FILL)		0.91											Bentonite		
		Stiff brown desiccated CLAY, contains root matter.		1.71													
		Dense light brown silty gravelly SAND.		2.44											June 12/09 ▽ Slotted Section Filter Sand		
		Very stiff to hard light brown layered CLAYEY SILT, trace to little sand and gravel, occasional fine sand partings.		3.35													
4		End of MONITORING WELL.															

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL26-4 (MW09-2-4)

SHEET 1 OF 2

LOCATION: See Figure 1

BORING DATE: June 9/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	20	40	60	80	10 <sup>-5</sup>	10 <sup>-5</sup>		
0		Ground Surface		0.00											
		Loose light brown sandy SILT, trace to some and gravel contains rootlets and wood debris. (FILL)		0.86											
		Stiff brown desiccated CLAY contains root matter.		1.37											
2		Dense light brown silty gravelly SAND.		2.23											
4		Very stiff to hard light brown layered CLAYEY SILT trace to little sand and gravel occasional fine sand partings.		6.81											
6				7.57											
8		Fresh, medium strong to strong, light grey and grey, BEDROCK some fractures.		10.82											
10		Fresh, strong, light grey, BEDROCK with a few fractures.		11.58											
12		becoming dark grey		12.95											
14		becoming grey													
16		Fresh, strong to very strong, grey BEDROCK.													
18															
20															

Stickup= 0.938m  
June 12/09

Bentonite Grout

CONTINUED NEXT PAGE

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL26-4 (MW09-2-4)

SHEET 2 OF 2

LOCATION: See Figure 1

BORING DATE: June 9/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m		HYDRAULIC CONDUCTIVITY, $k, \text{cm/s}$				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH		WATER CONTENT PERCENT					
								20	40	60	80	nat V. +			rem V. ⊕
20	Odex R-59 (B53)	Fresh, strong to very strong, grey BEDROCK. (continued)												Bentonite Grout  Bentonite  Slotted Section Filter Sand	
22															
24		Fresh, strong to very strong, dark grey BEDROCK.													
26		End of MONITORING WELL.		26.21											
28															
30															
32															
34															
36															
38															
40															

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ\_GLDR\_CAN.GDT 6/24/10

DEPTH SCALE

1 : 100



LOGGED: BS

CHECKED: PVA



PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL27-1 (MW09-3-1)

SHEET 1 OF 2

LOCATION: See Figure 1

BORING DATE: June 4/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, $k_v$ cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20 40 60 80		10 <sup>-6</sup> 10 <sup>-5</sup> 10 <sup>-4</sup> 10 <sup>-3</sup>		nat V. rem V.				+ Q - U	
0		Ground Surface															
		Loose dark brown organic SILT, trace to some sand (re-worked - Topsoil) (FILL). Stiff brown CLAY, trace to some silt, trace gravel (FILL).		0.10													
2		Compact brown silty SAND and GRAVEL, trace clay (FILL).		1.52	1	DO	12										
				2.19													
4		Stiff grey and brown thinly layered CLAY, occasional fine sand partings.			2	DO	7										
					3	DO	4										
					4	DO	4										
		Very loose to loose brown silty SAND. Soft brown CLAYEY SILT, trace fine sand.		5.03	5	DO	4										
					6	DO	4										
6		Soft to firm grey and brown layered CLAY grading to very soft to soft grey and brown layered CLAY.			7	DO	0										
					8	DO	1										
				8.53													
		Loose grey silty SAND and GRAVEL, trace to some clay.			9	DO	8										
				9.50													
10		Very stiff grey SILTY CLAY, little to some sand and gravel. (GLACIAL TILL)			10	DO	8										
					11	DO	19										
				11.94													
12		Hard dark grey and brown SILTY CLAY, trace to little sand.			12	DO	33										
				13.26													
14					13	DO	62										
					14	DO	75										
16																	
		Hard dark grey SILTY CLAY.			15	DO	>100										
18																	
20																	

Stickup= 2.003m

Bentonite Grout

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ G.LDR. CAN.GDT. 6/24/10

CONTINUED NEXT PAGE

DEPTH SCALE

1 : 100



LOGGED: BS

CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL27-1 (MW09-3-1)

SHEET 2 OF 2

LOCATION: See Figure 1

BORING DATE: June 4/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.	+ ⊕	Q - ⊙	U - ○	Wp			W
20	Olex R-59 (B53)	Hard dark grey SILTY CLAY. (continued)		21.18	16	DO	>100									Bentonite Grout Bentonite Slotted Section Filter Sand Bentonite	
22		Fresh, medium strong to strong, grey BEDROCK.		22.86	17	CS											
24		Fresh, medium strong to strong, dark grey BEDROCK, some fractures.		25.55	18	DO	>100										
26		Fresh, medium strong to strong, grey BEDROCK.		26.52	19	CS											
28		End of MONITORING WELL.  Note: Measured water level 0.73m above ground surface on June 16, 2009.			20	CS											

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE

1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL27-2 (MW09-3-2)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 5/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								20		40		60		80			10 <sup>-6</sup>
0		Ground Surface													Stickup= 0.76m		
0.10		Loose dark brown organic SILT, trace to some sand. (re-worked - Topsoil) (FILL)															
2		Stiff brown CLAY, trace to some silt, trace gravel. (FILL)															
2.59		Soft black organic clayey SILT. (FILL) Compact brown silty SAND and GRAVEL, some clay. (FILL)															
4		Stiff grey and brown thinly layered CLAY, occasional fine sand and silt partings.															
5.79		Soft to firm grey and brown layered CLAY grading to very soft to soft grey and brown layered CLAY.															
9.30		Very stiff grey SILTY CLAY, little to some sand and gravel. (GLACIAL TILL)			1	CS											
12.34		End of MONITORING WELL.															

June 12/09  
▽

Bentonite Grout

Bentonite

Slotted Section  
Filter Sand

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR CAN.GDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL27-3 (MW09-3-3)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 8/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH		WATER CONTENT PERCENT		WATER CONTENT PERCENT				
								20	40	60	80	nat V. rem V.	+ Q - U -			Wp
0	8.5/8" OD Hollow Stem Augers R-55 (B53)	Ground Surface		0.10											Stickup= 0.824m	
		Loose dark brown organic SILT, trace to some sand. (re-worked - Topsoil) (FILL)														
		Stiff brown CLAY, trace to some silt, trace gravel. (FILL)														
2		Soft black organic clayey SILT. (re-worked - Topsoil)			1.68											
					2.29											
4		Stiff grey and brown thinly layered CLAY, occasional fine sand and silt partings.													Bentonite Grout	
6				5.79												
8		Soft to firm grey and brown layered CLAY grading to very soft to soft grey and brown layered CLAY.													Bentonite	
10		Stiff grey SILTY CLAY, little to some sand and gravel. (GLACIAL TILL)													Slotted Section Filter Sand	
		End of MONITORING WELL.			9.91											

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION GPJ GLDR CAN.GDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL27-4 (MW09-3-4)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 9/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m		HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH		WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.		Wp			W
0	6" OD Solid Stem R-59 (B53)	Ground Surface		0.10										Stickup= 0.624m June 12/09 Bentonite Slotted Section Filter Sand	
0.10		Loose dark brown organic SILT, trace to some sand (re-worked - Topsoil) (Fill).													
1.27		Loose to compact sandy gravelly SILT, trace to some clay contains wood debris (Fill).													
1.78		Soft to firm black and brown clayey SILT (re-worked - Topsoil).													
2		Stiff grey and brown thinly layered CLAY, occasional fine sand and silt partings.													
2.44		End of MONITORING WELL.													
4															
6															
8															
10															
12															
14															
16															
18															
20															

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR. CAN.CDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA



PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL28-1 (MW09-4-1)

SHEET 1 OF 2

LOCATION: See Figure 1

BORING DATE: June 11/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. + Q - ● rem V. ⊕ U - ○		Wp				W	
0		Ground Surface		0.00			20	40	60	80	10 <sup>6</sup>	10 <sup>5</sup>	10 <sup>4</sup>	10 <sup>3</sup>	Stickup: 0.568m 437.96		
0.81		Stiff to very stiff brown desiccated CLAY.															
2.8		Very stiff grey layered SILTY CLAY, some fine sand and silt partings.		0.81	1	DO	9										
3.05		Loose oxidized brown SILT.		3.05	2	DO	5										
3.3		Firm to stiff grey layered SILTY CLAY, some fine sand partings.		3.3	3	DO	5										
4.32		Firm to stiff grey layered SILTY CLAY, some fine sand partings.		4.32	4	DO	9										
7.32		Loose brown silty fine SAND.		7.32	5	DO	1										
7.32		Loose brown silty fine SAND.		7.32	6	DO	1										
7.32		Loose brown silty fine SAND.		7.32	7	DO	3										
12.60		Very soft to soft grey thinly layered CLAY, occasional fine sand partings.		12.60	8	DO	0										
12.60		Very soft to soft grey thinly layered CLAY, occasional fine sand partings.		12.60	9	DO	0										
14.94		Very soft grey SILTY CLAY with occasional thin seams of clayey silt and fine to medium sand partings.		14.94	10	DO	0										
17.68		Very loose brown fine to medium SAND, some silt.		17.68	11	DO	>50										
19.20		Fresh, medium strong to strong, light grey BEDROCK with a few fractures.		19.20	11	DO	>50										

2.8  
33.66 4.3  
130.66 7.3

August 25/09  
435.16

Stickup: 0.568m  
437.96

Bentonite Grout

Bentonite

Slotted Section  
Filter Sand

Bentonite

CONTINUED NEXT PAGE

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION GPJ GLDR CAN GDT 6/24/10

DEPTH SCALE  
1 : 100



LOGGED: BS  
CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL28-1 (MW09-4-1)

SHEET 2 OF 2

LOCATION: See Figure 1

BORING DATE: June 11/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat. V. rem V. + ⊕ - ⊙		Wp		W			
20	Wash Boring R-59 (BS)	Fresh, medium strong to strong, light grey BEDROCK with a few fractures. (continued)													Bentonite		
22																	
24																	
26																	
26.37		Fresh, medium strong to strong, grey and dark grey BEDROCK with a few fractures.		26.37													
26.97				26.97													
28		Fresh, medium strong to strong, light grey BEDROCK with a few fractures.															
28.50		End of MONITORING WELL.		28.50													
30																	
32																	
34																	
36																	
38																	
40																	

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10



PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL28-2 (MW09-4-2)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 16/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION													
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT																
								Cu, kPa		nat V. rem V.	+ Q - U	Wp	W			W	W											
0		Ground Surface		0.00			20	40	60	80	10 <sup>-9</sup>	10 <sup>-5</sup>	10 <sup>-1</sup>	10 <sup>3</sup>	Stickup= 0.602m													
0.81		Stiff to very stiff brown desiccated CLAY (Grass @ surface).		0.81																								
2	8.5" OD Hollow Stem Augers R-59 (B53)	Very stiff grey layered SILTY CLAY, some fine sand and silt partings grading to firm to stiff grey layered SILTY CLAY, some fine sand and silt partings.	[Hatched Strata Plot]	4.47											Bentonite													
4																Loose brown silty fine SAND.	[Dotted Strata Plot]	7.01										August 25/09
6																												
8																												
10																												
12																												
14																												
16																												
18																												
20																												

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE

1 : 100



LOGGED: BS

CHECKED: PVA

PROJECT No.: 09-1440-0066

# RECORD OF MONITORING WELL: GL28-3 (MW09-4-3)

SHEET 1 OF 1

LOCATION: See Figure 1

BORING DATE: June 16/09

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES			DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m		HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH		WATER CONTENT PERCENT					
								20	40	60	80	nat V.			rem V.
0		Ground Surface		0.00											
0.81		Sliff to very stiff brown desicated CLAY.													
2	6" OD Solid Stem R-59 (BS3)	Very stiff grey layered SILTY CLAY, some fine sand and silt partings grading to firm to stiff grey layered SILTY CLAY, some fine sand and silt partings.		0.81											
4.06		End of MONITORING WELL.		4.06											

Stickup= 0.415m

Bentonite

August 25/09

Slotted Section  
Filter Sand

BOREHOLE 09-1440-0066 COMBINED FOR XSECTION.GPJ GLDR\_CAN.GDT 6/24/10

DEPTH SCALE

1 : 100



LOGGED: BS

CHECKED: PVA

GL 29-1

SLR CONSULTING (CANADA) LTD.					CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164	BOREHOLE LOG								
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
0					Ground Surface								stickup, jplug	444
0.5					SAND AND GRAVEL trace silt, loose, brown, moist									443
1					SAND AND SILT (till) trace to some clay, trace gravel, compact, brown, moist									442
2					- some clay, some gravel, dense at 1.8 m - sand becoming coarser									441
4		BH12-4A-1			- very dense at 4.9 m									440
5					- cobbles encountered at 6.1, 6.7, 7.3 and 7.9 m									439
6														438
7		BH12-4A-2												437
8					- wet from 8.2 to 8.5 m									436
9					- cobbles at 8.8 m - brown from 9.0 to 9.8 m									435
10					- grey at 9.8 m - green cobbles at 10.4 m									434
11					- cobbles at 11.3 m									433
12														432
13		BH12-4A-3			SAND fine, some silt, trace gravel, loose, grey, wet									431
14		BH12-4A-4			SAND AND SILT some clay, some gravel, very dense, grey, moist - becoming loose, increased cobble/gravel at 13.4 m									430
15					- dense from 14 to 16.2 m									429
16														428
17					- cobbles at 17.4 m - very dense to 18.9 m									427
18														426
19					- increased silt, loose, wet between 18.6 and 18.9 m									425

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

GW = 4.50 mbg  
(October 3, 2012)



GC29-1

**BOREHOLE LOG**



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

BOREHOLE NO: **BH12-4A**

SURFACE ELEVATION: 443.81 m

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
19.4		BH12-4A-5			- 0.3 m silt layer, wet at 19.4 m - loose, dry at 19.7 m									424
20.7		BH12-4A-6			<b>SAND</b> fine, some silt, trace clay, loose to compact, wet - medium grained at 20.7 m									423
21.2					<b>SAND AND SILT</b> some clay, some gravel, dense, grey, moist - wet, silty sand laminations at 21.2 m - compact, grey, wet from 21.3 to 21.8 m - very dense at 21.9 m									422
23.0		BH12-4A-7			- cobble at 23 m									421
25.0					- green rock pieces at 25 m									420
25.6		BH12-4A-8			- rusty rock pieces between 25.6 and 26.2 m									418
26.5					- green cobble at 26.5 m									417
27.4					- cobble at 27.4 m									416
28.5					- 5 cm seam medium to coarse sand at 28.5 m									415
29.3					- very dense between 29.3 and 32.3 m (core steaming)									414
32.3		BH12-4A-9												413
32.6		BH12-4A-10			- sand seam from 32.3 to 32.6 m									411
34.4					- rusty rock pieces at 34.4 m									409
38.0		BH12-4A-11												406

bentonite chips to 40.2 m

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample  
 DRILL DATE: September 26, 2012  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

Notes:  SONIC CORE SAMPLE

GL-29-1

SLR CONSULTING (CANADA) LTD.					BOREHOLE LOG								
CLIENT: <b>City of Kelowna</b> PROJECT: <b>Glenmore Landfill - Phase 3</b> ADDRESS: <b>2105 Glenmore Road North, Kelowna, BC</b> SLR JOB NO: <b>219.05164</b>					BOREHOLE NO: <b>BH12-4A</b> SURFACE ELEVATION: <b>443.81 m</b>								
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
					ORGANIC VAPOUR LEVEL (ppmv)								
					1	10	100	1000	10000				
40													404
41													403
42		BH12-4A-12											402
43													401
44		BH12-4A-13											400
- very dense to dense at 39.6 m  - dense to compact at 41.5 m  <b>BEDROCK</b> large rock pieces and crushed powdery rocks, white, dry													
End of borehole at 44.5 m  Well Completion Details: Screened interval from 41.5 m to 44.5 m below surface Elevation at top of casing (TOC) = 445.039 m  Groundwater Information: Depth to groundwater from TOC = 5.73 m (October 3, 2012)  (1) - Water added during drilling from surface to 44.5 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste  GSA %: BH12-4A-1: 18.6 Gravel, 32.5 Sand, 29.4 Silt, 19.5 Clay BH12-4A-3: 3.8 Gravel, 54.8 Sand, 36.5, Silt, 4.8 Clay BH12-4A-6: 8.4 Gravel, 63.1 Sand, 21.8 Silt, 6.7 Clay BH12-4A-7: 13.1 Gravel, 36.7 Sand, 31.1 Silt, 19.1 Clay													
DRILLING METHOD: Core Sample					Notes: <input type="checkbox"/> SONIC CORE SAMPLE								
DRILL DATE: September 26, 2012					LOGGED BY: JN DRILLER NAME: Mud Bay					Sheet 3 of 3			

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

GL29-2

SLR		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG										
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH12-4B SURFACE ELEVATION: 443.82 m										
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)	
						ORGANIC VAPOUR LEVEL (ppmv)									
						1	10	100	1000	10000					
0					Ground Surface								stickup, jplug	444	
0					<b>SAND AND GRAVEL</b> trace silt, loose, brown, moist									443	
1		BH12-4B-1			<b>SAND AND SILT (till)</b> trace to some clay, trace gravel, compact, brown, moist - gravel increases at 1.5 m  - becoming dense at 2.1 m									442	
2														441	
3													GW = 3.15 mbg (October 3, 2012)	440	
4					- cobbles at 4.0 m								bentonite chips to 12.8 m	439	
5					- cobbles at 4.9 m									438	
6					- increased sand, compact to loose from 5.5 to 6.7 m									437	
7														436	
8					- 7 cm layer coarse sand at 8.2 m								silica sand	435	
9														434	
10		BH12-4B-2			- 15 cm layer medium grained sand and gravel, loose, brown and wet - very dense at 9.8 m									433	
11		BH12-4B-3											sand	432	
12					No stratigraphy or samples from 11 to 14 m								bentonite pellets to 12.2 m	431	
13													slough	430	
14					End of borehole at 14.0 m										
Well Completion Details: Screened Interval from 7.9 m to 11.0 m below surface Elevation at top of casing (TOC) = 444.876 m															
Groundwater Information: Depth to groundwater from TOC = 4.20 m (October 3, 2012)															
(1) - Water added during drilling from surface to 14.0 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste															
GSA %: BH12-4B-2: 23.2 Gravel, 43.6 Sand, 25.7 Silt, 7.6 Clay															
DRILLING METHOD: Core Sample				Notes: <input type="checkbox"/> SONIC CORE SAMPLE											
DRILL DATE: September 26, 2012				LOGGED BY: JN DRILLER NAME: Mud Bay								Sheet 1 of 1			

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/14/13

GL30-1

SLR		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH11-13A1 SURFACE ELEVATION: 439.18 m						
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	440
0			1 50		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (metal and plastic), loose, brown, moist						439
1											438
2			2 70		<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes plastic, cloth, wire). Clay is firm, high plasticity, dark grey, moist					GW = 1.70 mbg (June 15, 2011)	437
3										bentonite seal	436
4											435
5					- black at 5.2 m						434
6											433
7			3 100		- 2 cm thick silt lens at 6.4 m - glass debris at 6.5 m <b>FAT CLAY (reworked soil, fill)</b> trace sand, soft, laminated, brown, moist - 10 cm thick fine sand lens at 7.5 m - increased silt and very soft from 7.8 to 9.4 m					silica sand	432
8		BH11-13A1-1									431
9											430
10		BH11-13A1-2	4 100		- wet at 10 m and 11.3 m						429
11					<b>FAT CLAY (native)</b> trace sand, soft, laminated, grey, moist						428
12		BH11-13A1-3			<b>silty SAND</b> sand is fine, loose, grey, moist						
					End of borehole at 12.0 m						
Well Completion Details: Screened interval from 6.6 m to 8.1 m below surface Elevation at top of casing (TOC) = 440.098 m											
Groundwater Information: Depth to groundwater from TOC = 2.62 m (June 15, 2011)											
(1) - Water added during drilling from surface to 12.0 m											
GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste											
DRILLING METHOD: Core Sample					Notes: <input type="checkbox"/> SONIC CORE SAMPLE						
DRILL DATE: May 17, 2011					LOGGED BY: JN DRILLER NAME: Beck						
Sheet 1 of 1											

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

PL 30-2

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH11-13B SURFACE ELEVATION: 439.48 m						
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
-1										stickup, jplug	440
0					Ground Surface						
0			1 40		Unconsolidated ORGANIC MATTER (wood pieces, grading to chips and sawdust), trace garbage (metal and plastic), loose, brown, moist						439
1											438
2			2 30							GW = 1.84 mbg (June 15, 2011)	437
3											436
4											435
5					Interbedded CLAY AND GARBAGE (MSW) (garbage includes plastic, cloth, wire). Clay is firm, high plasticity, dark grey, moist - no recovery from 5.5 to 8.5 m (refer to BH11-13A)					bentonite seal	434
6											433
7			3 0								432
8											431
9											430
10		BH11-13B-1	4 100		FAT CLAY (native) trace sand, very soft, grey, moist	GSA, Att, M					429
11					-wet from 11 to 11.3 m						428
12		BH11-13B-2			silty SAND trace clay, loose, grey, wet	GSA				silica sand	427
13		BH11-13B-3			FAT CLAY soft, laminated, grey, moist						426
14		BH11-13B-4	5 100			GSA, Att, M					425
					End of borehole at 14.6 m						
					Well Completion Details: Screened interval from 11.9 m to 12.8 m below surface Elevation at top of casing (TOC) = 440.968 m						
					Groundwater Information: Depth to groundwater from TOC = 3.33 m (June 15, 2011)						
					(1) - Water added during drilling from surface to 14.6 m GSA - grain size analysis M - moisture content Att - Atterberg limits						
DRILLING METHOD: Core Sample					Notes: <input type="checkbox"/> SONIC CORE SAMPLE						
DRILL DATE: May 4, 2011					LOGGED BY: JN DRILLER NAME: Beck						
					Sheet 1 of 2						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11



GC 30-2



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

### BOREHOLE LOG

BOREHOLE NO: **BH11-13B**  
 SURFACE ELEVATION: **439.48 m**

SLR CONSULTING (CANADA) LTD.


DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses	WATER LEVEL		
					MSW - Municipal solid waste				

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Core Sample**  
 DRILL DATE: **May 4, 2011**  
 LOGGED BY: **JN**  
 DRILLER NAME: **Beck**

Notes:  SONIC CORE SAMPLE

GL 30-3

SLR 		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164		BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.				BOREHOLE NO: BH11-13C		SURFACE ELEVATION: 439.40 m				
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses				
-1					Ground Surface				stickup, jplug	440
0					<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (glass, metal, plastic), loose, brown, dry					439
1			1 10							438
2					<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes plastic and wood). Clay is firm, high plasticity, odour, grey, moist					437
3										436
4			2 100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, trace gypsum crystals, brown, moist					435
5		BH11-13C-1								434
6										433
7		BH11-13C-2		3 100						432
8		BH11-13C-3			- becoming grey at 7 m - 10 cm thick wet, fine sand lens at 7.5 m - concretion at 8.2 m - 10 cm thick fine sand lens at 8.3 m				bentonite seal	431
9										430
10				4 100	- concretion at 10.1 m					429
11		BH11-13C-4			<b>FAT CLAY (native)</b> trace sand, soft, grey, moist					428
12										427
13		BH11-13C-5		5 100	<b>silty SAND</b> trace clay, trace gravel, loose, grey, wet	GSA				426
14		BH11-13C-6			<b>FAT CLAY</b> soft, laminated, grey, moist					425
15										424
16				6 100					silica sand	423
17		BH11-13C-7			- 1 mm thick fine sand lens at 17.1 m - coarse sand lens with silt and gravel from 17.5 to 17.7 m					422
					End of borehole at 17.7 m					

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample      Notes:  SONIC CORE SAMPLE

DRILL DATE: May 4, 2011      LOGGED BY: JN      DRILLER NAME: Beck

Sheet 1 of 2

GL30-3

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG				
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH11-13C SURFACE ELEVATION: 439.40 m				
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses			
					<p>Well Completion Details: Screened interval from 15.1 m to 16.0 m below surface Elevation at top of casing (TOC) = 440.790 m</p> <p>Groundwater Information: Depth to groundwater from TOC = 3.16 m (June 15, 2011)</p> <p>(1) - Water added during drilling from surface to 17.7 m</p> <p>GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste</p>				

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 4, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

GC31-1

SLR		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG				
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH11-18A1 SURFACE ELEVATION: 439.37 m				
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses			
0					Ground Surface			stickup, jplug	440
0-1			1 50	Unconsolidated ORGANIC MATTER	(wood pieces, grading to chips and sawdust), trace garbage (metal), loose, brown, moist				439
1-3				Interbedded CLAY AND GARBAGE (MSW)	Clay is firm, odour, dark grey, moist				438
3-4			2 100					GW = 2.04 mbg (June 15, 2011)	437
4-5				FAT CLAY (reworked soil, fill)	laminated, firm, trace gypsum crystals, brown, moist			bentonite seal	436
5-6		BH11-18A1-1							435
6-7		BH11-18A1-2							434
7-8		BH11-18A1-3							433
8-9		BH11-18A1-4	3 100		- large glass debris 7.2 to 8 m			silica sand	432
9-10		BH11-18A1-5							431
10-11		BH11-18A1-6			LEAN CLAY (native)				430
11-12					trace sand, soft, grey, wet				429
12-13					End of borehole at 8.8 m				428
13-14					Well Completion Details: Screened interval from 6.9 m to 8.4 m below surface Elevation at top of casing (TOC) = 440.243 m				427
14-15					Groundwater Information: Depth to groundwater from TOC = 2.91 m (June 15, 2011)				426
15-16					(1) - Water added during drilling from surface to 8.8 m				425
16-17					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste				424

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 18, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

GL312



CLIENT: City of Kelowna  
 PROJECT: Glenmore Landfill - Phase 3  
 ADDRESS: 2105 Glenmore Road North, Kelowna, BC  
 SLR JOB NO: 219.05164

**BOREHOLE LOG**

BOREHOLE NO: BH11-18B1  
 SURFACE ELEVATION: 439.17 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses	WATER LEVEL		
0					Ground Surface			stickup, jplug	440
0.5			1 75		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (plastic), loose, brown, moist				439
1.5					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Garbage includes asphalt. Clay is firm, odour, grey, moist				438
2.5			2 100		- wet from 4.3 to 4.9 m			GW = 1.67 mbg (June 15, 2011)	437
4.5					<b>FAT CLAY (reworked soil, fill)</b> laminated, firm, trace gypsum crystals, brown, moist			bentonite seal	436
6.5			3 100		- large glass debris at 6.8 to 7.8 m - wet from 7.0 to 7.6 m				435
8.5					<b>LEAN CLAY (native)</b> trace sand, soft, grey, moist				434
10.5		BH11-18B-1	4 100					silica sand	433
11.5		BH11-18B-2			<b>SILT with sand</b> some clay, loose, grey, wet				432
12.5		BH11-18B-3							431
13.5		BH11-18B-4	5 100						430
14.6					End of borehole at 14.6 m				429
					Well Completion Details: Screened interval from 10.6 m to 11.5 m below surface Elevation at top of casing (TOC) = 440.100 m				428
					Groundwater Information: Depth to groundwater from TOC = 2.60 m (June 15, 2011)				427
					(1) - Water added during drilling from surface to 14.6 m				426
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste				425

SLR CANADA V5.2, 219.05164, CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample      Notes:  SONIC CORE SAMPLE

DRILL DATE: May 10, 2011      LOGGED BY: JN  
 DRILLER NAME: Beck

Sheet 1 of 1



GL31-3

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH11-18C SURFACE ELEVATION: 439.53 m						
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	440
0-1			1 80		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace cobbles, trace garbage (cloth, metal, plastic), loose, brown, moist						439
1-2											438
2-3					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, dark grey, moist						437
3-4			2 90								436
4-5					- sand and gravel lens at 4.9 to 5 m - blue colour at 5.2 to 5.5 m						435
5-6					<b>FAT CLAY (reworked soil, fill)</b> laminated, firm, brown, moist						434
6-7											433
7-8			3 100		- large glass debris from 7.2 to 7.8 m - 2 mm thick fine sand lens at 7.3 m - wet from 7.5 to 7.8 m					bentonite seal	432
8-9					<b>LEAN CLAY (native)</b> trace sand, soft, grey, moist - wet and very soft from 8.8 to 10.5						431
9-10											430
10-11			4 100		<b>sandy SILT</b> some clay, soft, grey, moist						429
11-12											428
12-13					<b>LEAN CLAY</b> trace sand, soft, grey, moist - wet from 12.6 to 12.9 m						427
13-14		BH11-18C-1				GSA, Att, M					426
14-15		BH11-18C-2	5 100		<b>SILT</b> some fine sand, laminated, soft, grey, moist						425
15					- increased medium grained sand at 15.2 m					silica sand	425
					End of borehole at 15.3 m						
					Well Completion Details: Screened interval from 14.3 m to 15.3 m below surface Elevation at top of casing (TOC) = 440.379 m						
					Groundwater Information: Depth to groundwater from TOC = 2.91 m (June 15, 2011)						
					(1) - Water added during drilling from surface to 15.3 m GSA - grain size analysis M - moisture content Att - Atterberg limits						
DRILLING METHOD: Core Sample					Notes: <input type="checkbox"/> SONIC CORE SAMPLE						
DRILL DATE: May 10, 2011					LOGGED BY: JN DRILLER NAME: Beck						
Sheet 1 of 2											

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

GC313



CLIENT: City of Kelowna  
 PROJECT: Glenmore Landfill - Phase 3  
 ADDRESS: 2105 Glenmore Road North, Kelowna, BC  
 SLR JOB NO: 219.05164

**BOREHOLE LOG**

BOREHOLE NO: BH11-18C  
 SURFACE ELEVATION: 439.53 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
					MSW - Municipal solid waste						

SLR CANADA V5.2. 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 10, 2011

Notes:  SONIC CORE SAMPLE  
 LOGGED BY: JN  
 DRILLER NAME: Beck

GL32-1

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164		BOREHOLE LOG				
SLR CONSULTING (CANADA) LTD.				BOREHOLE NO: BH11-21A1		SURFACE ELEVATION: 438.06 m		
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		
						Laboratory Analyses	WELL COMPLETION WATER LEVEL	WELL COMPLETION NOTES
0					Ground Surface		stickup, jplug	438
0 - 1			1 55	Unconsolidated ORGANIC MATTER (wood pieces, grading to chips and sawdust), loose, brown, moist			GW = 0.73 mbg (June 15, 2011)	437
1 - 2				Interbedded CLAY AND GARBAGE (MSW) Garbage includes plywood and plastic. Some sand, clay is firm, odour, dark grey, moist				436
2 - 3				- blue colour from 2.4 to 3.3 m			bentonite seal	435
3 - 4			2 100	FAT CLAY (reworked soil, fill) laminated, firm, brown, moist				434
4 - 5				- gypsum crystals from 4.0 to 4.3 m				433
5 - 6				FAT CLAY (native) laminated, soft, grey, moist			silica sand	432
6 - 7		BH11-21A1-1		- fine sand lenses (approx. 1 cm thick) from 5.5 to 6.1 m				431
7 - 8		BH11-21A1-2	3 100	LEAN CLAY soft, grey, moist				430
8 - 8.5				- wet from 7.2 to 7.9 m				
End of borehole at 8.5 m					Well Completion Details: Screened interval from 4.6 m to 6.1 m below surface Elevation at top of casing (TOC) = 438.952 m			
Groundwater Information: Depth to groundwater from TOC = 1.62 m (June 15, 2011)					(1) - Water added during drilling from surface to 8.5 m			
GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste								


SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

GL 31-2

SLR CONSULTING (CANADA) LTD.				CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164		BOREHOLE LOG					
				BOREHOLE NO: BH11-21B		SURFACE ELEVATION: 437.63 m					
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	438
0.12					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Garbage includes plywood, styrofoam, and plastic. Clay is firm, odour, grey, moist					GW = 0.12 mbg (June 15, 2011)	437
1			1 50								436
2.4					- blue colour from 2.4 to 3.0 m						435
3					<b>FAT CLAY (reworked soil, fill)</b> laminated, firm, brown, moist - gypsum crystals from 3.1 to 3.6 m						434
4			2 100							bentonite seal	433
5					<b>FAT CLAY (native)</b> soft, grey, moist - wet and very soft from 4.7 to 5.5 m and 5.8 to 6.4 m						432
7					<b>LEAN CLAY</b> soft, fine sand lenses throughout, grey, moist						431
8			3 100								430
8.1		BH11-21B-1			<b>silty SAND</b> trace clay, loose, grey, moist						429
8.8					No recovery from 8.8 to 9.4 m						
9.4					End of borehole at 9.4 m						
<p>Well Completion Details: Screened interval from 8.1 m to 9.0 m below surface Elevation at top of casing (TOC) = 438.627 m</p> <p>Groundwater Information: Depth to groundwater from TOC = 1.12 m (June 15, 2011)</p> <p>(1) - Water added during drilling from surface to 9.4 m</p> <p>GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste</p>											
<p>DRILLING METHOD: Core Sample</p>						<p>Notes: <input type="checkbox"/> SONIC CORE SAMPLE</p>					
<p>DRILL DATE: May 11, 2011</p>						<p>LOGGED BY: JN DRILLER NAME: Beck</p>			<p>Sheet 1 of 1</p>		

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

BC32-3

SLR 		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164		BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.				BOREHOLE NO: BH11-21C1		SURFACE ELEVATION: 437.60 m				
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses				
0					Ground Surface				stickup, jplug	438
0					Interbedded CLAY AND GARBAGE (MSW) Garbage includes plywood and rocks. Clay is firm, odour, grey, moist				GW = 0.06 mbg (June 15, 2011)	437
1			1 50							436
2					- blue colour from 2.4 to 3.0 m					435
3					FAT CLAY (reworked soil, fill) laminated, firm, brown, moist - gypsum crystals from 3.0 to 4.0 m					434
4			2 100							433
5					FAT CLAY (native) soft, grey, wet				bentonite seal	432
6					LEAN CLAY trace sand, soft to very soft, grey, moist					431
7										430
8			3 100		- 5 cm thick sand lens at 7.0 m - 7 cm thick fine sand lens at 8.1 m - wet from 7.3 to 7.5 m					429
9					silty SAND trace clay, loose, grey, moist					428
9.9		BH11-21C-1			FAT CLAY laminated, soft, grey, moist					428
10					silty SAND trace clay, loose, grey, moist					427
10.5		BH11-21C-2	4 100		- 5 cm (approx.) thick clay lens at 9.9, 10.5, and 10.8 m - wet from 10.5 to 10.7 m	GSA			silica sand	427
11										426
End of borehole at 11.9 m										
Well Completion Details: Screened interval from 9.9 m to 10.9 m below surface Elevation at top of casing (TOC) = 438.635 m										
Groundwater Information: Depth to groundwater from TOC = 1.10 m (June 15, 2011)										
(1) - Water added during drilling from surface to 14.6 m										
GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste										
DRILLING METHOD: Core Sample					Notes: <input type="checkbox"/> SONIC CORE SAMPLE					
DRILL DATE: May 12, 2011					LOGGED BY: JN DRILLER NAME: Beck		Sheet 1 of 1			

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11





GL33-2

SLR		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG				
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH11-22B SURFACE ELEVATION: 439.47 m				
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses			
0					Ground Surface			stickup, jplug	440
0-1			1 80	Unconsolidated ORGANIC MATTER	(wood pieces, grading to chips and sawdust), some garbage, trace gravel, loose, brown, moist				439
1-3			2 100	Interbedded CLAY AND GARBAGE (MSW)	Garbage includes plywood and plastic. Some sand, clay is firm, odour, brown, moist - clay is black from 4.3 to 5.5 m			GW = 1.80 mbg (June 15, 2011)	438
3-5			3 100	FAT CLAY (reworked soil, fill)	soft, laminated, grey, moist - concretions at 5.8 m and 5.9 m - wet and increased silt from 5.8 to 5.9 m			bentonite seal	437
5-8			4 100	silty SAND with gravel (suspect till)	trace clay, sand is medium to coarse, loose, grey, wet - dense below 8.8 m - brown with green stripes from 8.8 to 11.0 m				436
8-9				Boulders	volcanic, soft, green, dry				435
9-10		BH11-22B-1							434
10-11		BH11-22B-2							433
11-11.6					End of borehole at 11.6 m				432
<p>Well Completion Details: Screened interval from 9.0 m to 10.5 m below surface Elevation at top of casing (TOC) = 440.489 m</p> <p>Groundwater Information: Depth to groundwater from TOC = 2.82 m (June 15, 2011)</p> <p>(1) - Water added during drilling from surface to 11.6 m</p> <p>GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste</p>									
<p>DRILLING METHOD: Core Sample</p> <p>DRILL DATE: May 13, 2011</p> <p>LOGGED BY: EM DRILLER NAME: Beck</p>						<p>Notes: <input type="checkbox"/> SONIC CORE SAMPLE</p>		<p>Sheet 1 of 1</p>	

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

GL333



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-22C**  
 SURFACE ELEVATION: **439.45 m**

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
-1										stickup, jplug	440
0					Ground Surface						
1			1 80		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), some garbage (styrofoam, asphalt, plastic), some sand, some gravel, loose, brown, moist						439
2											438
3					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Garbage includes plastic, carpet, wire. Clay is firm, odour, brown, moist - some sand and gravel from 3.0 to 3.6 m						437
4			2 50								436
5					- clay is black from 5.2 to 5.5 m						435
6					<b>FAT CLAY (reworked soil, fill)</b> soft, laminated, grey, moist						434
7			3 100		- very soft and wet at 6.7 m, 7.5 m, and 7.6 m (each section is approximately 5 cm thick)					bentonite seal	433
8					- fine sand lens at 7.8 m						432
9		BH11-22C-1			<b>silty SAND with gravel (suspect till)</b> trace gravel, sand is medium to coarse, loose, grey, wet - dense below 8.5 m - green layers at 9.3 m						431
10		BH11-22C-2	4 100								430
11		BH11-22C-3			<b>BOULDERS</b> volcanic, soft, green, dry						429
12		BH11-22C-4			<b>silty SAND with gravel (suspect till)</b> sand is medium to coarse, loose, green and brown, moist - orange mottles from 12.2 to 12.5 m						428
13		BH11-22C-5	5 100		<b>volcanic BEDROCK</b> weak, white with green layers, dry						427
14											426
					End of borehole at 14.6 m						425

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample      Notes:  SONIC CORE SAMPLE

DRILL DATE: May 13, 2011      LOGGED BY: EM      DRILLER NAME: Beck

Sheet 1 of 1

GL34-1



CLIENT: City of Kelowna  
 PROJECT: Glenmore Landfill - Phase 3  
 ADDRESS: 2105 Glenmore Road North, Kelowna, BC  
 SLR JOB NO: 219.05164

**BOREHOLE LOG**

BOREHOLE NO: BH11-26A

SURFACE ELEVATION: 439.17 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	439
0 - 1			1 60		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), loose, brown, moist						438
1 - 2					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is soft, odour, grey, moist					GW = 1.65 mbg (June 15, 2011)	437
2 - 3					- organic matter (roots, twigs) from 3.0 to 3.6 m					bentonite seal	436
3 - 4											435
4 - 5		BH11-26A-1	2 100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist - gypsum crystals from 4.5 to 5.5 m						434
5 - 6											433
6 - 7		BH11-26A-2	3 100		<b>FAT CLAY (native)</b> trace sand, soft, laminated, grey, moist - wet from 6.8 to 7.3 m - 7 cm thick fine sand lenses at 7.0 m and 7.2 m					silica sand	432
7 - 8		BH11-26A-3									431
8 - 8.5					- wet at 8.4 m End of borehole at 8.5 m						
<p>Well Completion Details:          Screened interval from 6.0 m to 7.5 m below surface          Elevation at top of casing (TOC) = 440.065 m</p> <p>Groundwater Information:          Depth to groundwater from TOC = 2.55 m (June 15, 2011)</p> <p>(1) - Water added during drilling from surface to 8.5 m</p> <p>GSA - grain size analysis          M - moisture content          Att - Atterberg limits          MSW - Municipal solid waste</p>						GSA, Att, M					

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 18, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

CL34-2

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164		BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.				BOREHOLE NO: BH11-26B		SURFACE ELEVATION: 439.23 m				
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses				
0					Ground Surface				stickup, jplug	439
0 - 2.12			1 40		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), loose, brown, moist				GW = 1.28 mbg (June 15, 2011)	438
2.12 - 3.6					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, grey, moist - blue-grey colour from 3 to 3.6 m					437
3.6 - 5.2			2 100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist - gypsum crystals from 3.9 to 5.2 m					436
5.2 - 6.4										435
6.4 - 7.0					- wet from 6.4 to 6.6 m				bentonite seal	434
7.0 - 8.5			3 100		<b>FAT CLAY (native)</b> trace sand, soft, laminated, grey, moist - wet from 7 to 7.5 m - 10 cm thick fine sand lens at 7.3 m					433
8.5 - 10.1					- very soft from 8.5 to 10.1 m - 2 cm thick fine sand lens at 9.1 m					432
10.1 - 10.7		BH11-26B-1								431
10.7 - 11.6		BH11-26B-2								430
11.6 - 10.2		BH11-26B-3								429
10.2 - 11.3		BH11-26B-4								428
11.3 - 11.9			4 100		<b>silty SAND</b> trace clay, sand is fine to medium, loose, grey, moist - clay layers at 10.2 and 10.8 m (approx. 10 cm thick) - wet from 10.4 to 10.8 m and 11.3 to 11.9 m	GSA			silica sand	428
11.9 - 12.2						GSA				
					End of borehole at 12.2 m					
					Well Completion Details: Screened interval from 10.7 m to 11.6 m below surface Elevation at top of casing (TOC) = 440.073 m					
					Groundwater Information: Depth to groundwater from TOC = 2.12 m (June 15, 2011)					
					(1) - Water added during drilling from surface to 12.2 m					
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste					
DRILLING METHOD: Core Sample					Notes: <input type="checkbox"/> SONIC CORE SAMPLE					
DRILL DATE: May 18, 2011					LOGGED BY: JN DRILLER NAME: Beck					
					Sheet 1 of 1					

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11



GL343

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164		BOREHOLE LOG						
SLR				BOREHOLE NO: BH11-26C SURFACE ELEVATION: 439.26 m						
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses				
0					Ground Surface				stickup, jplug	440
0			1 50		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), garbage includes foam and plastic, loose, brown, moist					439
1					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, grey, moist					438
2									GW = 1.28 mbg (June 15, 2011)	437
2			2 75		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist - gypsum crystals from 4.0 to 5.3 m					436
3					- soft at 5.8 m					435
4					<b>FAT CLAY (native)</b> soft, laminated, grey, moist - wet at 6.7 m - 10 cm thick fine sand lens at 7.5 m				bentonite seal	434
5										433
6										432
7			3 100		<b>FAT CLAY (native)</b> soft, laminated, grey, moist - wet at 6.7 m - 10 cm thick fine sand lens at 7.5 m					431
8										430
9					- wet from 8.8 to 9.8 m - fine sandy silt lenses at 8.9 and 10.4 m (approx. 2 - 3 cm thick)					429
10			4 100		<b>silty SAND</b> trace clay, soft, grey, moist - 10 cm thick clay layer at 10.7 m (grey, firm, laminated) - wet from 10.8 to 11.1 m and 11.6 to 12.5 m					428
11										427
12										426
13		BH11-26C-1								426
13		BH11-26C-2			<b>LEAN CLAY</b> trace sand, firm, laminated, grey, moist - wet from 13.4 to 13.7 m	GSA, Att, M				425
14		BH11-26C-3			<b>FAT CLAY</b> trace sand, firm, laminated, grey, moist - concretion at 14.0 m	GSA, Att, M			silica sand	425
14		BH11-26C-4	5 100							424
15					End of borehole at 15.3 m					
Well Completion Details: Screened interval from 13.6 m to 14.5 m below surface Elevation at top of casing (TOC) = 440.158 m										
Groundwater Information: Depth to groundwater from TOC = 2.17 m (June 15, 2011)										
(1) - Water added during drilling from surface to 15.3 m										
GSA - grain size analysis										
DRILLING METHOD: Core Sample				Notes: <input checked="" type="checkbox"/> SONIC CORE SAMPLE						
DRILL DATE: May 19, 2011				LOGGED BY: JN DRILLER NAME: Beck						
Sheet 1 of 2										

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

GL34-3



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-26C**  
 SURFACE ELEVATION: 439.26 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
					M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 19, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

GL 35-1

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164		BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.				BOREHOLE NO: BH11-31A SURFACE ELEVATION: 438.13 m						
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses				
0					Ground Surface				stickup, jplug	438
0			1 70		<b>sandy GRAVEL</b> some cobbles, loose, grey, moist				GW = 0.60 mbg (June 15, 2011)	437
1					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, laminated, odour. Garbage includes plastic, grey, moist					436
2					- black from 1.8 to 2.4 m					435
3									bentonite seal	434
4		BH11-31A-1	2 100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist					433
5		BH11-31A-2			- mottles from 3.5 to 3.8 m					432
6		BH11-31A-3			- fine to medium sand lenses at 3.8 m, 4.6 m, and 5.3 m					431
7		BH11-31A-4			- soft at 5.5 m					430
8		BH11-31A-5	3 100		<b>silty SAND</b> some clay, sand is medium, soft, grey, wet				silica sand	430
9		BH11-31A-6			<b>LEAN CLAY</b> soft, laminated, grey, moist					
		BH11-31A-7			- wet from 7.9 to 8.4 m - 1 mm thick fine sandy silt lenses throughout from 7.9 m to 8.8 m - glass debris at 8.1 m - 10 cm thick fine sand lens at 9 m					
					End of borehole at 9.1 m					
Well Completion Details: Screened interval from 6.1 m to 7.6 m below surface Elevation at top of casing (TOC) = 438.917 m										
Groundwater Information: Depth to groundwater from TOC = 1.40 m (June 15, 2011)										
(1) - Water added during drilling from surface to 9.1 m										
GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste										
DRILLING METHOD: Core Sample						Notes: <input type="checkbox"/> SONIC CORE SAMPLE				
DRILL DATE: May 25, 2011						LOGGED BY: JN DRILLER NAME: Beck				
						Sheet 1 of 1				

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

GL35-2



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-31B**  
 SURFACE ELEVATION: **438.13 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	438
0.5			1 70	sandy GRAVEL some cobbles, loose, grey, moist	Interbedded CLAY AND GARBAGE (MSW) Clay is firm, laminated, odour, contains wood debris, brown, moist					GW = 0.18 mbg (June 15, 2011)	437
2.4					- grey from 2.4 to 3.6 m						436
3.6			2 100	FAT CLAY (reworked soil, fill) firm, laminated, brown, moist	- mottles from 3.6 to 4.0 m - glass debris at 4.3 and 5.4 m						434
4.3										bentonite seal	433
6.0			3 30	LEAN CLAY trace sand, soft, laminated, grey, moist							432
8.5					- fine silty sand lenses at 8.5 m, 11.1 m, and 12.1 m (3 - 15 cm thick)						431
10.6		BH11-31B-1									428
11.1		BH11-31B-2	4 100		- wet from 11.1 to 11.4 m					silica sand	427
12.2		BH11-31B-3									426
					End of borehole at 12.2 m						
					Well Completion Details: Screened interval from 10.6 m to 12.2 m below surface Elevation at top of casing (TOC) = 439.013 m						
					Groundwater Information: Depth to groundwater from TOC = 1.06 m (June 15, 2011)						
					(1) - Water added during drilling from surface to 12.2 m						
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 25, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

GL35-3

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG					
SLR CONSULTING (CANADA) LTD.					BOREHOLE NO: BH11-31C SURFACE ELEVATION: 438.40 m					
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA Laboratory Analyses	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
0					Ground Surface				stickup, jplug	439
0					<b>sandy GRAVEL</b> some cobbles, loose, grey, moist				GW = 0.47 mbg (June 15, 2011)	438
1			1 50		<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, laminated, odour, grey, moist					437
2										436
3										435
4			2 100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist - mottles from 3.6 to 4.1 m - glass debris at 4.4 and 5.3 m					434
5					- 2 mm thick fine sand lens at 5.3 m - no recovery from 5.5 to 8.5 m					433
6										432
7			3 0						bentonite seal	431
8										430
9					<b>LEAN CLAY</b> trace fine sand, laminated, very soft					429
10			4 75							428
11					- 2 mm thick fine sand lenses at 11.3 and 11.4 m					427
12		BH11-31C-1			<b>silty SAND with gravel (Till)</b> sand is fine to medium, trace clay, loose, grey, moist - sand becoming coarse at 11.8 m - wet from 12.2 to 12.8 m	GSA				426
13		BH11-31C-2								425
14		BH11-31C-3			- wet from 13.0 to 13.7 m	GSA				425
15		BH11-31C-4			- compact to dense below 13.7 m				silica sand	424
15		BH11-31C-5	5 100			GSA				424
					End of borehole at 15.2 m					
					Well Completion Details: Screened interval from 13.3 m to 14.8 m below surface Elevation at top of casing (TOC) = 439.245 m					
					Groundwater Information: Depth to groundwater from TOC = 1.32 m (June 15, 2011)					
					(1) - Water added during drilling from surface to 15.2 m GSA - grain size analysis M - moisture content Att - Atterberg limits					
DRILLING METHOD: Core Sample					Notes: <input type="checkbox"/> SONIC CORE SAMPLE					
DRILL DATE: May 25, 2011					LOGGED BY: JN DRILLER NAME: Beck					

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11



GC35-3



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-31C**  
 SURFACE ELEVATION: **438.40 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
					MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: **Core Sample**  
 DRILL DATE: **May 25, 2011**  
 LOGGED BY: **JN**  
 DRILLER NAME: **Beck**

Notes:  SONIC CORE SAMPLE

GL 36-1

SLR CONSULTING (CANADA) LTD.		CLIENT: City of Kelowna PROJECT: Glenmore Landfill - Phase 3 ADDRESS: 2105 Glenmore Road North, Kelowna, BC SLR JOB NO: 219.05164			BOREHOLE LOG						
SLR CONSULTING (CANADA) LTD.		SLR JOB NO: 219.05164			BOREHOLE NO: BH11- 3A		SURFACE ELEVATION: 439.15 m				
DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
-1										stickup, jplug	440
0					Ground Surface						439
1			1 40		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (shingles, wire), loose, brown, dry						438
2										GW = 1.55 mbg (June 15, 2011)	437
3		BH11-3A-1			<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes plastic and newspaper), soft, odour, grey/blue, moist					bentonite seal	436
4			2 100		<b>FAT CLAY (reworked soil, fill)</b> trace find sand, soft, brown, moist						435
5		BH11-3A-2									434
6		BH11-3A-3			<b>FAT CLAY (native)</b> trace fine sand, very soft, grey, wet						433
7			3 100		- 10 cm thick sand layer at 7.3 m					silica sand	432
8		BH11-3A-4			- 1 cm thick sand lens at 8.2 m	GSA, M, Att					431
9					End of borehole at 9.0 m						
					Well Completion Details: Screened interval from 5.5 m to 8.5 m below surface Elevation at top of casing (TOC) = 440.270 m  Groundwater Information: Depth to groundwater from TOC = 2.66 m (June 15, 2011)  (1) - Water added during drilling from surface to 9 m  GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample	Notes: <input type="checkbox"/> SONIC CORE SAMPLE
DRILL DATE: April 20, 2011	LOGGED BY: EM DRILLER NAME: Beck
Sheet 1 of 1	

GL36-2



CLIENT: City of Kelowna  
 PROJECT: Glenmore Landfill - Phase 3  
 ADDRESS: 2105 Glenmore Road North, Kelowna, BC  
 SLR JOB NO: 219.05164

**BOREHOLE LOG**

BOREHOLE NO: BH11- 3B  
 SURFACE ELEVATION: 439.22 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	440
0-1			1 50	Unconsolidated ORGANIC MATTER	(wood pieces, grading to chips and sawdust), trace garbage (shingles, wire), loose, brown, dry					GW = 0.99 mbg (June 15, 2011)	439
1-3			2 100	Interbedded CLAY AND GARBAGE (MSW)	(garbage includes plastic and newspaper), soft, odour, grey/blue, moist						438
3-5			3 100	FAT CLAY (reworked soil, fill)	trace fine sand, soft, brown, moist					bentonite seal	437
5-6				FAT CLAY (native)	trace fine sand, very soft, grey, wet						436
6-8			3 100		- increased fine sand from 7.3 - 7.6 m and 8.2 - 8.5 m						435
8-10			4 100								434
10-11				sandy SILT	sand is fine grained, loose, grey, wet						433
11-12		BH11-3B-1									432
12					End of borehole at 12.0 m						431
Well Completion Details:											430
Screened interval from 10.2 m to 11.7 m below surface											429
Elevation at top of casing (TOC) = 440.287 m											428
Groundwater Information:											
Depth to groundwater from TOC = 2.06 m (June 15, 2011)											
(1) - Water added during drilling from surface to 12 m											
GSA - grain size analysis											
M - moisture content											
Att - Atterberg limits											
MSW - Municipal solid waste											

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: April 20, 2011  
 LOGGED BY: EM  
 DRILLER NAME: Beck

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

CL 36-3



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11- 3C**  
 SURFACE ELEVATION: **439.23 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Ground Surface					stickup, jplug	440
0.5			1 50	Unconsolidated ORGANIC MATTER	(wood pieces, grading to chips and sawdust), trace garbage (plastic), loose, brown, moist					GW = 0.90 mbg (June 15, 2011)	439
1.5				Interbedded CLAY AND GARBAGE (MSW)	(garbage includes plastic and newspaper), firm, laminated. Fine sand lenses throughout, brown, moist - wet, grey, and soft at 2.0 - 2.3 m and 3.3 - 4.2 m						438
2.5			2 100	FAT CLAY (reworked soil, fill)	trace fine sand, laminated, soft, brown, moist						437
3.5				FAT CLAY (native)	trace fine sand, soft, grey, wet					bentonite seal	436
4.5					- increased fine sand from 7.3 - 7.6 m and 8.1 - 9.8 m						435
5.5			3 100								434
6.5											433
7.5			4 100								432
8.5											431
9.5											430
10.5											429
11.5											428
12.5		BH11-3C-1					GSA				427
13.5		BH11-3C-2					GSA			silica sand	426
14.5		BH11-3C-3	5 100				GSA, Att, M				425
14.9					End of borehole at 14.9 m						
<p>Well Completion Details:          Screened interval from 12.7 m to 13.6 m below surface          Elevation at top of casing (TOC) = 440.183 m</p> <p>Groundwater Information:          Depth to groundwater from TOC = 1.85 m (June 15, 2011)</p> <p>(1) - Water added during drilling from surface to 14.9 m          GSA - grain size analysis          M - moisture content          Att - Atterberg limits          MSW - Municipal solid waste</p>											

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 21, 2011  
 LOGGED BY: EM/JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

6L37



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-11**

SURFACE ELEVATION: **439.31 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
0					Ground Surface									440
0					<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage, loose, brown, moist								stickup, jplug	439
1													bentonite pellets to 1.2 m	438
2													silica sand	437
2.23													GW = 2.23 mbg (October 3, 2012)	437
3					<b>interbedded medium grained SAND, CLAY AND GARBAGE (MSW)</b> black/grey, moist to wet - loose, odourous, black, wet from 2.7 to 4.9 m									436
5		BH12-11-1			<b>CLAY</b> poor recovery, silty layers with wood chunks, soft to firm, brown, moist to wet									434
7.9					End of borehole at 7.9 m									432
<p>Well Completion Details:          Screened interval from 1.8 m to 7.9 m below surface          Elevation at top of casing (TOC) = 440.289 m</p> <p>Groundwater Information:          Depth to groundwater from TOC = 3.21 m (October 3, 2012)</p> <p>(1) - Water added during drilling from surface to 7.9 m          GSA - grain size analysis          M - moisture content          Att - Atterberg limits          MSW - Municipal solid waste</p>														

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample  
 DRILL DATE: September 27, 2012  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

Notes:  SONIC CORE SAMPLE



GL38



CLIENT: City of Kelowna  
 PROJECT: Glenmore Landfill - Phase 3  
 ADDRESS: 2105 Glenmore Road North, Kelowna, BC  
 SLR JOB NO: 219.05164

**BOREHOLE LOG**

BOREHOLE NO: BH12-10

SURFACE ELEVATION: 439.27 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
0					Ground Surface									440
0.5					Unconsolidated ORGANIC MATTER (wood pieces, grading to chips and sawdust), trace garbage, loose, brown, moist									439
1.5					Interbedded silty CLAY AND GARBAGE (MSW) soft, grey, moist									438
2.5					- layer medium grained sand from 4.9 to 3.7 m - grey/black, odourous, compact, moist to wet									437
3.5					FAT CLAY (reworked soil, fill) soft, grey/blue, moist to wet									436
4.5	No samples				No Recovery to 7.9 m									435
5.5														434
6.5														433
7.5														432
<p>End of borehole at 7.9 m</p> <p>Well Completion Details:          Screened interval from 1.8 m to 7.9 m below surface          Elevation at top of casing (TOC) = 440.321 m</p> <p>Groundwater Information:          Depth to groundwater from TOC = 3.18 m (October 3, 2012)</p> <p>(1) - Water added during drilling from surface to 7.9 m          GSA - grain size analysis          M - moisture content          Att - Atterberg limits          MSW - Municipal solid waste</p>														

DRILLING METHOD: Core Sample

DRILL DATE: September 27, 2012

LOGGED BY: JN

DRILLER NAME: Mud Bay

Notes:

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

PROJECT No.: Glenmore Landfill

# RECORD OF BOREHOLE: P 2

SHEET 1 OF 1


LOCATION: See Figure 1

BORING DATE: Mar 3 2005

DATUM:

SAMPLER HAMMER, 140lbs.; DROP, 30in.

INCLINATION: -90°

DEPTH SCALE METRES	BORING METHOD	SOIL PROFILE		SAMPLES		DYNAMIC PENETRATION RESISTANCE, BLOWS/0.3m				HYDRAULIC CONDUCTIVITY, k, cm/s				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION  P 2		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	SHEAR STRENGTH				WATER CONTENT PERCENT					
								Cu, kPa		nat V. rem V.	+ Q- U	- O	Wp			W	Wi
0		GROUND SURFACE		0.00													
2	Foundex Explorations Borradler Simco 2800 120 mm dia. Mud Rotary	LANDFILL REFUSE (Paper, plastic, wood etc. and soil) (FILL)													Bentonite seal		
4																50 mm dia. PVC Screen	
6																	Pea gravel
8		End of BOREHOLE.		9.14											Landfill refuse		
10																	
12																	
14																	
16																	
18																	
20																	

BOREHOLE BOREHOLES.GPJ\_GLDR\_CAN.GDT\_10/1/06

DEPTH SCALE

1 : 100



LOGGED: RR

CHECKED: GTI

PROJECT: BASELINE GW QUALITY ASSESSMENT	CLIENT: WINSOME HILLS JOINT VENTURE	BOREHOLE NO: 06BH01
LOCATION: TUTT RANCH ON GLENMERE ROAD	CONTRACTOR: KAMLOOPS ENV. DRILLING LTD.	PROJECT NO: 808-8840400.001
KELOWNA, BC	EQUIPMENT: HOLLOW STEM AUGER	ELEVATION:
SAMPLE TYPE <input checked="" type="checkbox"/> GRAB <input checked="" type="checkbox"/> NO RECOVERY <input checked="" type="checkbox"/> SPT <input type="checkbox"/> A-CASING <input type="checkbox"/> SHELBY TUBE <input type="checkbox"/> CORE		
BACKFILL TYPE <input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND		

Depth(m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	HEAD SPACE VAPOUR (ppm)	STANDARD PENETRATION (N) ▲				WELL INSTALLATION	COMMENTS	Depth(ft)
						16	32	46	64			
0.0		TOPSOIL/silt, organics, grass roots, moist dark.								BENTONITE	0.0	
1.0		CLAY, stiff, low plasticity, damp, olive grey.									5.0	
3.0		- becomes wet and soft from 2.7-3.3m.		1A							10.0	
4.0		CLAY, stiff, damp.								SOLID PIPE	15.0	
5.0		SAND, trace silt, loose, wet, brown.		1B							20.0	
6.0		CLAY, soft, high plasticity, moist, light grey.								SLOUGH	25.0	
7.0		SAND, trace silt, loose, wet, brown.									30.0	
8.0		CLAY, soft, high plasticity, moist, greenish grey.									35.0	
9.0				1C						BENTONITE		
10.0												
11.0										SLOUGH		
12.0												

EBA Engineering Consultants Ltd. Kelowna, B.C.	LOGGED BY: LM	COMPLETION DEPTH: 19.5 m
	REVIEWED BY: RT	COMPLETE: 06/04/11
	Fig. No: 06BH01	Page 1 of 2

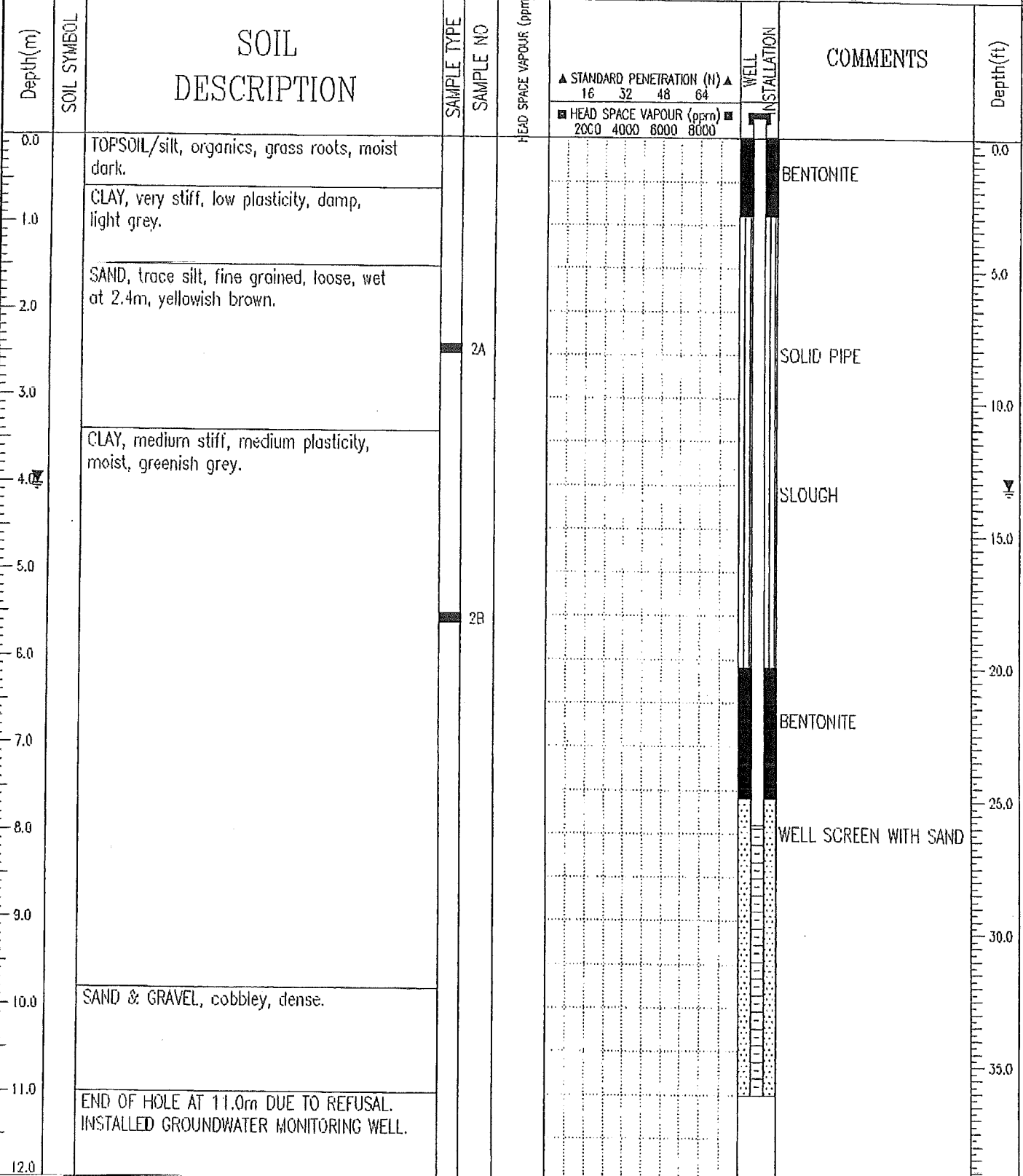
PROJECT: BASELINE GW QUALITY ASSESSMENT	CLIENT: WINSOME HILLS JOINT VENTURE	BOREHOLE NO: 06BH01
LOCATION: TUTT RANCH ON GLENMORE ROAD	CONTRACTOR: KAMLOOPS ENV. DRILLING LTD.	PROJECT NO: 808-8840400.001
KELOWNA, BC	EQUIPMENT: HOLLOW STEM AUGER	ELEVATION:
SAMPLE TYPE <input checked="" type="checkbox"/> GRAB <input type="checkbox"/> NO RECOVERY <input checked="" type="checkbox"/> SPT <input type="checkbox"/> A-CASING <input type="checkbox"/> SHELBY TUBE <input type="checkbox"/> CORE		
BACKFILL TYPE <input checked="" type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input checked="" type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND		

Depth(m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NO	HEAD SPACE VAPOUR (ppm)	STANDARD PENETRATION (N) ▲				WELL INSTALLATION	COMMENTS	Depth(ft)
						16	32	48	64			
12.0											40.0	
13.0											45.0	
14.0											50.0	
15.0											55.0	
16.0		SILT, trace sand, trace clay, wet, dark grey.									60.0	
17.0											65.0	
18.0		SAND, trace gravel, medium grained, dense, wet, grey.									70.0	
19.0											75.0	
20.0		SAND & GRAVEL (TILL), very dense.									80.0	
21.0		END OF HOLE AT 19.8m. INSTALLED GROUNDWATER MONITORING WELL.									85.0	
22.0											90.0	
23.0											95.0	
24.0											100.0	

EBA Engineering Consultants Ltd. Kelowna, B.C.	LOGGED BY: LM	COMPLETION DEPTH: 19.5 m
	REVIEWED BY: RT	COMPLETE: 06/04/11
	Fig. No: 06BH01	Page 2 of 2

PROJECT: BASELINE GW QUALITY ASSESSMENT	CLIENT: WINSOME HILLS JOINT VENTURE	BOREHOLE NO: 06BH02
LOCATION: TUTT RANCH ON GLENMORE ROAD	CONTRACTOR: KAMLOOPS ENV. DRILLING LTD.	PROJECT NO: 808-8840400.001
KELOWNA, BC	EQUIPMENT: HOLLOW STEM AUGER	ELEVATION:

SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB	<input type="checkbox"/> NO RECOVERY	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> A-CASING	<input type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE
BACKFILL TYPE	<input checked="" type="checkbox"/> BENTONITE	<input type="checkbox"/> PEA GRAVEL	<input type="checkbox"/> SLOUGH	<input type="checkbox"/> GROUT	<input type="checkbox"/> DRILL CUTTINGS	<input type="checkbox"/> SAND



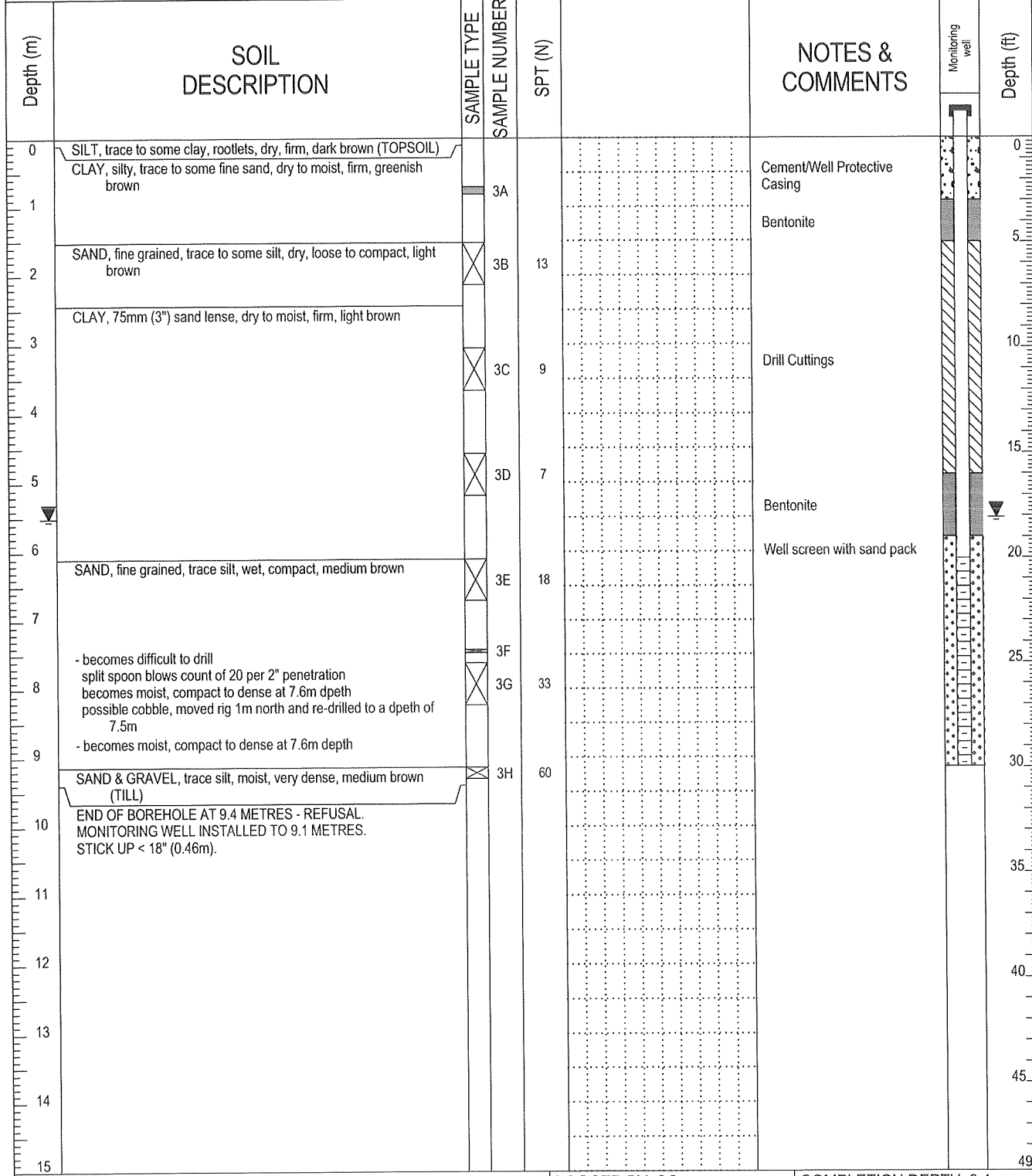
EBA Engineering Consultants Ltd.  
Kelowna, B.C.


LOGGED BY: LM  
REVIEWED BY: RT  
Fig. No: 06BH02

COMPLETION DEPTH: 11 m  
COMPLETE: 06/04/11



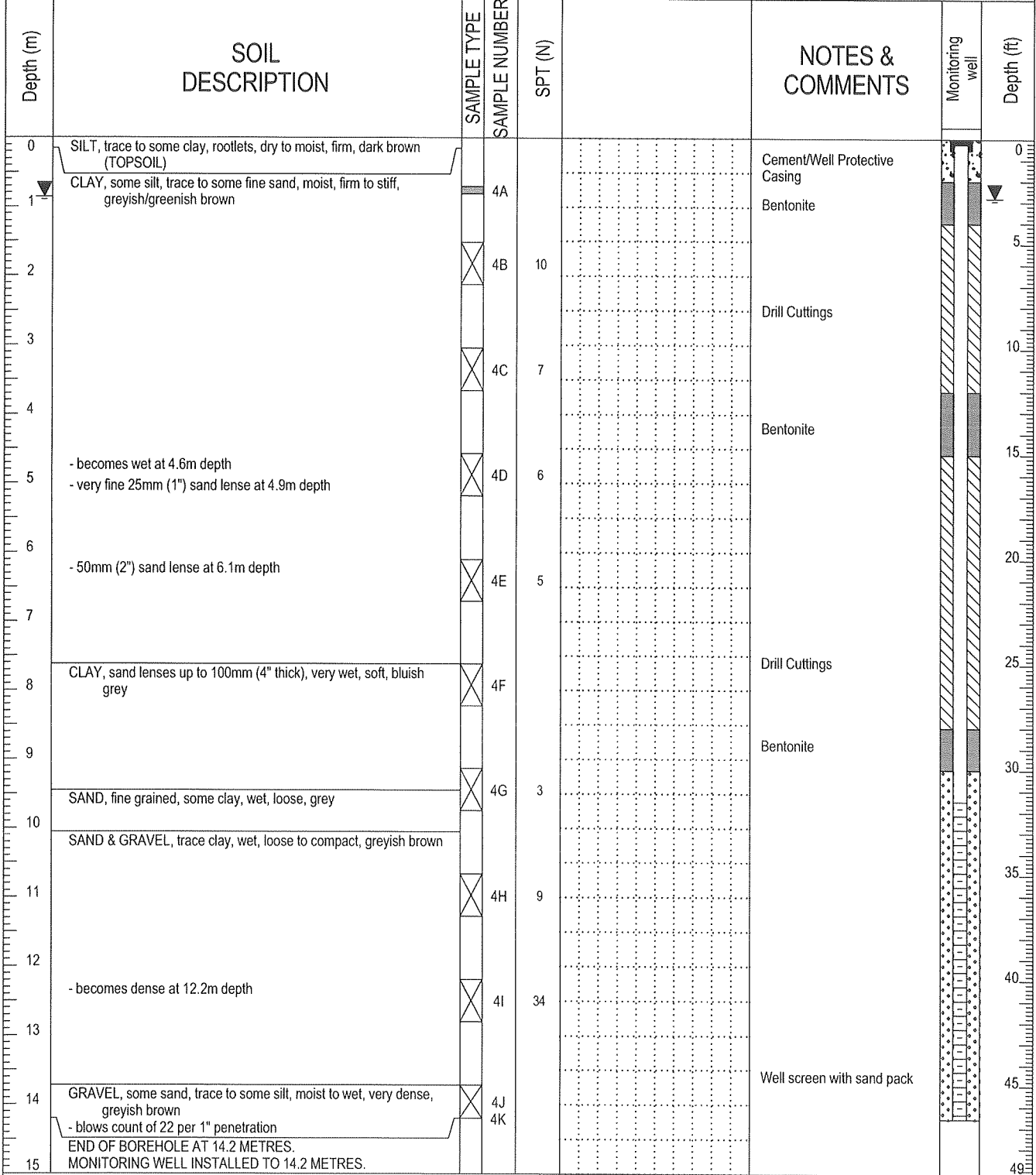
Project: Tutt Ranch - 2009 Drilling Program	Client: The University of British Columbia	PROJECT NO. - BOREHOLE NO.
Tutt Ranch on Glenmore Road	Contractor: KEL Drilling	K23101360.002 - 09BH03
Kelowna, BC	Drilling Method: Hollow Stem Auger	
<b>SAMPLE TYPE</b>	<input type="checkbox"/> DISTURBED <input checked="" type="checkbox"/> NO RECOVERY <input checked="" type="checkbox"/> SPT <input type="checkbox"/> A-CASING <input type="checkbox"/> SHELBY TUBE <input type="checkbox"/> CORE	
<b>BACKFILL TYPE</b>	<input type="checkbox"/> BENTONITE <input type="checkbox"/> PEA GRAVEL <input type="checkbox"/> SLOUGH <input type="checkbox"/> GROUT <input type="checkbox"/> DRILL CUTTINGS <input type="checkbox"/> SAND	



	LOGGED BY: CC	COMPLETION DEPTH: 9.4m
	REVIEWED BY: CC	COMPLETE: 6/22/2009
	DRAWING NO: 09BH03	Page 1 of 1

Project: Tutt Ranch - 2009 Drilling Program	Client: The University of British Columbia	PROJECT NO. - BOREHOLE NO.
Tutt Ranch on Glenmore Road	Contractor: KEL Drilling	K23101360.002 - 09BH04
Kelowna, BC	Drilling Method: Hollow Stem Auger	

SAMPLE TYPE	DISTURBED	NO RECOVERY	SPT	A-CASING	SHELBY TUBE	CORE
BACKFILL TYPE	BENTONITE	PEA GRAVEL	SLOUGH	GROUT	DRILL CUTTINGS	SAND



	LOGGED BY: CC	COMPLETION DEPTH: 14.2m
	REVIEWED BY: CC	COMPLETE: 6/22/2009
	DRAWING NO: 09BH04	Page 1 of 1

Project: Tutt Ranch - 2009 Drilling Program		Client: The University of British Columbia		PROJECT NO. - BOREHOLE NO.				
Tutt Ranch on Glenmore Road		Contractor: KEL Drilling		K23101360.002 - 09BH05				
Kelowna, BC		Drilling Method: Hollow Stem Auger						
<b>SAMPLE TYPE</b> DISTURBED NO RECOVERY SPT A-CASING SHELBY TUBE CORE								
<b>BACKFILL TYPE</b> BENTONITE PEA GRAVEL SLOUGH GROUT DRILL CUTTINGS SAND								
Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	NOTES & COMMENTS	Monitoring well	Monitoring well	Depth (ft)
0	SILT, trace sand, rootlets, moist, firm, dark brown		6A		Cement/Well Protective Casing			0
1	CLAY, some silt, trace to some sand, moist, firm, greenish brown - stiff at 0.8m depth		6B	12	Bentonite			5
2	Deep Well Groundwater Level at 0.126m Shallow Well Groundwater Level at 0.127m		6C	15				5
3	- becomes trace sand, thin sand lense, moist at 2.3m depth		6D	8	Drill Cuttings			10
4	- becomes moist to damp, firm at 3.0m depth		6E	8				10
5	- thin 1mm sand lense at 3.8m depth		6F	6	Bentonite			15
6	- two 1mm thin sand lenses, soft to firm at 4.6m depth		6G	7				15
7	CLAY & SILT, trace sand, moist to wet, soft, greenish brown		6H	7				20
8	- becomes wet at 5.8m depth		6I					20
9			6J	5				20
10			6K	4				25
11	- 12mm sand seam at 7.3m depth		6L	3				25
12	- becomes bluish green to grey at 7.6m depth		6M					30
13			6N	4				30
14	- becomes silty at 9.1m depth		6O		Bentonite			35
15	SAND, fine grained, some silt to silty, wet, loose to dense, grey		6P	16	Well screen with sand pack			35
16			6Q	7				40
17			6R	12	Drill Cuttings			40
18			6S					45
19			6T	12				45
20	CLAY, some silt, trace sand, moist to wet, soft, grey		6U	2	Bentonite			49



LOGGED BY: CC

REVIEWED BY: CC

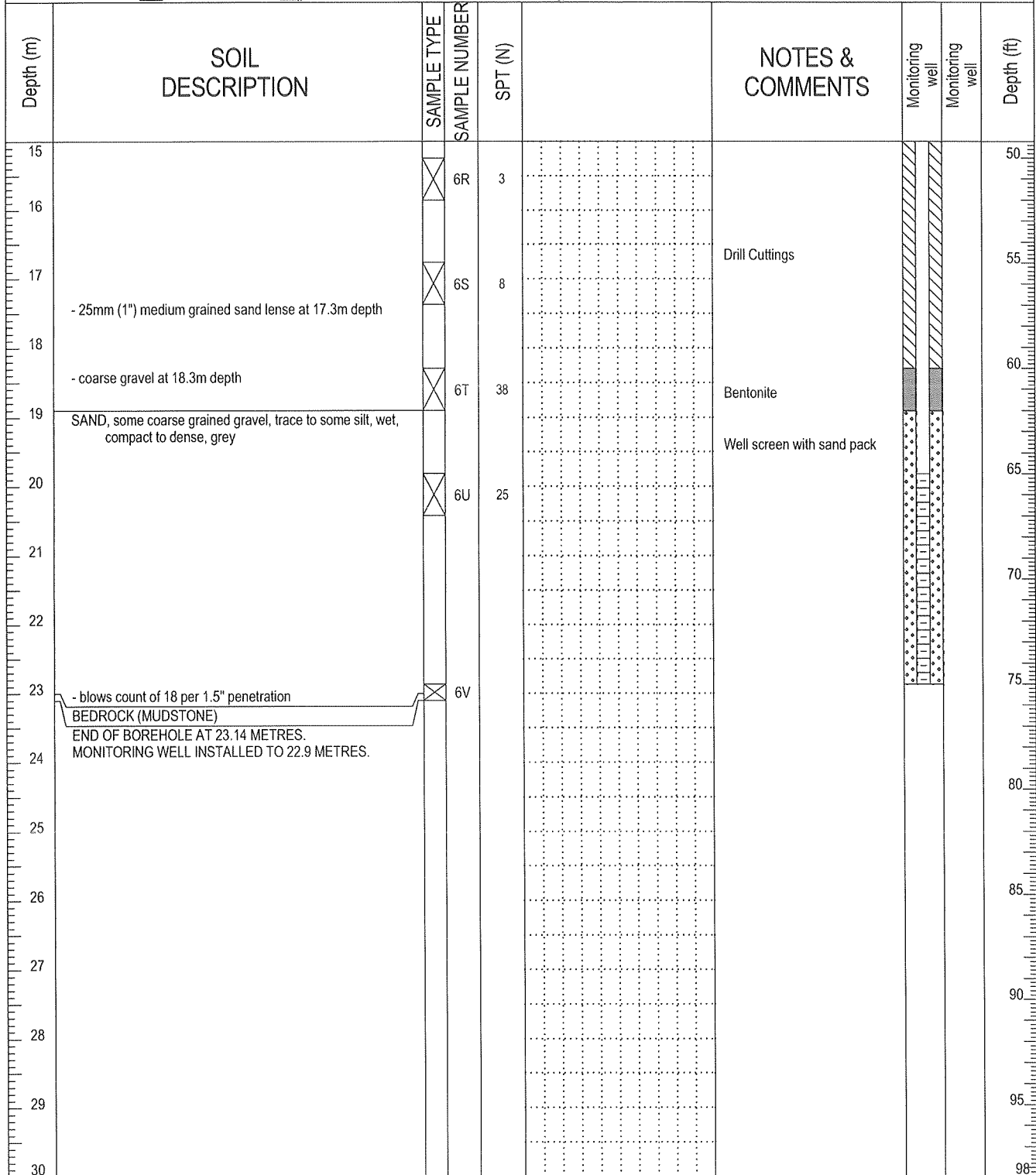
DRAWING NO: 09BH05

COMPLETION DEPTH: 23.1m

COMPLETE: 6/24/2009

Page 1 of 2

Project: Tutt Ranch - 2009 Drilling Program	Client: The University of British Columbia	PROJECT NO. - BOREHOLE NO.				
Tutt Ranch on Glenmore Road	Contractor: KEL Drilling	K23101360.002 - 09BH05				
Kelowna, BC	Drilling Method: Hollow Stem Auger					
SAMPLE TYPE	DISTURBED	NO RECOVERY	SPT	A-CASING	SHELBY TUBE	CORE
BACKFILL TYPE	BENTONITE	PEA GRAVEL	SLOUGH	GROUT	DRILL CUTTINGS	SAND



LOGGED BY: CC	COMPLETION DEPTH: 23.1m
REVIEWED BY: CC	COMPLETE: 6/24/2009
DRAWING NO: 09BH05	Page 2 of 2

Project: Tutt Ranch - 2009 Drilling Program	Client: The University of British Columbia	PROJECT NO. - BOREHOLE NO.
Tutt Ranch on Glenmore Road	Contractor: KEL Drilling	K23101360.002 - 09BH06
Kelowna, BC	Drilling Method: Hollow Stem Auger	

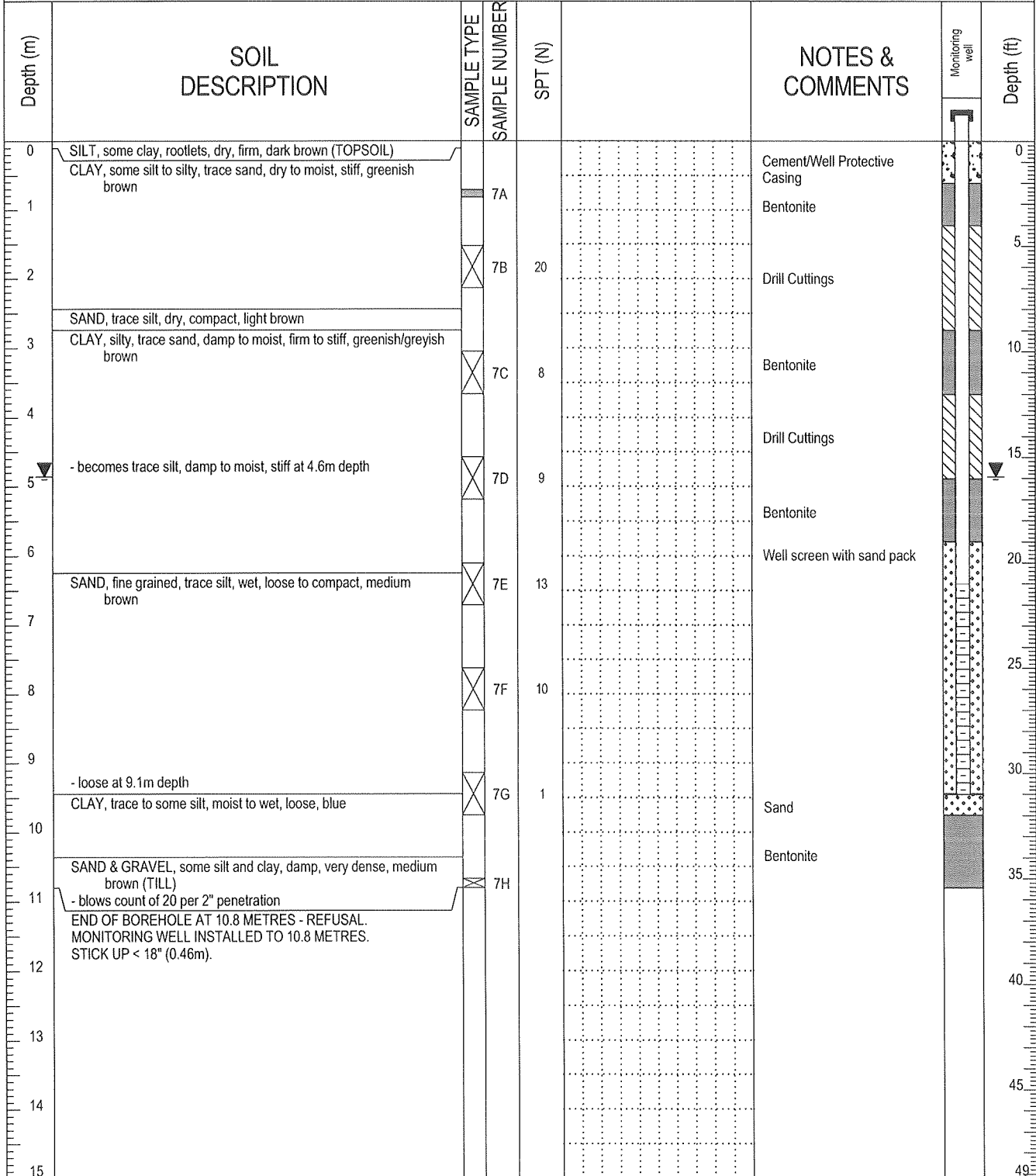
<b>SAMPLE TYPE</b>	DISTURBED	NO RECOVERY	SPT	A-CASING	SHELBY TUBE	CORE
<b>BACKFILL TYPE</b>	BENTONITE	PEA GRAVEL	SLOUGH	GROUT	DRILL CUTTINGS	SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	NOTES & COMMENTS	Monitoring well	Monitoring well	Depth (ft)
0	SILT, trace clay, rootlets, dry, firm, dark brown (TOPSOIL)		5A		Cement/Well Protective Casing			0
1	CLAY, silty, trace fine sand, dry, stiff, greenish brown Deep Well Groundwater Level at 0.659m Shallow Well Groundwater Level at 0.931m		5B	10	Bentonite			3
2			5C	9	Drill Cuttings			6
3	- becomes damp to moist, some silt with thin 1mm sand lense at 2.3m depth		5D	8	Bentonite			9
4	- 25mm thin silty sand lense at 3.2m depth - becomes wet at 3.8m depth		5E	6	Well screen with sand pack			12
5	CLAY, silty to some silt, trace fine sand seams, moist to wet, soft, greyish brown		5F	5	Drill Cuttings			15
6			5G	6				18
7	- becomes trace to some sand at 5.3m depth		5H	2	Bentonite			21
8	- sand seam at 5.8m depth		5I					24
9	SAND, fine grained, some silt to silty, wet, loose, grey		5J	2	Well screen with sand pack			27
10			5K	9				30
11	- becomes some silt, loose at 7.6m depth		5L	3	Drill Cuttings			33
12			5M	1				36
13	- becomes some silt to silty, some clay, coarse grained SAND at 9.0m depth		5N	9				39
14	- trace gravel at 9.8m depth		5O	32				42
15	BEDROCK (MUDSTONE) END OF BOREHOLE AT 10.4 METRES - REFUSAL ON BEDROCK (MUD STONE). MONITORING WELL INSTALLED TO 10.0 METRES.							45

	LOGGED BY: CC	COMPLETION DEPTH: 10.4m
	REVIEWED BY: CC	COMPLETE: 6/24/2009
	DRAWING NO: 09BH06	Page 1 of 1



Project: Tutt Ranch - 2009 Drilling Program	Client: The University of British Columbia	PROJECT NO. - BOREHOLE NO.				
Tutt Ranch on Glenmore Road	Contractor: KEL Drilling	K23101360.002 - 09BH07				
Kelowna, BC	Drilling Method: Hollow Stem Auger					
<b>SAMPLE TYPE</b>	<input type="checkbox"/> DISTURBED	<input type="checkbox"/> NO RECOVERY	<input checked="" type="checkbox"/> SPT	<input type="checkbox"/> A-CASING	<input type="checkbox"/> SHELBY TUBE	<input type="checkbox"/> CORE
<b>BACKFILL TYPE</b>	<input type="checkbox"/> BENTONITE	<input type="checkbox"/> PEA GRAVEL	<input type="checkbox"/> SLOUGH	<input type="checkbox"/> GROUT	<input type="checkbox"/> DRILL CUTTINGS	<input type="checkbox"/> SAND



LOGGED BY: CC	COMPLETION DEPTH: 10.8m
REVIEWED BY: CC	COMPLETE: 6/23/2009
DRAWING NO: 09BH07	Page 1 of 1



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **09BH01 (Decom)**

SURFACE ELEVATION:

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA	WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)
						Laboratory Analyses				
1					Monitoring well decommissioned August 26, 2011				concrete to 0.9 m	1.0
2						2.0				
3						3.0				
4						4.0				
5						5.0				
6						6.0				
7						7.0				
8						8.0				
9						9.0				
10						10.0				
11						11.0				
12						12.0				
13						13.0				
End of borehole at 13.7 m										
Groundwater Information: Depth to groundwater from TOC = 4.30 m (August 30, 2011)										

SLR CANADA V5.2: 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Solid Stem Auger Drilling

Notes:

DRILL DATE: August 26, 2011

LOGGED BY: EM  
 DRILLER NAME: Beck



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11- 1**  
 SURFACE ELEVATION: **439.28 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 100	Unconsolidated ORGANIC MATTER (wood pieces, grading to chips and sawdust), some sand, some gravel, loose, dry to 0.9 m - moist below 0.9 m						concrete to 1.2 m	
2				Interbedded CLAY AND GARBAGE (MSW) (garbage includes plastic and newspaper), odour, wet						grout from 1.2 to 4.6 m	
3			2 100	FAT CLAY (reworked soil, fill) trace silt, trace gypsum crystals, laminated, firm, brown							
4				sandy SILT (native) soft, grey, wet		GSA, At, M					-434
5		BH11-1-1		FAT CLAY soft, grey, wet							-433
6				sandy SILT fine grained sand, soft, grey, wet							-432
7		BH11-1-2	3 100	FAT CLAY soft, grey, wet							-431
8		BH11-1-3		sandy SILT fine grained sand, soft, grey, wet							-430
9		BH11-1-4		silty SAND trace clay, loose, grey, wet		GSA, M					-429
10		BH11-1-5	4 100	FAT CLAY trace sand, laminated, soft, grey, wet							-428
11				End of borehole at 15.2 m							-427
12				(1) - Water added during drilling from surface to 15.2 m							-426
13		BH11-1-6	5 100	GSA - grain size analysis M - moisture content At - Atterberg limits MSW - Municipal solid waste							-425
14		BH11-1-7									
15											

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 18, 2011  
 LOGGED BY: EM  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-2**  
 SURFACE ELEVATION: **439.68 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 100		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), some sand, some gravel, loose, dry to 0.9 m					concrete to 1.0 m	439
2					- 5 cm sand and gravel layer at 1.8 m						438
3										grout from 1.0 to 6.1 m	437
4			2 50		<b>Interbedded CLAY AND GARBAGE</b> (garbage includes plastic and newspaper), odour (MSW), grey, moist						436
5											435
6					<b>FAT CLAY (reworked soil, fill)</b> trace silt, trace sand, laminated, soft, grey, moist						434
7	■	BH11-2-1	3 100								433
8	■	BH11-2-2			<b>sandy SILT (native)</b> sand is fine to medium, soft, grey, wet						432
9	■	BH11-2-3			<b>FAT CLAY</b> trace sand, soft, grey, moist	GSA, M					431
10	■	BH11-2-4			<b>silty SAND</b> sand is fine to medium, loose, grey, wet	GSA					430
11	■	BH11-2-5	4 100		<b>SILT</b> some clay, trace sand, soft, grey, wet						429
12					<b>FAT CLAY</b> trace sand, laminated, soft, grey, moist					bentonite seal	428
13	■	BH11-2-6	5 100		- 5 cm long concretion at 12.5 m	GSA, M					427
14					- wet at 14.0 m						426
15	■	BH11-2-7			<b>LEAN CLAY</b> trace sand, laminated, soft, grey, wet	GSA, M					425
					End of borehole at 15.2 m						
					(1) - Water added during drilling from surface to 15.2 m						
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 19, 2011  
 LOGGED BY: EM  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11- 4**  
 SURFACE ELEVATION: **439.08 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 60		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), some sand, some gravel, trace garbage (plastic), loose, brown, moist					concrete to 0.9 m	439
2											438
3					<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes plastic and rope), soft, brown, moist					grout from 0.8 to 6.0 m	437
4		BH11-4-1	2 50								436
5											435
6					<b>FAT CLAY (reworked soil, fill)</b> trace fine sand, laminated, soft, grey, moist						434
7		BH11-4-2	3 100		<b>LEAN CLAY (native)</b> some fine sand, laminated, soft, grey, moist - wet at 6.4 - 7.0 m and 8.8 - 9.1 m	GSA, Att, M					433
8		BH11-4-3									432
9					- thin sand lenses (approximately 1 mm thick) from 8.4 m to 8.5 m						431
10											430
11		BH11-4-4	4 100		<b>silty SAND</b> trace clay, sand is fine grained, loose, grey, wet - 3 - 5 cm thick clay lenses at 10.4 m and 11.4 m	GSA, M				bentonite seal	429
12		BH11-4-5									428
13		BH11-4-6			- increased silt from 12.5 to 13.1 m						427
14		BH11-4-7	5 100		<b>FAT CLAY</b> trace sand, trace gravel, soft, grey, moist	GSA, Att, M					426
15											425
15.5					End of borehole at 15.5 m						424

(1) - Water added during drilling from surface to 15.5 m

GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11- 5**  
 SURFACE ELEVATION: **439.06 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 20		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), some sand, some gravel, some garbage (plastic, wire), loose, brown, moist					concrete to 0.9 m	438
2											437
3					<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes plastic and rope). Clay is firm, high plasticity, grey, moist					grout from 0.6 to 4.3 m	436
4		BH11-5-1	2 100		<b>FAT CLAY (reworked soil, fill)</b> laminated, soft, brown, moist						435
5		BH11-5-2									434
6					- wet and grey at 5.8 - 6.4 m						433
7		BH11-5-3	3 100		<b>LEAN CLAY (native)</b> trace gravel, trace sand, laminated, brown, moist	GSA, Att, M					432
8					- medium to coarse sand lens at 8.2 m						431
9											430
10		BH11-5-4	4 100		<b>silty SAND</b> trace clay, loose, grey, wet	GSA, M				bentonite seal	429
11		BH11-5-5			- medium to coarse sand lens with trace gravel at 11.1 - 11.3 m	GSA					428
12					- 10 cm thick coarse sand lens at 12.3 m						427
13					<b>FAT CLAY</b> some sand, trace gravel, laminated, soft, grey, moist						426
14		BH11-5-6	5 100		- medium sand lenses at 13.1 m, 14.3 m, 14.5 m, and 15.15 m (approximately 2 mm thick)	GSA, Att, M					425
15					End of borehole at 15.1 m						424

(1) - Water added during drilling from surface to 15.1 m

GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: April 21, 2011

LOGGED BY: EM/JN  
 DRILLER NAME: Beck

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

### BOREHOLE LOG

BOREHOLE NO: **BH11-6**  
 SURFACE ELEVATION: **438.81 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1	20	Unconsolidated <b>ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), some black sand, some garbage, loose, brown, moist					concrete to 0.9 m	438
2											437
3					Interbedded <b>CLAY AND GARBAGE (MSW)</b> (garbage includes rope). Clay is firm, high plasticity, blue/grey, moist						436
4		BH11-6-1	2	100	<b>FAT CLAY (reworked soil, fill)</b> laminated, soft, brown, moist - 2 cm fine sand lens at 3.6 m					grout from 0.9 to 6.7 m	435
5											434
6		BH11-6-2									433
7			3	100	<b>LEAN CLAY (native)</b> some fine sand, laminated, soft, grey, moist						432
8		BH11-6-3									431
9											430
10		BH11-6-4	4	100							429
11					<b>sandy SILT</b> some clay, soft, sand is fine to medium, grey, moist					bentonite seal	428
12		BH11-6-5				GSA, M					427
13			5	100							426
14					<b>FAT CLAY</b> trace sand, trace gravel, soft, laminated, brown, moist - fine sand lens at 14.2 m (approximately 4 cm thick)						425
15		BH11-6-6				GSA, M					424
					End of borehole at 15.2 m						
					(1) - Water added during drilling from surface to 15.2 m						
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: April 25, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-7**  
 SURFACE ELEVATION: **438.71 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1	65	Unconsolidated ORGANIC MATTER (wood pieces, grading to chips and sawdust), some garbage (shingles and plastic), loose, brown, moist					concrete to 0.9 m	438
2											437
3			2	75	Interbedded CLAY AND GARBAGE (MSW) (garbage includes plastic, cloth, wire). Clay is firm, high plasticity, dark grey, moist					grout from 0.9 to 6.7 m	436
4											435
5											434
6					FAT CLAY (reworked soil, fill) trace sand, trace garbage (wire and plastic) laminated, soft, brown, moist						433
7		BH11-7-1	3	100	- 2 cm fine sand lens at 7.3 m						432
8											431
9					- wet at 9.1 - 9.9 m						430
10			4	100	sandy LEAN CLAY (native) sand is fine to medium, very soft, grey, moist	GSA, M				bentonite seal	428
11		BH11-7-2			- occasional cobbles at 11.6 m						427
12											426
13					FAT CLAY trace sand, laminated, very soft, grey, moist						425
14		BH11-7-3	5	100		GSA, M					424
15					- fine grained sand lens at 14.8 m (approximately 1 mm thick)						424
					End of borehole at 15.3 m						
					(1) - Water added during drilling from surface to 15.25 m						
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 25, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11- 8**  
 SURFACE ELEVATION: **438.72 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 30		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace grey clay, some garbage (wire, plastic, metal debris), loose, brown, moist					concrete to 0.9 m	438
2											437
3					<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes rope). Clay is soft, high plasticity, odour, grey, moist						436
4			2 100		- 3 cm thick fine sand lens at 3.9 m - glass debris at 4.5 - 5.8 m					grout from 0.9 to 6.0 m	435
5	■	BH11-8-1			<b>FAT CLAY (reworked soil, fill)</b> trace sand, laminated, very soft, brown, moist						434
6					<b>FAT CLAY (native)</b> trace sand, laminated, soft, grey, moist						433
7			3 100								432
8					- 2 mm thick fine sand lens at 8.1 m						431
9	■	BH11-8-2									430
10			4 100		<b>silty SAND</b> some clay, sand is fine to medium, loose, grey, wet					bentonite seal	429
11											428
12	■	BH11-8-3				GSA, M					427
13			5 100								426
14											425
15					<b>poorly graded SAND with gravel</b> very loose, grey, wet					slough	424
					End of borehole at 15.2 m						
					(1) - Water added during drilling from surface to 15.2 m						
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 26, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-9**

SURFACE ELEVATION: **438.63 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses	WATER LEVEL		
1			1	80		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (plastic), loose, brown, moist			concrete to 0.9 m	438
2						<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes asphalt, wire). Clay is soft, high plasticity, odour, dark grey, moist				437
3						<b>No recovery</b>				436
4			2	0						435
5										434
6										433
7			3	0					grout from 0.9 to 11.6 m	432
8										431
9						<b>Interbedded CLAY AND GARBAGE (MSW)</b> some silt, high plasticity, large glass debris, very soft, grey, moist				430
10		BH11-9-1	4	100						429
11						<b>LEAN CLAY (native)</b> trace sand, laminated, very soft, grey, moist				428
12		BH11-9-2				- 1 mm thick fine sand lens at 12.2 m	GSA, M			427
13			5	100		- 1 cm fine sand lens at 13.1 m				426
14		BH11-9-3				<b>SILT</b> grading to sandy silt, some clay, sand is fine to medium, very soft, grey, moist				425
15		BH11-9-4				- wet at 14.9 to 15.2 m	GSA			424
16			6	100		<b>FAT CLAY</b> trace sand, occasional cobbles, laminated, very soft, grey, moist				423
17		BH11-9-5					GSA, Att, M			422
18										421
19		BH11-9-6	7	100						420

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 26, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

Sheet 1 of 3





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-9**  
 SURFACE ELEVATION: **438.63 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		ELEVATION (m)
						Laboratory Analyses	WELL COMPLETION WATER LEVEL	
21			7 100		- becoming soft at 19.8 m			418
21					- wet at 20.7 - 21.0 m			417
22		BH11-9-7	8 100		- 2 mm thick fine sand lenses from 22.6 m to 23.8 m			416
24		BH11-9-8			clayey GRAVEL some medium sand, some silt, laminated, very soft, grey, moist	GSA		415
24		BH11-9-9						414
25					silty SAND some gravel, some silt, loose, grey, wet			413
26		BH11-9-10	9 100					412
27		BH11-9-11			- coarse sand lens from 26.7 to 27 m (sand is brown, loose, moist)			411
28								410
28		BH11-9-12	10 100		clayey GRAVEL (till) some sand, dense, grey, moist			410
29					- green layers at 27.1 m and from 29.6 to 29.9 m			409
30					- wet and white in colour from 29.4 to 29.6 m			408
30					Weathered volcanic BEDROCK weak, grey, dry			407
31		BH11-9-13	11 100					406
32					- green from 32.6 to 32.9 m, 33.5 to 33.8 m, and 35.4 to 35.7 m			405
34		BH11-9-14	12 100					404
37		BH11-9-18						403
38		BH11-9-15 BH11-9-16	13 100					402
39		BH11-9-17			- basalt-like material from 38.7 to 38.9 m (black, glassy, weak)			400
								399

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: April 26, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11- 9**  
 SURFACE ELEVATION: **438.63 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)		
						Laboratory Analyses							
41		BH11-9-19	14 100		- soft and green with black layers from 41.4 to 41.8 m and from 43.3 to 45.7 m						398		
		BH11-9-20											397
42		BH11-9-21											396
43		BH11-9-22											395
44		BH11-9-23	15 100										394
45													393
					End of borehole at 45.7 m								
					(1) - Water added during drilling from surface to 45.7 m								
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste								

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: April 26, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck

Sheet 3 of 3



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-10**  
 SURFACE ELEVATION: **438.74 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1	75	Unconsolidated ORGANIC MATTER (wood pieces, grading to chips and sawdust), some sand, trace cobbles, loose, brown, moist					concrete to 1.1 m	438
2					Interbedded CLAY AND GARBAGE (MSW) (garbage includes styrofoam, plastic, wire). Clay is soft, high plasticity, laminated, odour, brown, moist - black at 2.1 m - plywood pieces from 2.1 to 5.5 m						437
3											436
4			2	25							435
5											434
6					No recovery					grout from 1.1 to 10.7 m	433
7			3	0							432
8											431
9					Interbedded CLAY AND GARBAGE (MSW) (garbage includes plywood), some silt. Clay is soft, high plasticity, grey, moist						430
10	BH11-10-1 BH11-10-2				silty SAND (native) trace clay, loose, grey, wet						429
11	BH11-10-3		4	100	FAT CLAY trace sand, laminated, soft, grey, moist silty SAND tracy clay, loose, grey, wet - 4 cm thick clay lens at 11 m	GSA					428
12					FAT CLAY some silt, laminated, soft, grey, moist - thin sand lenses at 12.0 m, 13.1 m, and 14.5 m						427
13	BH11-10-4		5	100							426
14											425
15											424
16											423
17	BH11-10-5		6	100	silty GRAVEL with sand trace clay, occasional cobbles, loose, grey, wet	GSA					422
18	BH11-10-6				silty GRAVEL with sand (Till) trace clay, dense, green, moist - pink colour at 17.4 m	GSA				bentonite seal	421
19	BH11-10-8		7	100							420
											419

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: April 28, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck




CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-10**  
 SURFACE ELEVATION: **438.74 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	TEST DATA			ELEVATION (m)	
						Laboratory Analyses	WELL COMPLETION	WATER LEVEL		
21		BH11-10-7	7	100	 Volcanic bedrock grey, dry - black and glassy (basalt-like) at 20.3 to 20.4 m - wet from 20.7 to 21.0 m				-418	
22		BH11-10-9	8	100						-417
23					End of borehole at 23.8 m					-416
					(1) - Water added during drilling from surface to 23.8 m					-415
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste					

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 28, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-11**  
 SURFACE ELEVATION: **438.68 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses				
0					0-20.7 m: not logged Refer to BH11-10				concrete to 0.6 m	438
1										437
2										436
3										435
4										434
5									grout from 0.6 to 9.8 m	433
6										432
7										431
8										430
9										429
10			1 100							428
11										427
12										426
13										425
14										424
15										423
16										422
17										421
18										420
19										419

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 29, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

Sheet 1 of 3





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-11**  
 SURFACE ELEVATION: **438.68 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses	WATER LEVEL		
21			1 100		<b>Volcanic Bedrock</b> grey, dry - green laminations from 20.9 to 21.2 m				418
22			2 100		- black layer at 21.9 to 22.2 m				417
23					- green laminations from 23.2 to 24.4 m, 28.6 to 28.8 m, and 29.9 to 32.9 m				416
24									415
25		BH11-11-1	3 85						414
26								bentonite seal	413
27									412
28		BH11-11-2	4 65						411
29		BH11-11-3			- rusty layers from 28.9 to 29.1 m				410
30									409
31		BH11-11-4	5 100						408
32									407
33					- moist from 32.9 to 33.2 m - dry and green from 33.2 to 34.4 m				406
34		BH11-11-5	12 100						405
35									404
36					- white from 36.3 to 37.2 m				403
37									402
38		BH11-11-6	13 100						401
39		BH11-11-7							400
									399

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: April 29, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-11**  
 SURFACE ELEVATION: **438.68 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses	WATER LEVEL		
41		BH11-11-8	14 100						398
42					End of borehole at 42.1 m  (1) - Water added during drilling from surface to 42.1 m  GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste  0 to 20.7 m not logged, refer to BH11-10				397

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: April 29, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-12**  
 SURFACE ELEVATION: **439.34 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 50		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace cobbles, loose, brown, dry					concrete to 0.6 m	439
2											438
3					<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes cloth, plastic). Clay is soft, high plasticity, odour, grey, moist						437
4			2 40							grout from 0.6 to 7.3 m	436
5											435
6											434
7		BH11-12-1	3 100		<b>LEAN CLAY (native)</b> trace sand, laminated, very soft, grey, moist - 2 cm thick sand lens at 6.4 m						433
8					- wet from 8.8 to 9.4 m						432
9											431
10											430
11		BH11-12-2	4 100		<b>silty SAND with gravel</b> trace clay, loose, grey, wet	GSA					429
12		BH11-12-3			<b>silty GRAVEL with sand (Till)</b> trace clay, trace cobbles, dense, grey, moist - wet from 11 to 11.3 m	GSA				bentonite seal	428
13		BH11-12-4			- green laminations from 11.3 to 11.6 m	GSA					427
14		BH11-12-5			<b>silty SAND with gravel (Till)</b> trace clay, trace cobbles, dense, grey, moist						426
15		BH11-12-6			<b>Boulder</b> soft, green and white, dry						425
16		BH11-12-7			<b>clayey GRAVEL</b> dense, green, moist						425
17					End of borehole at 15.1 m						

(1) - Water added during drilling from surface to 15.1 m

- GSA - grain size analysis
- M - moisture content
- Att - Atterberg limits
- MSW - Municipal solid waste

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 3, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-14**  
 SURFACE ELEVATION: **439.34 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses					
1			1	50		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace cobbles, trace garbage (rebar, metal, plastic), loose, brown, dry					concrete to 0.5 m	439
2												438
3						<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes metal, rubber, plastic). Clay is firm, high plasticity, odour, brown, moist						437
4			2	100							grout from 0.5 to 7.3 m	436
5												435
6						- clay is black and has a strong odour at 5.5 m						434
7		BH11-14-1	3	100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, grey, moist						433
8						- very soft from 7 to 8.5 m						432
9						- increased silt from 7.8 to 8.5						431
10						No recovery below 8.5 m						430
11			4	0								429
12											bentonite seal	428
13			5	0								427
14												426
15												425
16			6	0								424
End of borehole at 16.2 m												
(1) - Water added during drilling from surface to 16.2 m												
GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste												

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 5, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-15**  
 SURFACE ELEVATION: **439.42 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses					
1			1	50		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (cloth and plastic), loose, brown, dry					concrete to 0.8 m	439
2												438
3						<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes wood and plastic). Clay is firm, high plasticity, odour, dark grey, moist						437
4			2	70							grout from 0.8 to 7.3 m	436
5						- 15 cm thick gravel layer at 4.6 m						435
6												434
7		BH11-15-1	3	100		<b>FAT CLAY (reworked soil, fill)</b> laminated, soft, grey, moist						433
8												432
9						- wet at 9.1 m						431
10		BH11-15-2	4	100		- small concretion at 9.5 m						430
11												429
12						- 1 mm fine sand lens at 11.4					bentonite seal	428
13						No recovery below 11.6 m						427
14			5	0								426
15												425
16			6	0								424
						End of borehole at 16.2 m						
						(1) - Water added during drilling from surface to 16.2 m						
						GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 6, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-16**  
 SURFACE ELEVATION: **438.95 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses					
1			1	80		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (foam and plastic), loose, brown, moist					concrete to 0.8 m	438
2						<b>Interbedded CLAY AND GARBAGE (MSW)</b> (garbage includes metal, wood and plastic). Clay is firm, high plasticity, odour, dark grey, moist						437
3												436
4			2	40							grout from 0.8 to 6.8 m	435
5												434
6						<b>FAT CLAY (reworked soil, fill)</b> trace sand, firm, grey, moist						433
7		BH11-16-1	3	100		- glass debris at 6.4 m - gypsum crystals from 6.1 to 6.7 m						432
8		BH11-16-2				- increased silt at 7.9 m						431
9						No recovery below 8.5 m						430
10			4	0								429
11												428
12												427
13			5	0								426
14												425
15												424
16			6	0								423
17												422
						End of borehole at 17.7 m						
						(1) - Water added during drilling from surface to 17.7 m						
						GSA - grain size analysis M - moisture content						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 6, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE

Sheet 1 of 2



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-16**  
 SURFACE ELEVATION: **438.95 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses	WATER LEVEL		
					Att - Atterberg limits MSW - Municipal solid waste				

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 6, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck



CLIENT: City of Kelowna  
 PROJECT: Glenmore Landfill - Phase 3  
 ADDRESS: 2105 Glenmore Road North, Kelowna, BC  
 SLR JOB NO: 219.05164

**BOREHOLE LOG**

BOREHOLE NO: BH11-17

SURFACE ELEVATION: 439.05 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 70		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (plastic), loose, brown, moist					concrete to 0.5 m	438
2					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, dark grey, moist						437
3											436
4			2 100							grout from 0.5 to 7.0 m	435
5					- increased garbage from 4.9 to 5.5 m						434
6					<b>FAT CLAY (reworked soil, fill)</b> trace sand, firm, grey, moist						433
7		BH11-17-1	3 100		- wet at 7.3 m						432
8		BH11-17-2			<b>LEAN CLAY (native)</b> laminated, very soft, fine sand lenses throughout, grey, wet						431
9											430
10		BH11-17-3	4 100								429
11											428
12		BH11-17-4			<b>sandy LEAN CLAY</b> soft, grey, moist					bentonite seal	427
13		BH11-17-5	5 100		- wet at 12.5 m	GSA					426
14											425
15		BH11-17-6			<b>silty SAND</b> trace gravel, trace clay, sand is medium to coarse, loose, grey, wet End of borehole at 15.2 m	GSA					424

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 9, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-19**  
 SURFACE ELEVATION: **438.26 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 70		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace cobbles, trace garbage (cloth, metal, plastic), loose, brown, moist					concrete to 0.5 m	438
2					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, dark grey, moist					grout from 0.5 to 4.3 m	437
3					- blue colour at 3 to 3.6 m						436
4		BH11-19-1	2 100		<b>FAT CLAY (reworked soil, fill)</b> laminated, firm, brown, moist - 5 cm thick fine sand lens at 4.0 m - trace gypsum crystals from 4.0 to 5.5 m - orange mottles from 4.0 to 4.6 m						435
5		BH11-19-2			- very soft and wet from 5.8 to 6.7 m						434
6					<b>FAT CLAY (native)</b> laminated, soft, grey, moist						433
7			3 100		<b>LEAN CLAY</b> grey, moist						432
8		BH11-9-3			- wet at 9.9 m					bentonite seal	431
9					<b>LEAN CLAY with sand</b> grey, moist - wet from 10.5 to 11.0 m - thin sand lenses throughout						430
10			4 100		<b>sandy LEAN CLAY</b> grey, moist						429
11		BH11-9-4			- wet from 13.0 to 13.4 m	GSA					428
12		BH11-9-5			<b>silty SAND</b> trace clay, trace gravel, soft, grey, moist						427
13			5 100			GSA					426
14		BH11-9-6									425
15					End of borehole at 15.2 m						424

(1) - Water added during drilling from surface to 15.2 m

GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 10, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck

Sheet 1 of 1



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-20**  
 SURFACE ELEVATION: **438.71 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
1			1 50		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage (metal, plastic), loose, brown, moist					concrete to 0.8 m	438
2					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, dark grey, moist						437
3										grout from 0.8 to 6.1 m	436
4			2 90								435
5					- blue colour from 4.6 to 5.5 m - cobble at 5.5 m						434
6					<b>FAT CLAY (reworked soil, fill)</b> laminated, firm, brown, moist						433
7		BH11-20-1	3 100		- large glass debris at 6.7 to 8.2 m - 2 mm thick fine sand lens at 7.2 m						432
8											431
9					<b>FAT CLAY (native)</b> soft, grey, moist						430
10					- very soft at 9.1 m						429
11		BH11-20-2	4 100		<b>LEAN CLAY</b> laminated, soft, grey, moist - very soft and wet at 9.4 to 10.4 m					bentonite seal	428
12											427
13					<b>silty SAND</b> trace clay, sand is fine, very soft, grey, moist - wet at 12.6 m						426
14		BH11-20-3	5 100		- 10 cm thick sand lenses at 13.4, 13.9, and 14.2 m						425
15		BH11-20-4			- sand becoming medium grained at 14.6 m		GSA				424
					End of borehole at 15.2 m						
					(1) - Water added during drilling from surface to 15.2 m						
					GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 11, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-23**  
 SURFACE ELEVATION: **437.70 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses					
1			1	60	Interbedded CLAY AND GARBAGE (MSW)	Clay is firm, odour, laminated, grey, moist					concrete to 0.6 m	437
2												436
3		BH11-23-1	2	100	FAT CLAY (reworked soil, fill)	firm, laminated, brown, moist					grout from 0.6 to 6.7 m	435
4												434
5		BH11-23-2				- very soft, grey, and increased moisture at 4.5 m - 1-2 mm thick sand lenses at 4.7, 4.9, and 5.2 m						433
6		BH11-23-3				- some garbage (plastic) and odour from 5.5 to 6.4 m (suspect carry-down from surface material)						432
7		BH11-23-4	3	100	LEAN CLAY (native)	soft, laminated, thin sand lenses throughout (1-2 mm thick), grey, moist						431
8		BH11-23-5										430
9		BH11-23-6			poorly graded SAND with silt	trace gravel, trace clay, medium sand, loose, grey, wet	GSA					429
10		BH11-23-7	4	100	FAT CLAY	trace sand, laminated, brown, moist	GSA					428
11						- concretion at 11.1 m - thin sand lenses (approx. 2mm thick) from 11.3 to 11.6 m						427
12		BH11-23-8			poorly graded GRAVEL with silt and sand	trace clay, loose, brown, wet	GSA				bentonite seal	426
13		BH11-23-9	5	100	clayey SAND with gravel (suspect till)	some silt, dense to very dense, brown and green, moist	GSA					425
14		BH11-23-10										424
15		BH11-23-11			BOULDERS	volcanic, soft, platy, green, dry						423
16		BH11-23-12			silty GRAVEL with sand (till)	dense to very dense, grey, wet						422
17		BH11-23-13	6	100	volcanic BEDROCK	weak, some black crystals throughout, green and white, dry						421
17.7						End of borehole at 17.7 m						420

(1) - Water added during drilling from surface to 17.7 m

GSA - grain size analysis  
 M - moisture content

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 14, 2011

LOGGED BY: EM  
 DRILLER NAME: Beck



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-23**

SURFACE ELEVATION: 437.70 m

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
					At - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 14, 2011  
 LOGGED BY: EM  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-24**  
 SURFACE ELEVATION: **437.70 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses					
1			1	60	Interbedded <b>CLAY AND GARBAGE (MSW)</b> some coarse sand. Clay is firm, odour, laminated, grey, moist					concrete to 0.8 m	437	
2						- clay is blue-grey at 1.8 to 2.1 m					436	
3					<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist					grout from 0.8 to 3.6 m	435	
4			2	100		- gypsum crystals from 3.3 to 4.0 m					434	
5		BH11-24-1				- thin sand lens at 4.7 m					433	
6						- trace gravel at 5.8 m					432	
7		BH11-24-2	3	100	<b>silty SAND (native)</b> trace gravel, trace clay, sand is medium, grey, moist		GSA				431	
8		BH11-24-3				- wet from 6.8 to 7.2 m		GSA, Att, M			430	
8		BH11-24-4				- fat clay layer from 7.3 to 7.6 m (trace sand, grey, moist)		GSA			429	
9						- 5 cm thick clay layer at 8.4 m					428	
10					<b>FAT CLAY</b> trace sand, laminated, soft, grey, moist					bentonite seal	427	
11		BH11-24-5	4	100				GSA, Att, M			426	
12						- concretion at 11.1 m - wet from 11.3 to 11.4 m - 2 cm thick coarse sand lenses at 11.7 m and 12.5 m					425	
13		BH11-24-6				- wet from 12.5 to 12.6 m		GSA			424	
14		BH11-24-7	5	100	<b>silty SAND with gravel (suspect till)</b> trace clay, compact, grey, moist						423	
14		BH11-24-8			<b>volcanic BEDROCK</b> hard, white, dry						423	
End of borehole at 14.8 m												
(1) - Water added during drilling from surface to 14.8 m												
GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste												

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 16, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-25**  
 SURFACE ELEVATION: **437.53 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0.6					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Garbage includes plywood. Clay is firm, odour, laminated, grey, moist					concrete to 0.6 m	437
1.0			1 30								436
2.0										grout from 0.6 to 3.6 m	435
3.0					<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist						434
4.0		BH11-25-1	2 100		<b>FAT CLAY (native)</b> trace sand, soft, laminated, grey, moist - wet from 5.0 to 5.2 m  - fine sand lenses from 5.5 to 7.8 m (approx. 4 - 5 cm thick)						433
5.0											432
7.0		BH11-25-2	3 100								431
8.0					<b>silty SAND</b> trace clay, trace gravel, loose, grey, moist  - wet from 8.6 to 9.9 m and from 10.2 to 10.5 m	GSA					430
9.0		BH11-25-3									429
10.0			4 100							bentonite seal	428
11.0		BH11-25-4			<b>FAT CLAY</b> soft, laminated, grey, moist - concretion at 11.3 m - fine silty sand lenses at 11.4 and 12.3 m  - 2 cm thick coarse sand lens at 12.5 m - wet from 12.5 to 12.8 m						427
12.0											426
13.0		BH11-25-5	5 100		<b>silty SAND with gravel (Till)</b> trace clay, loose, grey, moist  - compact below 13.9 m - wet from 14.3 to 14.7 m	GSA					425
14.0		BH11-25-6									424
14.3		BH11-25-7									423
15.0		BH11-25-8									423
15.2					End of borehole at 15.2 m  (1) - Water added during drilling from surface to 15.2 m  GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste						

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 16, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-27**

SURFACE ELEVATION: **438.12 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run # % Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						Laboratory Analyses					
0					Unconsolidated <b>ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), loose, brown, moist					concrete to 0.4 m	438
1			1 90		Interbedded <b>CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, grey, moist						437
2										grout from 0.4 to 4.9 m	436
3											435
4		BH11-27-1	2 100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist - gypsum crystals from 4 to 4.6 m						434
5		BH11-27-2									433
6											432
7		BH11-27-3			<b>silty SAND (native)</b> trace clay, sand is medium, soft, brown, moist						431
8		BH11-27-4	3 100		<b>LEAN CLAY</b> trace sand, laminated, firm, grey, wet - wet from 7.5 to 7.9 m	GSA, Att, M					430
9		BH11-27-5			<b>silty SAND</b> some clay, soft, grey, moist - wet from 8.2 to 8.4 m	GSA					429
10		BH11-27-6				GSA					428
11		BH11-27-7	4 100		- Clay lenses at 9.8 m and 10.8 m (5 to 10 cm thick) - wet from 9.9 to 10.7 m and 11.9 to 12.8 m  - trace gravel at 10.7 m					bentonite seal	427
12		BH11-27-8				GSA					426
13		BH11-27-9									425
14		BH11-27-10	5 100		<b>FAT CLAY</b> trace cobbles, laminated, firm, grey, moist <b>silty SAND with gravel (Till)</b> trace clay, sand is coarse, compact, grey, moist  - wet from 14.6 to 14.9 m	GSA					424
15					End of borehole at 15.2 m						423

(1) - Water added during drilling from surface to 15.2 m

GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 19, 2011

LOGGED BY: JN  
 DRILLER NAME: Beck





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-28**  
 SURFACE ELEVATION: **438.11 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses					
1			1	90		<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), loose, brown, moist  <b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, odour, grey, moist				concrete to 0.4 m	438	
2										grout from 0.4 to 4.0 m	437	
3											436	
4		BH11-28-1	2	100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist - gypsum crystals from 4.1 to 4.9 m - mottles at 4.3 m - glass debris at 4.9 m					435	
5		BH11-28-2				<b>FAT CLAY (native)</b> laminated, soft, grey, moist					434	
6		BH11-28-3				- very soft at 5.9 m - silt lenses at 5.9 m, 6.2 m, 6.4 m, and 7.3 m					433	
7			3	100							432	
8		BH11-28-4				<b>sandy LEAN CLAY</b> soft, grey, moist	GSA				431	
9						<b>FAT CLAY</b> very soft, grey, moist				bentonite seal	430	
10		BH11-28-5									429	
11		BH11-28-6	4	100		<b>silty SAND with gravel (Till)</b> trace clay, occasional cobbles, compact, dark grey, moist - very dense below 10.7 m					428	
12		BH11-28-7									427	
13		BH11-28-8	5	100			GSA				426	
14											425	
						End of borehole at 14.6 m  (1) - Water added during drilling from surface to 14.6 m  GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste					424	

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL\_FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-29**  
 SURFACE ELEVATION: **437.81 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses	WATER LEVEL		
1			1	100		Interbedded <b>CLAY AND GARBAGE (MSW)</b> Clay is firm, some gravel, odour, grey, moist			concrete to 0.9 m	-437
2						- dark grey and wet from 2.4 to 3.6 m			grout from 0.9 to 3.6 m	-436
3						- FAT CLAY (reworked soil, fill) soft, laminated, brown, moist				-435
4		BH11-29-1	2	50		- one cobble at 4.6 m				-434
5						- grey and very soft below 5.5 m				-433
6		BH11-29-2				- glass debris at 6.6 m				-432
7		BH11-29-3	3	100		- LEAN CLAY (native) trace sand, laminated, very soft, grey, moist - wet from 7.1 to 7.3 m and 8.2 to 8.4 m	GSA, Att, M			-431
8		BH11-29-4				- sandy LEAN CLAY sand is fine to medium, soft, grey, wet	GSA		bentonite seal	-430
9		BH11-29-5	4	100		- thin clay seams throughout from 10 to 10.5 m				-429
10						- sand is coarse from 11.0 to 11.3 m				-428
11		BH11-29-6				- FAT CLAY trace sand, soft, laminated, grey, moist	GSA, Att, M			-427
12		BH11-29-7				- silty SAND trace clay, sand is fine, loose, grey, wet - clay seam at 12.2 m	GSA			-426
13		BH11-29-8	5	100		- FAT CLAY trace sand, laminated, soft, grey, moist - wet from 13.1 to 13.7 m				-425
14		BH11-29-9					GSA, Att, M			-424
14.9						End of borehole at 14.9 m				-423

(1) - Water added during drilling from surface to 14.9 m

GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: May 20, 2011

LOGGED BY: EM  
 DRILLER NAME: Beck



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-30**  
 SURFACE ELEVATION: **437.57 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses					
1			1	70		<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is soft, odour, grey, moist					concrete to 0.9 m	437
2											grout from 0.3 to 4.3 m	436
3												435
4	■	BH11-30-1	2	100		<b>FAT CLAY (reworked soil, fill)</b> firm, laminated, brown, moist - gypsum crystals from 3.6 to 5.5 m - mottles from 3.6 to 4.3 m						434
5	■	BH11-30-2										433
6	■	BH11-30-3				- grey and very soft below 5.2 m						432
7	■	BH11-30-4				- fine sand lens at 6.1 m						431
8	■	BH11-30-5	3	100		- large glass debris at 6.7 m, 7.5 m, and 8.3 m						430
9						- wet from 8.5 to 9.1 m						429
10	■	BH11-30-6	4	100		<b>LEAN CLAY (native)</b> soft, grey, moist						428
11	■	BH11-30-7										427
12	■	BH11-30-8				<b>LEAN CLAY with sand</b> very soft, grey, moist - 2 cm thick medium sand lens at 11.4 m						426
13	■	BH11-30-9				<b>silty SAND</b> some to trace clay, sand is fine to medium, loose, grey, moist - 5 cm thick clay lenses at 11.7 m, 12 m, and 12.8 m - wet from 11.7 to 12.8 m and 13.2 to 14.6 m	GSA					425
14	■	BH11-30-10										424
15	■	BH11-30-11				<b>FAT CLAY</b> trace sand, very soft, grey, moist	GSA					423
16	■	BH11-30-12	6	100								422
17	■	BH11-30-13										421
18	■	BH11-30-14				<b>SILT</b> some clay, trace sand, very soft, laminated, grey, moist / <b>FAT CLAY</b> trace sand, very soft, laminated, grey, moist					bentonite seal	420
19	■		7	100		- silt lenses at 19.4 m and 20.3 m (1 - 3 cm thick)	GSA, Att, M					419
20												418

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 24, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE  
 Sheet 1 of 2



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH11-30**  
 SURFACE ELEVATION: **437.57 m**

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	Sample Run #	% Recovery	SOIL TYPE	SOIL DESCRIPTION	TEST DATA		WELL COMPLETION NOTES	ELEVATION (m)
							Laboratory Analyses	WATER LEVEL		
21		BH11-30-15	7	100		- concretions at 20.1 m and 22.4 m				-417
22		BH11-30-16	8	100		- fine sand lenses from 22.6 m through 23.8 m (approx. 1 mm thick)				-416
23		BH11-30-17					GSA, Att, M			-415
24						- cobble at 23.8 m				-414
25		BH11-30-18	9	90		<b>silty SAND with gravel (Till)</b> trace clay, sand is coarse, occasional cobbles, compact to dense, grey, moist				-413
26						- wet from 25.3 to 26.2 m	GSA			-412
27		BH11-30-19				- dark grey below 26.4 m - very dense below 26.8 m				-411
28		BH11-30-20	10	100						-410
29										-409
						End of borehole at 29.9 m				-408
						(1) - Water added during drilling from surface to 29.9 m				
						GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste				

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL FINAL.GPJ SLR\_CAN V5.2.GDT 9/22/11

DRILLING METHOD: Core Sample  
 DRILL DATE: May 24, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Beck

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-2**  
 SURFACE ELEVATION: **439.12 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1					Unconsolidated organic matter & garbage (MSW) (wood pieces, grading to chips and sawdust), trace garbage (metal, plastic), loose, misc, wet							concrete	439	
2					Interbedded CLAY AND GARBAGE (MSW) layers of black sand with heavy odour, grey, moist								438	
3													437	
4					FAT CLAY (Native) silty, high plasticity, firm, brown, moist - crystals at 4.3 m								436	
5		BH12-2-1			- becoming grey, soft at 5.2 m							bentonite seal	435	
6													434	
7					- very soft, wet at 6.7 m								433	
8													432	
9		BH12-2-2			- very soft, wet from 8.5 to 9.4 m								431	
9.4					End of borehole at 9.4 m								430	

(1) - Water added during drilling from surface to 9.4 m  
 GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

GSA %:  
 BH12-2-1: <0.10 Gravel, 0.28 Sand, 9.11 Silt, 90.6 Clay  
 BH12-2-2: <0.10 Gravel, 0.15 Sand, 29.4 Silt, 70.1 Clay

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: September 25, 2012 LOGGED BY: JN  
 DRILLER NAME: Mud Bay





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-3**

SURFACE ELEVATION: **437.90 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1					<b>SAND AND SILT</b> trace clay, loose, rootlets, dark brown, dry to moist								concrete	437
2					<b>silty CLAY</b> high plasticity, firm, brown, moist									436
3					<b>interbedded CLAY AND GARBAGE (MSW)</b> some sand, odour									435
4					<b>silty CLAY</b> high pasticity, firm, brown, moist - crystals at 3.0 and 3.7 m									434
5					- becoming grey and soft at 4.9 m - wet at 5.2 m								bentonite seal	433
6														432
7		BH12-3-1			- wet at 6.7 m - 5 mm seam fine sand at 7.0 m - 5 mm seam fine sand at 7.3 m									431
8					- wet from 8.2 m to 8.8 m									430
9														429
					End of borehole at 9.4 m									
					(1) - Water added during drilling from surface to 9.4 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste									

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/19/13

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: September 26, 2012 LOGGED BY: JN  
 DRILLER NAME: Mud Bay



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-5**

SURFACE ELEVATION: **441.62 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1	■	BH12-5-1			<b>SAND AND SILT (fill)</b> fine to medium sand, some clay, compact, brown, moist - becoming grey at 0.6 m - trace landfill waste (plastic) at 0.9 m								concrete	441
2					- increasing sand content, occasional cobble at 1.5 m - increasing clay at 1.8 m									440
3					<b>silty CLAY &amp; MSW</b> interbedded layers, some sand, some garbage (plastic, foil), some cobbles, odourous, grey to black, moist									439
4					<b>Unconsolidated ORGANIC MATTER</b> (wood chips grading to chips and sawdust) loose, black, moist									438
5					- layer garbage at 5.0 m									437
6					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, laminated, odourous. Garbage includes plastic, grey, moist								backfilled with bentonite	436
7														435
8	■	BH12-5-2			<b>silty CLAY - FAT CLAY (native)</b> laminations, firm, high plasticity, crystals to 7.9 m, black, moist									434
9														433
10	■	BH12-5-3			- soft at 9.4 m - very soft, wet at 9.8 m									432
11					- grey at 10.7 m End of borehole at 11.0 m									431

(1) - Water added during drilling from surface to 11.0 m  
 GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

GSA %:  
 BH12-5-1: <0.10 Gravel, 0.51 Sand, 21.7 Silt, 70.1 Clay  
 BH15-5-3: <0.10 Gravel, <0.10 Sand, 28.3 Silt, 71.7 Clay

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: September 27, 2012  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-6**  
 SURFACE ELEVATION: **439.18 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1					<b>Unconsolidated ORGANIC MATTER</b> (wood chips grading to chips and sawdust) loose, black, moist								concrete	439
2														438
3					<b>Interbedded CLAY AND GARBAGE (MSW)</b> Clay is firm, laminated, odourous. Garbage includes plastic, grey, moist									437
4														436
5		BH12-6-1			<b>silty CLAY - FAT CLAY (native)</b> laminations, firm, high plasticity, crystals at 4.6 and 5.2 m, black, moist - soft at 5.5 m								bentonite chips	435
6														434
7					- very soft, grey, wet from 6.4 to 9.4 m									433
8														432
9		BH12-6-2												431
					End of borehole at 9.4 m									430

(1) - Water added during drilling from surface to 9.4 m  
 GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample

Notes:  SONIC CORE SAMPLE

DRILL DATE: September 27, 2012 LOGGED BY: JN  
 DRILLER NAME: Mud Bay



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-7**

SURFACE ELEVATION: **439.34 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1				[Cross-hatched pattern]	<b>Unconsolidated ORGANIC MATTER</b> (wood chips grading to chips and sawdust) loose, brown, dry						[Diagonal lines]		concrete	439
2				[Dotted pattern]	<b>SAND AND GRAVEL (roadbase fill)</b> some silt, loose, brown, moist						[Solid black]		bentonite chips	437
3				[Dotted pattern]							[Solid black]			436
4		BH12-7-1		[Diagonal lines]	- odourous, black, wet layer at 4.0 m						[Solid black]			435
		BH12-7-2		[Diagonal lines]	<b>FAT CLAY (reworked soil fill)</b> some silt, firm, grey/blue, moist						[Solid black]			
				[Diagonal lines]	<b>silty CLAY (native)</b> firm, crystals, brown, moist End of borehole at 4.9 m						[Solid black]			

(1) - Water added during drilling from surface to 4.9 m  
 GSA - grain size analysis  
 M - moisture content  
 Att - Atterberg limits  
 MSW - Municipal solid waste

GSA %:  
 BH12-6-1: 48.3 Gravel, 32.0 Sand, 11.1 Silt, 8.6 Clay  
 BH12-7-2: <0.10 Gravel, 5.0 Sand, 5.0 Silt, 90.0 Clay

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample  
 DRILL DATE: September 27, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-8**  
 SURFACE ELEVATION: **438.75 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1					<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage, loose, brown, moist								concrete	438
2					<b>No recovery to 12.8 m</b> very soft									437
3														436
4														435
5														434
6														433
7														432
8													bentonite chips	431
9														430
10														429
11					<b>Interbedded silty CLAY AND GARBAGE (MSW)</b> soft, grey, moist - black layer (plastic, wood chips) from 11.6 to 11.9 m									428
12					- black layer (plastic, wood chips) from 12.5 to 12.8 m									427
13		BH12-8-1 BH12-8-2			<b>silty CLAY (native ?)</b> very soft, grey, wet - increased silt, saturated from 13.1 to 13.4 m									426
14		BH12-8-3			<b>SAND</b> some silt, loose, grey, moist to wet End of borehole at 14.0 m									425

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample  
 DRILL DATE: September 27, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-9**

SURFACE ELEVATION: **438.68 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1				X	<b>Unconsolidated ORGANIC MATTER</b> (wood pieces, grading to chips and sawdust), trace garbage, loose, brown, moist								concrete	438
2				X	<b>Interbedded silty CLAY AND GARBAGE (MSW)</b> soft, grey, moist  - wet from 4.3 to 4.9 m									437
3				X										436
4				X										435
5					<b>No Recovery to 11.0 m</b>									434
6													bentonite chips	433
7														432
8														431
9														430
10														429
11					End of borehole at 11.0 m									428
					(1) - Water added during drilling from surface to 11.0 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste									

No samples taken

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample  
 DRILL DATE: September 27, 2011  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

Notes:





CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-12**

SURFACE ELEVATION: **437.97 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)	
						ORGANIC VAPOUR LEVEL (ppmv)									
						1	10	100	1000	10000					
1					<b>SAND AND SILT (fill)</b> trace clay, compact, brown, moist										437
2					- organics, wet from 0.8 to 0.9 m <b>Interbedded CLAY AND GARBAGE (MSW)</b> some wood chips, blue/grey, moist										436
3					<b>SILT AND CLAY (native)</b> high plasticity laminations, firm, brown, moist										435
4					- crystals from 3.4 to 3.8 m										434
5															433
6					- very soft, wet from 6.4 to 7.0 m										432
7					- 3 cm seam medium grained sand at 6.9 m - wet from 7.3 to 7.9 m										431
					End of borehole at 7.9 m										
					(1) - Water added during drilling from surface to 7.9 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste  GSA %: BH12-12-1: <0.10 Gravel, 5.02 Sand, 53.9 Silt, 41.1 Clay										

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample  
 DRILL DATE: September 28, 2012  
 LOGGED BY: JN  
 DRILLER NAME: Mud Bay

Notes:  SONIC CORE SAMPLE



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-13**  
 SURFACE ELEVATION: **437.97 m**

SLR CONSULTING (CANADA) LTD.

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	ELEVATION (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
1					<b>SAND AND SILT (fill)</b> trace clay, compact, brown, moist - organics, wet from 0.8 to 0.9 m							concrete	437	
2					<b>Interbedded CLAY AND GARBAGE (MSW)</b> some wood chips, blue/grey, moist								436	
3					<b>SILT AND CLAY (native)</b> high plasticity laminations, firm, brown, moist - crystals from 3.4 to 3.8 m								435	
4		No samples										bentonite chips	434	
5													433	
6													432	
7					- very soft, wet from 6.4 to 7.0 m - 3 cm seam medium grained sand at 6.7 m - increased silt, wet at 7.3 m								431	
					End of borehole at 7.9 m									
					(1) - Water added during drilling from surface to 7.9 m GSA - grain size analysis M - moisture content Att - Atterberg limits MSW - Municipal solid waste									

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL NOV 2012.GPJ SLR\_CAN V5.2.GDT 2/13/13

DRILLING METHOD: Core Sample

Notes:

DRILL DATE: September 28, 2012

LOGGED BY: JN  
 DRILLER NAME: Mud Bay



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-15**

SLR CONSULTING (CANADA) LTD.

SURFACE ELEVATION:

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					BOREHOLE COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
0 to 1.5				diagonal lines	<b>silty CLAY</b> overburden, trace broken rock, compact, less rock starting at 1.5 m						rock pattern			0 to 1.5
1.5 to 2.1				diagonal lines	garbage observed at 2.1 m, brown, moist						rock pattern			1.5 to 2.1
2.1 to 5.5		BH12-15-1 BH12-15-2 BH12-15-3		cross-hatch	<b>Interbedded CLAY AND GARBAGE (MSW)</b> silty CLAY, garbage includes mostly organics such as wood and plastics, brown, moist						rock pattern		backfilled with drill cuttings	2.1 to 5.5
5.5 to 5.5					could not drill past 5.5 m End of borehole at 5.5 m									5.5 to 5.5
5.5 to 5.5					No well installed									5.5 to 5.5

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL DEC 2012.GPJ SLR\_CAN V5.2.GDT 12/4/12

DRILLING METHOD: Hollow Stem Auger Drilling

Notes:  SPOON SAMPLE

DRILL DATE: November 16, 2012  
 LOGGED BY: Amber McAfee  
 DRILLER NAME: On the Mark Locates, Antin

*Destroyed leachate trench*



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-16**  
 SURFACE ELEVATION:

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
-1.0														-1.0
0.0					Ground Surface									0.0
0.0 - 2.1				diagonal lines	<b>silty CLAY</b> overburden, trace broken rock, compact, less rock starting at 1.5 m  garbage observed at 2.1 m, brown, moist									
2.1 - 8.1				cross-hatch	<b>Interbedded CLAY AND GARBAGE (MSW)</b> silty CLAY, garbage includes mostly organics such as wood and plastics, brown, moist									
8.1 - 8.3				diagonal lines	<b>FAT CLAY (reworked soil, fill)</b> soft, grey/blue, wet									
8.3 - 8.5				diagonal lines	garbage (MSW) observed 0.2 m thick at 8.1 and 10.2 m depths									
8.5 - 8.8				horizontal lines										
8.8 - 9.0				horizontal lines										
9.0 - 9.2				horizontal lines										
9.2 - 9.5				horizontal lines										
9.5 - 10.0				horizontal lines										
10.0 - 10.2				horizontal lines										
10.2 - 10.5				horizontal lines										
10.5 - 11.0				horizontal lines										
11.0 - 11.5				horizontal lines										
11.5 - 12.0				horizontal lines										
12.0 - 12.5				horizontal lines										
12.5 - 13.0				horizontal lines										
13.0 - 13.5				horizontal lines										
13.5 - 14.0				horizontal lines										
14.0 - 14.5				horizontal lines										
14.5 - 15.0				horizontal lines										
15.0 - 15.5				horizontal lines										
15.5 - 16.0				horizontal lines										
16.0 - 16.5				horizontal lines										
16.5 - 17.0				horizontal lines										
17.0 - 17.5				horizontal lines										
17.5 - 18.0				horizontal lines										
18.0 - 18.5				horizontal lines										
18.5 - 19.0				horizontal lines										
19.0 - 19.5				horizontal lines										
19.5 - 20.0				horizontal lines										
20.0 - 20.5				horizontal lines										
20.5 - 21.0				horizontal lines										
21.0 - 21.5				horizontal lines										
21.5 - 22.0				horizontal lines										
22.0 - 22.5				horizontal lines										
22.5 - 23.0				horizontal lines										
23.0 - 23.5				horizontal lines										
23.5 - 24.0				horizontal lines										
24.0 - 24.5				horizontal lines										
24.5 - 25.0				horizontal lines										
25.0 - 25.5				horizontal lines										
25.5 - 26.0				horizontal lines										
26.0 - 26.5				horizontal lines										
26.5 - 27.0				horizontal lines										
27.0 - 27.5				horizontal lines										
27.5 - 28.0				horizontal lines										
28.0 - 28.5				horizontal lines										
28.5 - 29.0				horizontal lines										
29.0 - 29.5				horizontal lines										
29.5 - 30.0				horizontal lines										
30.0 - 30.5				horizontal lines										
30.5 - 31.0				horizontal lines										
31.0 - 31.5				horizontal lines										
31.5 - 32.0				horizontal lines										
32.0 - 32.5				horizontal lines										
32.5 - 33.0				horizontal lines										
33.0 - 33.5				horizontal lines										
33.5 - 34.0				horizontal lines										
34.0 - 34.5				horizontal lines										
34.5 - 35.0				horizontal lines										
35.0 - 35.5				horizontal lines										
35.5 - 36.0				horizontal lines										
36.0 - 36.5				horizontal lines										
36.5 - 37.0				horizontal lines										
37.0 - 37.5				horizontal lines										
37.5 - 38.0				horizontal lines										
38.0 - 38.5				horizontal lines										
38.5 - 39.0				horizontal lines										
39.0 - 39.5				horizontal lines										
39.5 - 40.0				horizontal lines										
40.0 - 40.5				horizontal lines										
40.5 - 41.0				horizontal lines										
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41.5 - 42.0				horizontal lines										
42.0 - 42.5				horizontal lines										
42.5 - 43.0				horizontal lines										
43.0 - 43.5				horizontal lines										
43.5 - 44.0				horizontal lines										
44.0 - 44.5				horizontal lines										
44.5 - 45.0				horizontal lines										
45.0 - 45.5				horizontal lines										
45.5 - 46.0				horizontal lines										
46.0 - 46.5				horizontal lines										
46.5 - 47.0				horizontal lines										
47.0 - 47.5				horizontal lines										
47.5 - 48.0				horizontal lines										
48.0 - 48.5				horizontal lines										
48.5 - 49.0				horizontal lines										
49.0 - 49.5				horizontal lines										
49.5 - 50.0				horizontal lines										

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL DEC 2012.GPJ SLR\_CAN V5.2.GDT 12/4/12

DRILLING METHOD: Hollow Stem Auger Drilling  
 DRILL DATE: November 16, 2012  
 LOGGED BY: Amber McAfee  
 DRILLER NAME: On the Mark Locates, Antin

Notes:  SPOON SAMPLE

*Destroyed*



CLIENT: **City of Kelowna**  
 PROJECT: **Glenmore Landfill - Phase 3**  
 ADDRESS: **2105 Glenmore Road North, Kelowna, BC**  
 SLR JOB NO: **219.05164**

**BOREHOLE LOG**

BOREHOLE NO: **BH12-16**

SURFACE ELEVATION:

DEPTH (m)	SAMPLE TYPE	SAMPLE ID	SPT COUNT	SOIL TYPE	SOIL DESCRIPTION	FIELD TEST DATA					WELL COMPLETION	WATER LEVEL	WELL COMPLETION NOTES	DEPTH (m)
						ORGANIC VAPOUR LEVEL (ppmv)								
						1	10	100	1000	10000				
9.0		BH12-16-3												9.0
10.0		BH12-16-4												10.0
11.0														11.0
12.0														12.0
		BH12-16-5			<p><b>silty SAND</b>            sand is fine to medium grained, loose, grey, wet            End of borehole at 12.2 m</p> <p>Well Completion Details:            Screened interval from 6.1 m to 10.7 m below surface            Elevation at top of casing (TOC) = m</p> <p><b>FAT CLAY</b>            soft, grey, wet</p>									

backfilled with drill cuttings

SLR CANADA V5.2 219.05164 CITY OF KELOWNA GLENMORE LANDFILL DEC 2012.GPJ SLR\_CAN V5.2.GDT 12/4/12

DRILLING METHOD: Hollow Stem Auger Drilling

Notes:  SPOON SAMPLE

DRILL DATE: November 16, 2012  
 LOGGED BY: Amber McAfee  
 DRILLER NAME: On the Mark Locates, Antin



# Attachment 1

Borehole Logs





Client  
City of Kelowna

Borehole No. : GL39-1

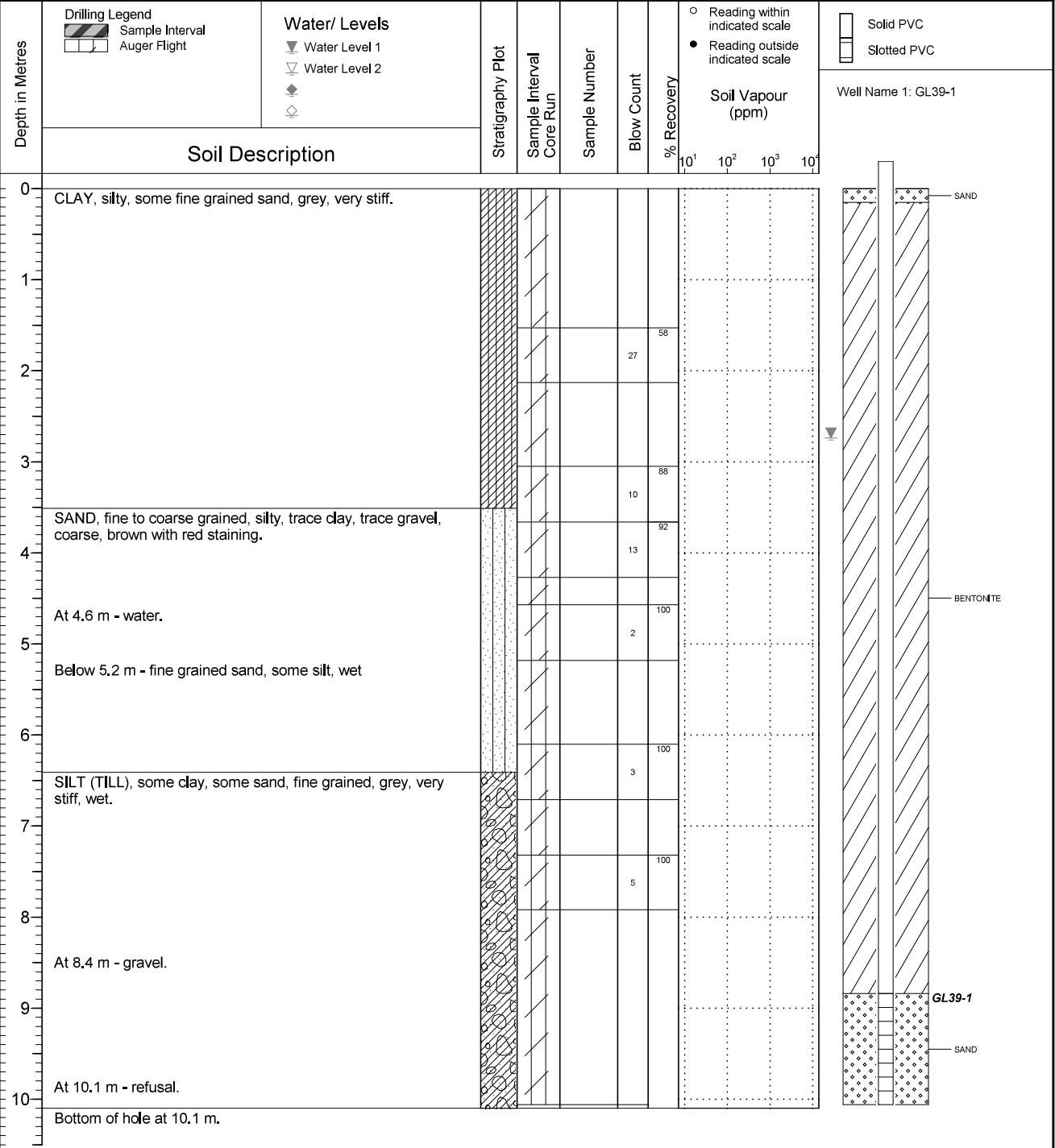
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 1

Drilling Contractor On The Mark  
Drilling Method Hollow Stem Auger  
Borehole Dia. (m) 0.05  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 439.530  
Top of Casing Elev. (m) 440.410  
Northing: 5535296.786 Easting: 326790.420

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 10 22  
Log Typed By: SGP/KP



**NOTES**

QA RRW 2020 01 28 Print Date: 2020-01-31



Client  
City of Kelowna

Borehole No. : GL39-2

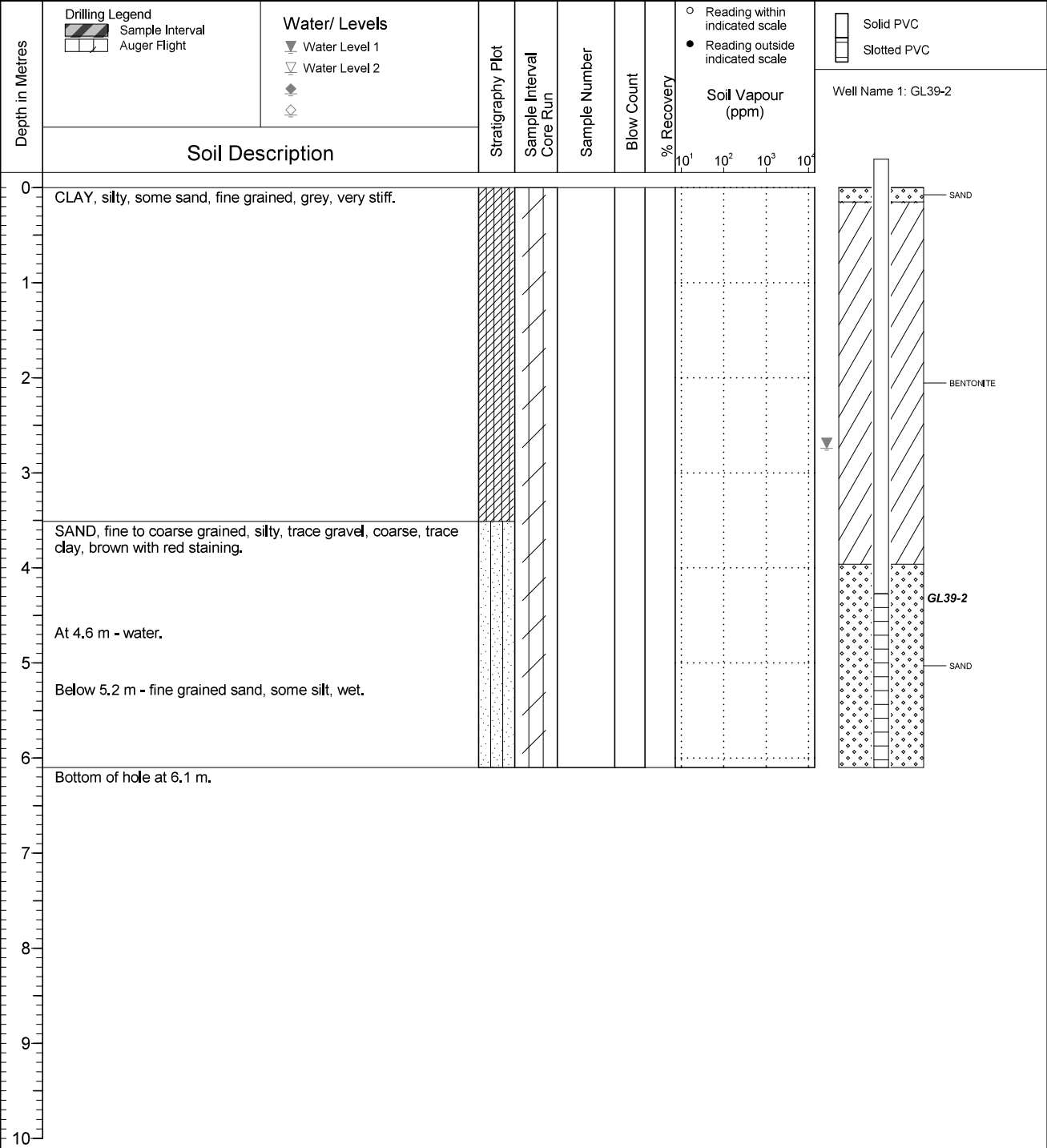
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 1

Drilling Contractor On The Mark  
 Drilling Method Hollow Stem Auger  
 Borehole Dia. (m) 0.05  
 Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
 Ground Surface Elev. (m) 439.560  
 Top of Casing Elev. (m) 440.460  
 Northing: 5535297.554 Easting: 326789.145

Project Number: 662036  
 Borehole Logged By: NL  
 Date Drilled: 2019 10 21  
 Log Typed By: SGP/KP



NOTES



Client  
City of Kelowna

Borehole No. : GL39-3

Location  
Glenmore Landfill, Kelowna, BC

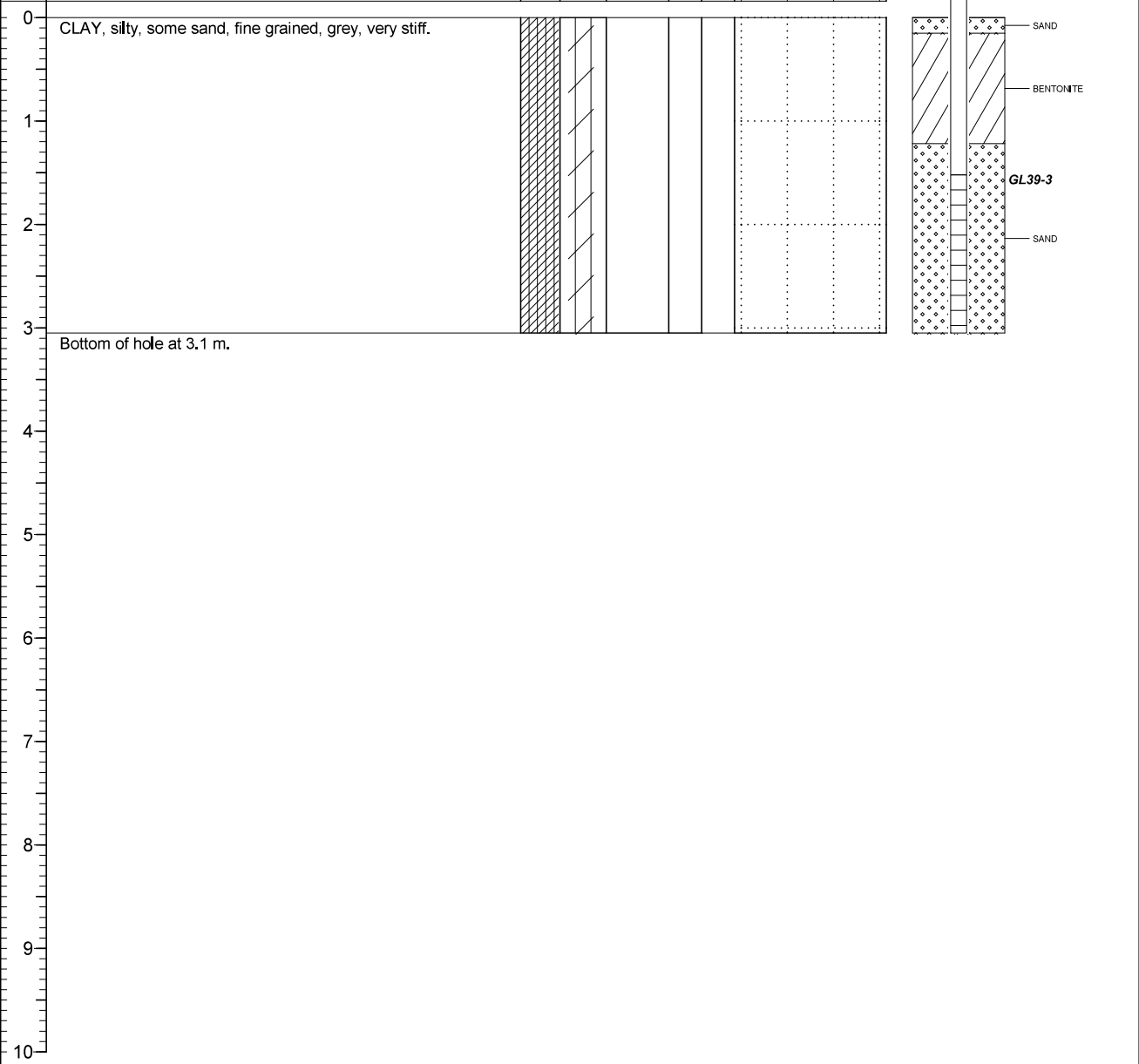
PAGE 1 OF 1

Drilling Contractor On The Mark  
 Drilling Method Hollow Stem Auger  
 Borehole Dia. (m) 0.05  
 Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
 Ground Surface Elev. (m) 439.630  
 Top of Casing Elev. (m) 440.560  
 Northing: 5535298.264 Easting: 326787.825

Project Number: 662036  
 Borehole Logged By: NL  
 Date Drilled: 2019 10 21  
 Log Typed By: SGP/KP

Depth in Metres	<b>Drilling Legend</b> Sample Interval Auger Flight	<b>Water/ Levels</b> Water Level 1 Water Level 2  	Stratigraphy Plot	Sample Interval Core Run	Sample Number	Blow Count	% Recovery	○ Reading within indicated scale ● Reading outside indicated scale  <b>Soil Vapour (ppm)</b> 10 <sup>1</sup> 10 <sup>2</sup> 10 <sup>3</sup> 10 <sup>4</sup>	Solid PVC Slotted PVC
	Soil Description								Well Name 1: GL39-3



**NOTES**



Client  
City of Kelowna

Borehole No. : GL40-1

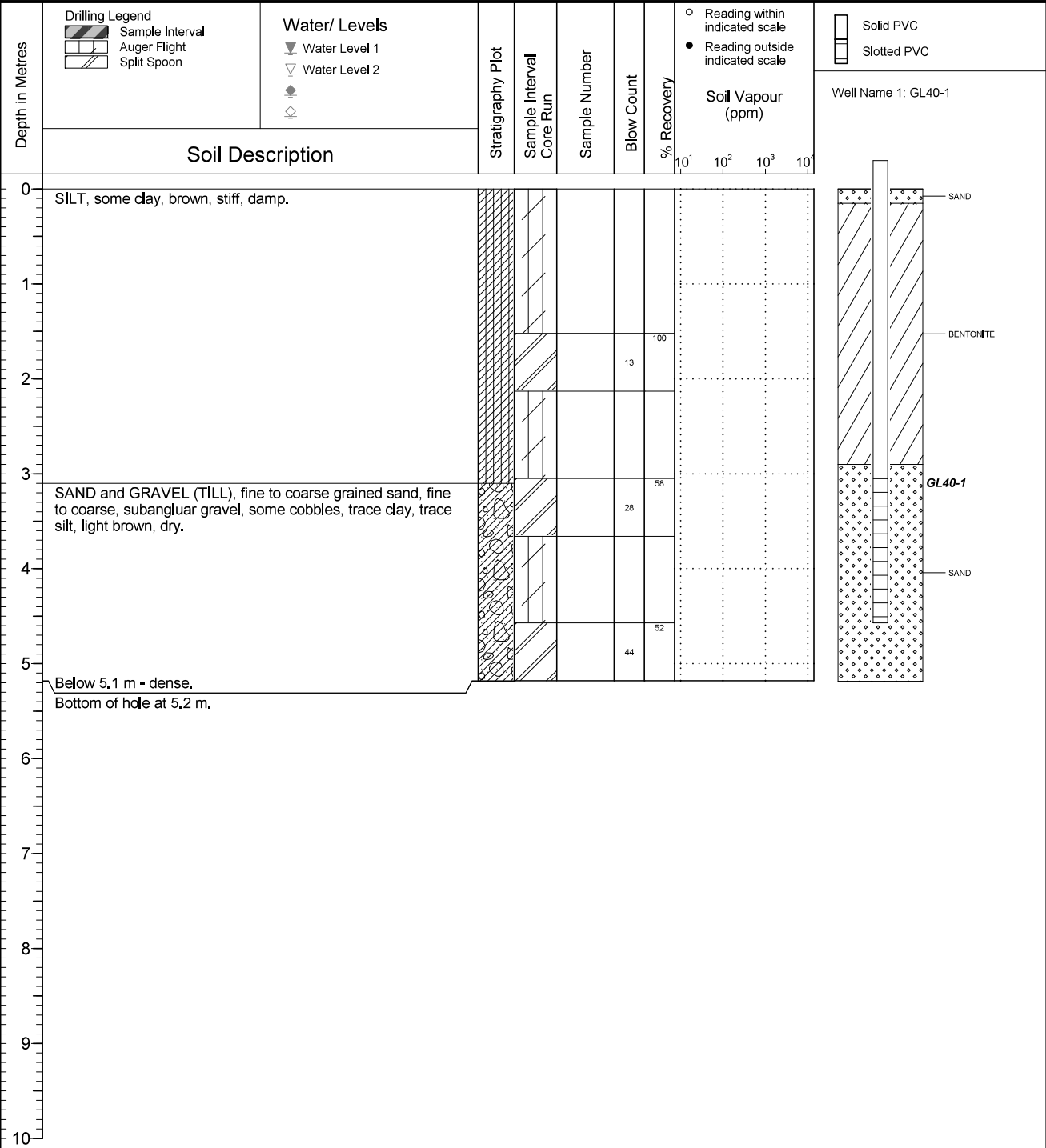
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 1

Drilling Contractor On The Mark  
 Drilling Method Hollow Stem Auger  
 Borehole Dia. (m) 0.05  
 Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
 Ground Surface Elev. (m) 449.750  
 Top of Casing Elev. (m) 450.490  
 Northing: 5535525.235 Easting: 326465.169

Project Number: 662036  
 Borehole Logged By: NL  
 Date Drilled: 2019 10 22  
 Log Typed By: SGP/KP



NOTES



Client  
City of Kelowna

Borehole No. : GL40-2/3

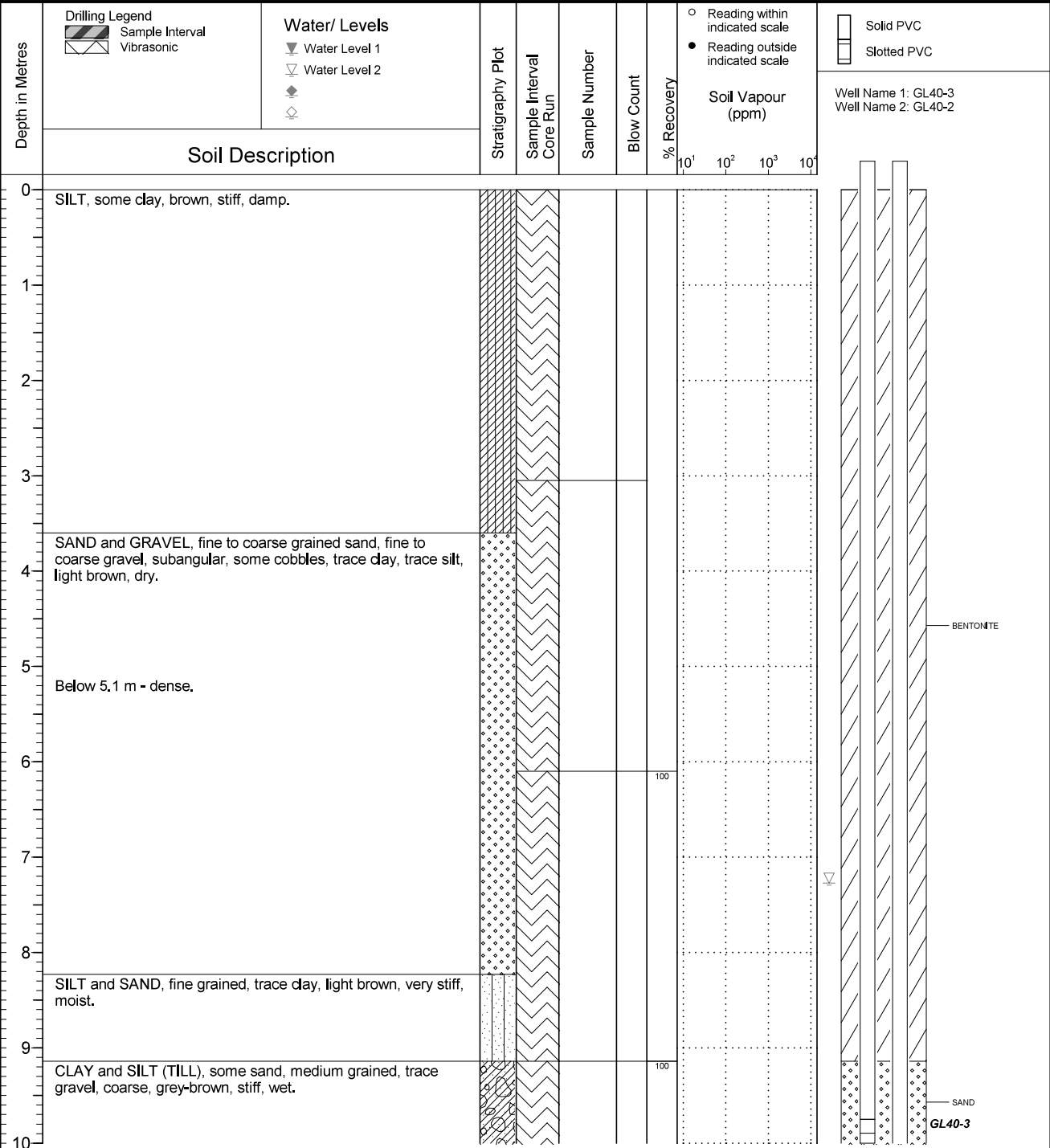
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 2

Drilling Contractor VanMars Drilling Ltd.  
Drilling Method Vibratory Sonic  
Borehole Dia. (m) 0.15  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 449.650  
Top of Casing Elev. (m) 450.440 450.450  
Northing: 5535523.760 Easting: 326466.400

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 11 15  
Log Typed By: KP



NOTES

QA RRW 2020 01 28 Print Date: 2020-02-04



Client  
City of Kelowna

Borehole No. : GL40-2/3

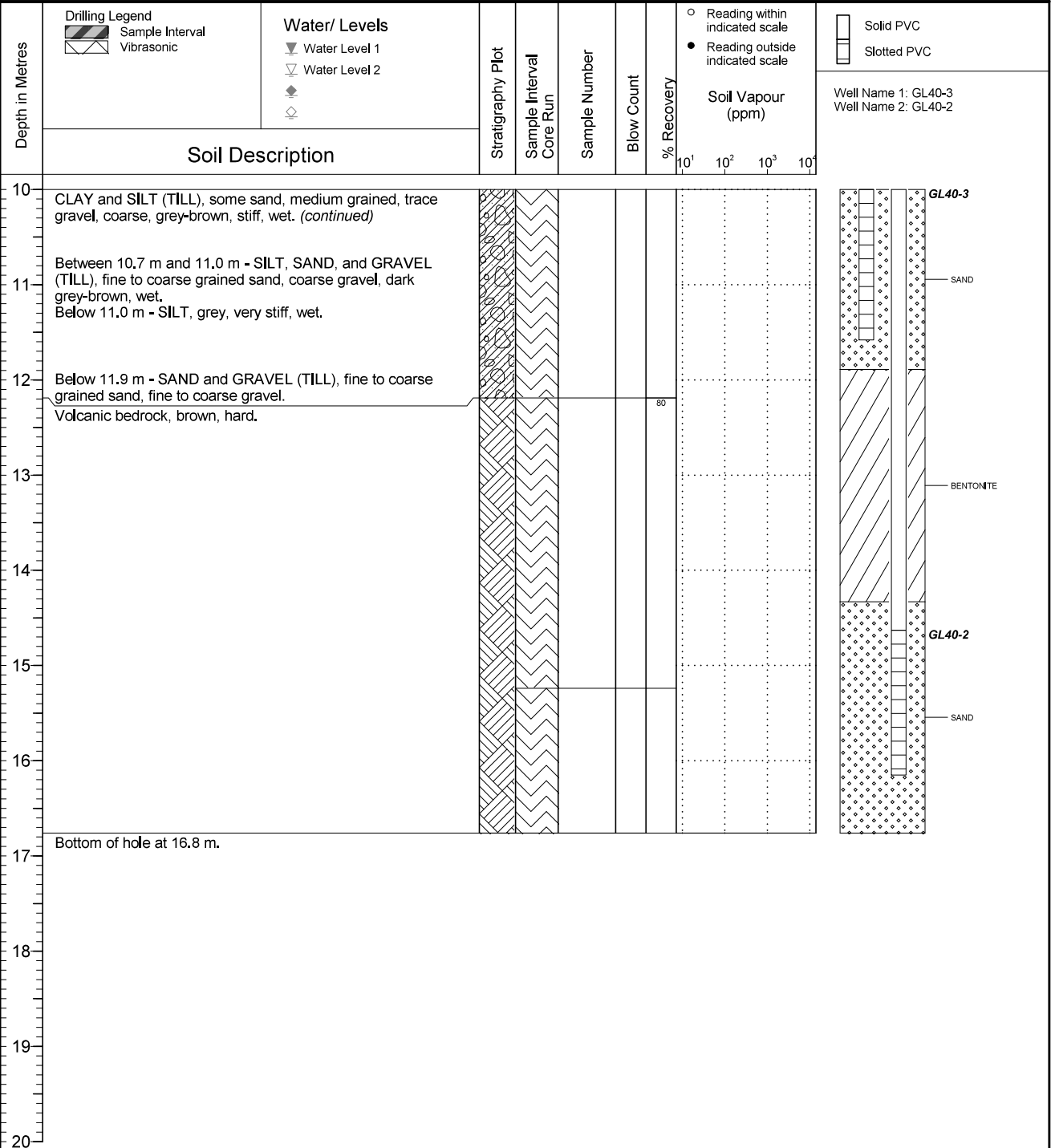
Location  
Glenmore Landfill, Kelowna, BC

PAGE 2 OF 2

Drilling Contractor VanMars Drilling Ltd.  
Drilling Method Vibratory Sonic  
Borehole Dia. (m) 0.15  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 449.650  
Top of Casing Elev. (m) 450.440 450.450  
Northing: 5535523.760 Easting: 326466.400

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 11 15  
Log Typed By: KP



NOTES





Client  
City of Kelowna

Borehole No. : GL41-1/2

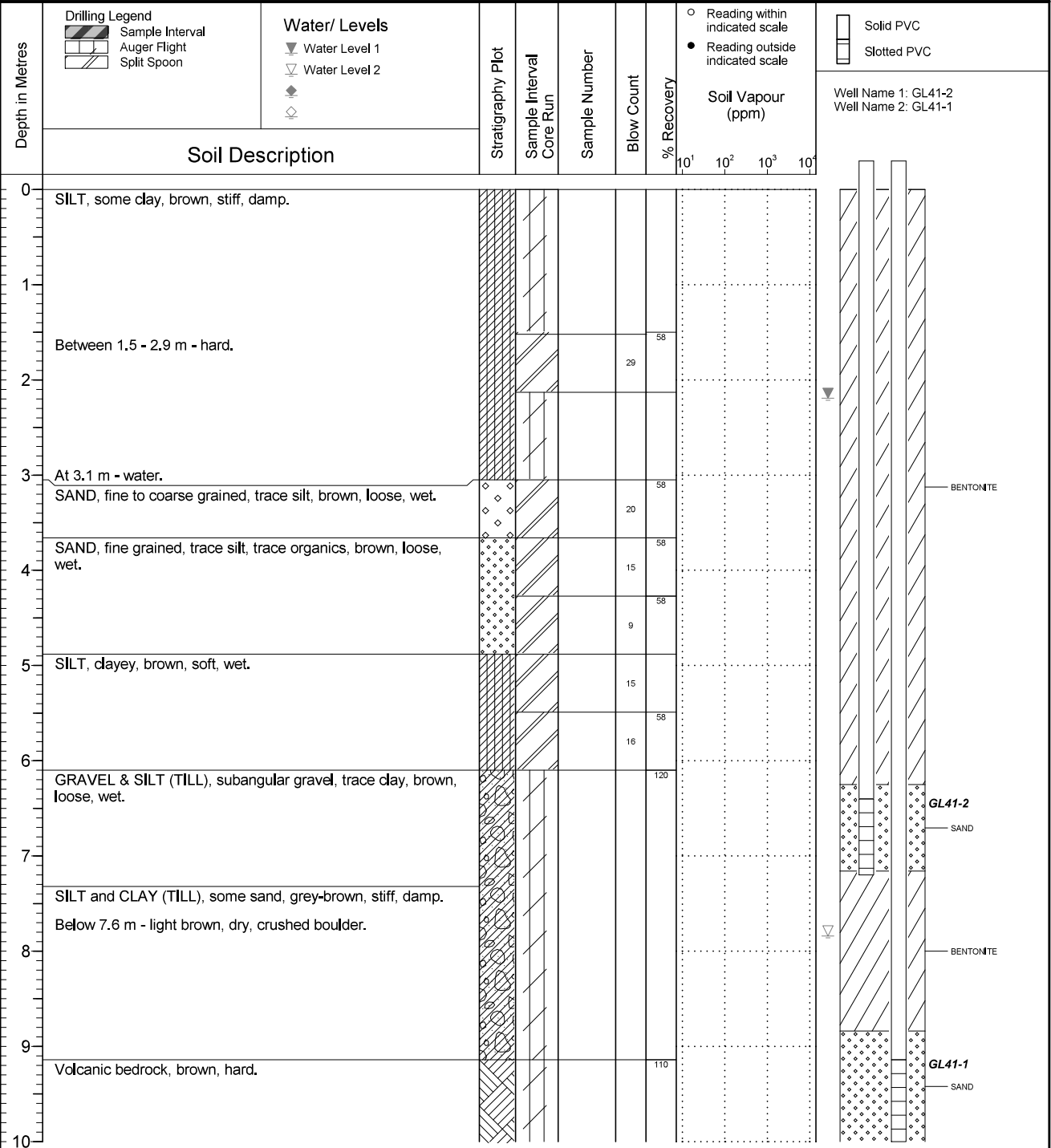
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 2

Drilling Contractor VanMars Drilling Ltd.  
Drilling Method Vibratory Sonic  
Borehole Dia. (m) 0.15  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 449.710  
Top of Casing Elev. (m) 450.570 450.550  
Northing: 5537673.352 Easting: 326191.337

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 11 15  
Log Typed By: KP



NOTES





Client  
City of Kelowna

Borehole No. : GL41-3

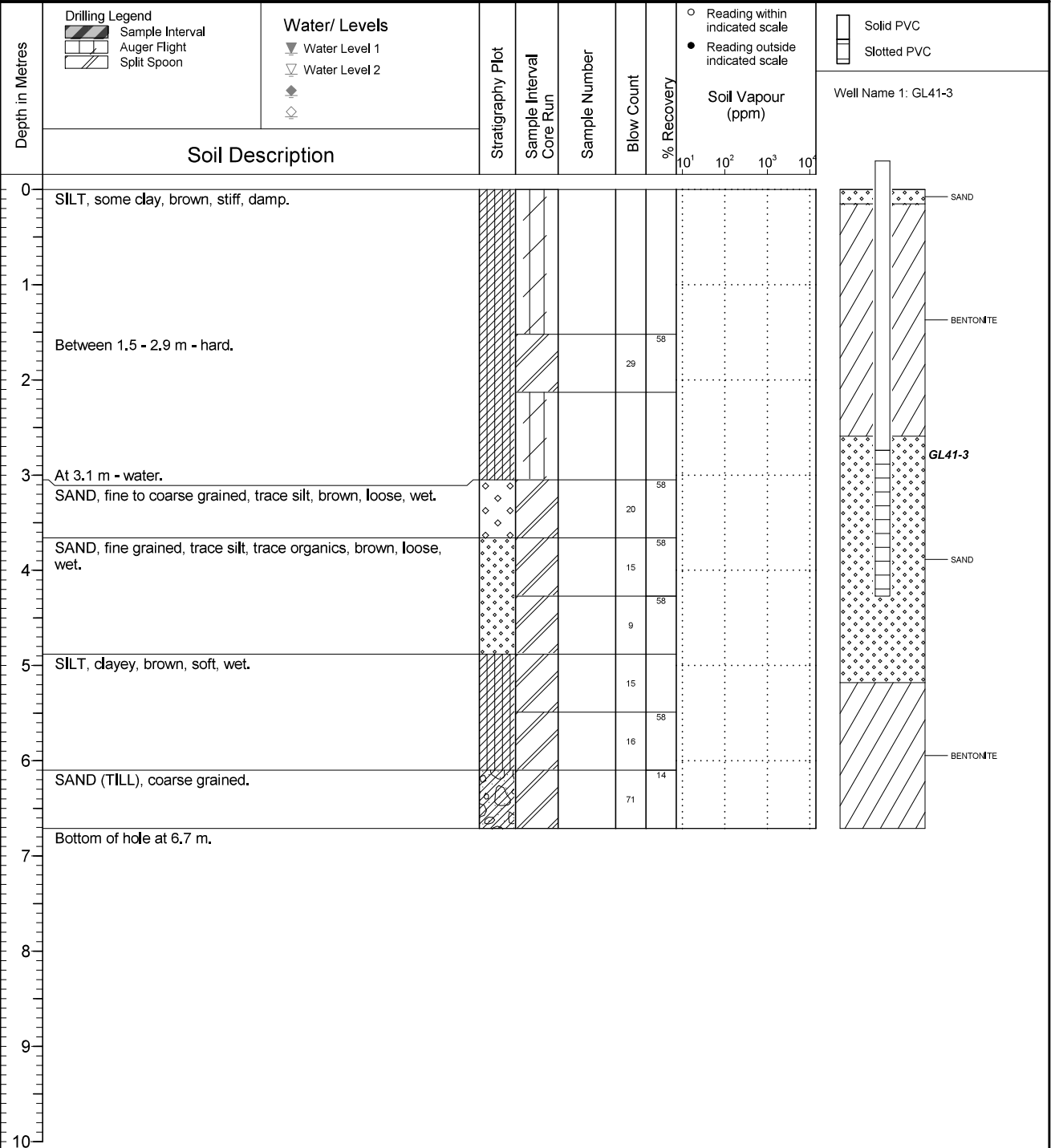
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 1

Drilling Contractor On The Mark  
Drilling Method Hollow Stem Auger  
Borehole Dia. (m) 0.05  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 449.720  
Top of Casing Elev. (m) 450.570  
Northing: 5537675.680 Easting: 326192.748

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 10 22  
Log Typed By: SGP/KP



QA\_RRW\_2020\_01\_28 Print Date: 2020-01-31

**NOTES**



Client  
City of Kelowna

Borehole No. : GL42-1/2

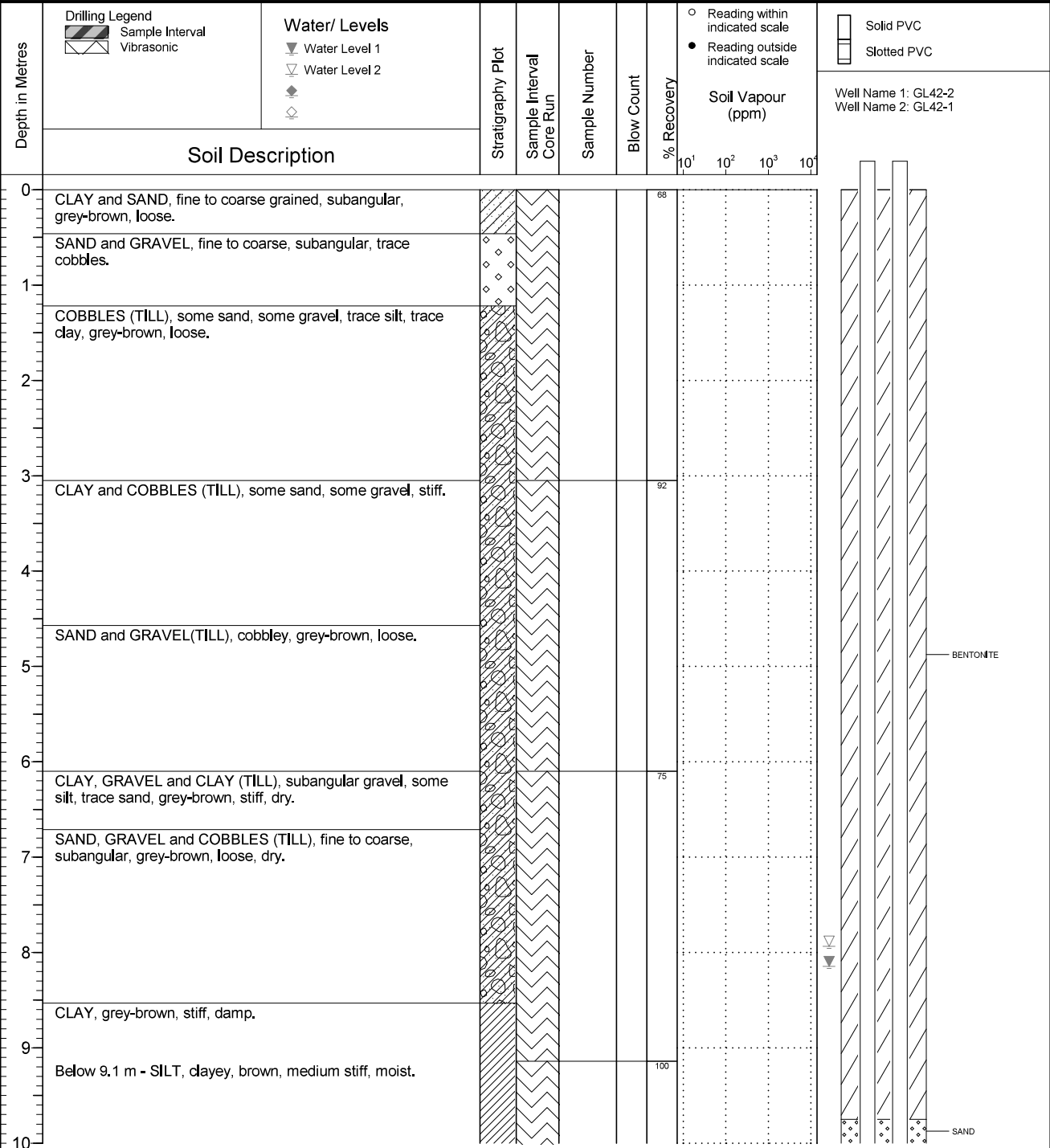
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 3

Drilling Contractor VanMars Drilling Ltd.  
Drilling Method Vibratory Sonic  
Borehole Dia. (m) 0.15  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 447.650  
Top of Casing Elev. (m) 448.430 448.420  
Northing: 5535422.733 Easting: 326636.214

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 11 14  
Log Typed By: KP



NOTES



Client  
City of Kelowna

Borehole No. : GL42-1/2

Location  
Glenmore Landfill, Kelowna, BC

PAGE 2 OF 3

Drilling Contractor VanMars Drilling Ltd.  
Drilling Method Vibratory Sonic  
Borehole Dia. (m) 0.15  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 447.650  
Top of Casing Elev. (m) 448.430 448.420  
Northing: 5535422.733 Easting: 326636.214

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 11 14  
Log Typed By: KP

Depth in Metres	Soil Description	Stratigraphy Plot	Sample Interval Core Run	Sample Number	Blow Count	% Recovery	Soil Vapour (ppm)				Well Name 1: GL42-2 Well Name 2: GL42-1	
							10 <sup>1</sup>	10 <sup>2</sup>	10 <sup>3</sup>	10 <sup>4</sup>		
10	CLAY, grey-brown, stiff, damp. (continued)											
11												
12	At 12.2 m - sandy, some gravel, damp.					100						
13	COBBLES and SAND (TILL), subangular, trace silt, grey-brown, damp.											
14	SILT (TILL), sandy, trace clay, grey-brown, stiff, loose, dry.											
15	SAND, GRAVEL and COBBLES (TILL), grey, stiff, dry.											
16	CLAY (TILL), some silt, some gravel, subangular, grey, stiff, moist.					99						
17	COBBLES (TILL), some clay, some sand, fine grained, grey, stiff.											
18												
19	SAND and GRAVEL (TILL), fine to coarse, subangular, trace silt, dark grey-brown, loose, moist.					97						
20	At 19.5 m - boulder. Below 19.8 m - cobbles and gravel, subangular, some sand,											

NOTES

QA RRVW 2020 01 28 Print Date: 2020-01-31



Client  
City of Kelowna

Borehole No. : GL42-1/2

Location  
Glenmore Landfill, Kelowna, BC

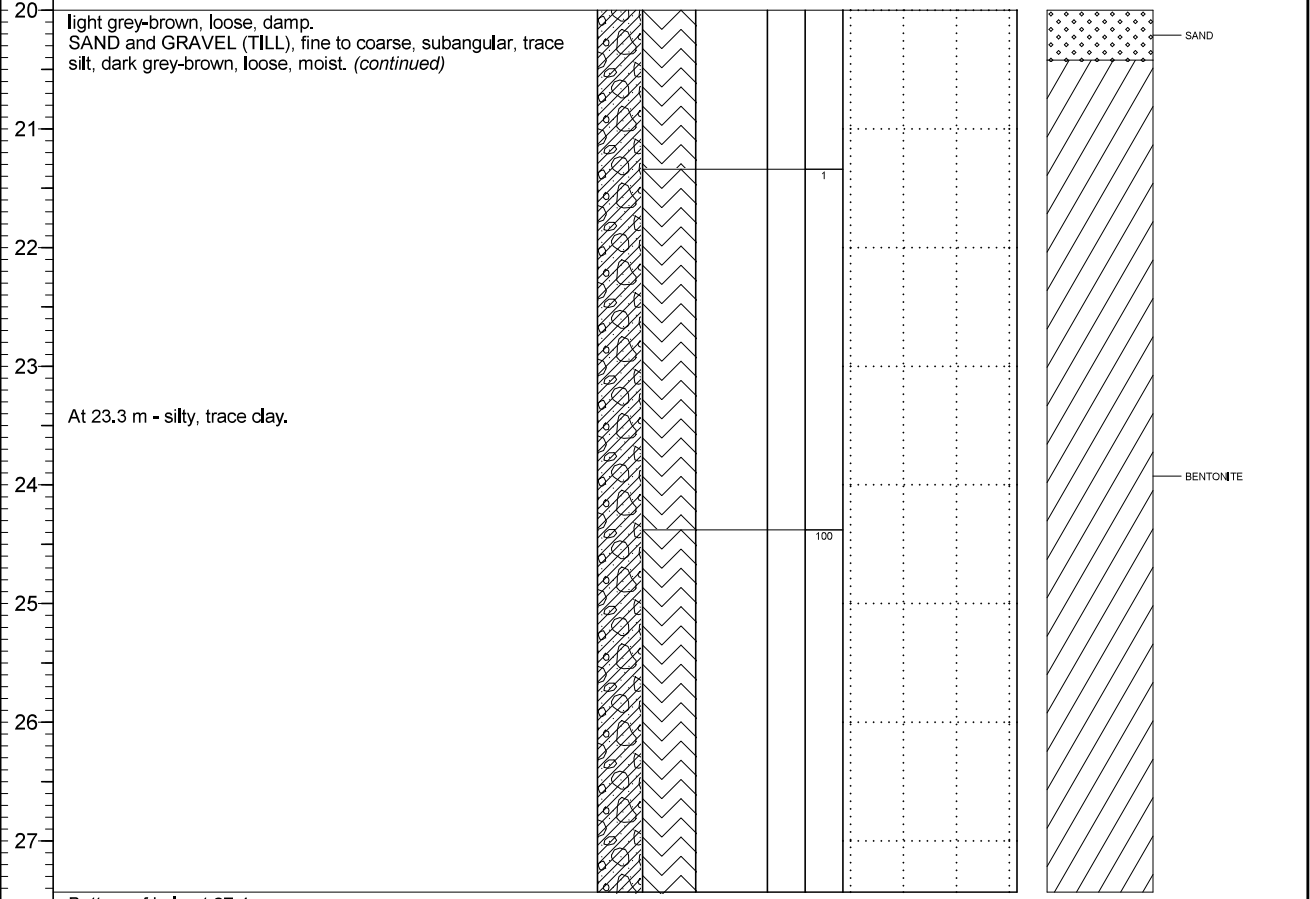
PAGE 3 OF 3

Drilling Contractor VanMars Drilling Ltd.  
Drilling Method Vibratory Sonic  
Borehole Dia. (m) 0.15  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 447.650  
Top of Casing Elev. (m) 448.430 448.420  
Northing: 5535422.733 Easting: 326636.214

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 11 14  
Log Typed By: KP

Depth in Metres	<b>Drilling Legend</b> Sample Interval Vibrasonic	<b>Water/ Levels</b> Water Level 1 Water Level 2  	Stratigraphy Plot	Sample Interval Core Run	Sample Number	Blow Count	% Recovery	<input type="checkbox"/> Reading within indicated scale <input checked="" type="checkbox"/> Reading outside indicated scale	Solid PVC Slotted PVC
	Soil Description	Soil Vapour (ppm)						Well Name 1: GL42-2 Well Name 2: GL42-1	



NOTES





Client  
City of Kelowna

Borehole No. : GL42-3

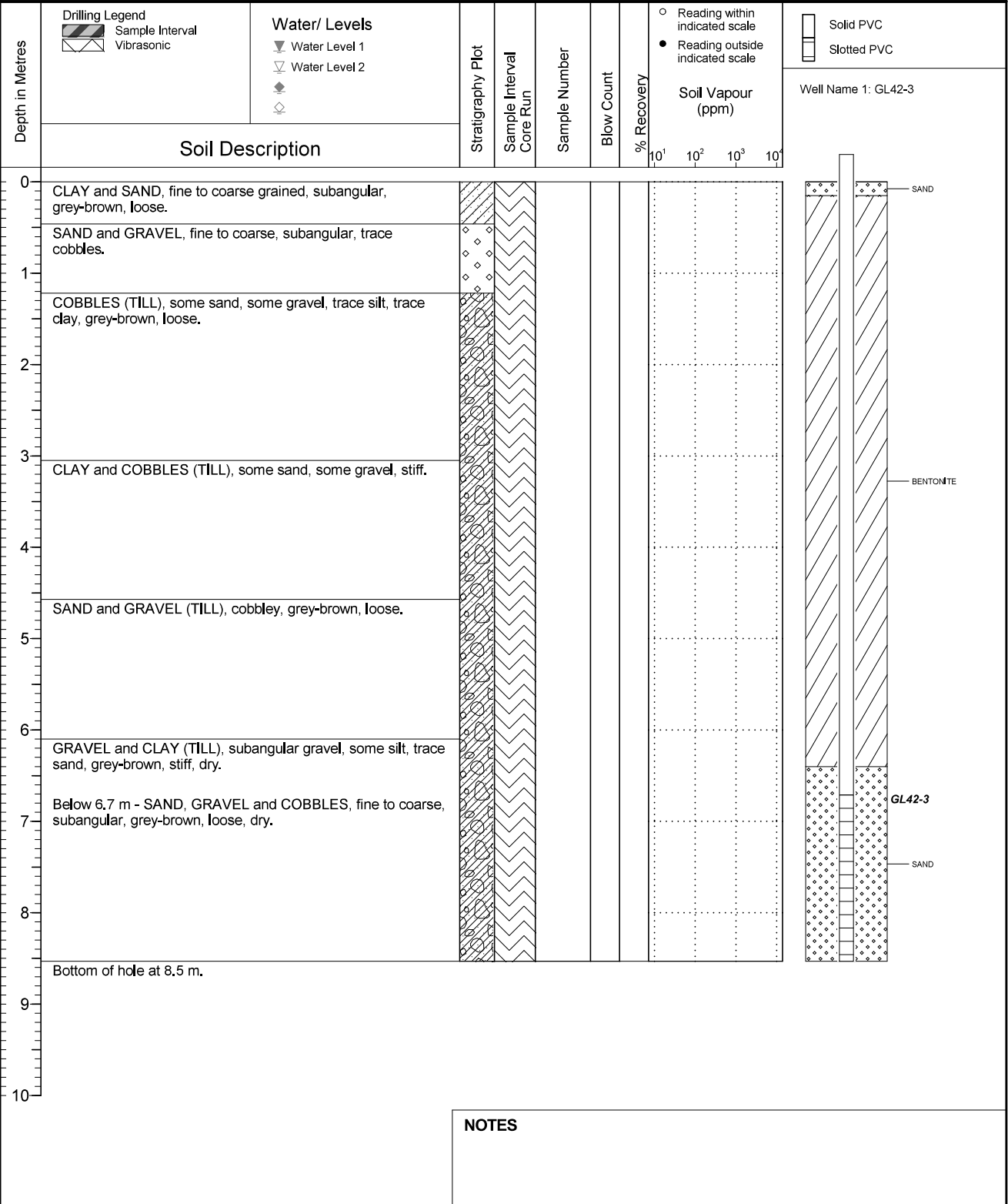
Location  
Glenmore Landfill, Kelowna, BC

PAGE 1 OF 1

Drilling Contractor VanMars Drilling Ltd.  
Drilling Method Vibratory Sonic  
Borehole Dia. (m) 0.15  
Pipe/Slotted Pipe Dia. (m) 0.05/0.05

Date Monitored 2019 12 03  
Ground Surface Elev. (m) 447.660  
Top of Casing Elev. (m) 448.470  
Northing: 5535423.945 Easting: 326637.566

Project Number: 662036  
Borehole Logged By: NL  
Date Drilled: 2019 11 14  
Log Typed By: KP

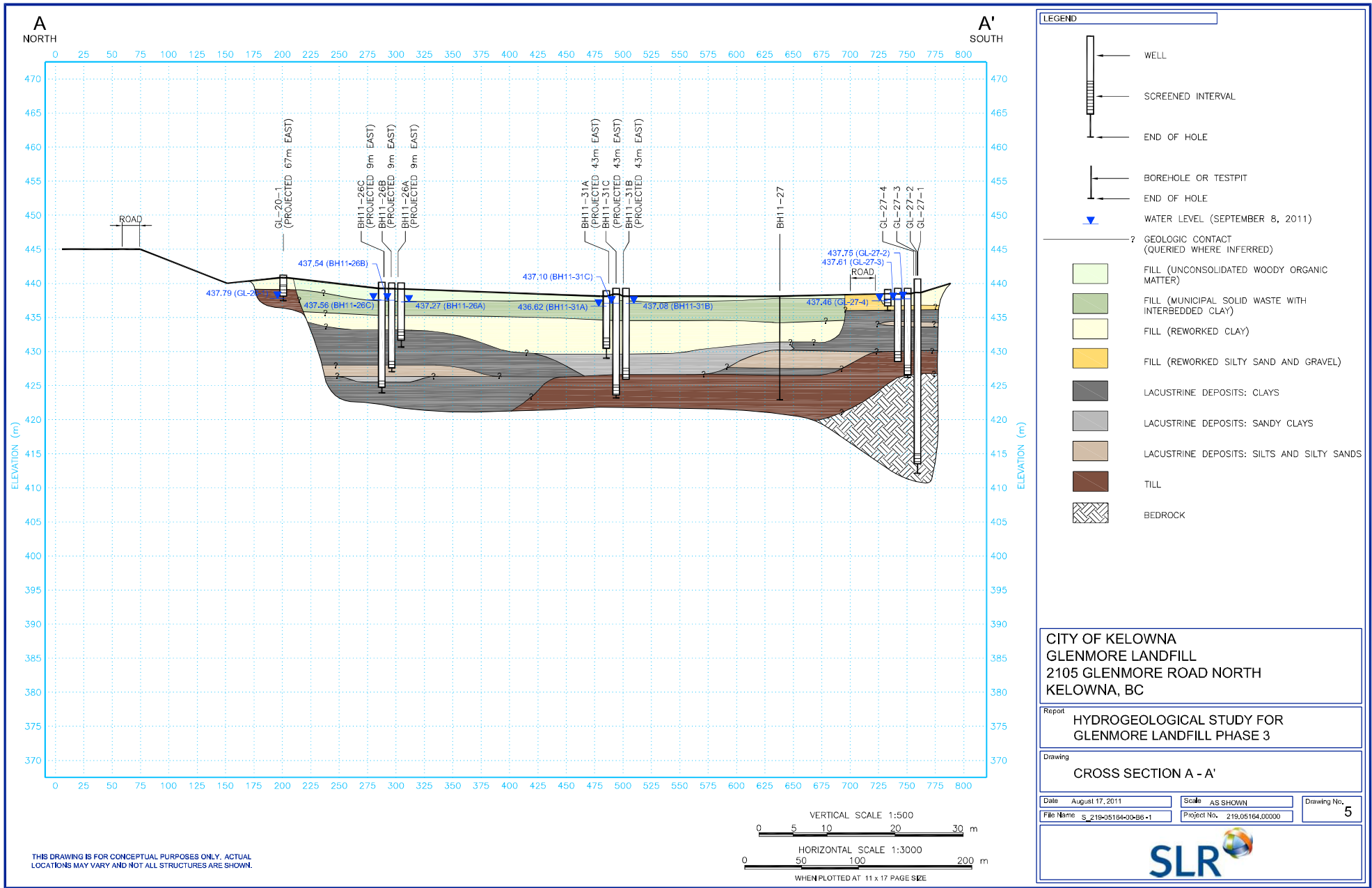


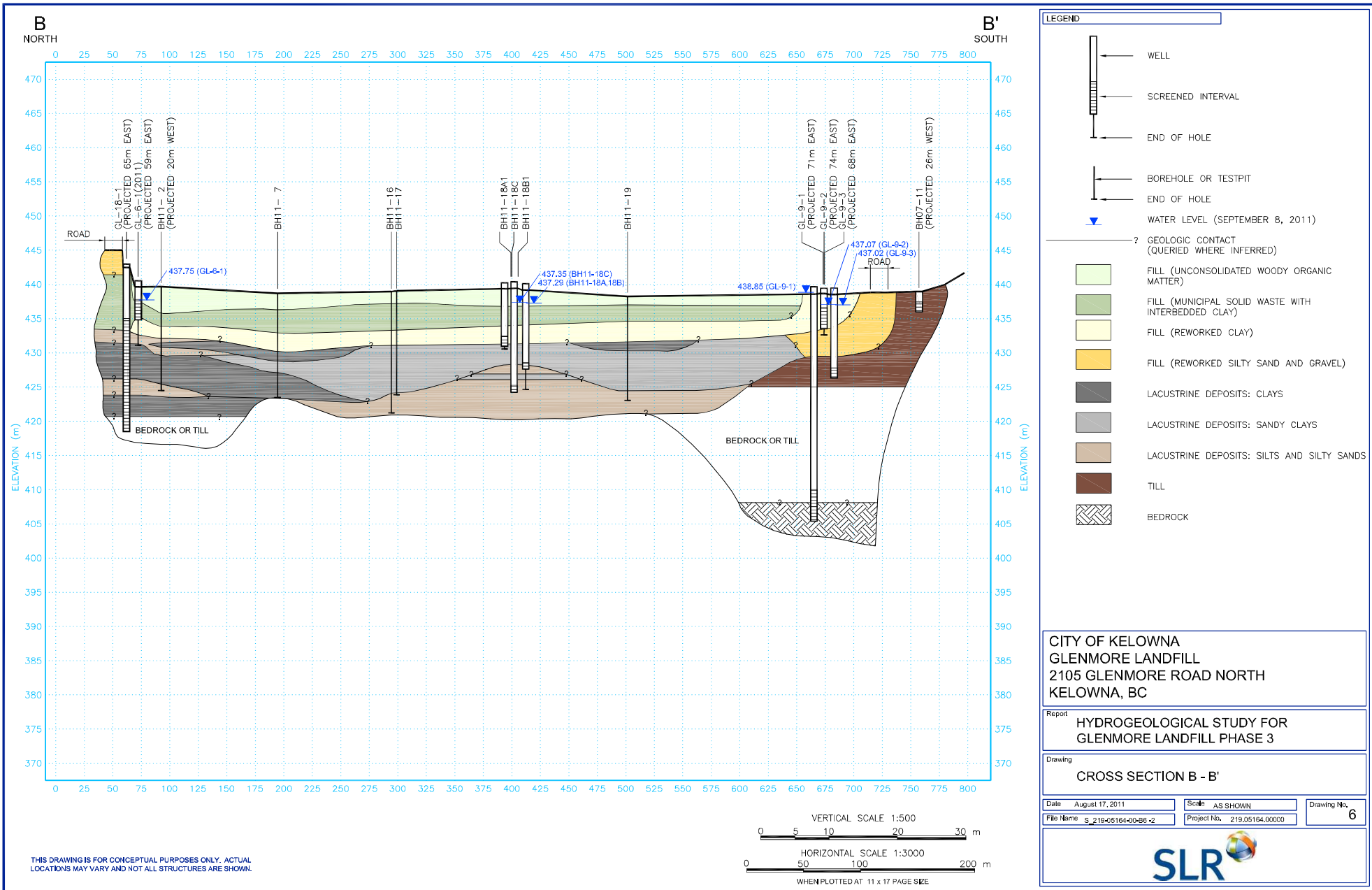
QA\_RRW\_2020\_01\_28 Print Date: 2020-01-31

NOTES

# **Appendix C.2**

**SLR Cross-Sections**





**LEGEND**

- WELL
- SCREENED INTERVAL
- END OF HOLE
- BOREHOLE OR TESTPIT
- END OF HOLE
- WATER LEVEL (SEPTEMBER 8, 2011)
- GEOLOGIC CONTACT (QUERIED WHERE INFERRED)
- FILL (UNCONSOLIDATED WOODY ORGANIC MATTER)
- FILL (MUNICIPAL SOLID WASTE WITH INTERBEDDED CLAY)
- FILL (REWORKED CLAY)
- FILL (REWORKED SILTY SAND AND GRAVEL)
- LACUSTRINE DEPOSITS: CLAYS
- LACUSTRINE DEPOSITS: SANDY CLAYS
- LACUSTRINE DEPOSITS: SILTS AND SILTY SANDS
- TILL
- BEDROCK

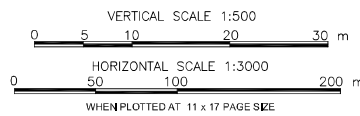
**CITY OF KELOWNA**  
**GLENMORE LANDFILL**  
**2105 GLENMORE ROAD NORTH**  
**KELOWNA, BC**

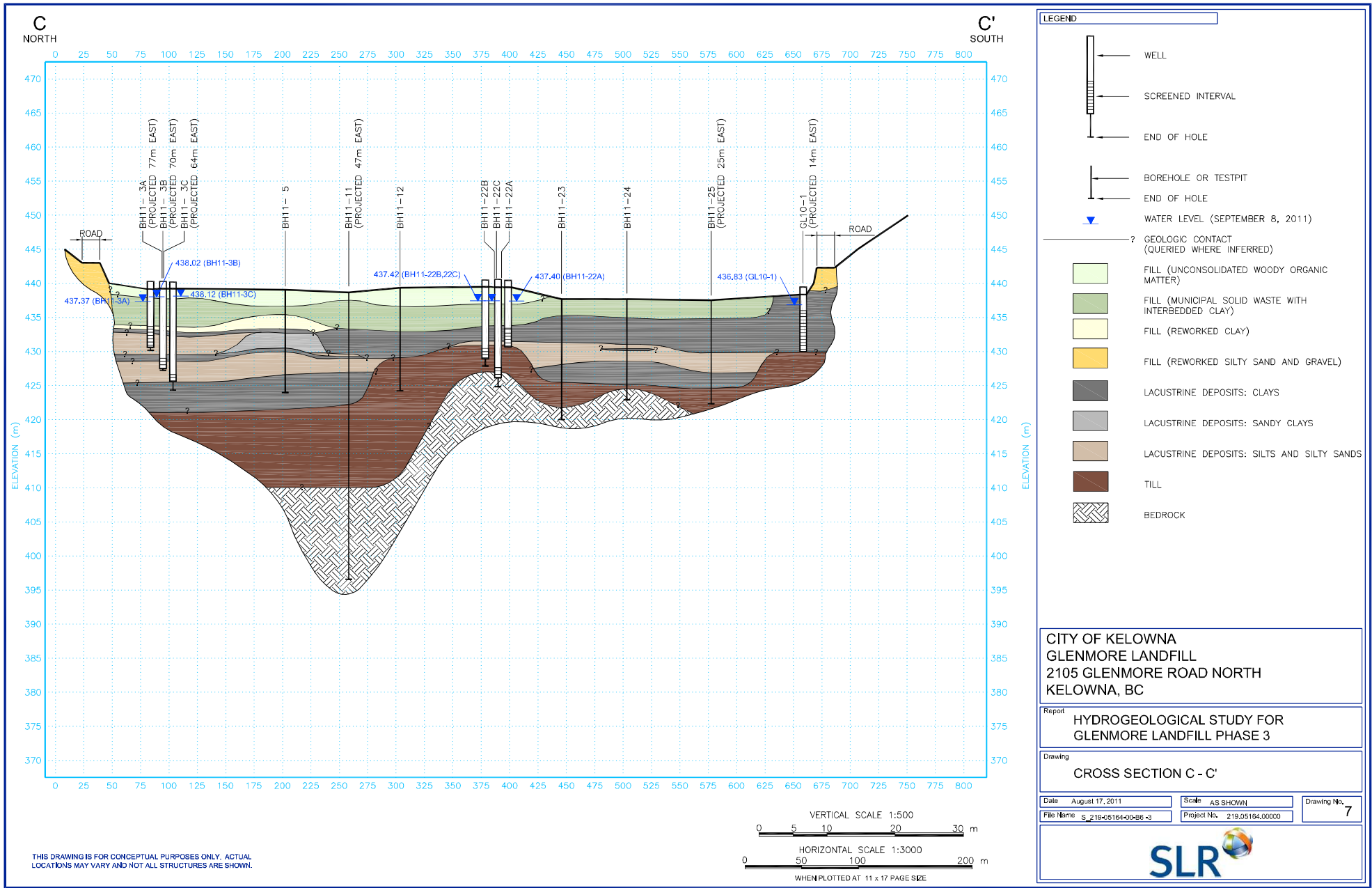
Report  
**HYDROGEOLOGICAL STUDY FOR GLENMORE LANDFILL PHASE 3**

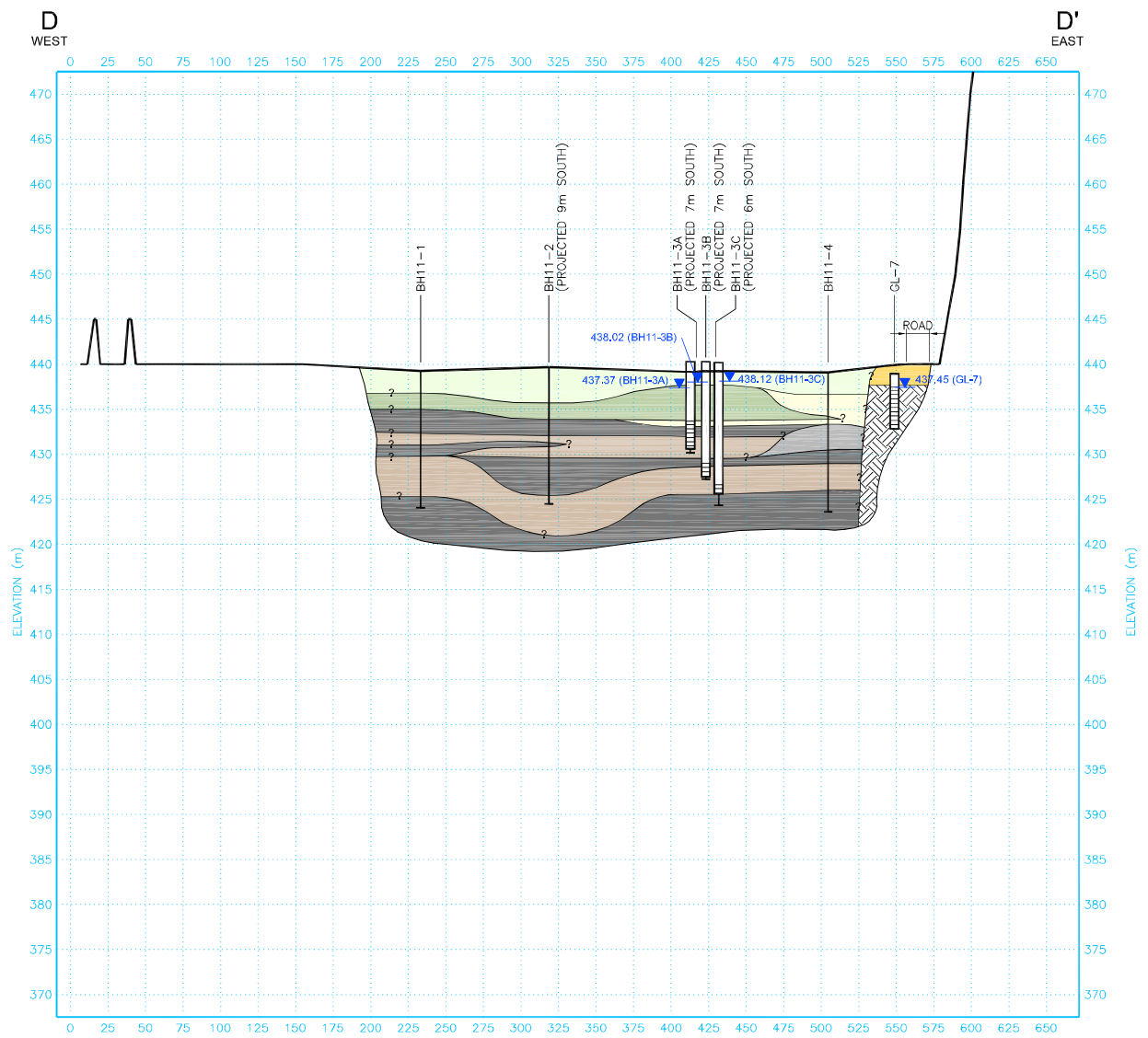
Drawing  
**CROSS SECTION B - B'**

Date: August 17, 2011	Scale: AS SHOWN	Drawing No.:
File Name: S_219-05164-00-B6-x2	Project No.: 219.05164.00000	<b>6</b>

THIS DRAWING IS FOR CONCEPTUAL PURPOSES ONLY. ACTUAL LOCATIONS MAY VARY AND NOT ALL STRUCTURES ARE SHOWN.







**LEGEND**

- WELL
- SCREENED INTERVAL
- END OF HOLE
- BOREHOLE OR TESTPIT
- END OF HOLE
- WATER LEVEL (SEPTEMBER 8, 2011)
- GEOLOGIC CONTACT (QUERIED WHERE INFERRED)
- FILL (UNCONSOLIDATED WOODY ORGANIC MATTER)
- FILL (MUNICIPAL SOLID WASTE WITH INTERBEDDED CLAY)
- FILL (REWORKED CLAY)
- FILL (REWORKED SILTY SAND AND GRAVEL)
- LACUSTRINE DEPOSITS: CLAYS
- LACUSTRINE DEPOSITS: SANDY CLAYS
- LACUSTRINE DEPOSITS: SILTS AND SILTY SANDS
- TILL
- BEDROCK

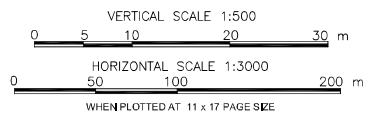
**CITY OF KELOWNA  
 GLENMORE LANDFILL  
 2105 GLENMORE ROAD NORTH  
 KELOWNA, BC**

Report  
**HYDROGEOLOGICAL STUDY FOR  
 GLENMORE LANDFILL PHASE 3**

Drawing  
**CROSS SECTION D - D'**

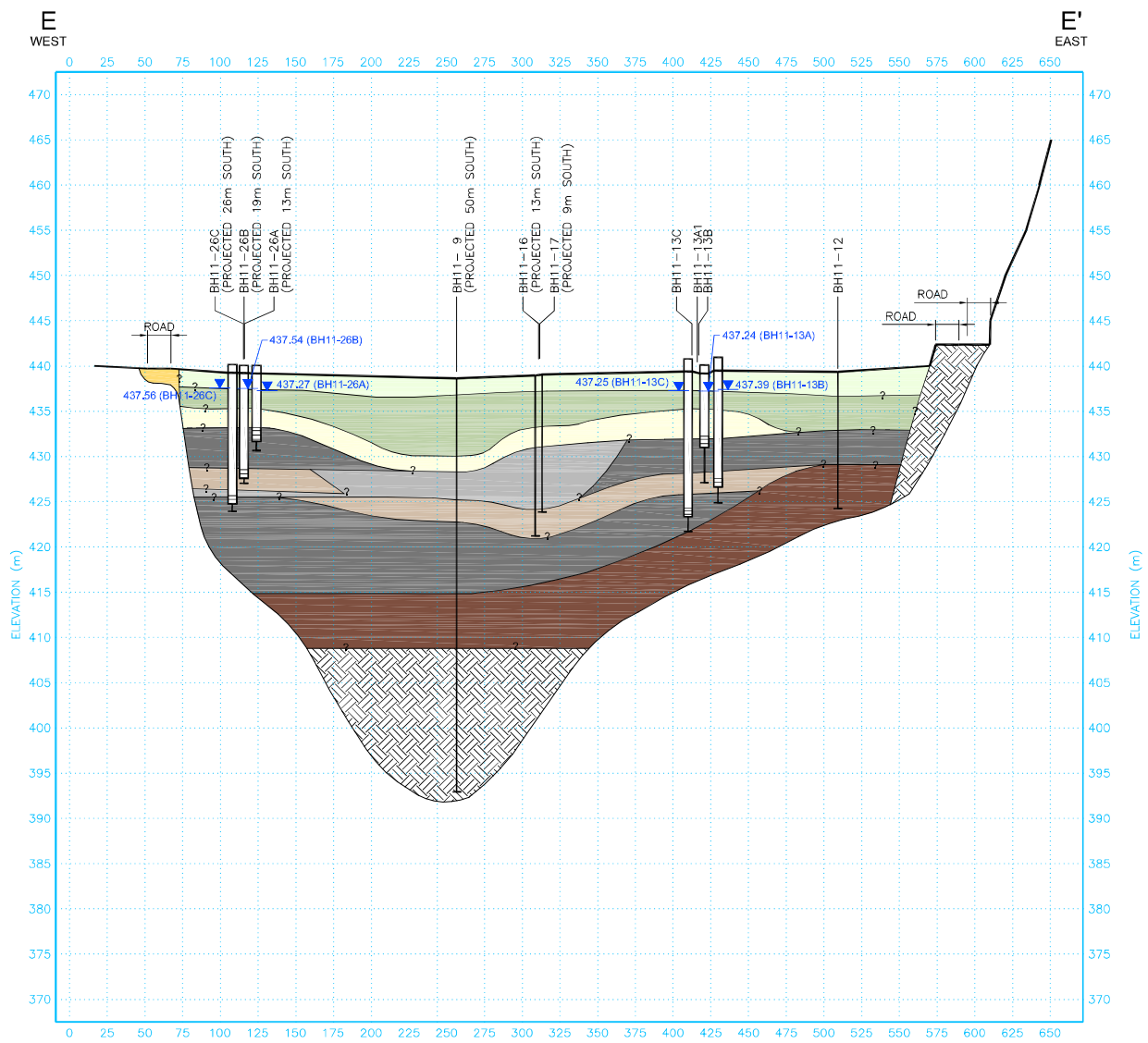
Date	August 17, 2011	Scale	AS SHOWN	Drawing No.	8
File Name	S_219-05164-00-08-e1	Project No.	219.05164.00000		

**SLR**



THIS DRAWING IS FOR CONCEPTUAL PURPOSES ONLY. ACTUAL LOCATIONS MAY VARY AND NOT ALL STRUCTURES ARE SHOWN.





**LEGEND**

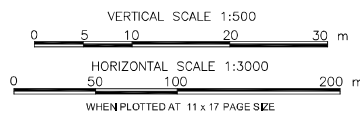
- WELL
- SCREENED INTERVAL
- END OF HOLE
- BOREHOLE OR TESTPIT
- END OF HOLE
- WATER LEVEL (SEPTEMBER 8, 2011)
- GEOLGIC CONTACT (QUERIED WHERE INFERRED)
- FILL (UNCONSOLIDATED WOODY ORGANIC MATTER)
- FILL (MUNICIPAL SOLID WASTE WITH INTERBEDDED CLAY)
- FILL (REWORKED CLAY)
- FILL (REWORKED SILTY SAND AND GRAVEL)
- LACUSTRINE DEPOSITS: CLAYS
- LACUSTRINE DEPOSITS: SANDY CLAYS
- LACUSTRINE DEPOSITS: SILTS AND SILTY SANDS
- TILL
- BEDROCK

**CITY OF KELOWNA**  
**GLENMORE LANDFILL**  
**2105 GLENMORE ROAD NORTH**  
**KELOWNA, BC**

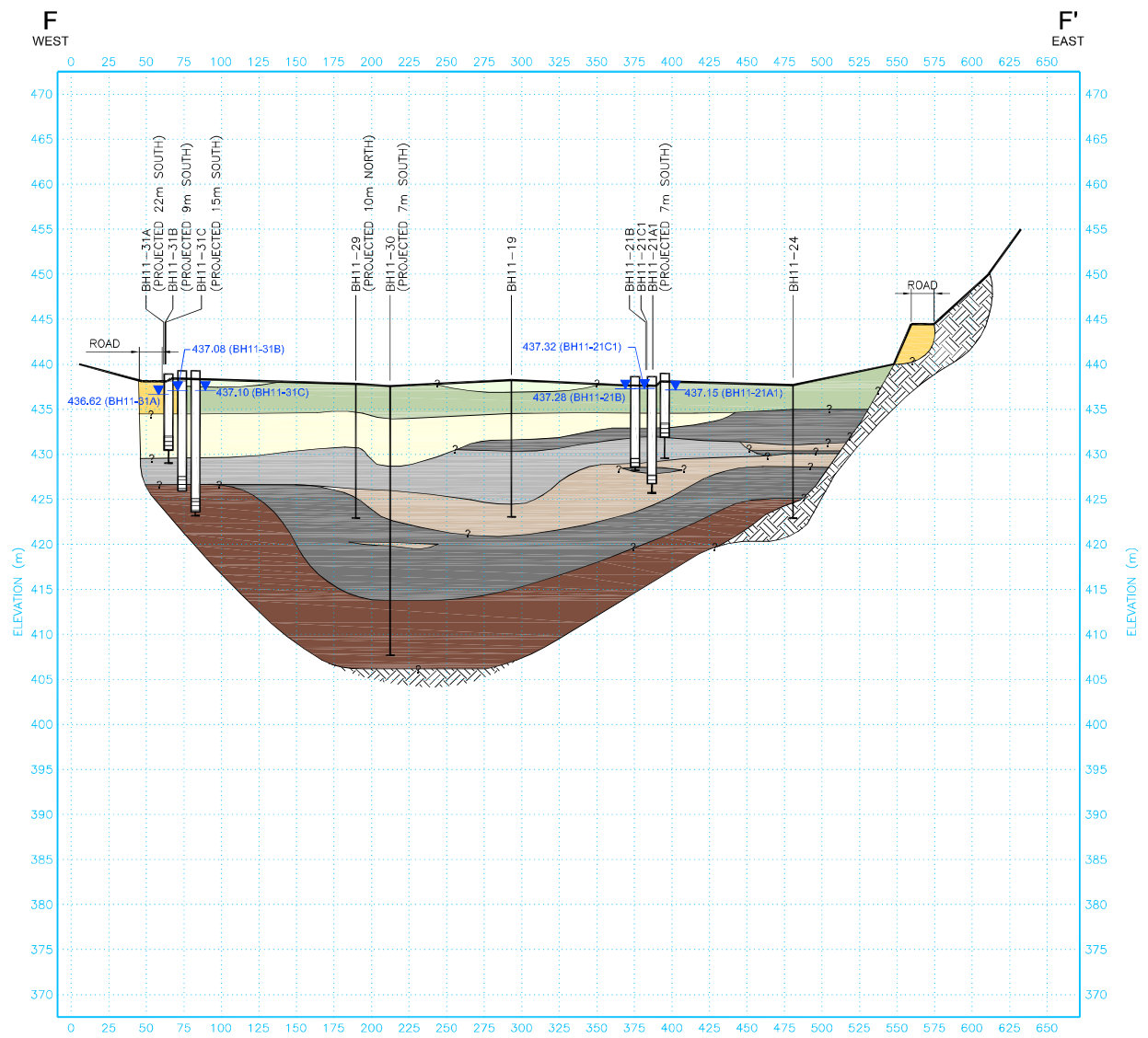
Report  
**HYDROGEOLOGICAL STUDY FOR GLENMORE LANDFILL PHASE 3**

Drawing  
**CROSS SECTION E - E'**

Date	August 17, 2011	Scale	AS SHOWN	Drawing No.	9
File Name	S_219-05164-00-08-s	Project No.	219.05164.00000		



THIS DRAWING IS FOR CONCEPTUAL PURPOSES ONLY. ACTUAL LOCATIONS MAY VARY AND NOT ALL STRUCTURES ARE SHOWN.



**LEGEND**

- WELL
- SCREENED INTERVAL
- END OF HOLE
- BOREHOLE OR TESTPIT
- END OF HOLE
- WATER LEVEL (SEPTEMBER 8, 2011)
- GEOLOGIC CONTACT (QUERIED WHERE INFERRED)
- FILL (UNCONSOLIDATED WOODY ORGANIC MATTER)
- FILL (MUNICIPAL SOLID WASTE WITH INTERBEDDED CLAY)
- FILL (REWORKED CLAY)
- FILL (REWORKED SILTY SAND AND GRAVEL)
- LACUSTRINE DEPOSITS: CLAYS
- LACUSTRINE DEPOSITS: SANDY CLAYS
- LACUSTRINE DEPOSITS: SILTS AND SILTY SANDS
- TILL
- BEDROCK

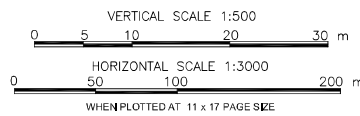
**CITY OF KELOWNA  
 GLENMORE LANDFILL  
 2105 GLENMORE ROAD NORTH  
 KELOWNA, BC**

Report  
**HYDROGEOLOGICAL STUDY FOR  
 GLENMORE LANDFILL PHASE 3**

Drawing  
**CROSS SECTION F - F'**

Date	August 17, 2011	Scale	AS SHOWN	Drawing No.	10
File Name	S_219-05164-00-B6-6	Project No.	219.05164.00000		

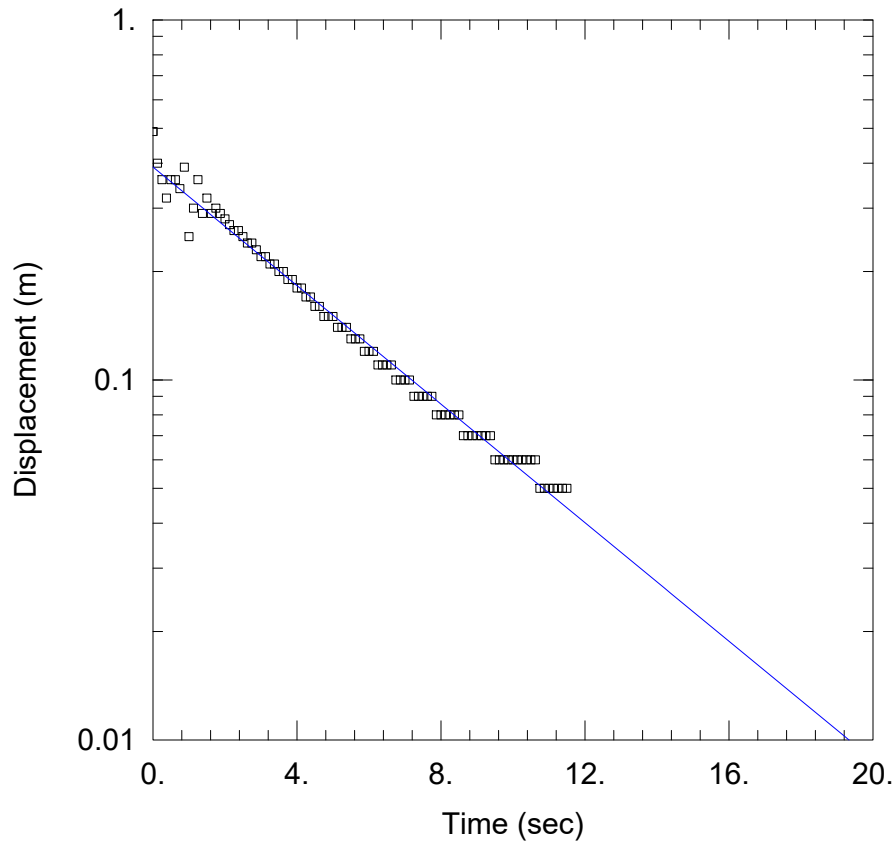
**SLR**



THIS DRAWING IS FOR CONCEPTUAL PURPOSES ONLY. ACTUAL LOCATIONS MAY VARY AND NOT ALL STRUCTURES ARE SHOWN.

# Appendix D

**AQTESOLVE Single Well Response Plots**



### GL5-2 TEST 1 FALLING HEAD

Data Set: \...\GL5-2 Test 1 Falling Head.aqt

Date: 07/11/23

Time: 17:32:41

### PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL5-2

Test Date: 6/8/2023

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 8.959E-5$  m/sec

$y_0 = 0.3901$  m

### AQUIFER DATA

Saturated Thickness: 5.55 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

### WELL DATA (GL5-2)

Initial Displacement: 0.49 m

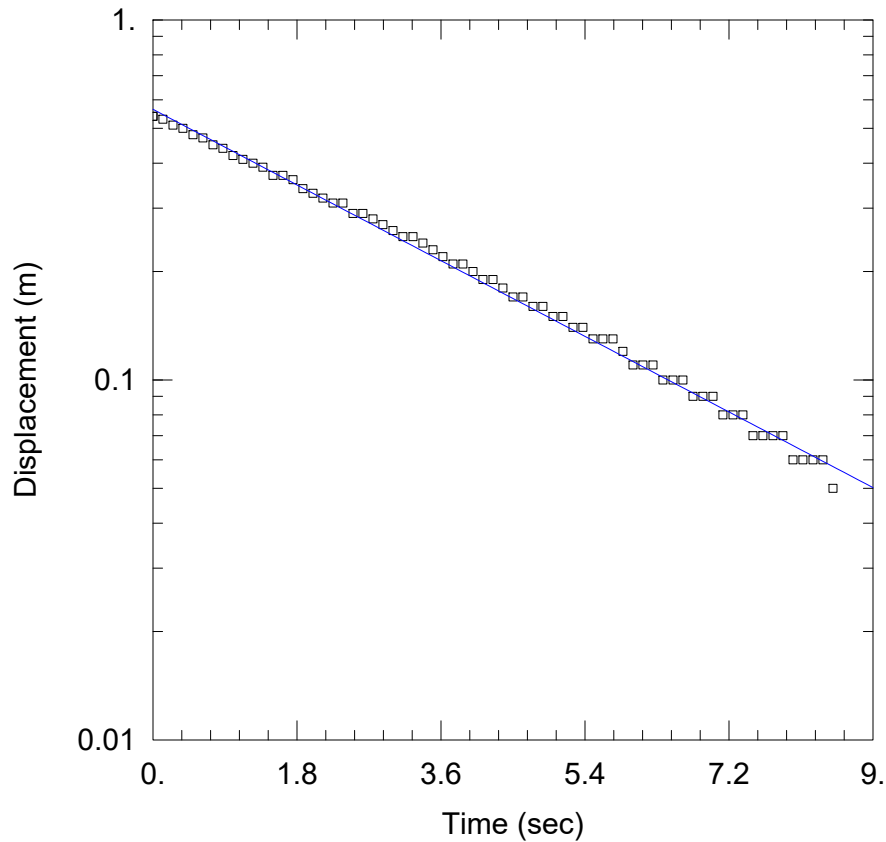
Total Well Penetration Depth: 8.05 m

Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m

Screen Length: 2.5 m

Well Radius: 0.075 m



GL5-2 TEST 2 RISING HEAD

Data Set: \...\GL5-2 Test 2 Rising Head.aqt

Date: 07/11/23

Time: 17:35:08

PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL5-2

Test Date: 6/8/2023

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.0001271$  m/sec

$y_0 = 0.5644$  m

AQUIFER DATA

Saturated Thickness: 5.55 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL5-2)

Initial Displacement: 0.54 m

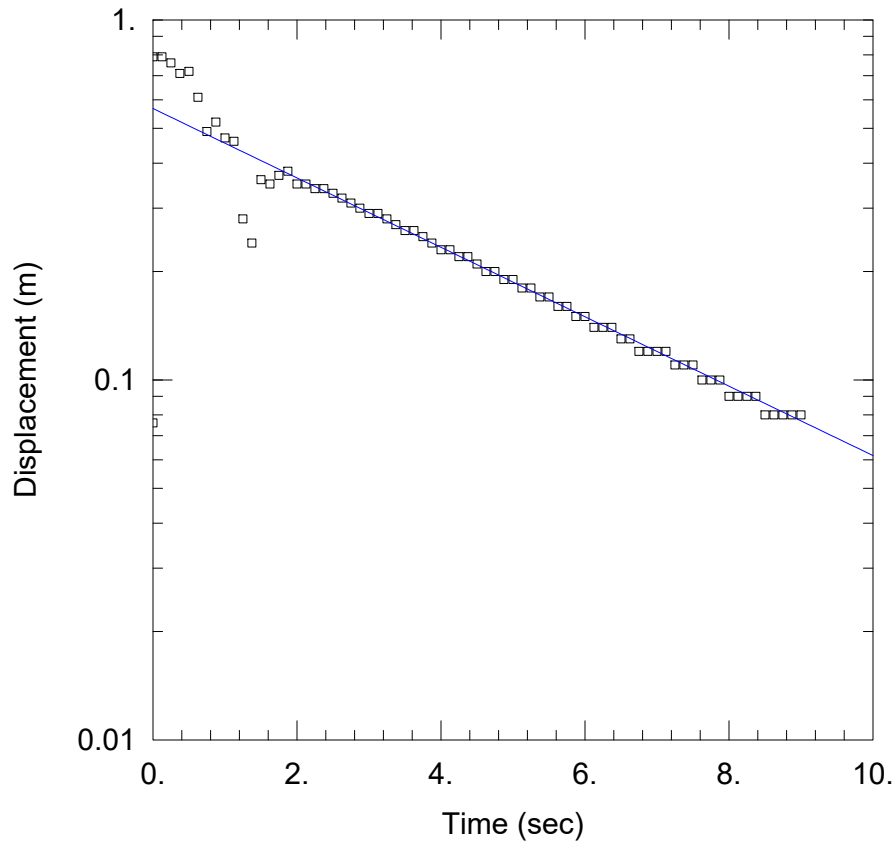
Total Well Penetration Depth: 8.05 m

Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m

Screen Length: 2.5 m

Well Radius: 0.075 m



GL5-2 TEST 3 FALLING HEAD

Data Set: \...\GL5-2 Test 3 Falling Head.aqt

Date: 07/11/23

Time: 17:40:44

PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL5-2

Test Date: 6/8/2023

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.0001049$  m/sec

$y_0 = 0.5673$  m

AQUIFER DATA

Saturated Thickness: 5.55 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL5-2)

Initial Displacement: 0.076 m

Total Well Penetration Depth: 8.05 m

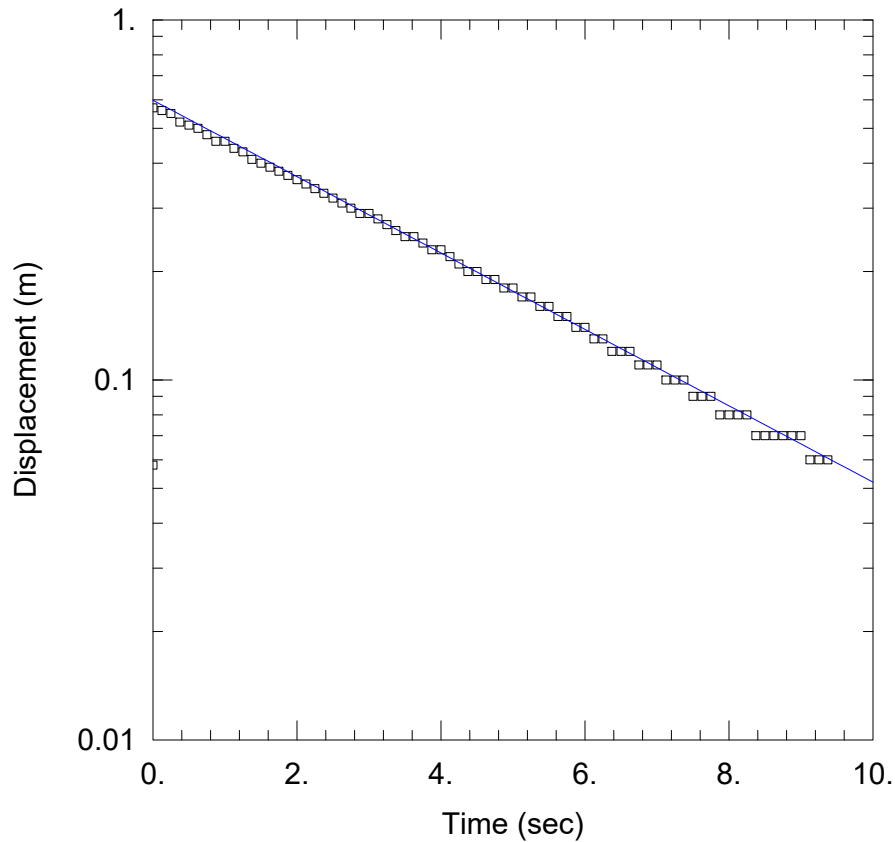
Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m

Screen Length: 2.5 m

Well Radius: 0.075 m





GL5-2 TEST 4 RISING HEAD

Data Set: \...\GL5-2 Test 4 Rising Head.aqt

Date: 07/11/23

Time: 17:42:27

PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL5-2

Test Date: 6/8/2023

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.0001149$  m/sec

$y_0 = 0.5843$  m

AQUIFER DATA

Saturated Thickness: 5.55 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL5-2)

Initial Displacement: 0.058 m

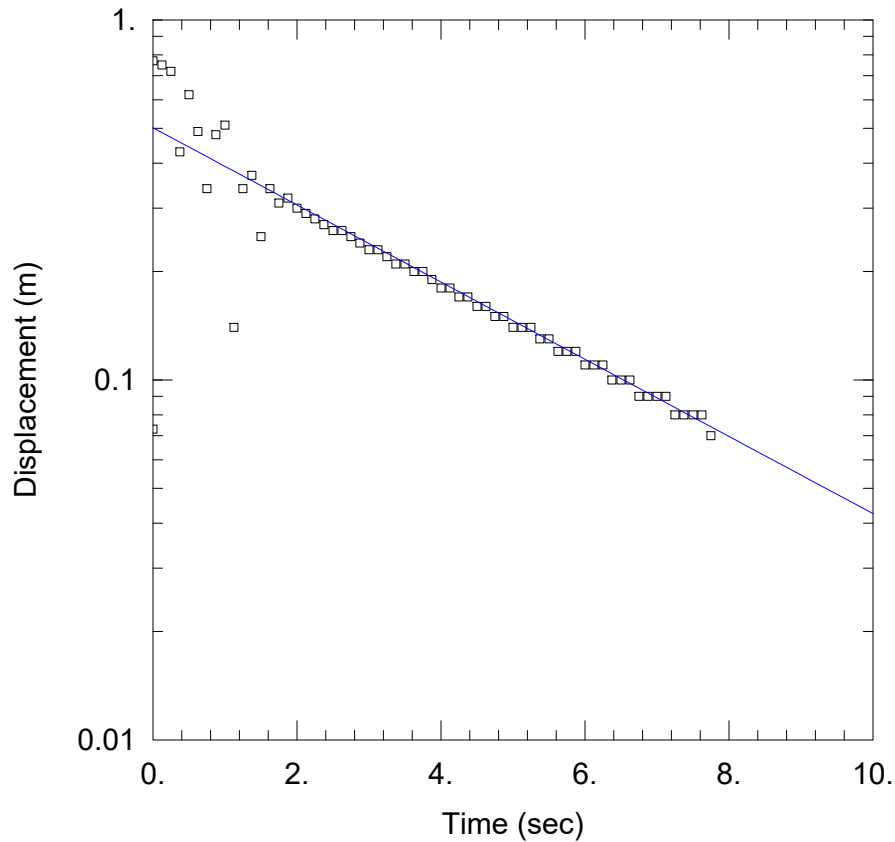
Total Well Penetration Depth: 8.05 m

Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m

Screen Length: 2.5 m

Well Radius: 0.075 m



GL5-2 TEST 5 FALLING HEAD

Data Set: \...\GL5-2 Test 5 Falling Head.aqt  
 Date: 07/11/23 Time: 17:43:52

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL5-2  
 Test Date: 6/8/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 0.0001166$  m/sec  
 $y_0 = 0.5016$  m

AQUIFER DATA

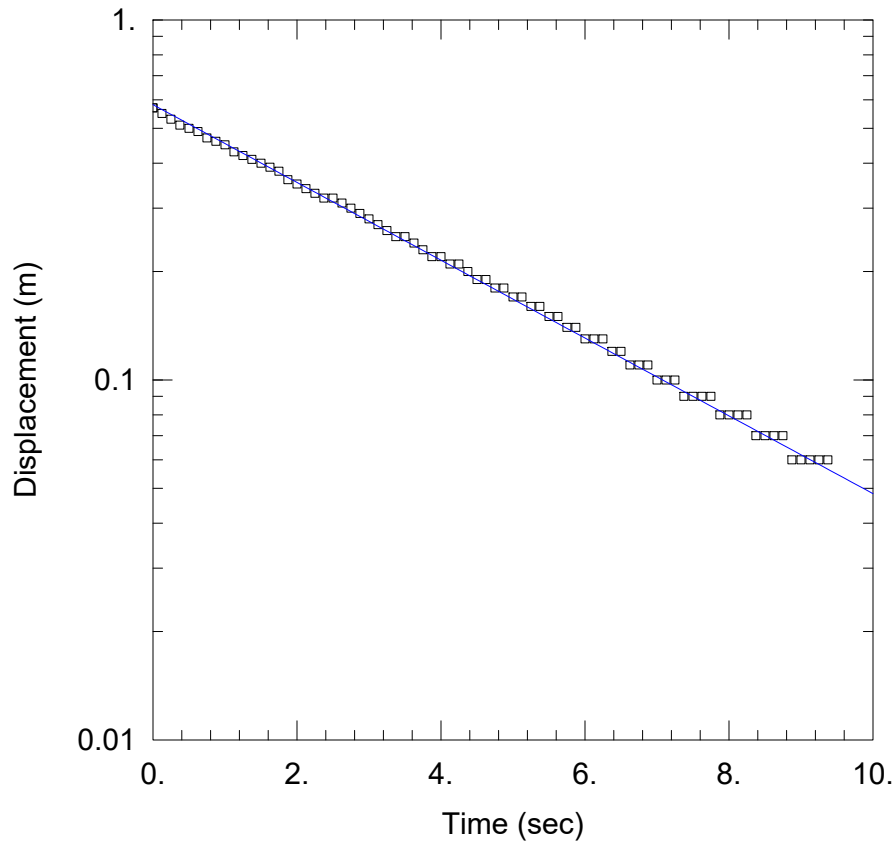
Saturated Thickness: 5.55 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL5-2)

Initial Displacement: 0.073 m  
 Total Well Penetration Depth: 8.05 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m  
 Screen Length: 2.5 m  
 Well Radius: 0.075 m



GL5-2 TEST 6 RISING HEAD

Data Set: \...\GL5-2 Test 6 Rising Head.aqt

Date: 07/11/23

Time: 17:45:18

PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL5-2

Test Date: 6/8/2023

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.0001176$  m/sec

$y_0 = 0.5815$  m

AQUIFER DATA

Saturated Thickness: 5.55 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL5-2)

Initial Displacement: 0.57 m

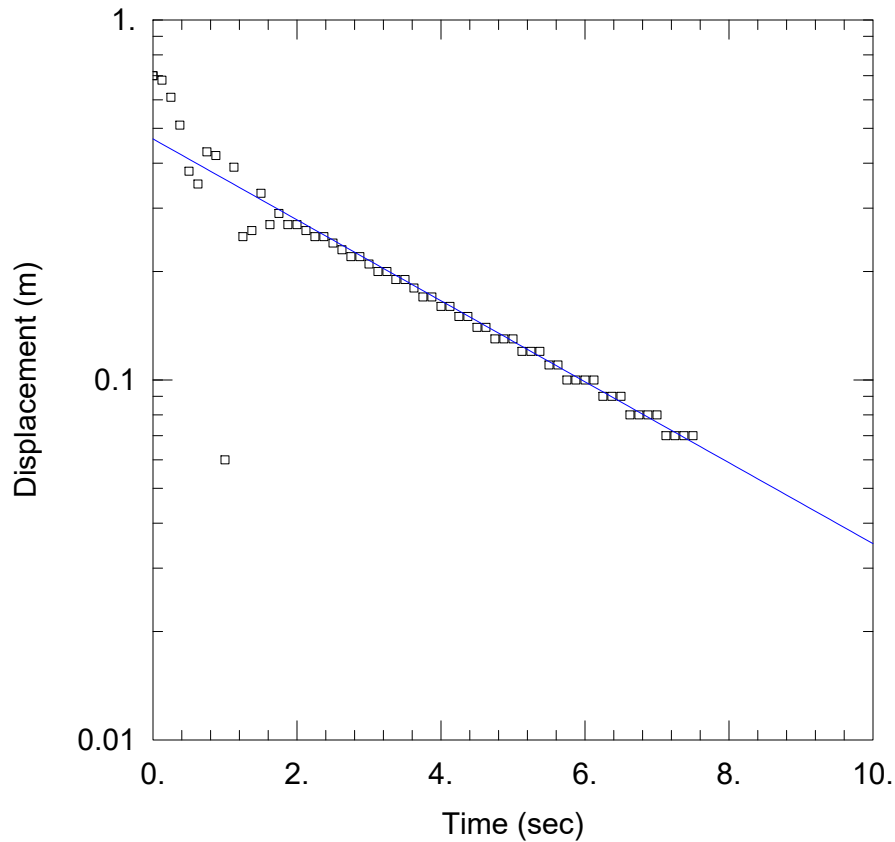
Total Well Penetration Depth: 8.05 m

Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m

Screen Length: 2.5 m

Well Radius: 0.075 m



### GL5-2 TEST 7 FALLING HEAD

Data Set: \...\GL5-2 Test 7 Falling Head.aqt

Date: 07/11/23

Time: 17:47:10

### PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL5-2

Test Date: 6/8/2023

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 0.0001224$  m/sec

$y_0 = 0.4671$  m

### AQUIFER DATA

Saturated Thickness: 5.55 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

### WELL DATA (GL5-2)

Initial Displacement: 0.7 m

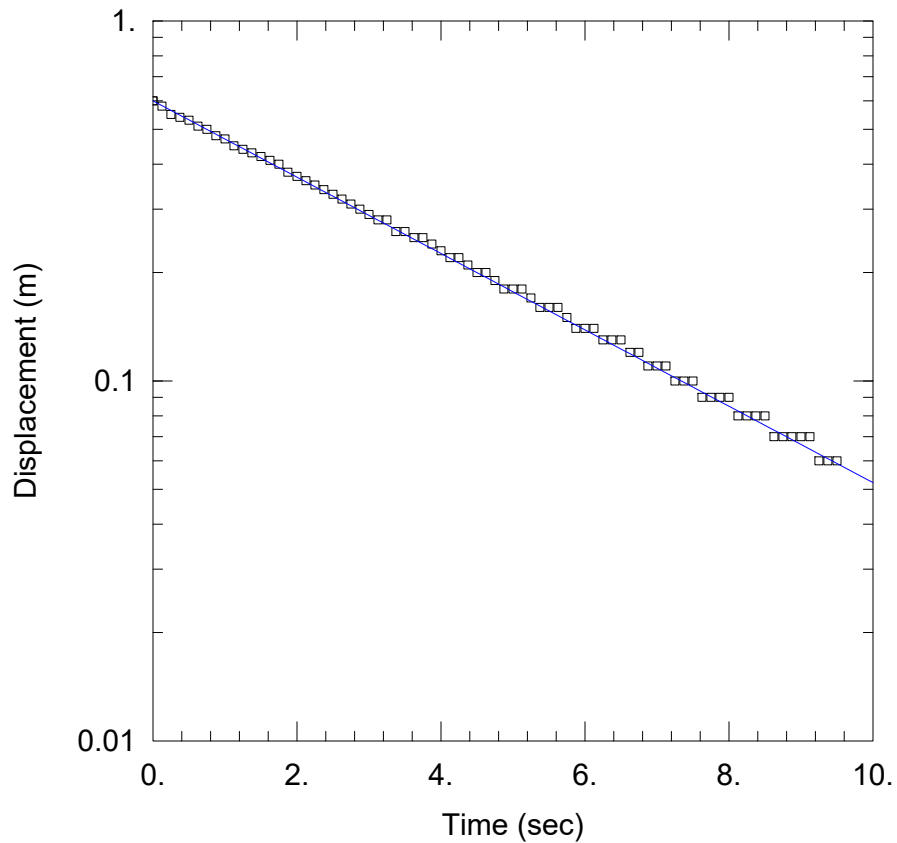
Total Well Penetration Depth: 8.05 m

Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m

Screen Length: 2.5 m

Well Radius: 0.075 m



GL5-2 TEST 8 RISING HEAD

Data Set: \...\GL5-2 Test 8 Rising Head.aqt

Date: 07/11/23

Time: 17:48:27

PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL5-2

Test Date: 6/8/2023

SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 0.0001154 m/sec

y0 = 0.5997 m

AQUIFER DATA

Saturated Thickness: 5.55 m

Anisotropy Ratio (Kz/Kr): 0.5

WELL DATA (GL5-2)

Initial Displacement: 0.6 m

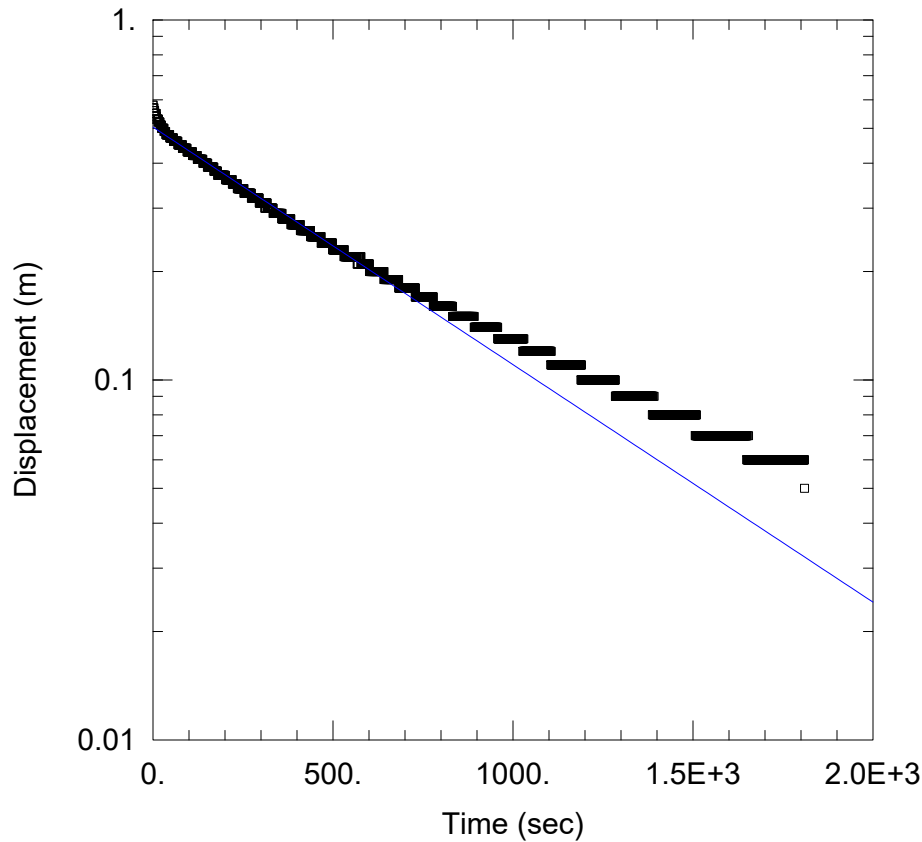
Total Well Penetration Depth: 8.05 m

Casing Radius: 0.0254 m

Static Water Column Height: 5.554 m

Screen Length: 2.5 m

Well Radius: 0.075 m



GL23-1 TEST 1- FALLING HEAD

Data Set: \...\GL23-1 Test 1 Falling Head June 6 2023.aqt  
 Date: 07/11/23 Time: 13:51:10

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL23-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 1.21E-6$  m/sec  
 $y_0 = 0.5039$  m

AQUIFER DATA

Saturated Thickness: 7.704 m

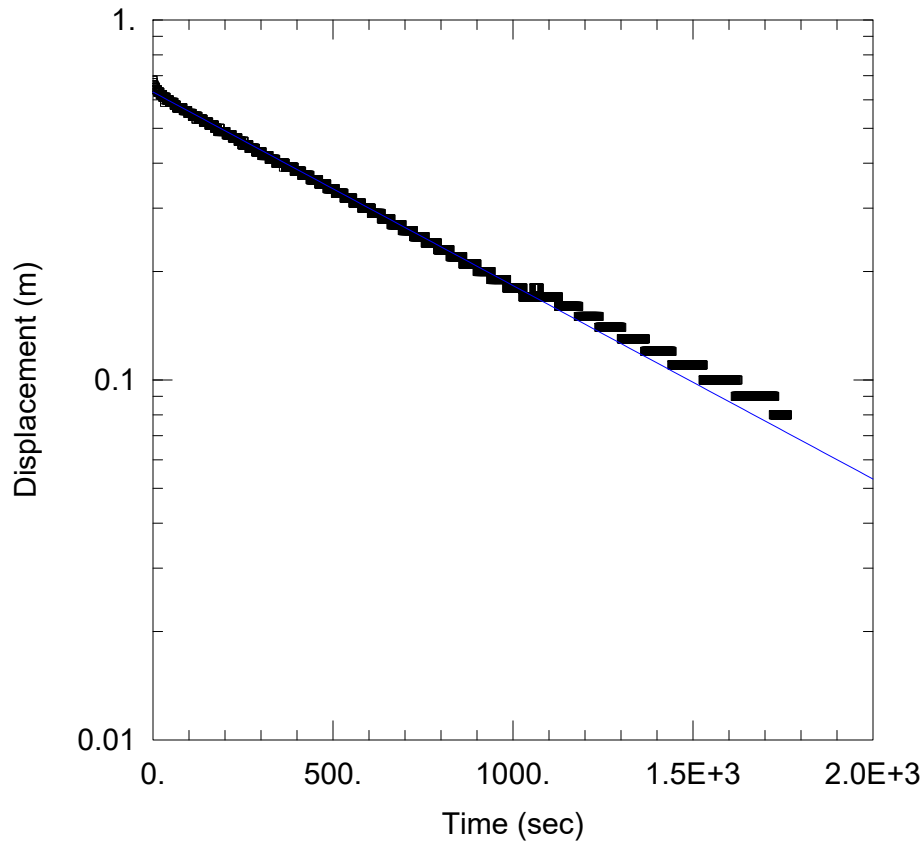
Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL23-1)

Initial Displacement: 0.58 m  
 Total Well Penetration Depth: 7.7 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 7.704 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m





GL23-1 TEST 2 - RISING HEAD

Data Set: \...\GL23-1 Test 2 Rising Head June 6 2023.aqt  
 Date: 07/11/23 Time: 13:54:21

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL23-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 9.855E-7$  m/sec  
 $y_0 = 0.6305$  m

AQUIFER DATA

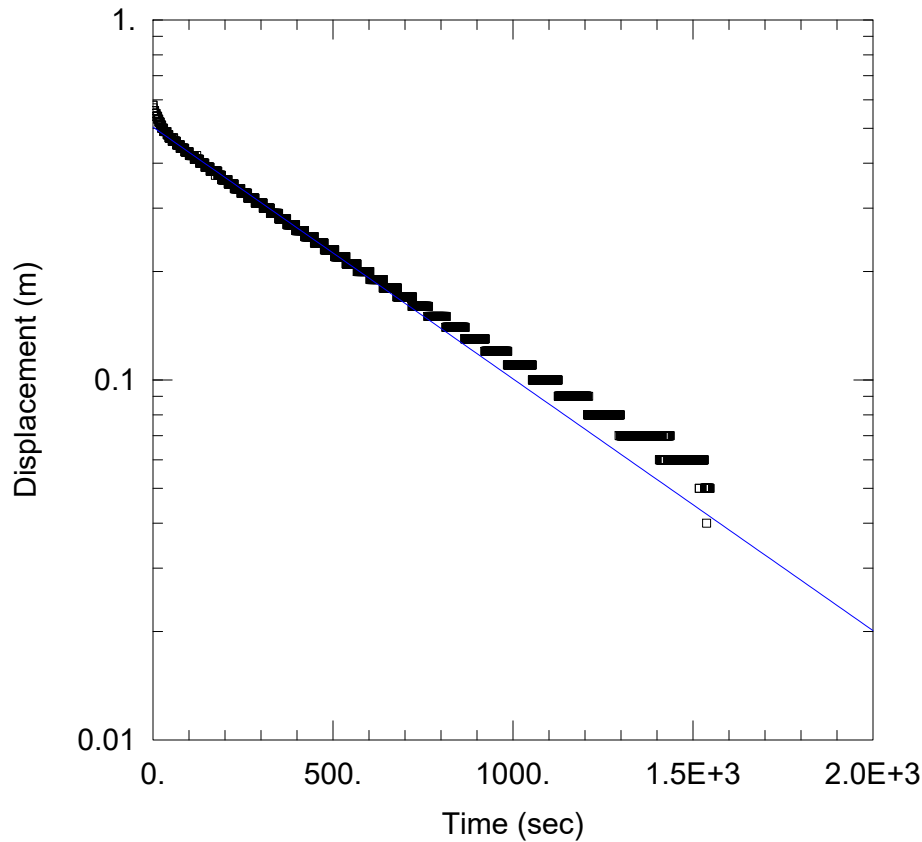
Saturated Thickness: 7.704 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL23-1)

Initial Displacement: 0.68 m  
 Total Well Penetration Depth: 7.7 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 7.704 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL23-1 TEST 3 - FALLING HEAD

Data Set: \...\GL23-1 Test 3 Falling Head June 6 2023.aqt  
 Date: 07/11/23 Time: 13:57:10

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL23-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 1.282E-6$  m/sec  
 $y_0 = 0.5039$  m

AQUIFER DATA

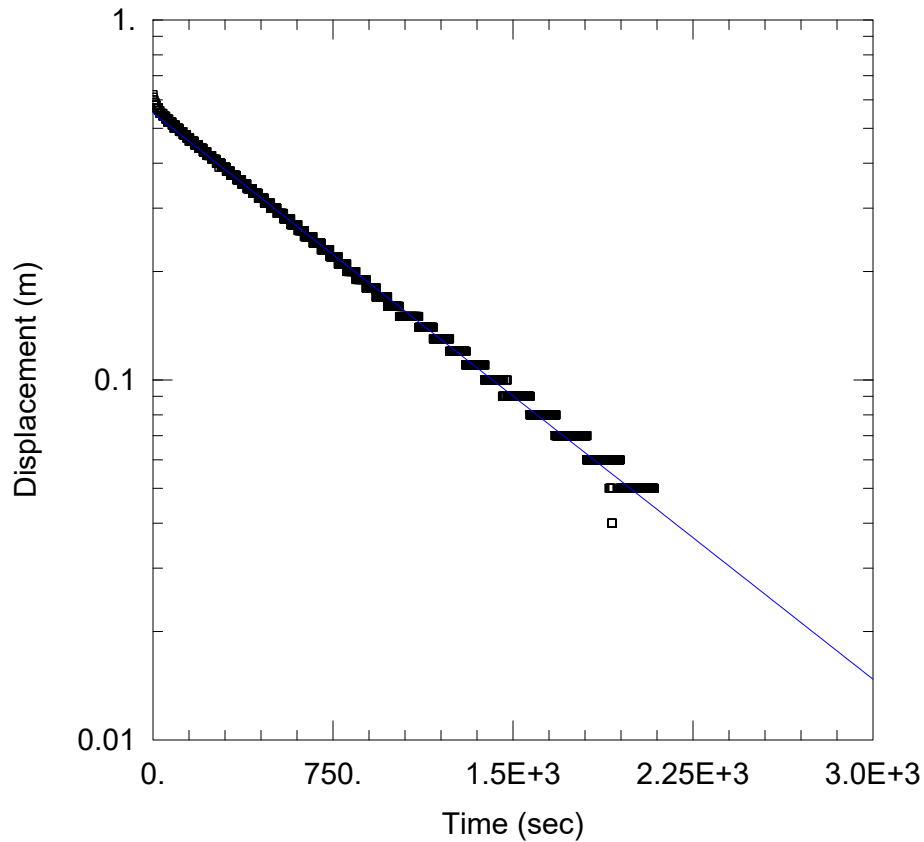
Saturated Thickness: 7.704 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL23-1)

Initial Displacement: 0.58 m  
 Total Well Penetration Depth: 7.7 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 7.704 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



### GL23-1 TEST 4 - RISING HEAD

Data Set: \...\GL23-1 Test 4 Rising Head June 6 2023.aqt  
 Date: 07/11/23 Time: 13:57:59

### PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL23-1  
 Test Date: 6/6/2023

### SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 9.616E-7$  m/sec  
 $y_0 = 0.5518$  m

### AQUIFER DATA

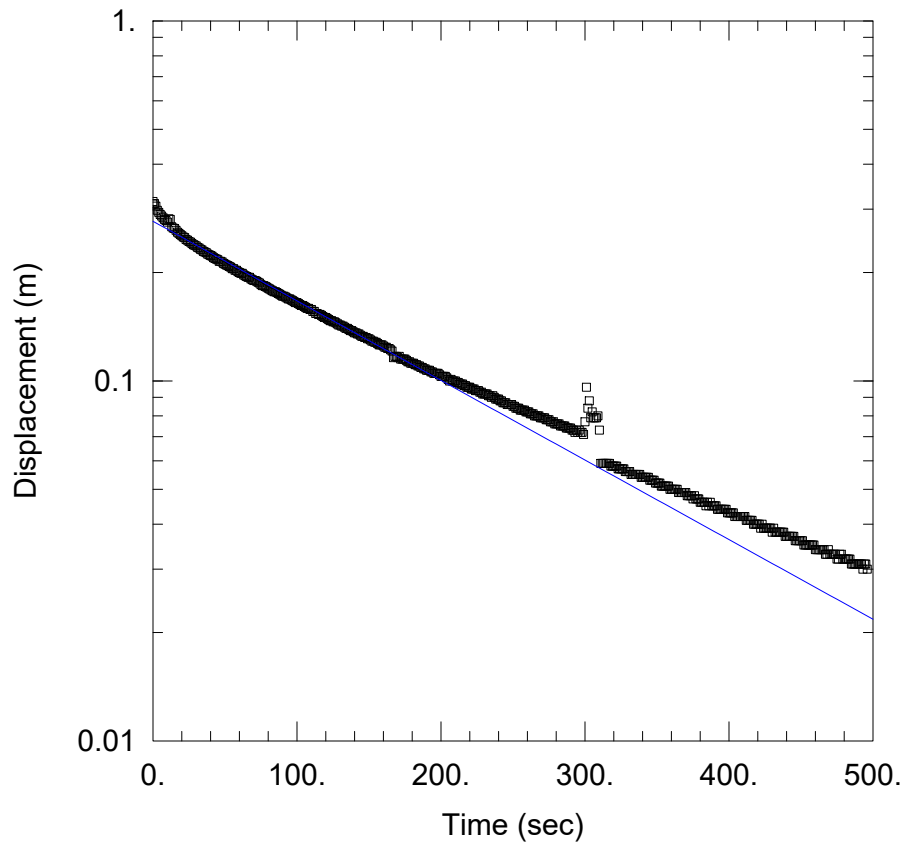
Saturated Thickness: 7.704 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

### WELL DATA (GL23-1)

Initial Displacement: 0.62 m  
 Total Well Penetration Depth: 7.7 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 7.704 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL24-1 TEST 1 FALLING HEAD

Data Set: \...\GL24-1 Test 1 Falling Head.aqt  
 Date: 11/03/23 Time: 10:18:24

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL24-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 9.648E-6$  m/sec  
 $y_0 = 0.2776$  m

AQUIFER DATA

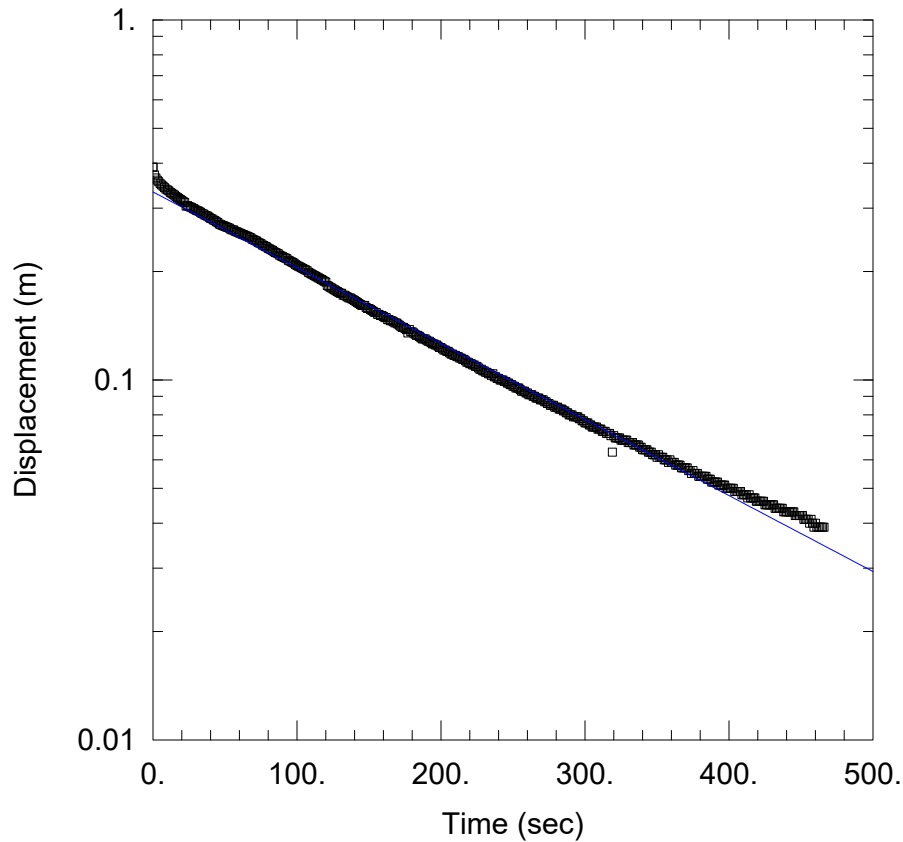
Saturated Thickness: 0.34 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL24-1)

Initial Displacement: 0.31 m  
 Total Well Penetration Depth: 2.34 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 0.338 m  
 Screen Length: 2. m  
 Well Radius: 0.075 m



GL24-1 TEST 2 RISING HEAD

Data Set: \...\GL24-1 Test 2 Rising Head.aqt  
 Date: 11/03/23 Time: 10:16:48

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL24-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 9.204E-6$  m/sec  
 $y_0 = 0.3328$  m

AQUIFER DATA

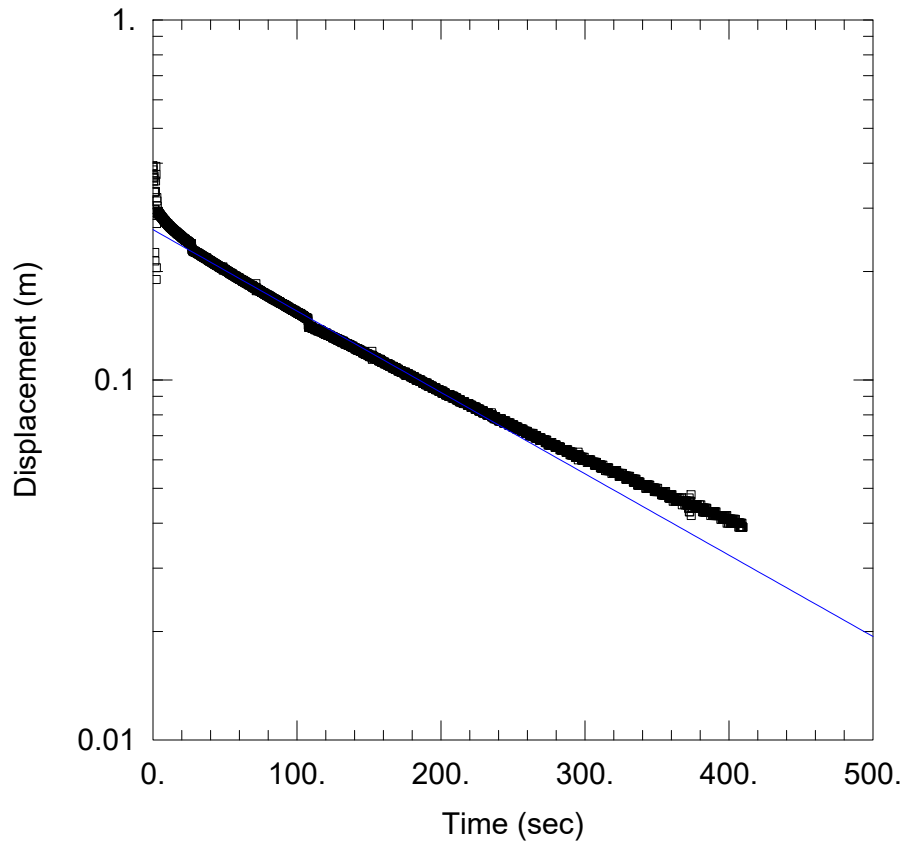
Saturated Thickness: 0.34 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL24-1)

Initial Displacement: 0.39 m  
 Total Well Penetration Depth: 2.34 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 0.338 m  
 Screen Length: 2. m  
 Well Radius: 0.075 m



GL24-1 TEST 3 FALLING HEAD

Data Set: \...\GL24-1 Test 3 Falling Head.aqt  
 Date: 11/03/23 Time: 10:16:04

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL24-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 9.866E-6$  m/sec  
 $y_0 = 0.2615$  m

AQUIFER DATA

Saturated Thickness: 0.34 m

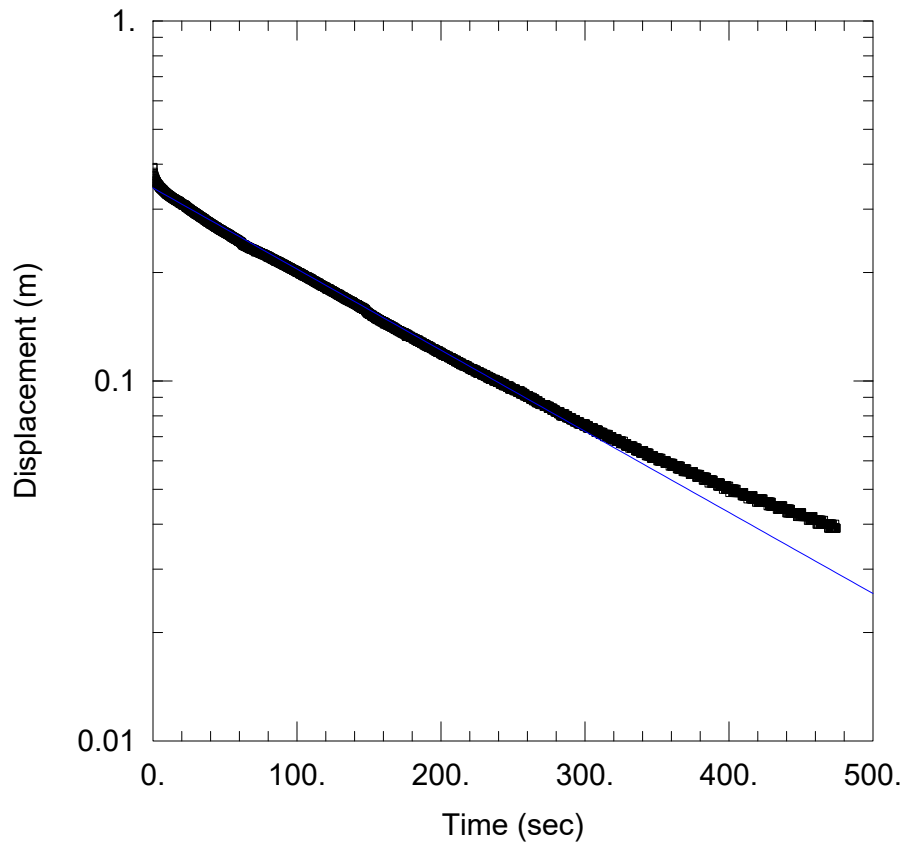
Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL24-1)

Initial Displacement: 0.39 m  
 Total Well Penetration Depth: 2.34 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 0.338 m  
 Screen Length: 2. m  
 Well Radius: 0.075 m





GL24-1 TEST 4 RISING HEAD

Data Set: \...\GL24-1 Test 4 Rising Head.aqt  
 Date: 11/03/23 Time: 10:17:42

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL24-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 9.835E-6$  m/sec  
 $y_0 = 0.3436$  m

AQUIFER DATA

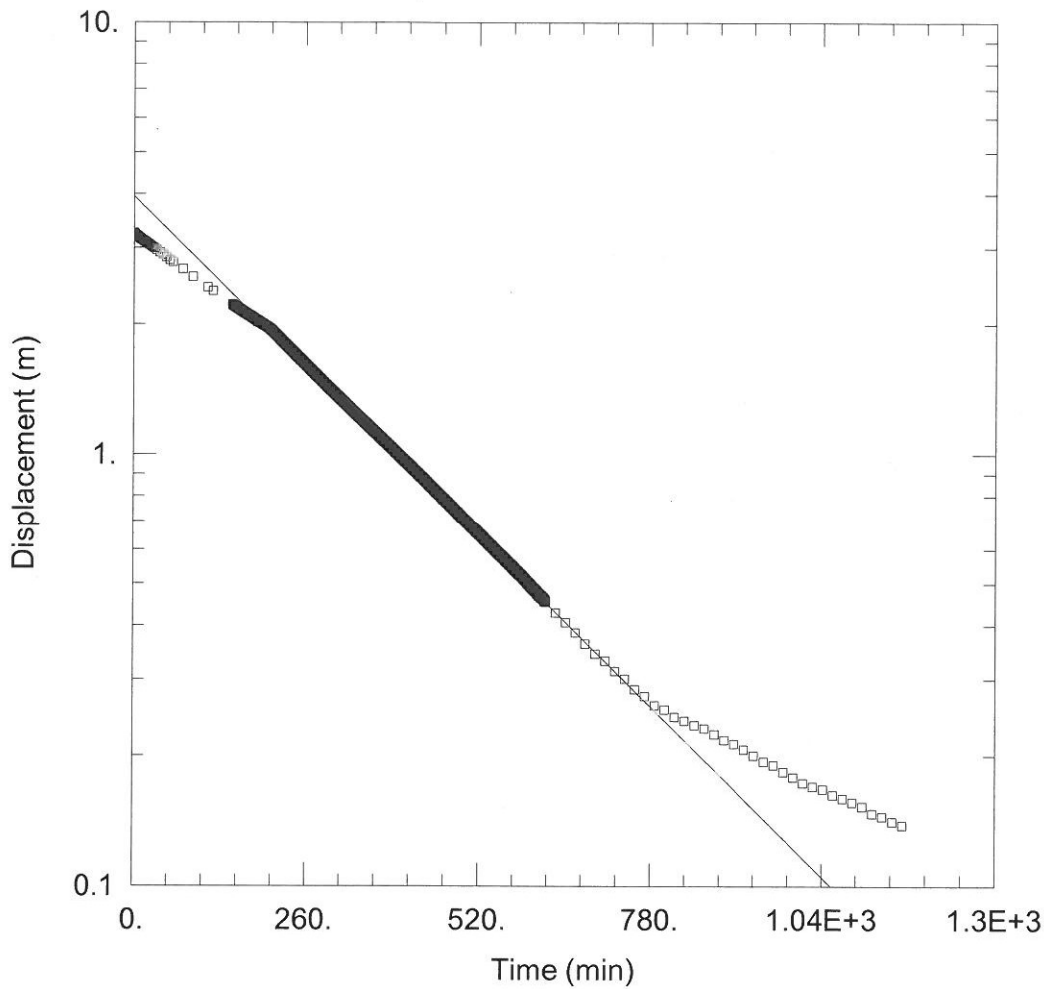
Saturated Thickness: 0.34 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL24-1)

Initial Displacement: 0.39 m  
 Total Well Penetration Depth: 2.34 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 0.338 m  
 Screen Length: 2. m  
 Well Radius: 0.075 m



HVORSLEV MW09-02-1

Data Set: N:\...\MW09-02-1 15Jun2009 Hvorslev.aqt

Date: 06/24/10

Time: 12:58:29

PROJECT INFORMATION

Company: Golder Associates Ltd.

Client: City of Kelowna

Project: 09-1444-0066

Location: Glenmore Landfill

Test Well: MW09-02-1

Test Date: June 15, 2009

AQUIFER DATA

Saturated Thickness: 3.426 m

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (MW09-02-1)

Initial Displacement: 3.25 m

Static Water Column Height: 3.426 m

Total Well Penetration Depth: 3.426 m

Screen Length: 1.521 m

Casing Radius: 0.0254 m

Well Radius: 0.0254 m

Gravel Pack Porosity: 0.3

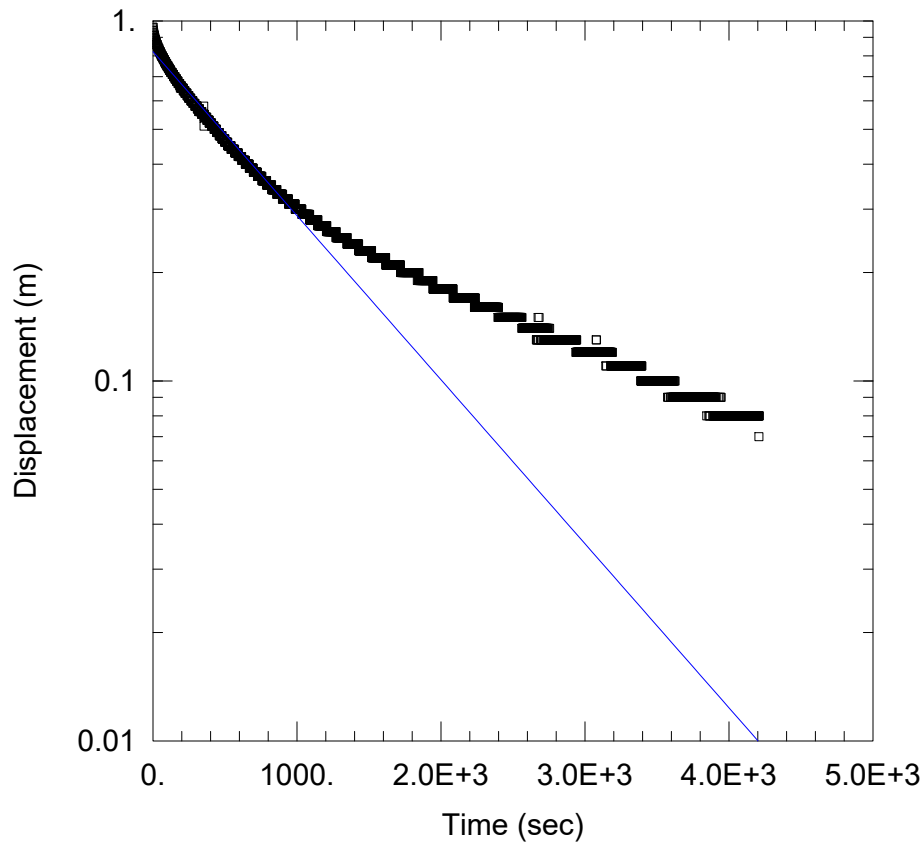
SOLUTION

Aquifer Model: Unconfined

Solution Method: Hvorslev

K = 5.9E-8 m/sec

y0 = 3.95 m



GL27-1 TEST 1 RISING HEAD

Data Set: \\...\GL27-1 Test 1 RH.aqt  
 Date: 07/11/23 Time: 15:26:05

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL27-1  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Confined  
 Solution Method: Hvorslev  
 $K = 1.092E-6$  m/sec  
 $y_0 = 0.8216$  m

AQUIFER DATA

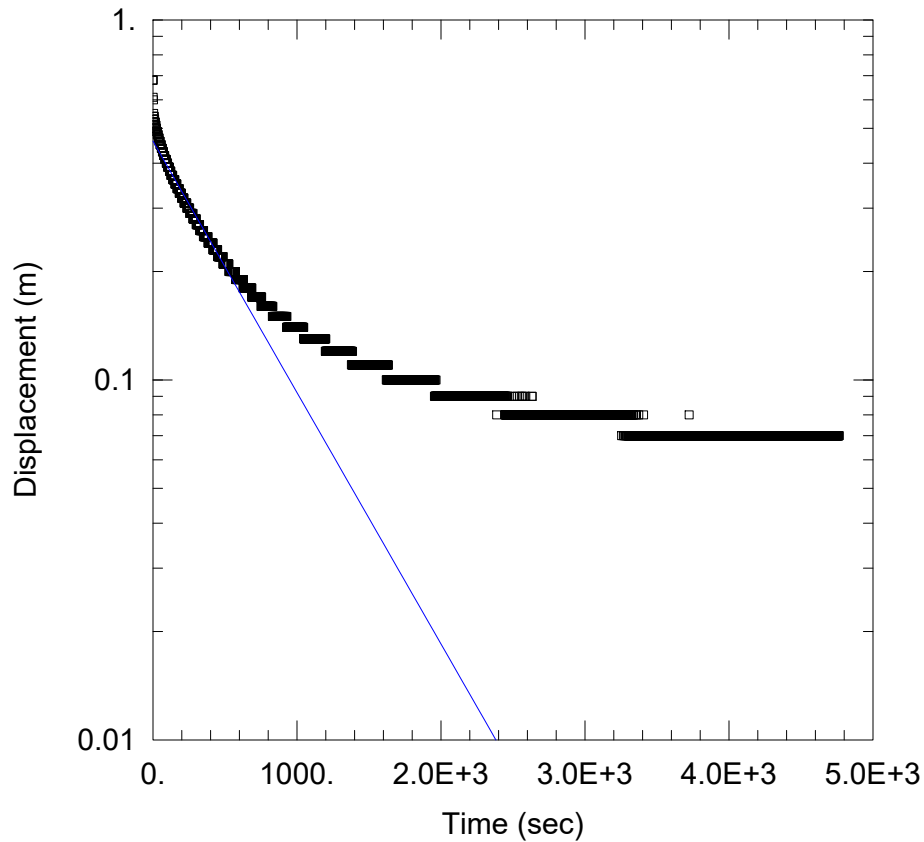
Saturated Thickness: 21.87 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.1

WELL DATA (GL27-1)

Initial Displacement: 0.96 m  
 Total Well Penetration Depth: 23.37 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 21.87 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL27-1 TEST 2 FALLING HEAD

Data Set: \\...\GL27-2 Test 2 FH.aqt

Date: 07/11/23

Time: 15:34:56

PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL27-1

Test Date: 6/6/2023

SOLUTION

Aquifer Model: Confined

Solution Method: Hvorslev

$K = 1.674E-6$  m/sec

$y_0 = 0.4604$  m

AQUIFER DATA

Saturated Thickness: 21.87 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.1

WELL DATA (GL27-1)

Initial Displacement: 0.68 m

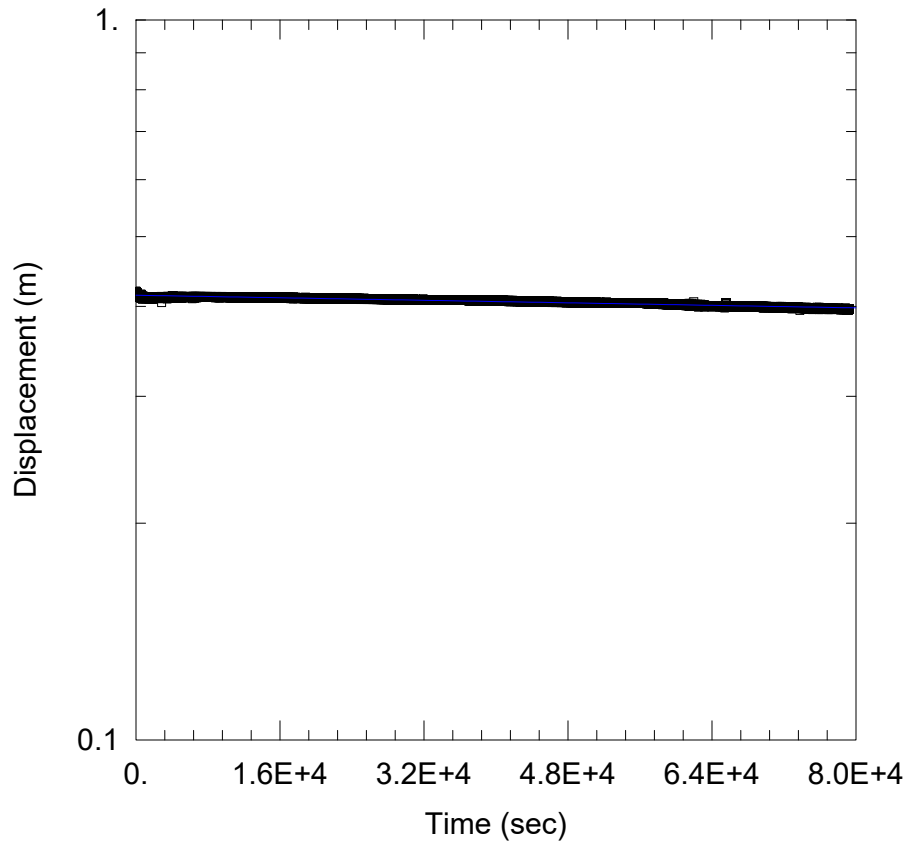
Total Well Penetration Depth: 23.37 m

Casing Radius: 0.0254 m

Static Water Column Height: 21.87 m

Screen Length: 1.5 m

Well Radius: 0.075 m



GL27-2 TEST 1 FALLING HEAD

Data Set: \...\GL27-2 Test 1 Falling Head.aqt  
 Date: 07/13/23 Time: 10:37:24

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL27-2  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 4.363E-10$  m/sec  
 $y_0 = 0.4146$  m

AQUIFER DATA

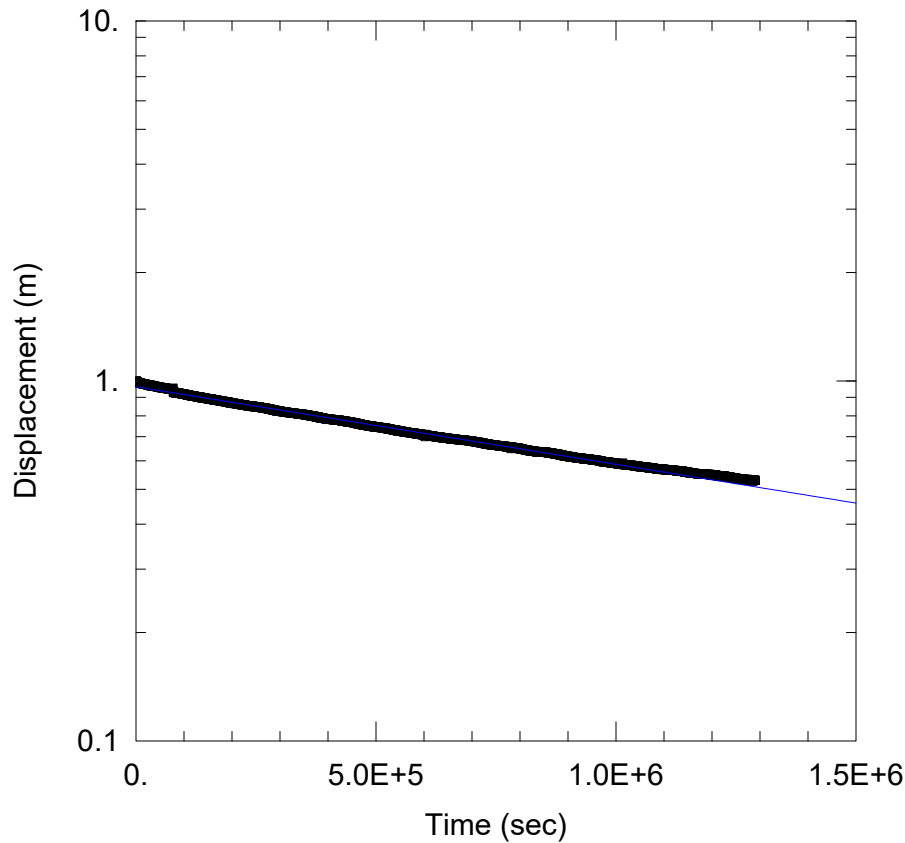
Saturated Thickness: 8.23 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.2

WELL DATA (GL27-2I)

Initial Displacement: 0.42 m  
 Total Well Penetration Depth: 9.73 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 8.227 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL27-2 TEST 2 RISING HEAD

Data Set: \...\GL27-2 Test 2 Rising Head.aqt  
 Date: 07/13/23 Time: 10:40:42

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL27-2  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 4.285E-10$  m/sec  
 $y_0 = 0.9633$  m

AQUIFER DATA

Saturated Thickness: 8.23 m

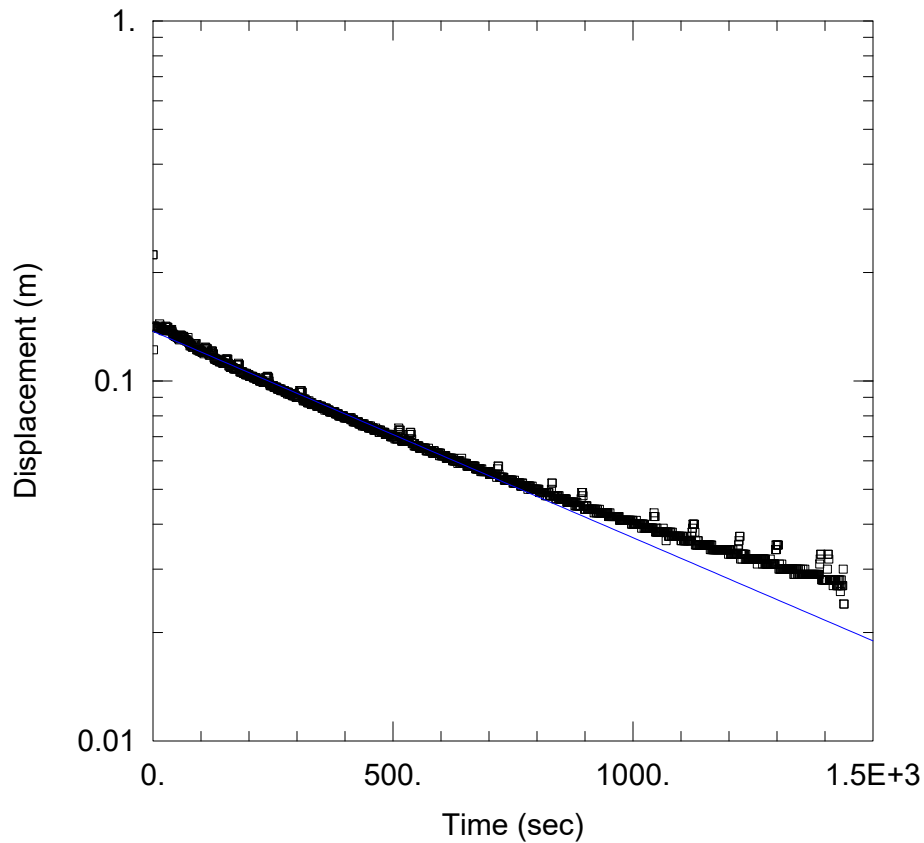
Anisotropy Ratio ( $K_z/K_r$ ): 0.2

WELL DATA (GL27-2)

Initial Displacement: 0.997 m  
 Total Well Penetration Depth: 9.73 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 8.227 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m





GL28-2 TEST 1 FALLING HEAD

Data Set: \...\GL28-2 Test 1 Falling Head.aqt  
 Date: 07/12/23 Time: 15:22:04

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL28-2  
 Test Date: 6/7/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 9.88E-7$  m/sec  
 $y_0 = 0.1373$  m

AQUIFER DATA

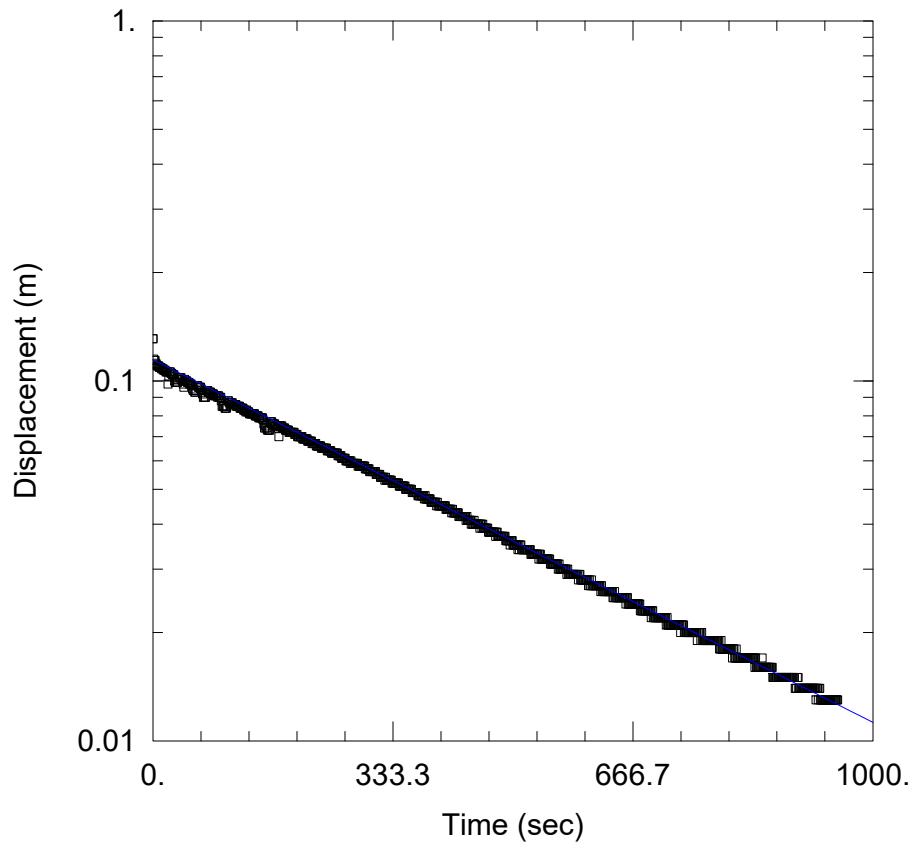
Saturated Thickness: 1.03 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL28-2)

Initial Displacement: 0.224 m  
 Total Well Penetration Depth: 2.53 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 1.034 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL28-2 TEST 2 RISING HEAD

Data Set: \...\GL28-2 Test 2 Rising Head.aqt  
 Date: 07/12/23 Time: 15:23:45

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL28-2  
 Test Date: 6/7/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bower-Rice  
 $K = 1.737E-6$  m/sec  
 $y_0 = 0.1146$  m

AQUIFER DATA

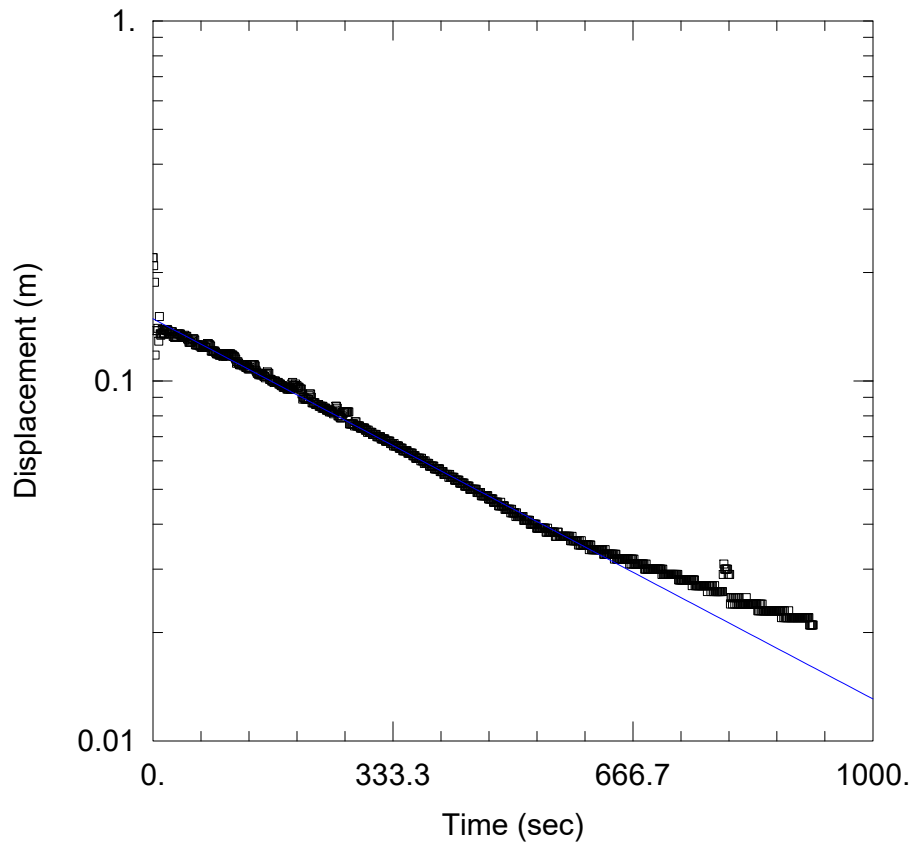
Saturated Thickness: 1.03 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL28-2)

Initial Displacement: 0.131 m  
 Total Well Penetration Depth: 2.53 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 1.034 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL28-2 TEST 3 FALLING HEAD

Data Set: \...\GL28-2 Test 3 Falling Head.aqt  
 Date: 07/12/23 Time: 15:25:18

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL28-2  
 Test Date: 6/7/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 1.82E-6$  m/sec  
 $y_0 = 0.1488$  m

AQUIFER DATA

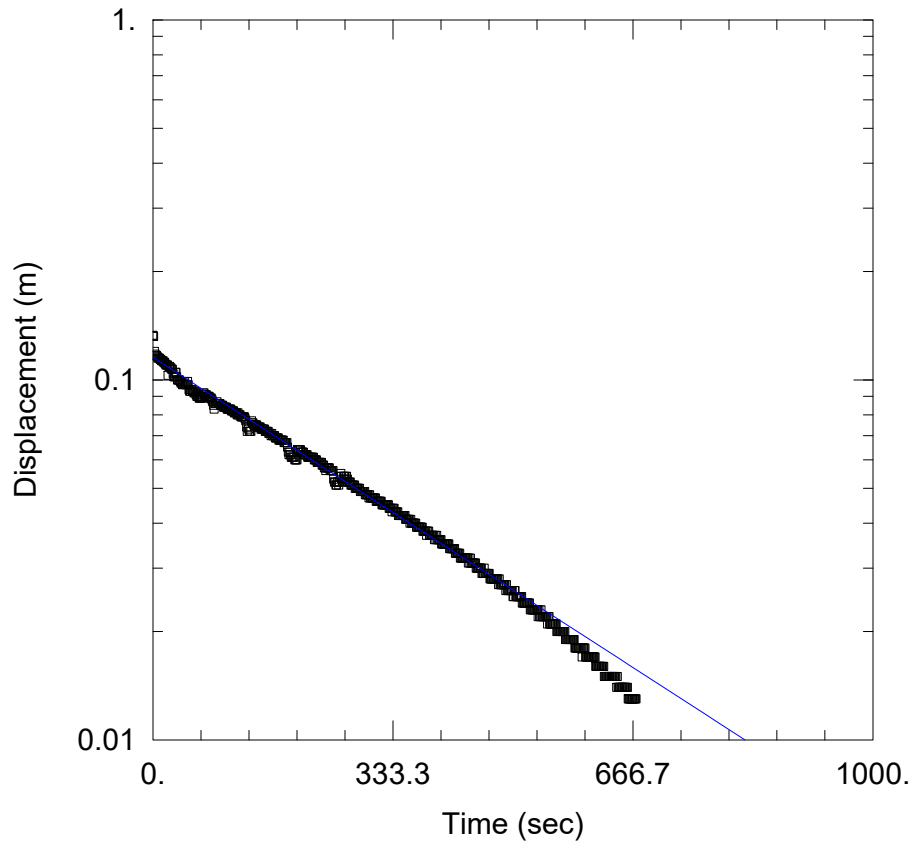
Saturated Thickness: 1.03 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL28-2)

Initial Displacement: 0.22 m  
 Total Well Penetration Depth: 2.53 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 1.034 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



### GL28-2 TEST 4 RISING HEAD

Data Set: \...\GL28-2 Test 4 Rising Head.aqt

Date: 07/12/23

Time: 15:26:47

### PROJECT INFORMATION

Company: GHD

Client: City of Kelowna

Project: 12605725

Location: Glenmore Landfill

Test Well: GL28-2

Test Date: 6/7/2023

### SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

$K = 2.228E-6$  m/sec

$y_0 = 0.1156$  m

### AQUIFER DATA

Saturated Thickness: 1.03 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

### WELL DATA (GL28-2)

Initial Displacement: 0.133 m

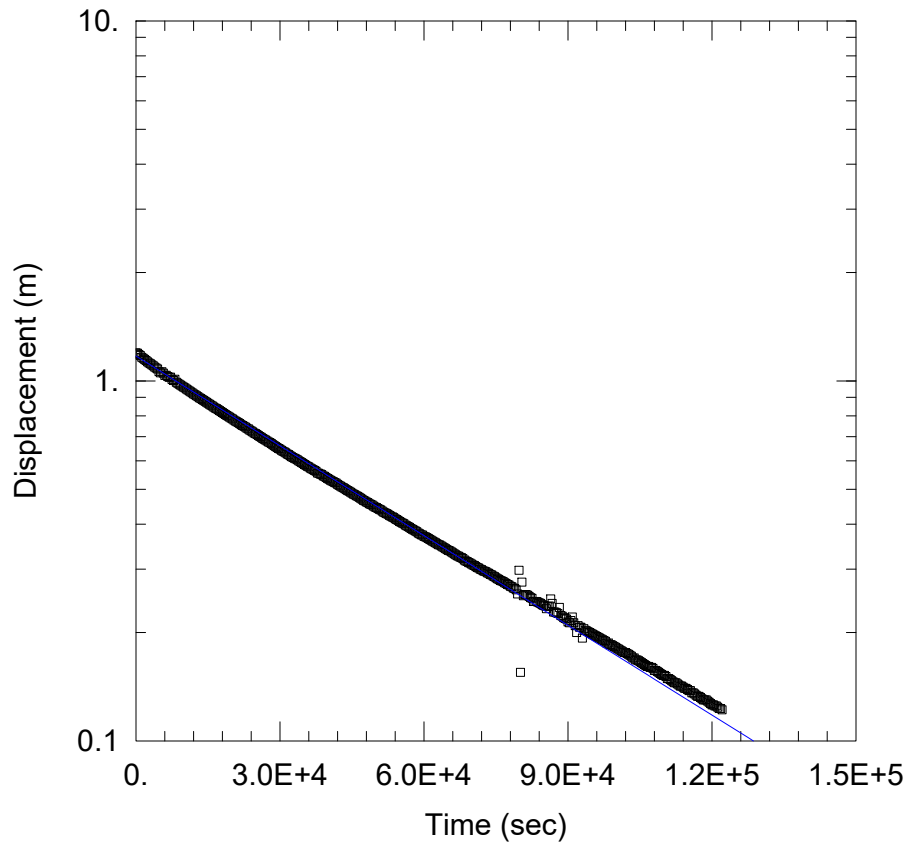
Total Well Penetration Depth: 2.53 m

Casing Radius: 0.0254 m

Static Water Column Height: 1.034 m

Screen Length: 1.5 m

Well Radius: 0.075 m



GL29-2 RISING HEAD TEST

Data Set: \...\GL29-2 Test 1 Rising Head.aqt  
 Date: 07/12/23 Time: 16:56:16

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL29-2  
 Test Date: 6/8/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 5.042E-9$  m/sec  
 $y_0 = 1.172$  m

AQUIFER DATA

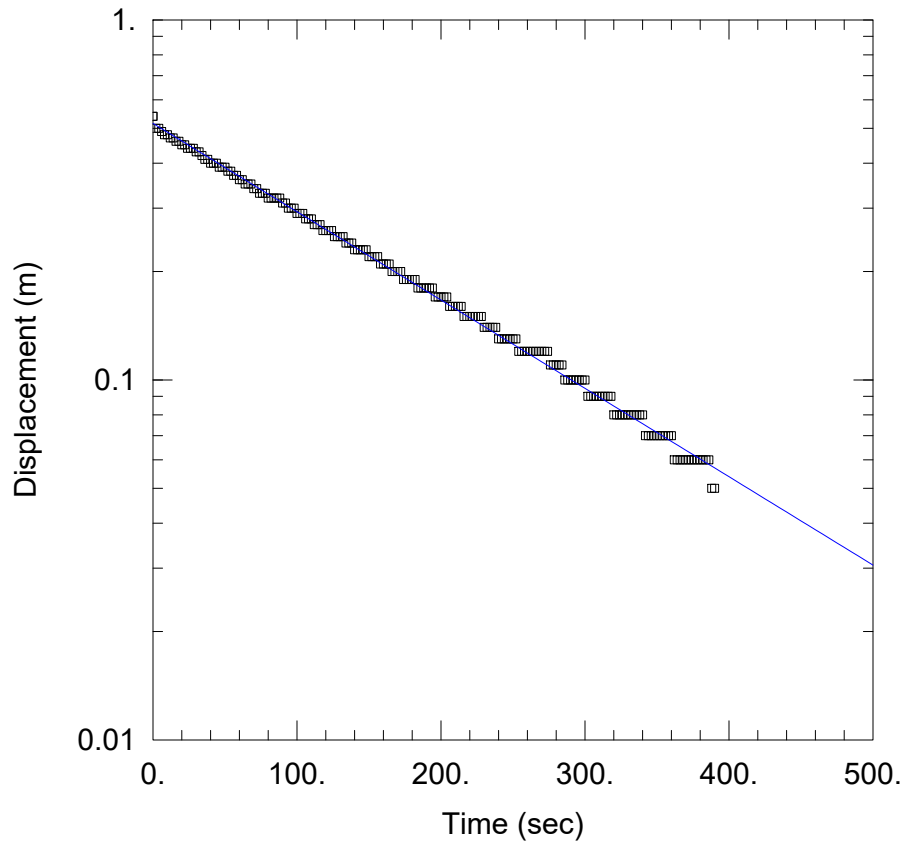
Saturated Thickness: 4.54 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL29-2)

Initial Displacement: 1.196 m  
 Total Well Penetration Depth: 11.14 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 4.536 m  
 Screen Length: 6.6 m  
 Well Radius: 0.075 m



### GL34-3 TEST 1 RISING HEAD

Data Set: \...\GL34-3 Test 1 Falling Head.aqt  
 Date: 07/12/23 Time: 10:52:13

### PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL34-3  
 Test Date: 6/7/2023

### SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 8.648E-6$  m/sec  
 $y_0 = 0.516$  m

### AQUIFER DATA

Saturated Thickness: 11.62 m

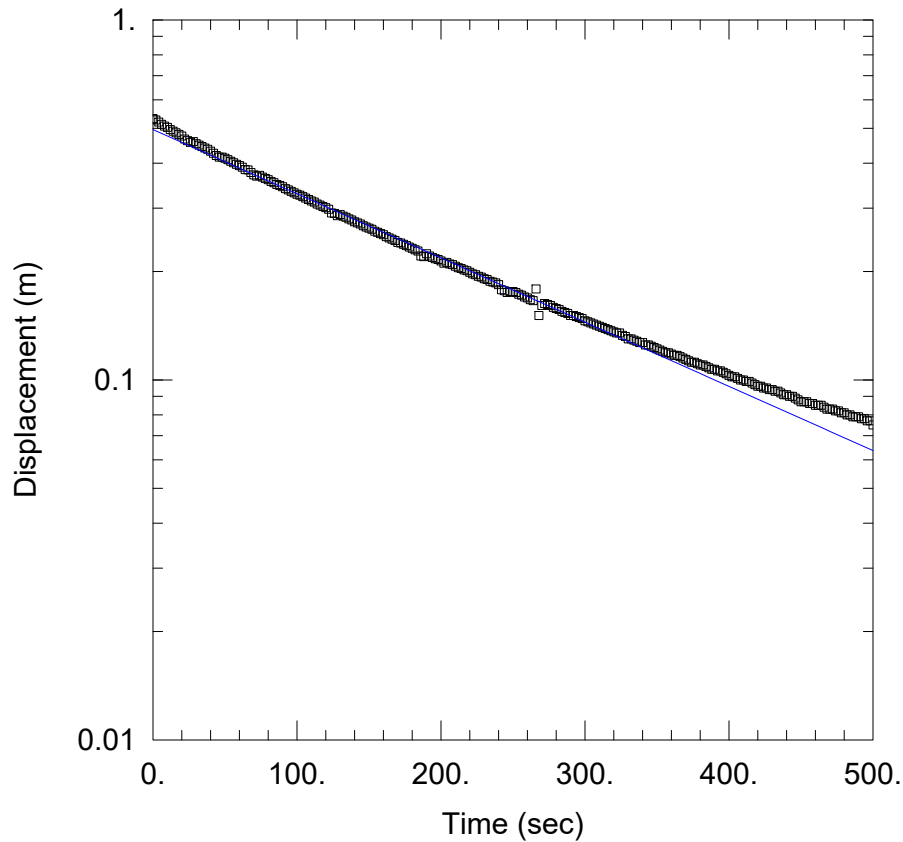
Anisotropy Ratio ( $K_z/K_r$ ): 0.1

### WELL DATA (GL34-3)

Initial Displacement: 0.54 m  
 Total Well Penetration Depth: 12.52 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 11.62 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m





GL34-3 TEST 2 FALLING HEAD

Data Set: \...\GL34-3 Test 2 Rising Head.aqt  
 Date: 07/12/23 Time: 10:55:19

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL34-3  
 Test Date: 6/7/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 6.284E-6$  m/sec  
 $y_0 = 0.4959$  m

AQUIFER DATA

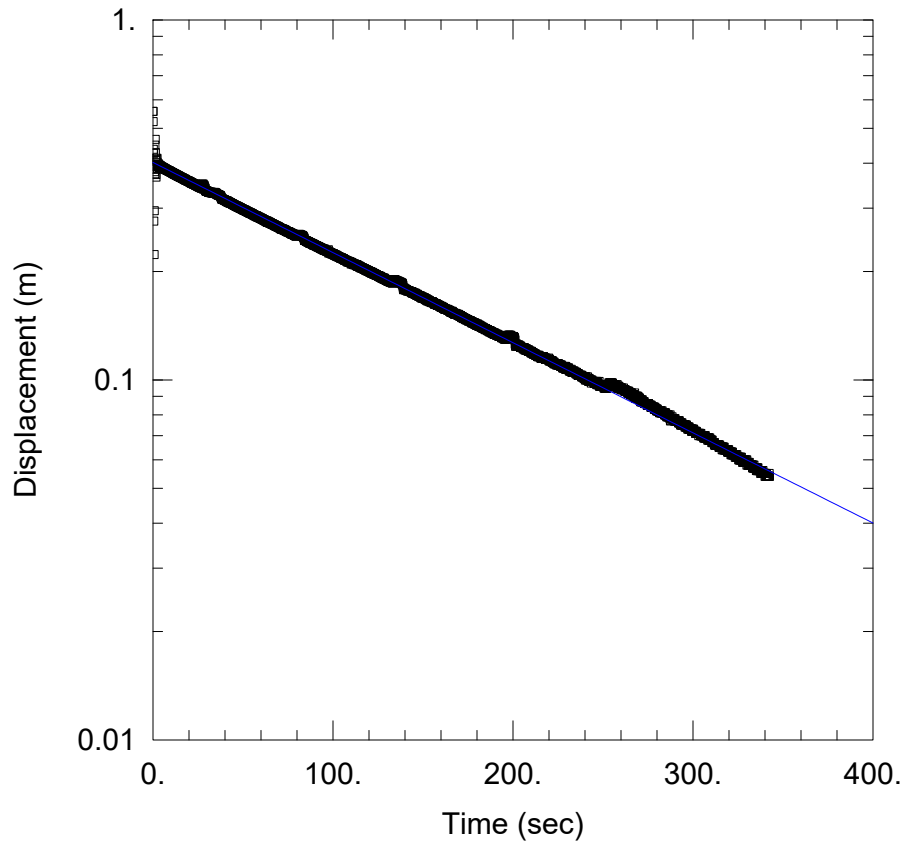
Saturated Thickness: 11.62 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.1

WELL DATA (GL34-3)

Initial Displacement: 0.53 m  
 Total Well Penetration Depth: 12.52 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 11.62 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



GL34-3 TEST 3 FALLING HEAD

Data Set: \...\GL34-3 Test 3 Falling Head.aqt  
 Date: 07/12/23 Time: 10:56:57

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL34-3  
 Test Date: 6/7/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 8.825E-6$  m/sec  
 $y_0 = 0.4019$  m

AQUIFER DATA

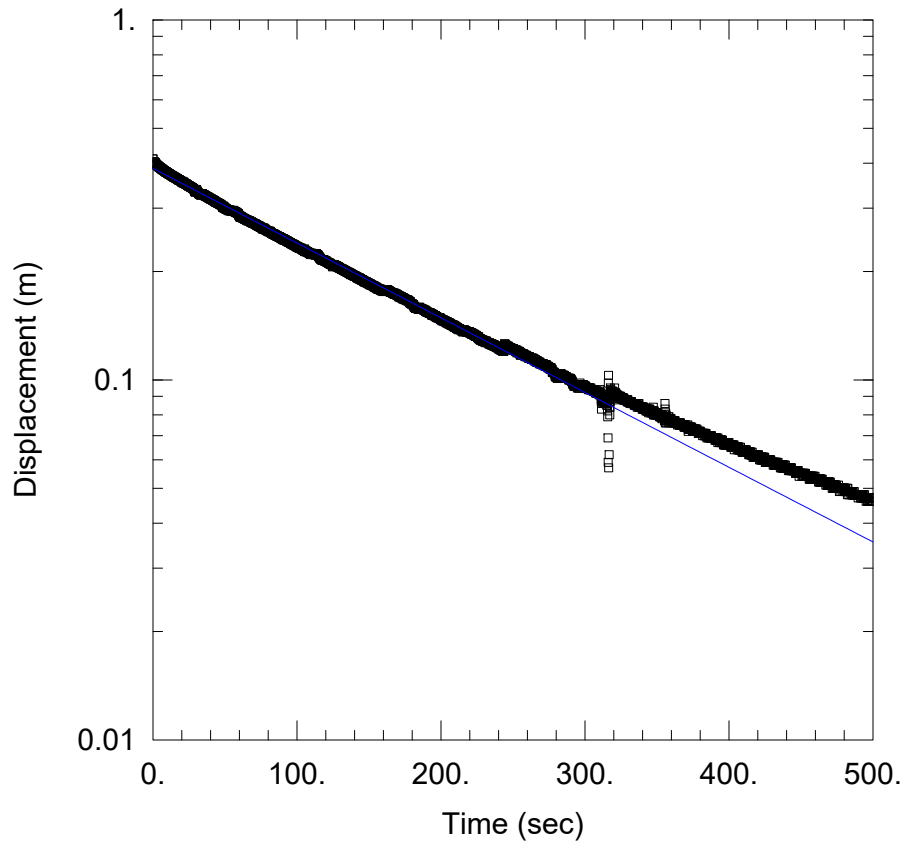
Saturated Thickness: 11.62 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.1

WELL DATA (GL34-3)

Initial Displacement: 0.557 m  
 Total Well Penetration Depth: 12.52 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 11.62 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



### GL34-3 TEST 4 RISING HEAD

Data Set: \...\GL34-3 Test 4 Rising Head.aqt  
 Date: 07/12/23 Time: 10:58:32

### PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL34-3  
 Test Date: 6/7/2023

### SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 7.313E-6$  m/sec  
 $y_0 = 0.3866$  m

### AQUIFER DATA

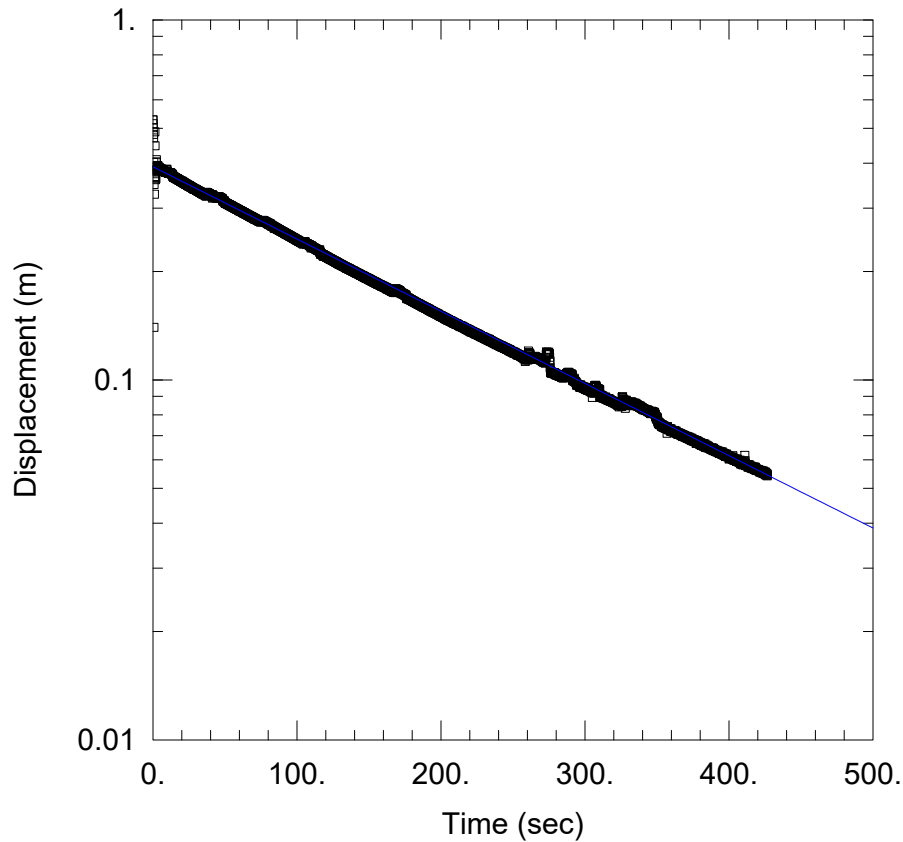
Saturated Thickness: 11.62 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.1

### WELL DATA (GL34-3)

Initial Displacement: 0.411 m  
 Total Well Penetration Depth: 12.52 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 11.62 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



GL34-3 TEST 5 FALLING HEAD

Data Set: \...\GL34-3 Test 5 Falling Head.aqt  
 Date: 07/12/23 Time: 11:00:06

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL34-3  
 Test Date: 6/7/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 7.071E-6$  m/sec  
 $y_0 = 0.3905$  m

AQUIFER DATA

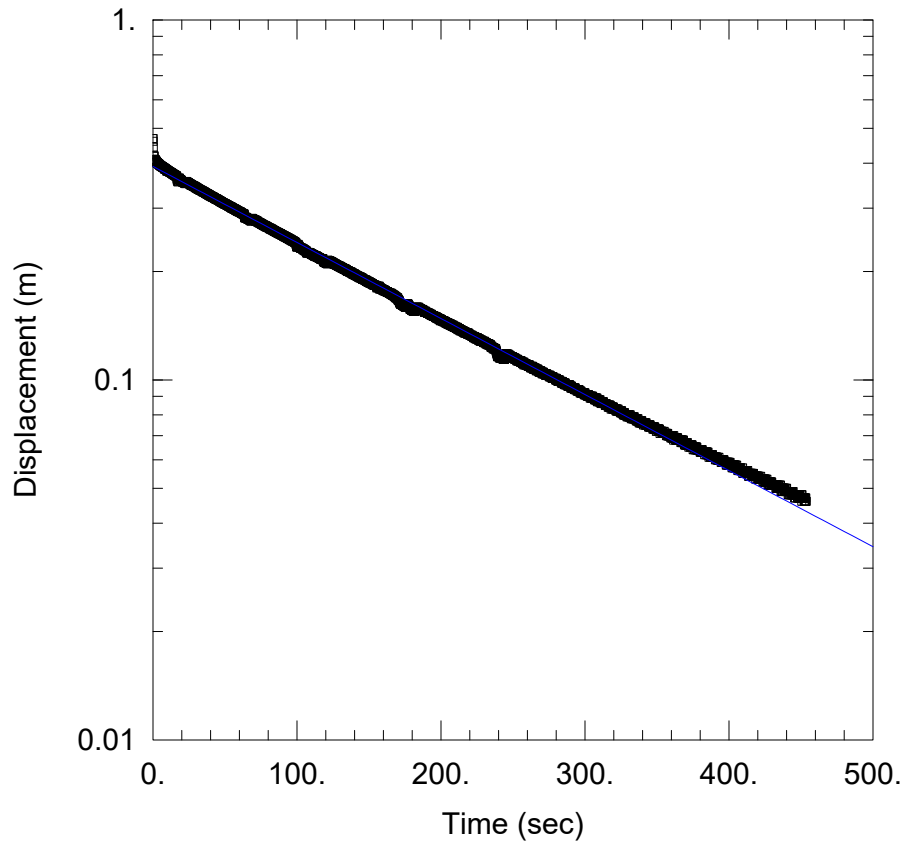
Saturated Thickness: 11.62 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.1

WELL DATA (GL34-3)

Initial Displacement: 0.528 m  
 Total Well Penetration Depth: 12.52 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 11.62 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



### GL34-3 TEST 6 RISING HEAD

Data Set: \...\GL34-3 Test 6 Rising Head.aqt  
 Date: 07/12/23 Time: 11:03:15

### PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL34-3  
 Test Date: 6/7/2023

### SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 7.445E-6$  m/sec  
 $y_0 = 0.3919$  m

### AQUIFER DATA

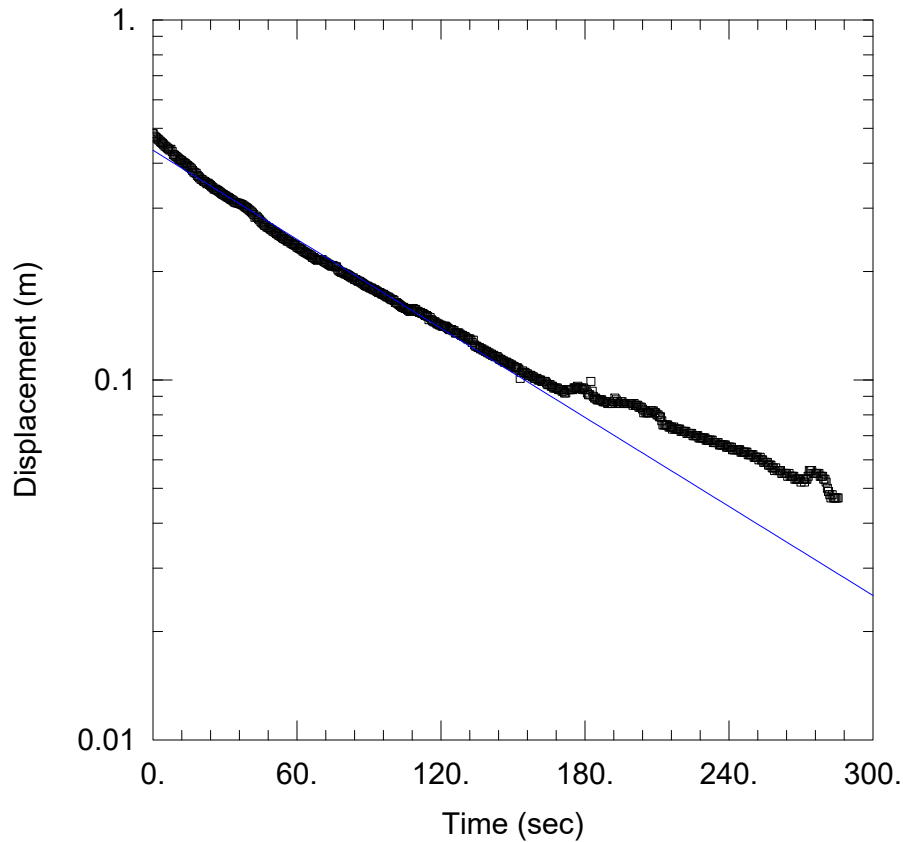
Saturated Thickness: 11.62 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.1

### WELL DATA (GL34-3)

Initial Displacement: 0.468 m  
 Total Well Penetration Depth: 12.52 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 11.62 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



GL35-3 TEST 1 FALLING HEAD

Data Set: \...\GL35-3 Test 1 Falling Head.aqt  
 Date: 07/12/23 Time: 12:33:51

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL35-3  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 7.442E-6$  m/sec  
 $y_0 = 0.4343$  m

AQUIFER DATA

Saturated Thickness: 12.22 m

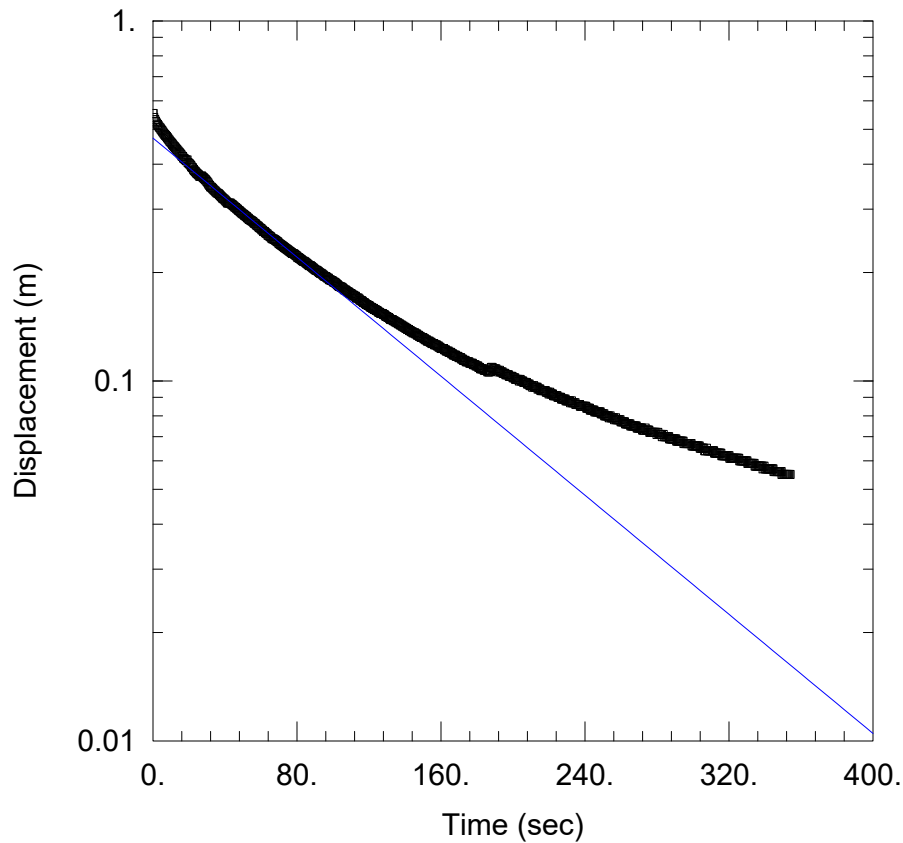
Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL35-3)

Initial Displacement: 0.483 m  
 Total Well Penetration Depth: 13.72 m  
 Casing Radius: 0.025 m

Static Water Column Height: 12.22 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m





GL35-3 TEST 2 RISING HEAD

Data Set: \...\GL35-3 Test 2 Rising Head.aqt  
 Date: 07/12/23 Time: 12:36:57

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL35-3  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 7.464E-6$  m/sec  
 $y_0 = 0.4726$  m

AQUIFER DATA

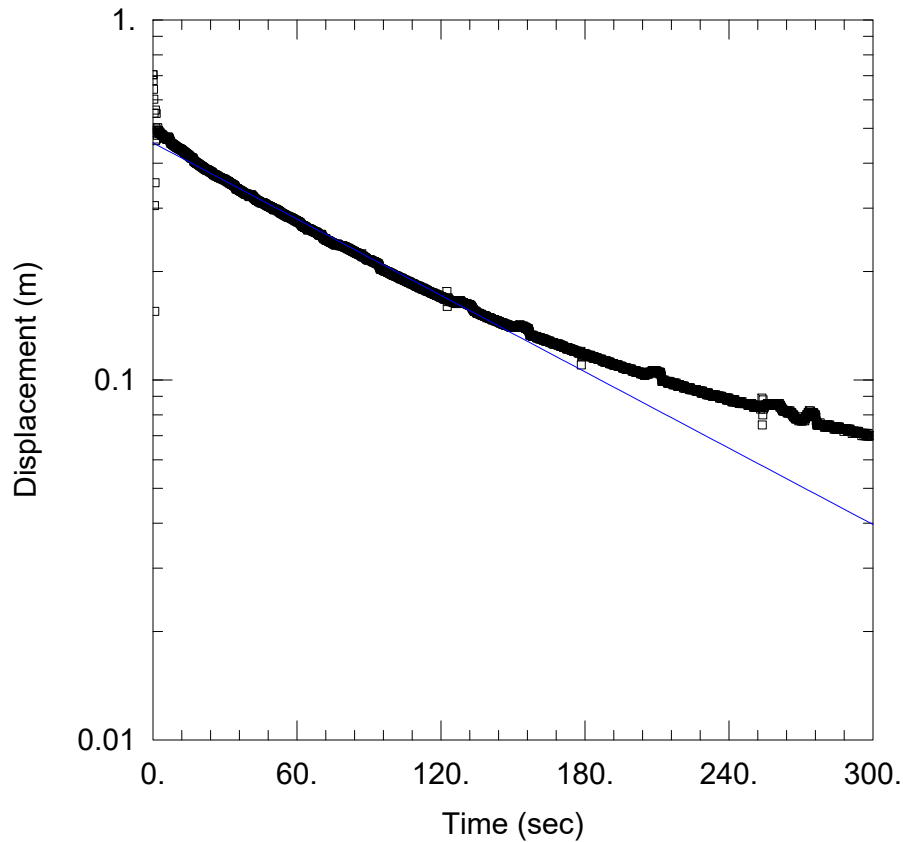
Saturated Thickness: 12.22 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL35-3)

Initial Displacement: 0.553 m  
 Total Well Penetration Depth: 13.72 m  
 Casing Radius: 0.025 m

Static Water Column Height: 12.22 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL35-3 TEST 3 FALLING HEAD

Data Set: \...\GL35-3 Test 3 Falling Head.aqt  
 Date: 07/12/23 Time: 12:38:32

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL35-3  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 6.38E-6$  m/sec  
 $y_0 = 0.4555$  m

AQUIFER DATA

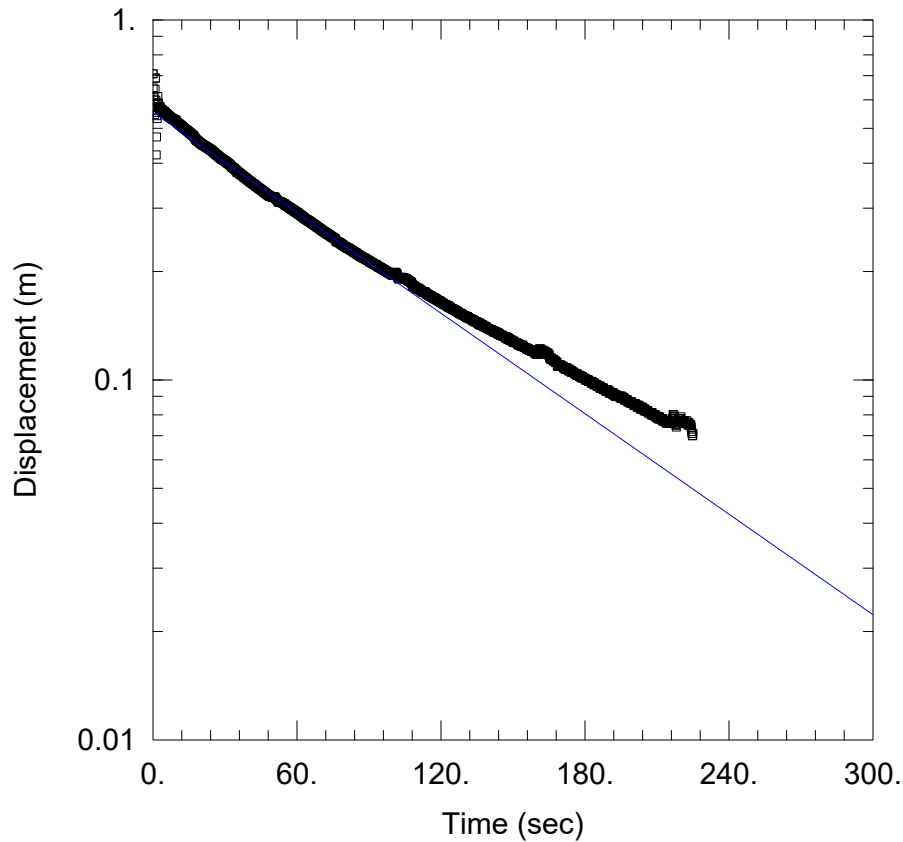
Saturated Thickness: 12.22 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL35-3)

Initial Displacement: 0.704 m  
 Total Well Penetration Depth: 13.72 m  
 Casing Radius: 0.025 m

Static Water Column Height: 12.22 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL35-3 TEST 5 FALLING HEAD

Data Set: \...\GL35-3 Test 5 Falling Head.aqt  
 Date: 07/12/23 Time: 12:41:04

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL35-3  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 8.4E-6$  m/sec  
 $y_0 = 0.5541$  m

AQUIFER DATA

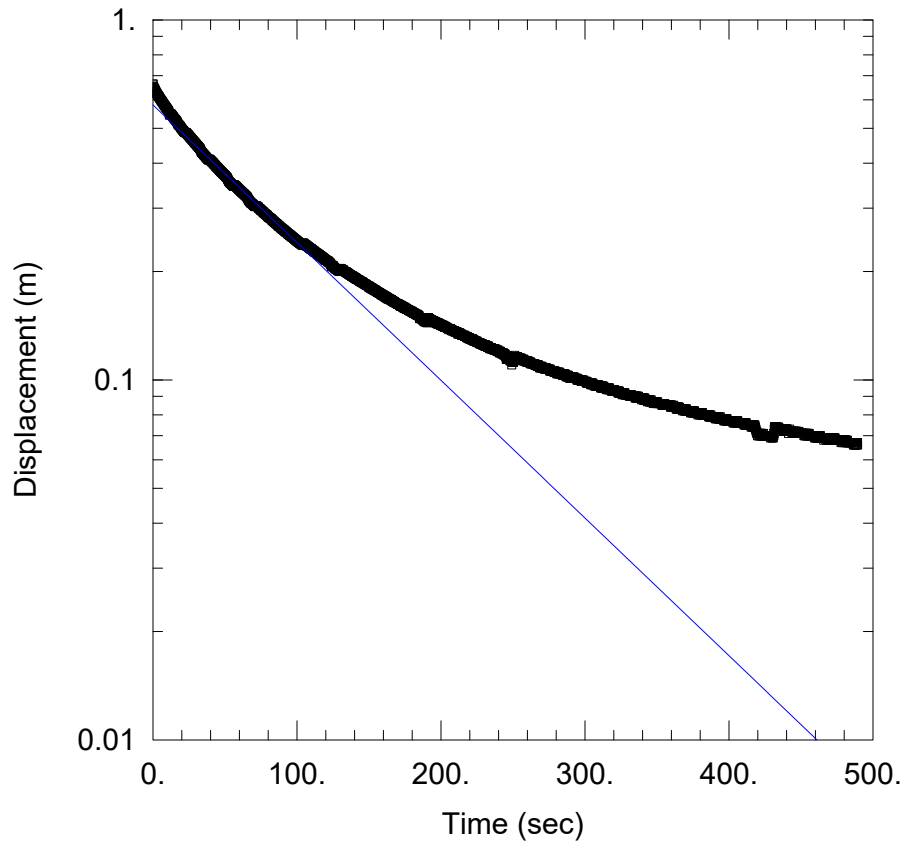
Saturated Thickness: 12.22 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL35-3)

Initial Displacement: 0.709 m  
 Total Well Penetration Depth: 13.72 m  
 Casing Radius: 0.025 m

Static Water Column Height: 12.22 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL35-3 TEST 6 RISING HEAD

Data Set: \...\GL35-3 Test 6 Rising Head.aqt  
 Date: 07/12/23 Time: 12:42:33

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL35-3  
 Test Date: 6/6/2023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 6.906E-6$  m/sec  
 $y_0 = 0.5806$  m

AQUIFER DATA

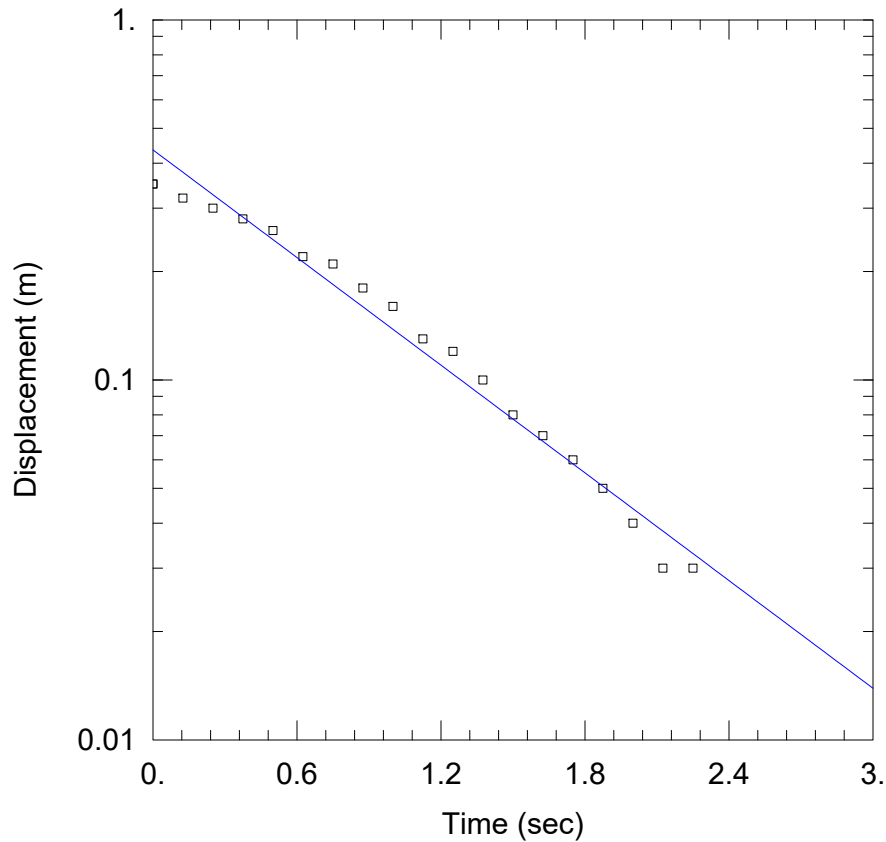
Saturated Thickness: 12.22 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL35-3)

Initial Displacement: 0.664 m  
 Total Well Penetration Depth: 13.72 m  
 Casing Radius: 0.025 m

Static Water Column Height: 12.22 m  
 Screen Length: 1.5 m  
 Well Radius: 0.075 m



GL41-2 TEST 2 RISING HEAD

Data Set: \...\GL41-2 Test 2 Rising Head.aqt  
 Date: 07/13/23 Time: 11:28:51

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL41-2  
 Test Date: 6/682023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 K = 0.001232 m/sec  
 y0 = 0.4354 m

AQUIFER DATA

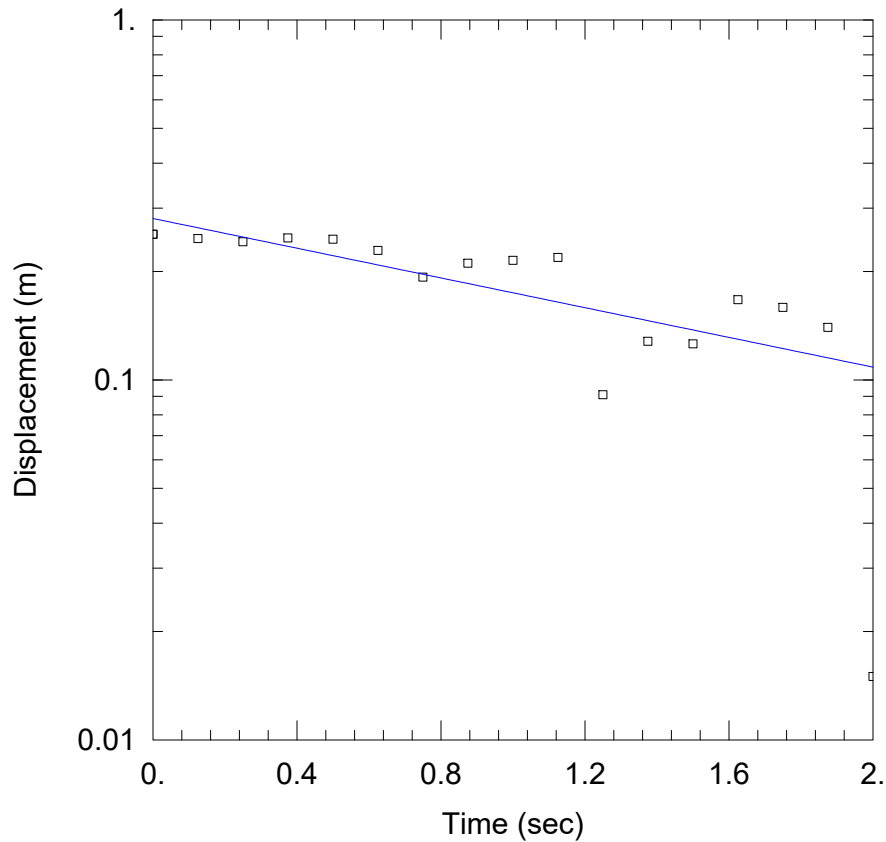
Saturated Thickness: 4.14 m

Anisotropy Ratio (Kz/Kr): 0.5

WELL DATA (GL41-2)

Initial Displacement: 0.35 m  
 Total Well Penetration Depth: 5.04 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 4.139 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



GL41-2 TEST 3 RISING HEAD

Data Set: \...\GL41-2 Test 3 Falling Head.aqt  
 Date: 07/13/23 Time: 11:31:21

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL41-2  
 Test Date: 6/682023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 0.0005105$  m/sec  
 $y_0 = 0.2808$  m

AQUIFER DATA

Saturated Thickness: 4.14 m

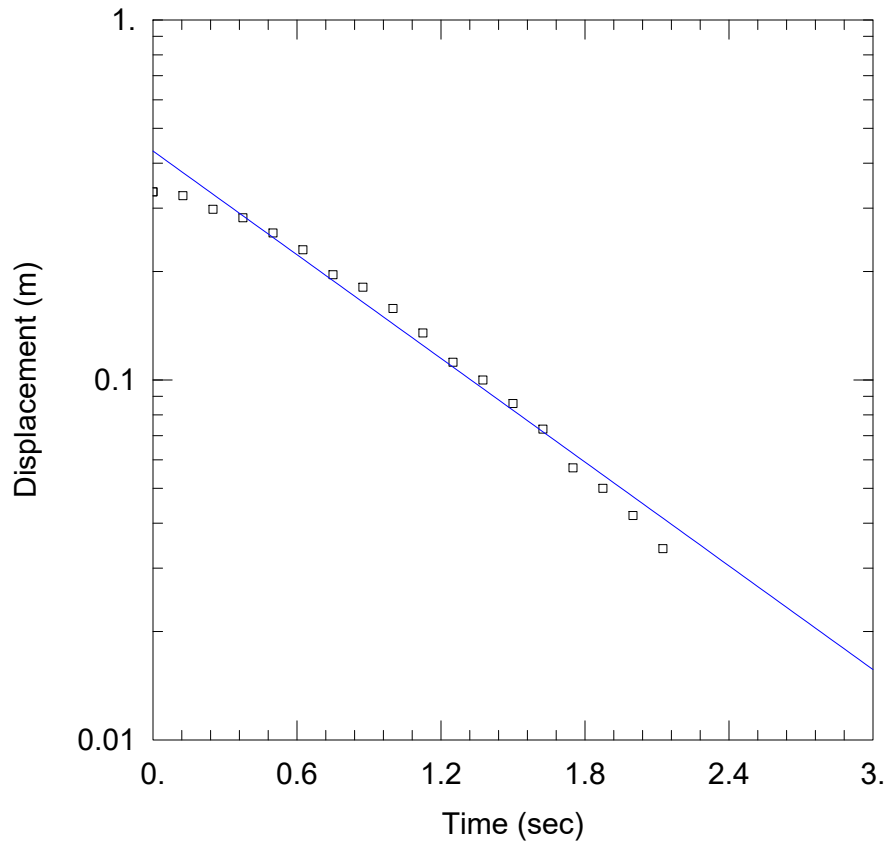
Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL41-2)

Initial Displacement: 0.254 m  
 Total Well Penetration Depth: 5.04 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 4.139 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m





GL41-2 TEST 4 RISING HEAD

Data Set: \...\GL41-2 Test 4 Rising Head.aqt  
 Date: 07/13/23 Time: 11:33:55

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL41-2  
 Test Date: 6/682023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 0.001187$  m/sec  
 $y_0 = 0.4323$  m

AQUIFER DATA

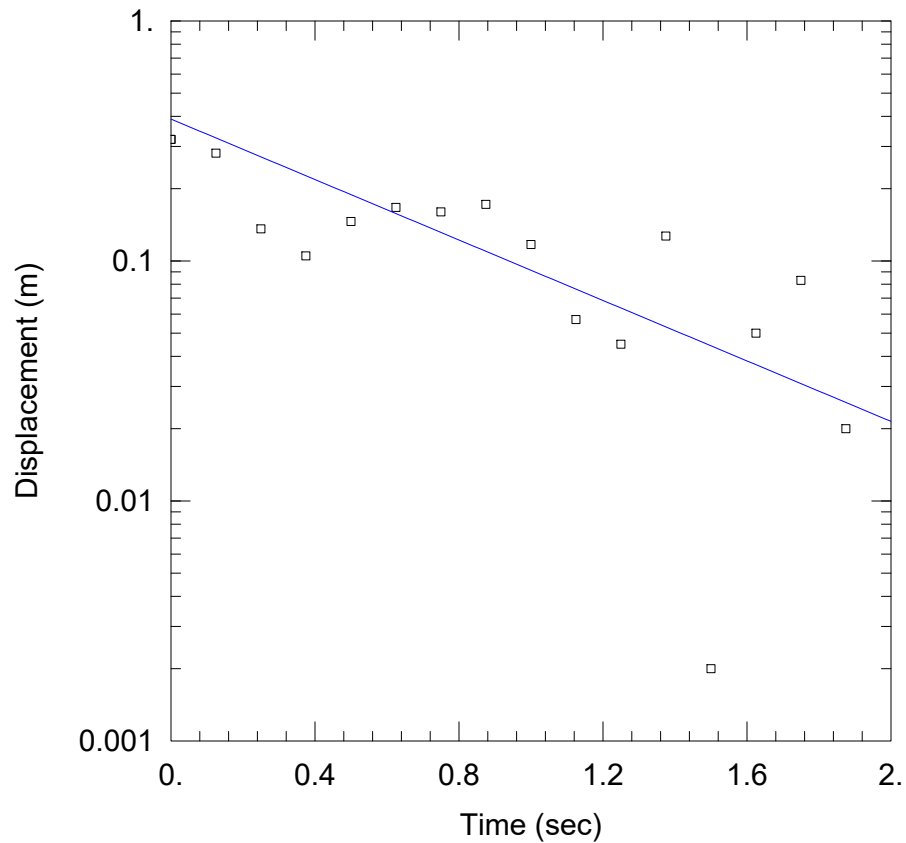
Saturated Thickness: 4.14 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL41-2)

Initial Displacement: 0.333 m  
 Total Well Penetration Depth: 5.04 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 4.139 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



GL41-2 TEST 5 FALLING HEAD

Data Set: \...\GL41-2 Test 5 Falling Head.aqt  
 Date: 07/13/23 Time: 11:36:01

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL41-2  
 Test Date: 6/682023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 0.001557$  m/sec  
 $y_0 = 0.3899$  m

AQUIFER DATA

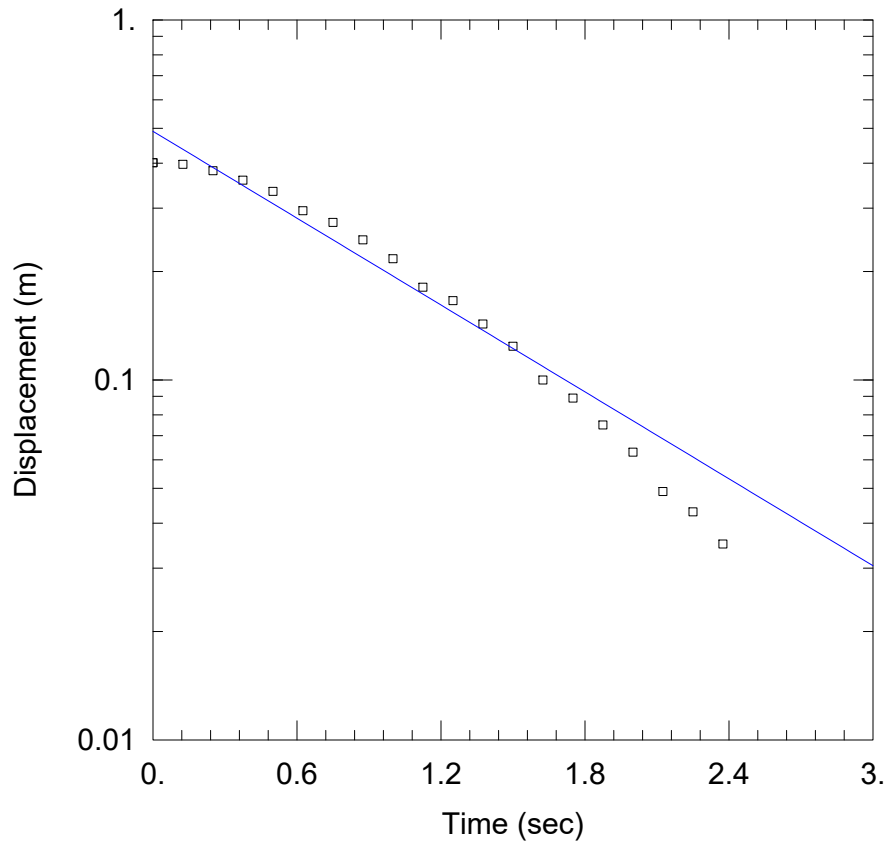
Saturated Thickness: 4.14 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL41-2)

Initial Displacement: 0.321 m  
 Total Well Penetration Depth: 5.04 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 4.139 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



GL41-2 TEST 6 RISING HEAD

Data Set: \...\GL41-2 Test 6 Rising Head.aqt  
 Date: 07/13/23 Time: 11:37:40

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL41-2  
 Test Date: 6/682023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 0.0009944$  m/sec  
 $y_0 = 0.4905$  m

AQUIFER DATA

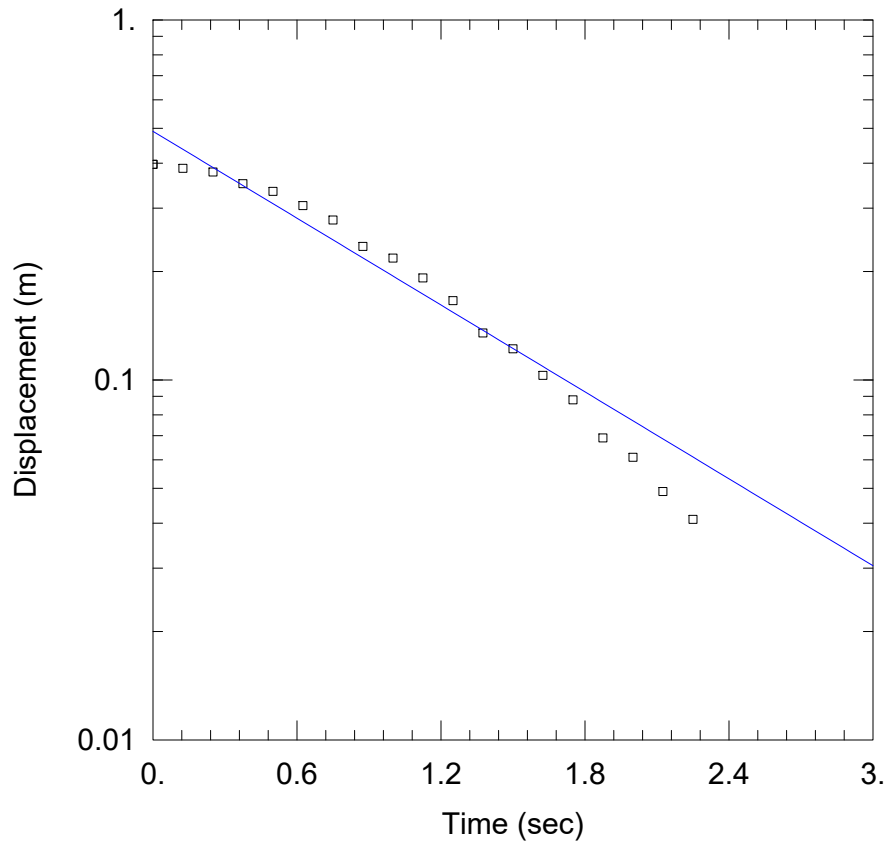
Saturated Thickness: 4.14 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL41-2)

Initial Displacement: 0.401 m  
 Total Well Penetration Depth: 5.04 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 4.139 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



GL41-2 TEST 8 RISING HEAD

Data Set: \...\GL41-2 Test 8 Rising Head.aqt  
 Date: 07/13/23 Time: 11:39:15

PROJECT INFORMATION

Company: GHD  
 Client: City of Kelowna  
 Project: 12605725  
 Location: Glenmore Landfill  
 Test Well: GL41-2  
 Test Date: 6/682023

SOLUTION

Aquifer Model: Unconfined  
 Solution Method: Bouwer-Rice  
 $K = 0.0009944$  m/sec  
 $y_0 = 0.4905$  m

AQUIFER DATA

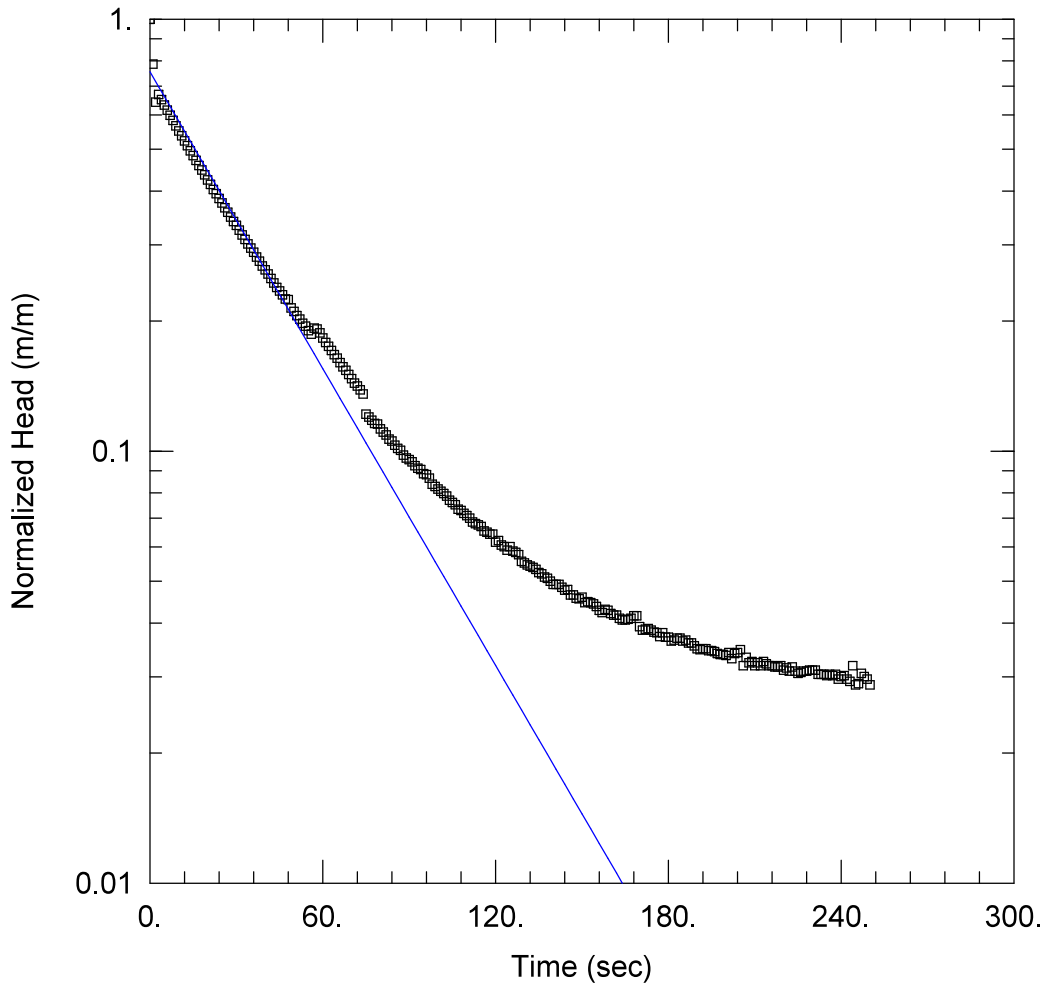
Saturated Thickness: 4.14 m

Anisotropy Ratio ( $K_z/K_r$ ): 0.5

WELL DATA (GL41-2)

Initial Displacement: 0.397 m  
 Total Well Penetration Depth: 5.04 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 4.139 m  
 Screen Length: 0.9 m  
 Well Radius: 0.075 m



WELL TEST ANALYSIS

Data Set: P:\...\GL39-1 falling head.aqt  
 Date: 12/13/19

Time: 14:28:01

PROJECT INFORMATION

Company: SNC Lavalin  
 Client: City of Kelowna  
 Project: 662036  
 Location: Glenmore Landfill, Kelowna, BC  
 Test Well: GL39-1  
 Test Date: 12 Dec 2019

AQUIFER DATA

Saturated Thickness: 10. m

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (GL39-1)

Initial Displacement: 0.5558 m  
 Total Well Penetration Depth: 6.92 m  
 Casing Radius: 0.0254 m

Static Water Column Height: 6.92 m  
 Screen Length: 1.2 m  
 Well Radius: 0.076 m

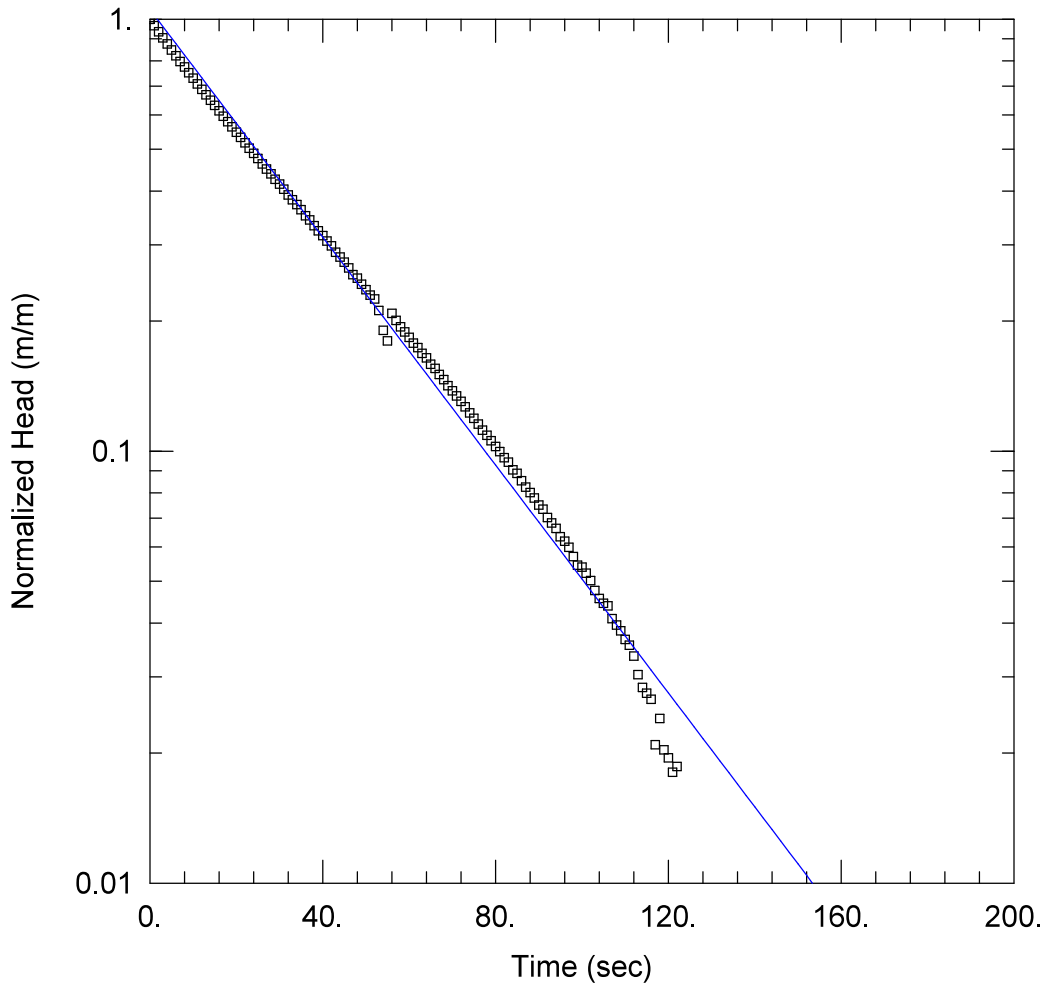
SOLUTION

Aquifer Model: Unconfined

Solution Method: Bouwer-Rice

K = 1.593E-5 m/sec

y0 = 0.4196 m



### WELL TEST ANALYSIS

Data Set: P:\...\GL39-1 rising head.aqt

Date: 12/13/19

Time: 14:33:28

### PROJECT INFORMATION

Company: SNC Lavalin

Client: City of Kelowna

Project: 662036

Location: Glenmore Landfill, Kelowna, BC

Test Well: GL39-1 Rising head

Test Date: 12 Dec 2019

### AQUIFER DATA

Saturated Thickness: 10. m

Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA (GL39-1)

Initial Displacement: 0.349 m

Static Water Column Height: 6.92 m

Total Well Penetration Depth: 6.92 m

Screen Length: 1.2 m

Casing Radius: 0.0254 m

Well Radius: 0.076 m

### SOLUTION

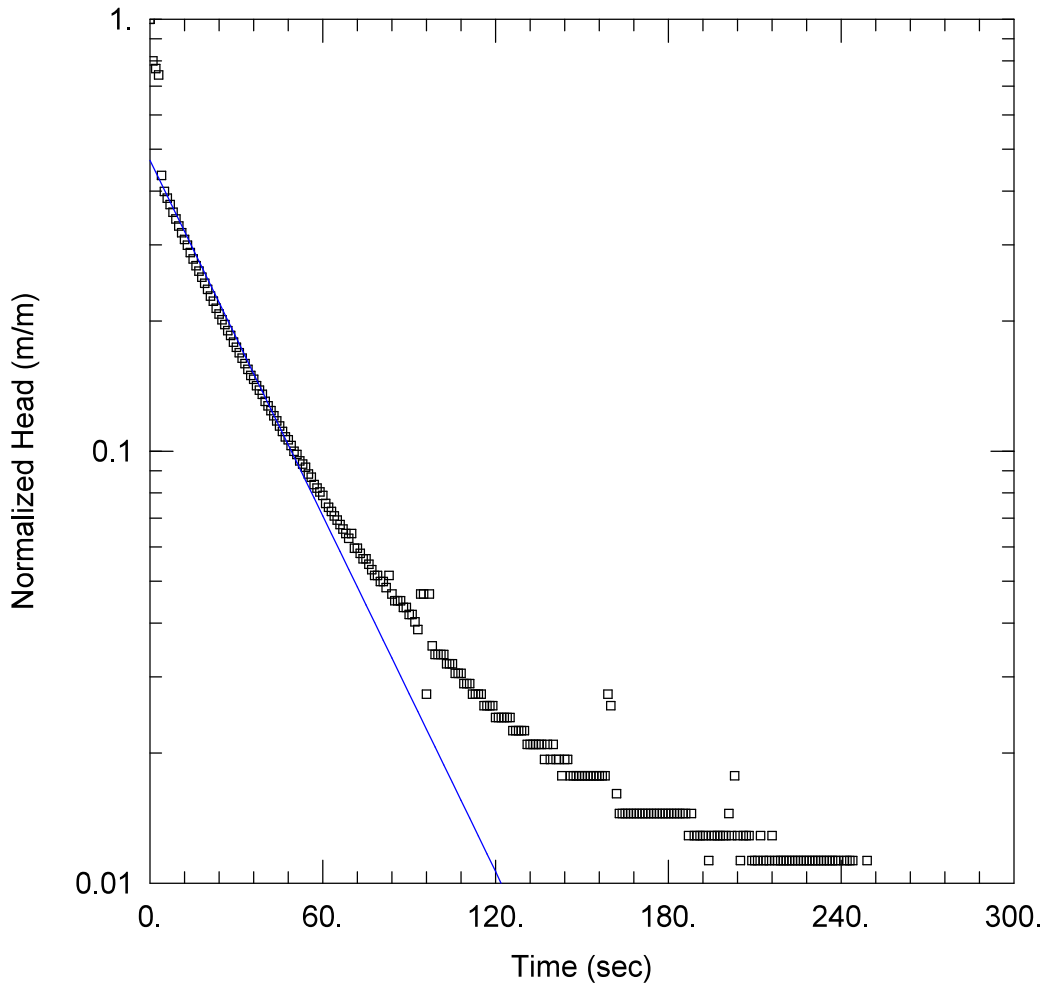
Aquifer Model: Unconfined

Solution Method: Bower-Rice

K = 1.834E-5 m/sec

y0 = 0.3674 m





### WELL TEST ANALYSIS

Data Set: P:\...\GL39-2 falling head.aqt

Date: 12/13/19

Time: 14:45:07

### PROJECT INFORMATION

Company: SNC Lavalin

Client: City of Kelowna

Project: 662036

Location: Glenmore Landfill, Kelowna, BC

Test Well: GL39-2 Falling Head

Test Date: 6 Dec 2019

### AQUIFER DATA

Saturated Thickness: 5. m

Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA (GL39-2)

Initial Displacement: 0.621 m

Static Water Column Height: 3.097 m

Total Well Penetration Depth: 3.097 m

Screen Length: 1.8 m

Casing Radius: 0.0254 m

Well Radius: 0.076 m

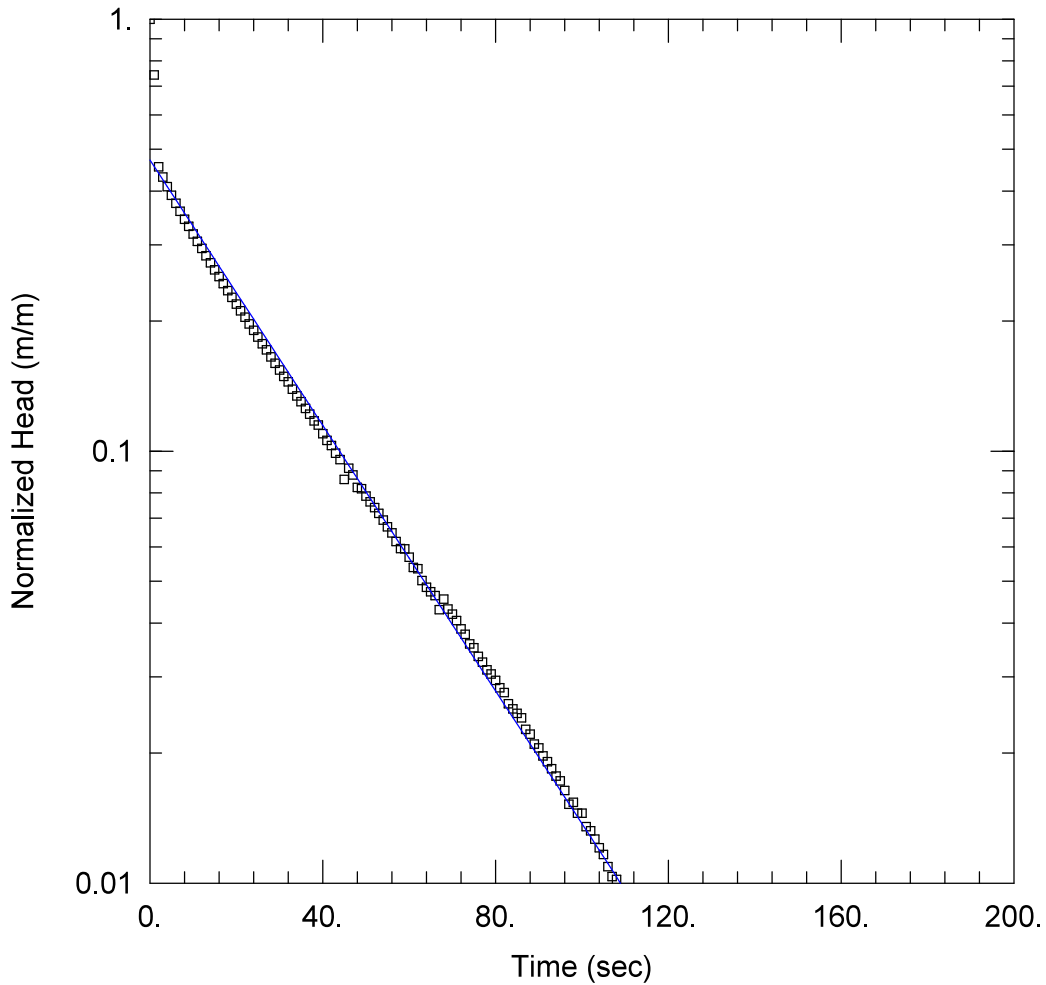
### SOLUTION

Aquifer Model: Unconfined

Solution Method: Bower-Rice

K = 1.284E-5 m/sec

y0 = 0.2925 m



### WELL TEST ANALYSIS

Data Set: P:\...\GL39-2 rising head.aqt

Date: 12/13/19

Time: 14:52:41

### PROJECT INFORMATION

Company: SNC Lavalin

Client: City of Kelowna

Project: 662036

Location: Glenmore Landfill, Kelowna, BC

Test Well: GL39-2 rising head

Test Date: 6 Dec 2019

### AQUIFER DATA

Saturated Thickness: 5. m

Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA (GL39-2)

Initial Displacement: 0.6958 m

Static Water Column Height: 3.097 m

Total Well Penetration Depth: 3.097 m

Screen Length: 1.8 m

Casing Radius: 0.0254 m

Well Radius: 0.076 m

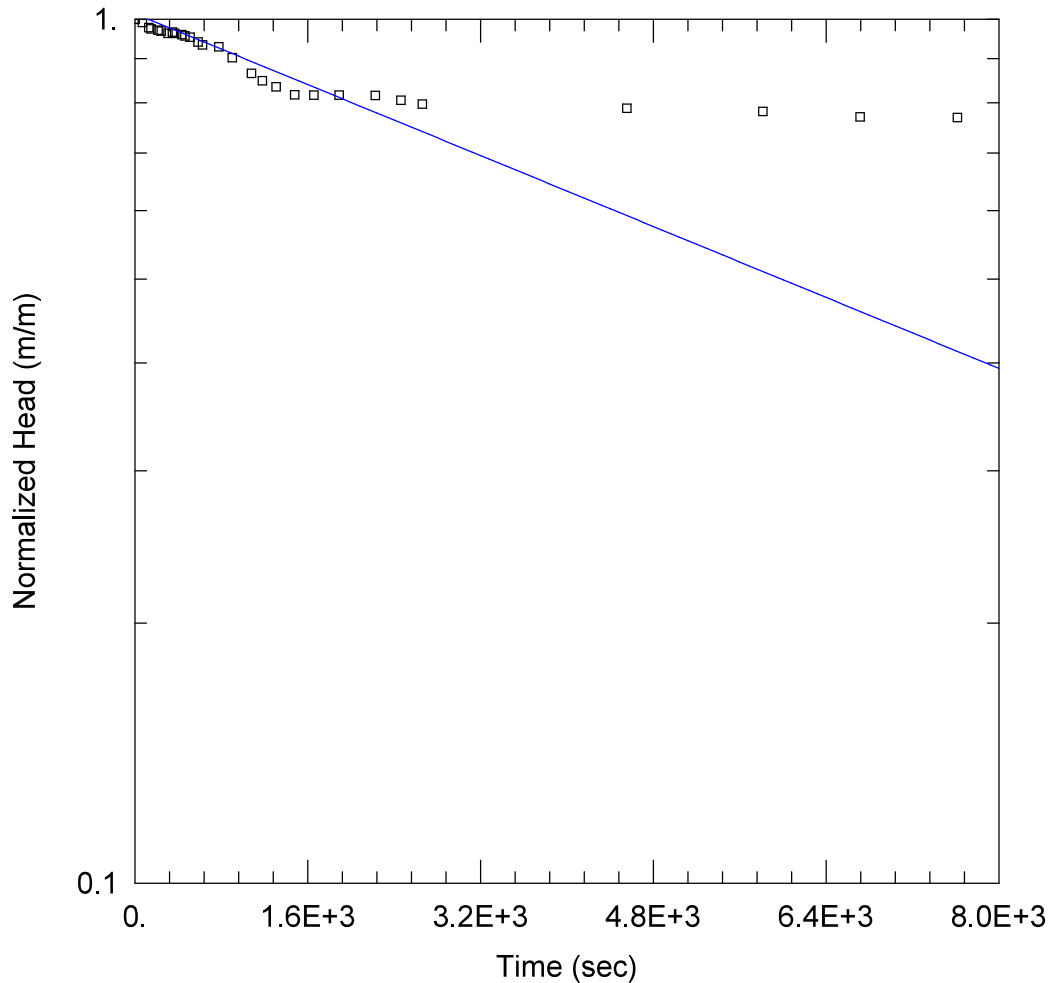
### SOLUTION

Aquifer Model: Unconfined

Solution Method: Bower-Rice

K = 1.438E-5 m/sec

y0 = 0.3284 m



WELL TEST ANALYSIS

Data Set: P:\...\GL40-2 rising head.aqt

Date: 12/13/19

Time: 15:02:33

PROJECT INFORMATION

Company: SNC Lavalin

Client: City of Kelowna

Project: 662036

Location: Glenmore Landfill, Kelowna, BC

Test Well: GL40-2 rising head

Test Date: 3 Dec 2019

AQUIFER DATA

Saturated Thickness: 1.6 m

Anisotropy Ratio (Kz/Kr): 1.

WELL DATA (GL40-2)

Initial Displacement: 10.86 m

Static Water Column Height: 11.02 m

Total Well Penetration Depth: 11.02 m

Screen Length: 1.6 m

Casing Radius: 0.0254 m

Well Radius: 0.076 m

Gravel Pack Porosity: 0.3

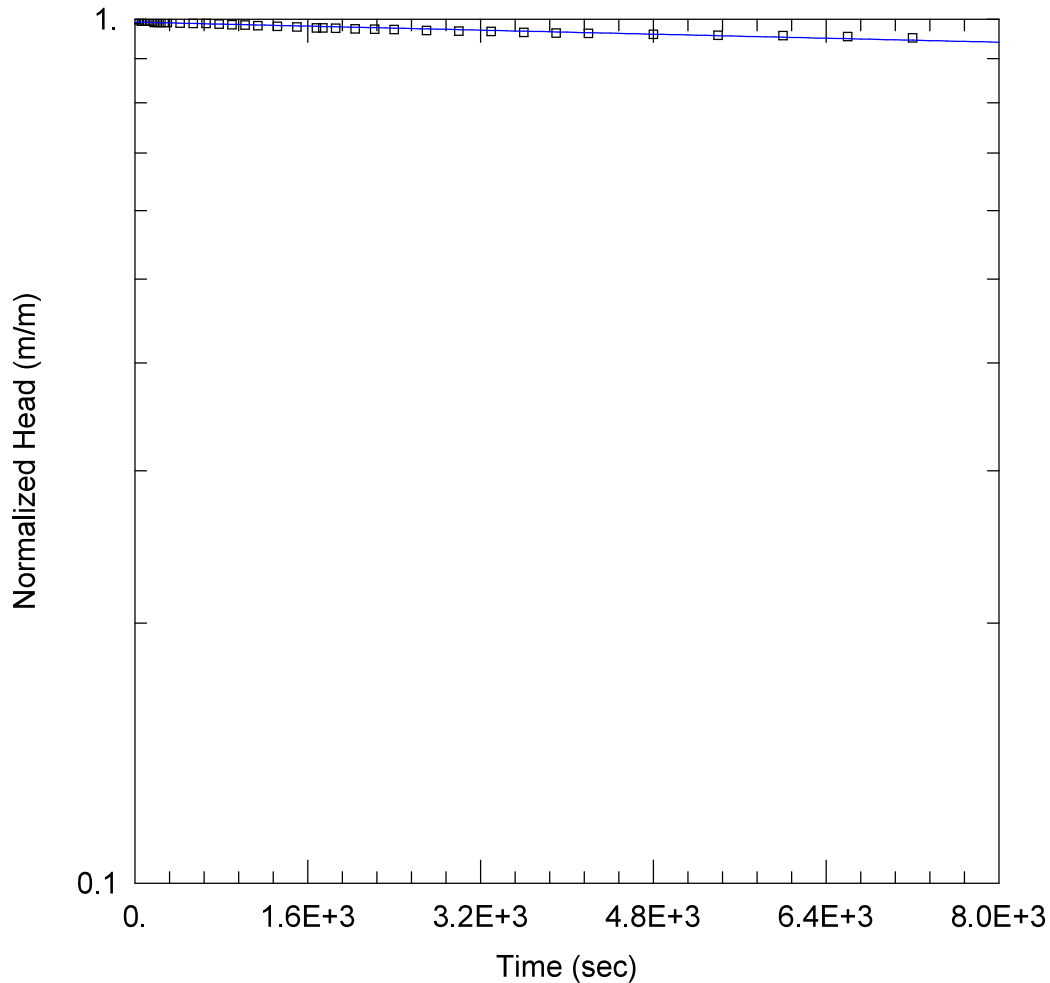
SOLUTION

Aquifer Model: Confined

Solution Method: Bower-Rice

K = 7.905E-8 m/sec

y0 = 11.01 m



### WELL TEST ANALYSIS

Data Set: P:\...\GL41-1 rising head.aqt

Date: 12/13/19

Time: 15:09:14

### PROJECT INFORMATION

Company: SNC Lavalin

Client: City of Kelowna

Project: 662036

Location: Glenmore Landfill, Kelowna, BC

Test Well: GL41-1 rising head

Test Date: 4 Dec 2019

### AQUIFER DATA

Saturated Thickness: 1.6 m

Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA (GL41-1)

Initial Displacement: 2.703 m

Static Water Column Height: 2.703 m

Total Well Penetration Depth: 2.703 m

Screen Length: 1.6 m

Casing Radius: 0.0254 m

Well Radius: 0.076 m

Gravel Pack Porosity: 0.3

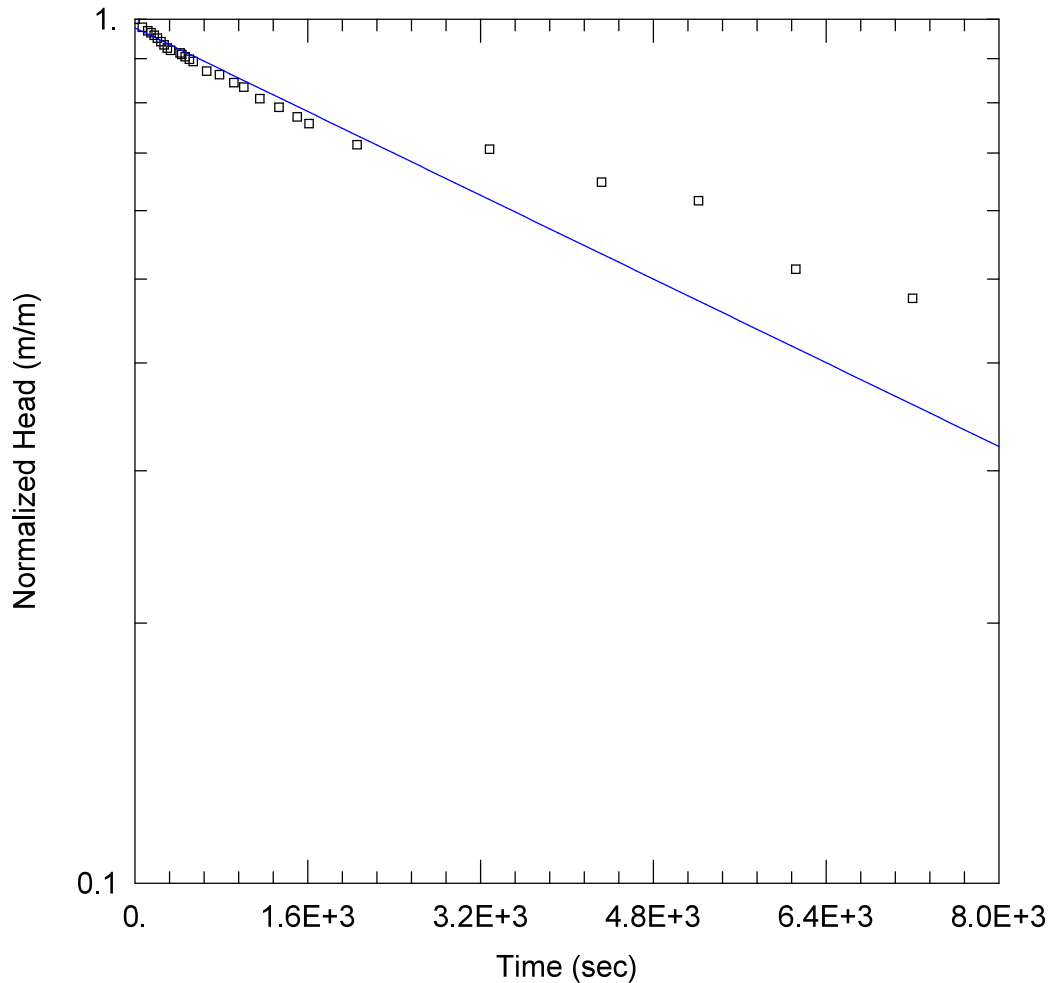
### SOLUTION

Aquifer Model: Confined

Solution Method: Bouwer-Rice

K = 3.479E-9 m/sec

y0 = 2.681 m



### WELL TEST ANALYSIS

Data Set: P:\...\GL42-1 rising head.aqt

Date: 12/13/19

Time: 15:19:09

### PROJECT INFORMATION

Company: SNC Lavalin

Client: City of Kelowna

Project: 662036

Location: Glenmore Landfill, Kelowna, BC

Test Well: GL42-1 rising head

Test Date: 3 Dec 2019

### AQUIFER DATA

Saturated Thickness: 3. m

Anisotropy Ratio (Kz/Kr): 1.

### WELL DATA (GL42-1)

Initial Displacement: 8.125 m

Static Water Column Height: 10.19 m

Total Well Penetration Depth: 10.19 m

Screen Length: 1.6 m

Casing Radius: 0.0254 m

Well Radius: 0.076 m

### SOLUTION

Aquifer Model: Confined

Solution Method: Bower-Rice

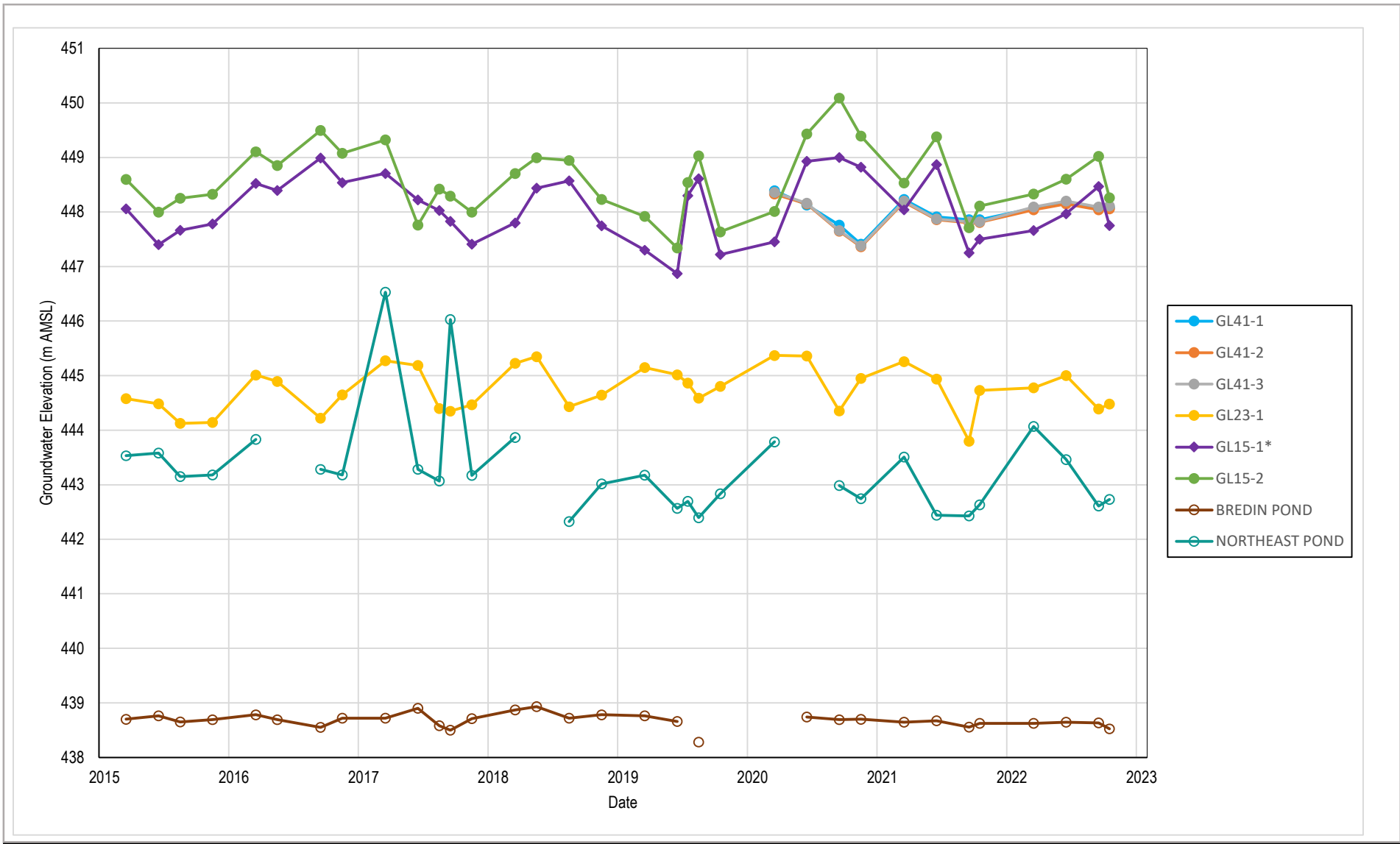
K = 9.221E-8 m/sec

y0 = 7.939 m

# Appendix E

Hydrographs





NOTES

\* Bedrock Well

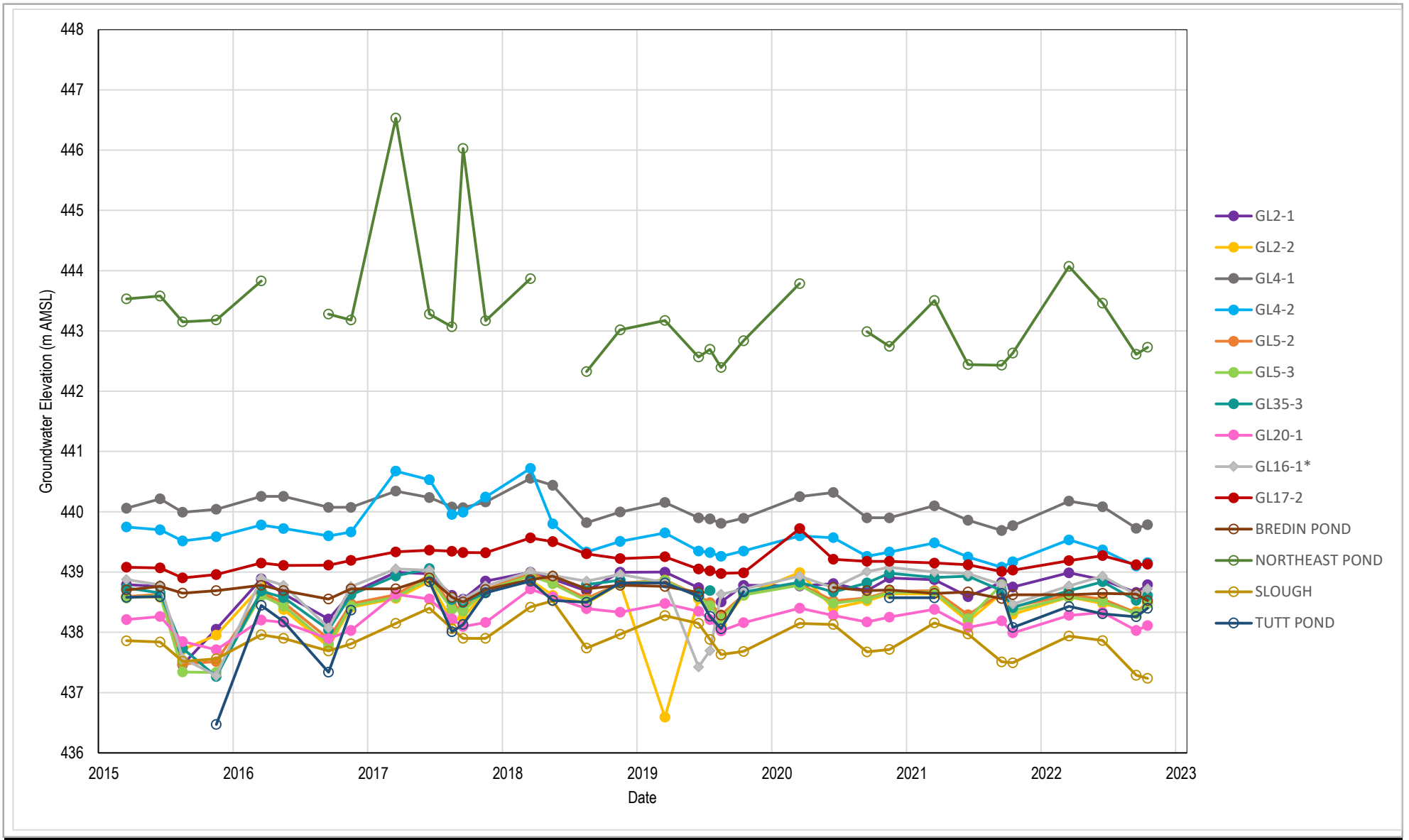


CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT

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 Date September 2023

Upgradient Wells Hydrograph 2015-2022

FIGURE E-1



NOTES

\* Bedrock Well

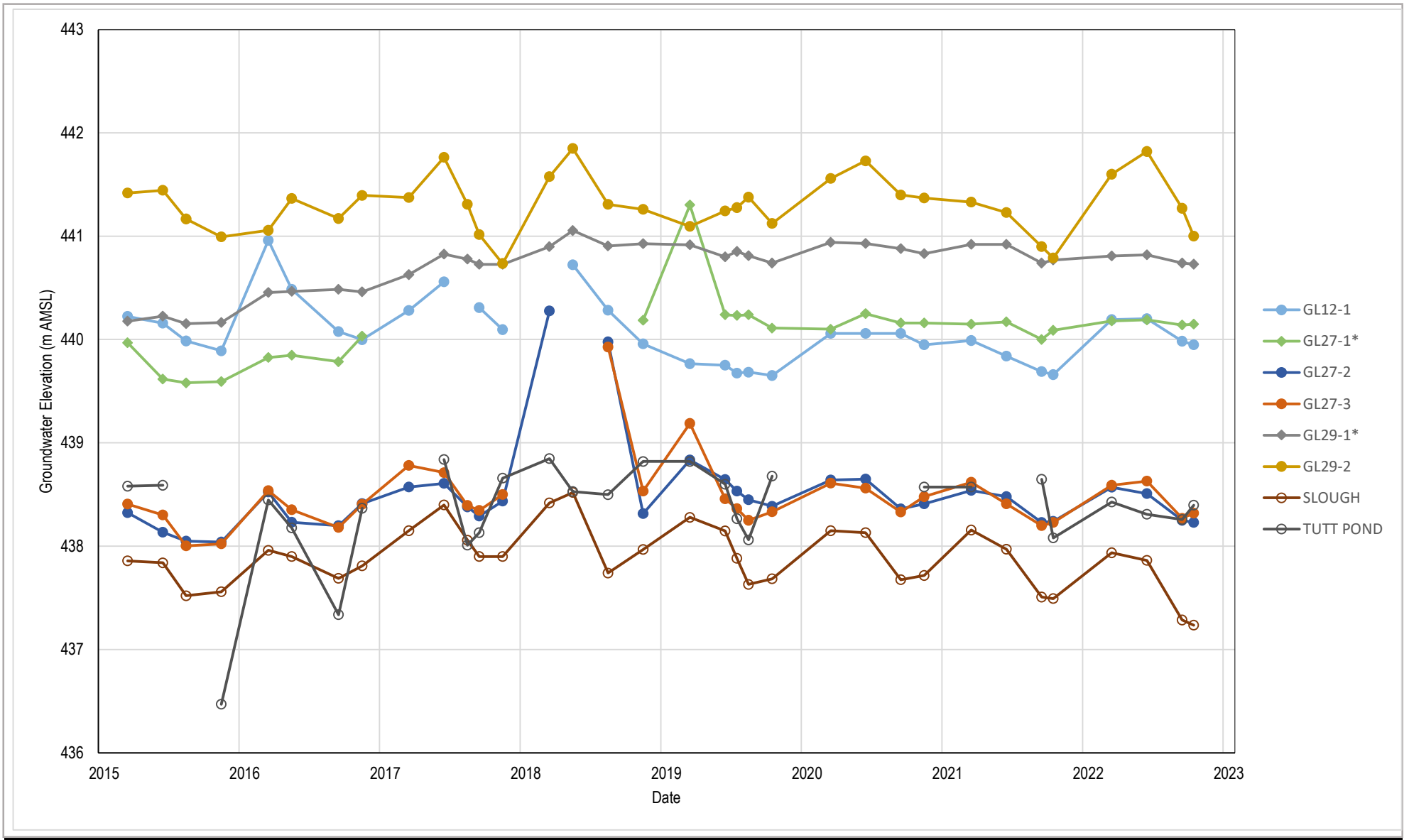


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 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT

Project No. 12605725  
 Date September 2023

Landfill Vicinity Wells Hydrograph 2015-2022

FIGURE E-2



NOTES  
\* Bedrock Well

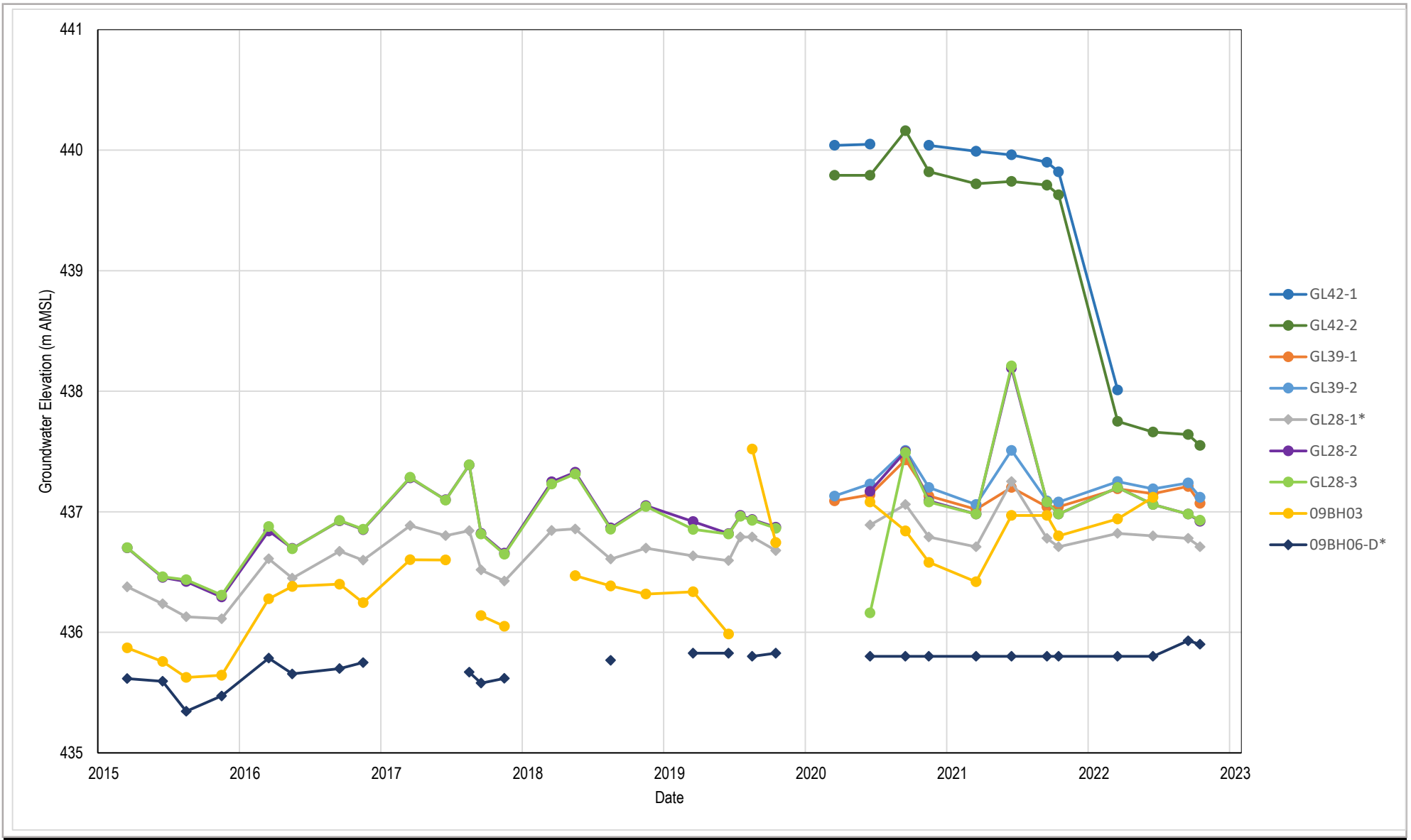


CITY OF KELOWNA  
GLENMORE LANDFILL  
HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT

Project No. 12605725  
Date September 2023

Compost Vicinity Wells Hydrograph 2015-2022

FIGURE E-3



NOTES

\* Bedrock Well

Reference elevations were used for artesian wells



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 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT

Project No. 12605725  
 Date September 2023

Downgradient Wells Hydrograph 2015-2022

FIGURE E-4

# **Appendix F**

## **Historical Water Quality Results**

Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics													
			pH	Total Hardness mg/L	pH (field)	Conductivity µS/cm	Field Conductivity µS/cm	Total Dissolved Solids mg/L	Dissolved Organic Carbon mg/L	Phosphate mg/L	Ammonia, Total (as N) µg/L	Nitrate (as N) µg/L	Nitrite (as N) µg/L	Chloride mg/L	Fluoride µg/L	Sulfate mg/L	Total Alkalinity mg/L	Alkalinity, Bicarbonate (as CaCO3) mg/L	Alkalinity, Carbonate (as CaCO3) mg/L	Alkalinity, Hydroxide (as CaCO3) mg/L	Alkalinity, Phenolphthalein (as CaCO3) mg/L	Bromide mg/L	Hydrogen Sulfide mg/L	Sulfide mg/L	Chemical Oxygen Demand mg/L	Dissolved Phosphate mg/L	Ortho-Phosphate mg/L		
09BH03	09BH03-20151105	2015 11 05	7.65	661	-	-	-	2,040	-	-	< 5.0	1,330	-	20	1,580	990	736	736	< 1.0	< 1.0	-	< 1.0	-	-	-	-	< 20	-	0.0079
	09BH03-20170601	2017 06 01	8.13	940	-	-	-	2,270	-	-	39.8	690	-	15	1,030	1,240	698	-	-	-	< 1.0	-	-	-	-	< 20	-	0.0087	
	09BH03-180604	2018 06 04	7.53	1,130	6.87	-	3,685	2,500	7.39	0.0075	< 20	< 10	< 10	26.2	790	1,500	788	788	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	30	0.0075	-	
	09BH03-190530	2019 05 30	7.80	929	6.81	-	3,120	2,450	5.85	0.0090	27.4	1,880	< 10	27.9	1,510	1,090	780	780	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	26	0.0090	-	
	09BH03-200609	2020 06 09	7.80	1,270	7.04	-	3,178	3,020	7.88	-	< 50	1,750	< 10	25.3	950	1,540	776	776	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	22	-	< 0.0050	
09BH04	09BH04-20151105	2015 11 05	7.94	812	7.08	-	2,869	1,800	7.73	-	120	1,010	< 100	11.1	< 1,000	939	713	713	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	< 0.0500	
	09BH04-20151105	2015 11 05	7.19	1,120	-	-	-	2,730	-	-	346	< 100	-	31	1,350	1,130	1,400	< 1.0	< 1.0	-	< 1.0	-	-	-	22	-	0.0012		
09BH06-S	09BH06-S-20131112	2013 11 12	-	353	-	-	-	700	-	-	87	< 50	-	8.3	940	230	392	-	-	-	-	-	-	-	-	< 20	-	-	
	09BH06-S-20140602	2014 06 02	-	358	-	-	-	700	-	-	91	< 50	-	10.9	1,010	244	444	-	-	-	-	< 0.50	-	-	-	< 20	-	0.0199	
	09BH06-S-20141117	2014 11 17	-	354	-	-	-	713	-	-	94	< 50	-	8	1,010	256	399	-	-	-	-	< 0.50	-	-	-	< 20	-	0.0177	
	09BH06-S-20150610	2015 06 10	8.22	351	-	-	-	716	-	-	95.1	< 25	-	7.1	960	252	394	-	-	-	-	< 0.25	-	-	-	< 20	-	0.0205	
	09BH06-S-20151105	2015 11 05	7.91	349	-	-	-	724	-	-	101	< 25	-	7.6	980	282	362	362	< 1.0	< 1.0	-	< 0.25	-	-	-	< 20	-	0.0157	
09BH06-D	09BH06-D-20131112	2013 11 12	-	372	-	-	-	706	-	-	94	< 50	-	9.1	940	243	397	-	-	-	-	-	-	-	-	< 20	-	-	
	DUP4-20131112	Duplicate	-	369	-	-	-	715	-	-	92	< 50	-	9	950	244	363	-	-	-	-	-	-	-	-	< 20	-	-	
	QA/QC RPD%	-	1	-	-	-	-	1	-	-	2	-	-	1	1	0	4	-	-	-	-	-	-	-	-	-	-	-	
	09BH06-D-20140602	2014 06 02	-	366	-	-	-	720	-	-	96	< 50	-	9.5	1,000	254	376	-	-	-	-	< 0.50	-	-	-	< 20	-	0.0125	
	09BH06-D-20141117	2014 11 17	-	372	-	-	-	743	-	-	99.5	< 50	-	8.3	1,010	272	407	-	-	-	-	< 0.50	-	-	-	42	-	0.009	
	09BH06-D-20150610	2015 06 10	8.21	385	-	-	-	770	-	-	102	< 25	-	7.9	940	285	398	-	-	-	-	< 0.25	-	-	-	< 20	-	0.0107	
	09BH06-D-20151105	2015 11 05	7.93	369	-	-	-	760	-	-	100	< 25	-	7.7	940	295	365	365	< 1.0	< 1.0	-	< 0.25	-	-	-	< 20	-	0.008	
	09BH06-D-20170606	2017 06 06	8.42	364	-	-	-	699	-	-	107	< 25	-	8.2	970	286	343	-	-	-	-	< 0.25	-	-	-	< 20	-	0.0092	
	09BH06-D-180604	2018 06 04	7.76	387	6.99	-	1,289	800	2.98	0.0055	167	< 10	< 10	7.16	450	282	355	355	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	0.0055	
	09BH06-D-190528	2019 05 28	8.04	435	7.08	-	1,229	968	2.88	0.0073	199	< 10	< 10	9.45	800	392	377	377	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	0.0073	
	09BH06-D-200609	2020 06 09	7.95	422	7.3	-	1,038	849	2.26	-	96	< 10	< 10	8.22	790	327	373	373	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	< 0.0050	
	09BH06-D-210608	2021 06 08	8.08	333	7.40	-	1,142	742	2.54	-	120	< 10	< 10	6.95	960	278	357	357	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	< 0.0050	
	GL0-1	GL0-1-20130625	2013 06 25	-	427	-	-	-	771	-	-	91.9	< 50	-	7.9	1,170	373	205	-	-	-	-	< 0.50	-	-	-	< 20	-	-
		GL0-1-20140603	2014 06 03	-	416	-	-	-	711	-	-	52.9	99	-	9.1	1,010	348	205	-	-	-	-	< 0.50	-	-	-	< 20	-	0.0596
		GL0-1-20141124	2014 11 24	-	436	-	-	-	711	-	-	58.4	< 50	-	9.3	970	355	209	-	-	-	-	< 0.50	-	-	-	< 20	-	0.0519
DUP1-20141124		Duplicate	-	430	-	-	-	680	-	-	62.1	< 50	-	7.9	1,140	355	205	-	-	-	-	< 0.50	-	-	-	< 20	-	0.0518	
QA/QC RPD%		-	1	-	-	-	-	4	-	-	6	-	-	16	16	0	2	-	-	-	-	-	-	-	-	-	-	0	
GL0-1-20150608		2015 06 08	7.59	423	-	-	-	665	-	-	48.9	116	-	7.3	884	345	209	-	-	-	-	< 0.10	-	-	-	< 20	-	0.0637	
GL0-1-20151103		2015 11 03	7.65	423	-	-	-	682	-	-	77.4	< 25	-	7.1	990	354	206	-	-	-	-	< 0.25	-	-	-	< 20	-	0.0617	
GL0-1-20160524		2016 05 24	8.19	423	-	-	-	673	-	-	38.4	65	-	7.1	980	346	198	198	< 1.0	< 1.0	-	< 0.25	-	-	-	< 20	-	0.0555	
GL0-1-20170524		2017 05 24	8.32	418	-	-	-	671	-	-	9.7	131	-	7.2	1,000	350	196	-	-	-	-	< 0.25	-	-	-	< 20	-	0.0614	
GL0-1-180529		2018 05 29	7.81	415	7.65	-	934	690	0.87	0.0516	43	82	< 10	6.47	640	281	187	187	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	0.0516	
GL0-1-190523	2019 05 23	8.09	384	7.65	-	859	691	1.69	0.0174	< 20	109	< 10	6.33	730	326	191	191	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	0.0174		
GL0-1-200310	2020 03 10	7.94	405	-	-	-	705	1.01	-	284	49	< 10	6.82	860	316	189	189	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	< 20	-	0.0175		

Associated CARO files available upon request.  
 Associated Enviva file(s): 712940, 714233, 756693, 756810, 757047, 811364, 811710, 812030, 812741, 812985, 813438, 846260, 878316, 879073, 909346, 909448, 909654.  
 All terms defined within the body of KelTech's report.  
 < - Denotes concentration less than indicated detection limit or RPD less than indicated value.  
 - - Denotes analysis not conducted.  
 n/a Denotes no applicable standard/guideline.  
 QA/QC RPD Denotes quality assurance/quality control relative percent difference  
 \* RPDs are not calculated where one or more concentrations are less than five times RDL.  
 RDL Denotes reported detection limit.







Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics													
			pH	Total Hardness	pH (field)	Conductivity	Field Conductivity	Total Dissolved Solids	Dissolved Organic Carbon	Phosphate	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bromide	Hydrogen Sulfide	Sulfide	Chemical Oxygen Demand	Dissolved Phosphate	Ortho-Phosphate		
			mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	µg/L	µg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
GL3-5	GL3-5-20130627	2013 06 27	-	1,260	-	-	-	1,950	-	48,000	< 100	-	90	960	< 10	2,100	-	-	-	-	-	-	-	-	-	-	152	-	-
	GL3-5 (2012)-20140809	2014 06 09	-	1,230	-	-	-	1,920	-	53,800	100	-	94	980	< 10	2,020	-	-	-	-	-	-	-	-	-	-	152	-	0.0016
	GL3-5 (2012)-20141125	2014 11 25	-	1,330	-	-	-	2,030	-	49,600	< 100	-	98	730	< 6.0	1,990	-	-	-	-	-	-	-	-	-	-	148	-	0.0018
	GL3-5 (2012)-20150609	2015 06 09	7.43	1,240	-	-	-	1,850	-	52,700	< 50	-	93.7	640	< 3.0	2,110	-	-	-	-	-	-	-	-	-	-	139	-	0.0015
	DUP1-20150609	Duplicate	7.41	1,230	-	-	-	1,860	-	48,100	< 25	-	92.6	600	< 1.5	2,140	-	-	-	-	-	0.8	-	-	-	-	138	-	0.0017
	QA/QC RPD%		0	1	-	-	-	1	-	9	-	-	1	6	-	1	-	-	-	-	-	8	-	-	-	1	-	-	-
GL4-1	GL3-5 (2012)-20151109	2015 11 09	6.8	1,280	-	-	-	1,990	-	49,900	< 100	-	93	940	< 6.0	1,960	-	-	-	-	-	-	-	-	-	-	139	-	< 0.0010
	GL 4-1-20091110	2009 11 10	-	630	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL 4-1-20120626	2012 06 26	-	-	-	-	-	1,170	-	-	-	-	7.4	-	142	792	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL 4-1-20120704	2012 07 04	-	580	-	-	-	-	-	8,700	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	70	-	1.4	
	GL4-1-20100810	2010 08 10	-	600	-	-	-	1,210	-	20	-	-	10.4	-	474	542	-	-	-	-	-	-	-	-	-	< 10	-	0.012	
	GL4-1-20110629	2011 06 29	-	613	-	-	-	1,190	-	760	-	-	10.6	-	442	571	-	-	-	-	-	-	-	-	-	10	-	0.148	
	GL4-1-20120625	2012 06 25	-	610	-	-	-	1,230	-	2,520	-	-	13.7	-	432	377	-	-	-	-	-	-	-	-	-	30	-	0.16	
	GL4-1-20121203	2012 12 03	-	548	-	-	-	1,210	-	170	< 100	-	12.1	-	458	542	-	-	-	-	-	-	-	-	-	20	-	0.008	
	GL4-1-20130627	2013 06 27	-	622	-	-	-	1,140	-	105	< 100	-	12	2,660	501	583	-	-	-	-	-	-	-	-	-	< 1.0	-	< 20	
	DUP4-20130627	Duplicate	-	638	-	-	-	1,130	-	102	< 100	-	13	2,520	501	560	-	-	-	-	-	-	-	-	-	< 1.0	-	< 20	
	QA/QC RPD%		-	3	-	-	-	1	-	3	-	-	8	5	-	4	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL4-1-20140603	2014 06 03	-	597	-	-	-	1,140	-	94.6	< 100	-	15	2,180	482	527	-	-	-	-	-	-	-	-	-	< 1.0	-	< 20	0.006
	GL4-1-20141124	2014 11 24	-	646	-	-	-	1,160	-	102	< 100	-	16	2,510	514	524	-	-	-	-	-	-	-	-	-	< 1.0	-	< 20	0.0057
	GL4-1-20150608	2015 06 08	8	625	-	-	-	1,110	-	102	< 50	-	12.9	2,100	505	536	-	-	-	-	-	-	-	-	-	< 0.50	-	< 20	0.0068
GL4-1-20151104	2015 11 04	8.09	591	-	-	-	1,130	-	117	< 50	-	12.2	2,010	492	522	-	-	-	-	-	-	-	-	-	< 0.50	-	< 20	0.0052	
GL4-1-200814	2020 08 14	8.18	642	7.95	-	1,846	1,280	2,82	-	126	< 100	< 100	16.7	1,540	498	563	563	< 1.0	< 1.0	< 1.0	< 1.00	< 1.0	-	-	< 20	-	< 0.0500		
GL4-1-201016	2020 10 16	8.11	616	7.89	-	1,582	1,260	3.18	-	116	< 10	< 10	17.7	1,900	501	536	536	< 1.0	< 1.0	< 1.0	< 0.10	< 1.0	-	-	< 20	-	< 0.0050		
GL4-1-210511	2021 05 11	8.17	618	7.62	-	1,831	1,300	3.18	-	113	11	< 10	16.6	1,910	482	562	562	< 1.0	< 1.0	< 1.0	< 0.10	< 1.0	-	-	< 20	-	< 0.0050		
GL4-2-20091116	2009 11 16	-	1,040	-	-	-	1,747	1,320	3,04	-	148	< 10	< 10	15.5	1,930	534	555	555	< 1.0	< 1.0	< 1.0	< 1.00	< 1.0	-	-	< 20	-	< 0.0050	
GL4-2	GL4-2-20100810	2010 08 10	-	1,000	-	-	-	1,760	-	-	< 10	-	-	-	395	956	-	-	-	-	-	-	-	-	-	20	-	0.011	
	GL4-2-20110629	2011 06 29	-	1,010	-	-	-	1,540	-	240	-	-	57	-	390	934	-	-	-	-	-	-	-	-	-	10	-	0.211	
	GL4-2-20120626	2012 06 26	-	1,000	-	-	-	1,550	-	140	-	-	51.1	-	386	1,000	-	-	-	-	-	-	-	-	-	20	-	0.021	
	GL4-2-20121203	2012 12 03	-	973	-	-	-	1,700	-	< 10	< 100	-	40.5	-	292	926	-	-	-	-	-	-	-	-	-	30	-	0.022	
	GL4-2-200814	2020 08 14	8.04	846	7.71	-	2,259	1,610	5.89	-	< 50	< 100	< 100	61.7	2,040	480	845	845	< 1.0	< 1.0	< 1.0	< 1.00	< 1.0	-	-	< 20	-	< 0.0500	
	GL4-2-201030	2020 10 30	8.01	765	7.46	-	2,207	1,460	4.41	-	< 50	< 10	< 10	49.4	2,520	473	812	812	< 1.0	< 1.0	< 1.0	0.27	< 1.0	-	-	< 20	-	< 0.0050	
	GL4-2-210511	2021 05 11	8.13	818	7.43	-	2,200	1,500	6.52	-	< 50	< 10	< 10	55.6	2,510	456	807	807	< 1.0	< 1.0	< 1.0	< 1.00	< 1.0	-	-	< 20	-	< 0.0050	
	GL4-2-211005	2021 10 05	7.95	829	7.40	-	2,023	1,760	4.25	-	< 50	< 10	< 10	46.0	2,670	475	843	843	< 1.0	< 1.0	< 1.0	< 1.00	< 1.0	-	-	< 20	-	< 0.0050	
	GL5-1	GL5-1-20091116	2009 11 16	-	77	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		GL5-1-20100810	2010 08 10	-	110	-	-	-	1,690	-	250	-	-	42.2	-	283	1,210	-	-	-	-	-	-	-	-	-	< 10	-	0.002
GL5-2-20180528		2018 05 28	7.83	671	-	-	-	1,370	-	52	6,270	-	266	500	201	472	472	< 1.0	< 1.0	-	< 5.00	-	-	-	< 20	-	< 0.0050		

Associated CARO files available upon request.  
 Associated Exova file(s): 712940, 714233, 714243, 756693, 756810, 757047, 811364, 811710, 812030, 812741, 812985, 813438, 846260, 878316, 879073, 909346, 909448, 909654.  
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Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics														
			pH	Total Hardness	pH (field)	Conductivity	Field Conductivity	Total Dissolved Solids	Dissolved Organic Carbon	Phosphate	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bromide	Hydrogen Sulfide	Sulfide	Chemical Oxygen Demand	Dissolved Phosphate	Ortho-Phosphate			
			mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	
GL6-1 (2011) (cont'd)	GL6-1 (2011)-20170530	2017 05 30	7.4	1,260	-	-	-	7,540	-	-	119	< 250	-	941	< 1,000	1,210	4,370	-	-	-	-	-	-	-	-	-	-	< 20	-	2,69
	GL6-1(2011)-20121205	2012 12 05	-	1,990	-	-	-	9,940	-	-	245,000	< 10,000a	-	828	-	2,080	814	-	-	-	-	-	-	-	-	-	-	1,280	-	4
	GL6-1-190604	2019 06 04	7.45	1,900	6,987.0	15,700	14,230	10,800	339	0.224	334,000	< 5,000a	276	1,570	< 50,000a	12,000	3,960	3,960	< 1.0	< 1.0	< 1.0	< 50.0	0.49	1.08	881	0.224	-	-	-	
	GL6-1 (2011)-190603	2019 06 03	7.80	1,270	7.42	11,200	11,903	6,100	175	1.15	227,000	< 1,000	< 1,000a	527	< 10,000a	2,380	3,600	3,600	< 1.0	< 1.0	< 1.0	< 10.0	0.82	8.44	705	1.15	-	-	-	
	DUP3-190603	Duplicate	7.72	1,240	7.42	-	-	11,903	8,100	180	0,560	236,000	< 1,000	< 1,000a	559	< 10,000a	2,350	3,510	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	705	0,560	-	-	
QA/QC RPD%			1	2	-	-	-	28	3	69	4	-	-	6	-	3	3	-	-	-	-	-	-	-	-	-	0	69	-	
GL7-1	GL6-1-200611	2020 06 11	7.82	962	7.1	8,440	6,871	5,220	241	-	194,000	< 100	< 100	652	< 1,000	282	3,980	3,980	< 1.0	< 1.0	< 1.0	4.43	10.7	25.5	621	-	-	0.576		
	GL6-1-210610	2021 06 10	7.07,7.2	1,230	6,99	8,020	7,919	4,570	211	-	210,000	< 100	< 100	659	< 1,000	25.0	3,990	3,990	< 1.0	< 1.0	< 1.0	5.22	0.29	6.00	842	-	-	0.413		
	GL7-1-20110704	2011 07 04	-	1,190	-	-	-	2,560	-	-	400	-	-	69.3	-	735	1,410	-	-	-	-	-	-	-	-	-	30	-	0.006	
	GL7-1-20120625	2012 06 25	-	1,150	-	-	-	2,590	-	-	360	-	-	69.2	-	709	1,540	-	-	-	-	-	-	-	-	-	30	-	< 0.002	
	GL7-1-20121205	2012 12 05	-	1,120	-	-	-	2,500	-	-	450	< 1,000	-	72	-	758	1,520	-	-	-	-	-	-	-	-	-	32	-	0.002	
	GL7-1-20130626	2013 06 26	-	1,110	-	-	-	2,500	-	-	442	< 100	-	69	2,490	771	1,440	-	-	-	-	< 1.0	-	-	-	-	34	-	-	
	GL7-1-20131114	2013 11 14	-	1,140	-	-	-	2,530	-	-	446	< 100	-	75	2,390	757	1,540	-	-	-	-	< 1.0	-	-	-	27	-	-		
	DUP1-20131114	Duplicate	-	1,130	-	-	-	2,500	-	-	444	< 100	-	73	2,500	778	1,610	-	-	-	-	< 1.0	-	-	-	20	-	-		
	QA/QC RPD%			1	-	-	-	-	1	-	0	-	-	3	4	2	4	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL7-1-20140604	2014 06 04	-	1,190	-	-	-	2,560	-	-	435	< 100	-	57	2,420	671	1,780	-	-	-	-	< 1.0	-	-	-	24	-	-	< 0.0010	
	GL7-1-20141125	2014 11 25	-	1,110	-	-	-	2,480	-	-	411	< 100	-	71	2,300	759	1,230	-	-	-	-	< 1.0	-	-	-	30	-	-	< 0.0010	
	GL7-1-20150609	2015 06 09	7.32	1,090	-	-	-	2,430	-	-	408	< 25	-	58.4	1,770	669	1,800	-	-	-	-	0.54	-	-	-	28	-	-	0.0014	
	GL7-1-20151109	2015 11 09	6.61	1,080	-	-	-	2,470	-	-	412	< 100	-	61	2,180	704	1,430	-	-	-	-	< 1.0	-	-	-	29	-	-	< 0.0010	
	GL8-1	GL 8-1-20091110	2009 11 10	-	60	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
		GL8-1-20100810	2010 08 10	-	630	-	-	-	2,710	-	-	430	-	-	55.9	-	1,230	650	-	-	-	-	-	-	-	-	< 10	-	-	0.037
GL8-2	GL 8-2-20091110	2009 11 10	-	1,190	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	GL8-2-20100810	2010 08 10	-	928	-	-	-	8,530	-	-	20	-	-	528	-	2,830	2,800	-	-	-	-	-	-	-	-	-	120	-	0.298	
	GL8-2-20110627	2011 06 27	-	1,040	-	-	-	7,520	-	-	220	-	-	512	-	2,760	2,520	-	-	-	-	-	-	-	-	-	100	-	0.158	
	GL8-2-20111217	2011 12 17	-	652	-	-	-	7,360	-	-	60	< 100	-	511	-	2,940	2,470	-	-	-	-	-	-	-	-	-	120	-	0.35	
	GL 8-2-20120626	2012 06 26	-	800	-	-	-	5,610	-	-	130	-	-	390	-	1,870	2,080	-	-	-	-	-	-	-	-	-	-	-	-	
	DUP 8-20120626	Duplicate	-	800	-	-	-	7,250	-	-	140	-	-	467	-	2,550	2,510	-	-	-	-	-	-	-	-	-	90	-	-	
	QA/QC RPD%			0	-	-	-	-	28	-	7	-	-	18	-	26	19	-	-	-	-	-	-	-	-	-	-	-	-	29
	GL 8-2-20120704	2012 07 04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.05
	GL8-2-20121204	2012 12 04	-	581	-	-	-	7,350	-	-	90	220	-	478	-	2,830	2,600	-	-	-	-	-	-	-	-	-	113	-	-	0.324
	GL8-2-20130626	2013 06 26	-	1,180	-	-	-	7,140	-	-	64.4	350	-	459	3,200	3,260	1,930	-	-	-	-	3.6	-	-	-	-	487	-	-	
	GL8-2-20131113	2013 11 13	-	800	-	-	-	7,050	-	-	25.8	< 250	-	460	3,600	2,870	2,210	-	-	-	-	-	-	-	-	-	76	-	-	
	DUP2-20131113	Duplicate	-	808	-	-	-	7,070	-	-	22.6	< 250	-	459	3,600	2,870	2,130	-	-	-	-	-	-	-	-	-	80	-	-	
QA/QC RPD%			1	-	-	-	0	-	-	*	-	-	0	0	0	4	-	-	-	-	-	-	-	-	-	5	-	-		
GL8-2-20140605	2014 06 05	-	768	-	-	-	6,600	-	-	14	6,340	-	390	3,000	3,000	1,850	-	-	-	-	3.4	-	-	-	-	68	-	-	0.0704	
GL8-2-20141118	2014 11 18	-	626	-	-	-	5,580	-	-	15.8	2,770	-	389	3,700	2,840	2,040	-	-	-	-	2.5	-	-	-	-	78	-	-	0.166	

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Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics													
			pH	Total Hardness	pH (field)	Conductivity	Field Conductivity	Total Dissolved Solids	Dissolved Organic Carbon	Phosphate	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bromide	Hydrogen Sulfide	Sulfide	Chemical Oxygen Demand	Dissolved Phosphate	Ortho-Phosphate		
			mg/L	mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	µg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
GL9-2 (cont'd)	GL9-2-20150610	2015 06 10	8.29	837	-	-	-	6,800	-	-	18.1	15,700	-	390	2,700	3,320	1,630	-	-	-	-	2.6	-	-	-	64	-	0.0773	
	DUP 2-20150610	Duplicate	8.3	833	-	-	-	6,900	-	-	20.5	15,400	-	383	2,700	3,280	1,650	-	-	-	-	2.7	-	-	-	70	-	0.0795	
QA/QC RPD%			0	0	-	-	-	0	-	-	0	0	-	2	0	1	1	-	-	-	-	4	-	-	-	9	-	3	
GL9-1	GL9-2-20151103	2015 11 03	8.03	683	-	-	-	6,730	-	-	12.4	11,200	-	392	3,700	3,290	1,580	-	-	-	-	2.7	-	-	-	59	-	0.141	
	GL 9-1-20091111	2009 11 11	-	510	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	GL9-1-20100810	2010 08 10	-	610	-	-	-	1,470	-	-	230	-	-	126	-	300	923	-	-	-	-	-	-	-	-	< 10	-	0.003	
	GL9-1-20110628	2011 06 28	-	375	-	-	-	1,220	-	-	120	-	-	132	-	270	677	-	-	-	-	-	-	-	-	< 10	-	0.026	
	GL 9-1-20120627	2012 06 27	-	420	-	-	-	1,320	-	-	140	-	-	163	-	263	690	-	-	-	-	-	-	-	-	20	-	< 0.002	
	GL9-1-20121204	2012 12 04	-	392	-	-	-	1,350	-	-	160	< 100	-	162	-	299	684	-	-	-	-	-	-	-	-	18	-	< 0.002	
	GL9-1-20130626	2013 06 26	-	418	-	-	-	1,260	-	-	167	< 100	-	163	770	279	727	-	-	-	-	< 1.0	-	-	-	< 20	-	-	
	GL9-1-20131114	2013 11 14	-	410	-	-	-	1,230	-	-	155	< 100	-	165	580	254	872	-	-	-	-	< 1.0	-	-	-	< 20	-	-	
	GL9-1-20140604	2014 06 04	-	374	-	-	-	1,190	-	-	106	< 100	-	156	820	244	879	-	-	-	-	< 1.0	-	-	-	< 20	-	< 0.0010	
	DUP1-20140604	Duplicate	-	366	-	-	-	1,190	-	-	92.2	< 50	-	153	720	238	849	-	-	-	-	0.63	-	-	-	< 20	-	< 0.0010	
	QA/QC RPD%			2	2	-	-	-	0	-	14	-	-	2	13	2	3	-	-	-	-	-	-	-	-	-	-	-	-
	GL9-1-20141125	2014 11 25	-	404	-	-	-	1,310	-	-	189	< 100	< 10	154	640	250	778	-	-	-	-	< 1.0	-	-	-	-	28	-	< 0.0010
	GL9-1-20150609	2015 06 09	8.9	332	-	-	-	1,140	-	-	76.2	< 25	-	153	590	224	833	-	-	-	-	0.72	-	-	-	< 20	-	< 0.0010	
	GL9-1-20151109	2015 11 09	8.97	326	-	-	-	1,220	-	-	74.2	< 100	< 10	153	600	218	684	-	-	-	-	< 1.0	-	-	-	< 20	-	< 0.0010	
	GL9-1-20170530	2017 05 30	8.9	363	-	-	-	1,150	-	-	314,000	< 50	< 10	159	660	223	693	-	-	-	-	0.71	-	-	-	1,150	-	< 0.0010	
	GL9-1-180604	2018 06 04	8.03	480	7.21	-	2,027	1,390	2.53	< 0.0050	261	< 100	< 10	153	650	314	739	739	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	< 0.0050	-	
	GL9-1-190530	2019 05 30	8.33	407	8.25	-	1,961	1,330	1.44	< 0.0050	280	< 10	< 10	140	720	270	713	701	12.0	< 1.0	6.0	0.39	-	-	-	< 20	< 0.0050	-	
	GL9-1-200611	2020 06 11	7.90	584	7.06	-	2,032	1,470	1.77	-	255	< 100	< 100	109	< 1,000	267	1,060	1,060	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	
	DUPC-200611	Duplicate	7.86	570	-	-	-	1,450	1.26	-	255	< 100	< 100	113	< 1,000	276	1,050	1,050	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	
	QA/QC RPD%			1	2	-	-	-	1	-	0	-	-	4	-	3	1	1	-	-	-	-	-	-	-	-	-	-	-
	GL9-2	GL9-1-210611	2021 06 11	7.75	746	6.79	-	2,568	1,630	0.74	-	239	< 100	< 100	99.0	< 1,000	277	1,220	1,220	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	35	-	< 0.0500
		GL 9-2-20091111	2009 11 11	-	9,280	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
GL9-2-20100810		2010 08 10	-	6,980	-	-	-	40,200	-	-	800	-	-	1,300	-	23,000	720	-	-	-	-	-	-	-	-	100	-	0.011	
GL9-2-20110628		2011 06 28	-	8,320	-	-	-	40,500	-	-	40	-	-	1,150	-	25,300	606	-	-	-	-	-	-	-	-	110	-	0.095	
GL 9-2-20120627		2012 06 27	-	8,200	-	-	-	41,400	-	-	< 10	-	-	1,130	-	26,000	588	-	-	-	-	-	-	-	-	190	-	0.006	
GL9-2-20121204		2012 12 04	-	8,370	-	-	-	39,400	-	-	100	< 1,000	< 100	1,210	-	27,000	564	-	-	-	-	-	-	-	-	101	-	0.009	
DUP-B-20121204		Duplicate	-	7,980	-	-	-	39,800	-	-	< 100	< 1,000	< 100	1,120	-	27,100	564	-	-	-	-	-	-	-	-	89	-	0.006	
QA/QC RPD%			5	5	-	-	-	1	-	-	-	-	8	-	0	0	-	-	-	-	-	-	-	-	13	-	40		
GL9-2-20130626		2013 06 26	-	7,670	-	-	-	40,500	-	-	140	< 500	< 100	1,250	3,040	26,900	898	-	-	-	-	< 5.0	-	-	-	78	-	-	
DUP2-20130626		Duplicate	-	7,870	-	-	-	41,900	-	-	129	< 500	< 100	1,240	3,300	26,800	1,000	-	-	-	-	< 5.0	-	-	-	82	-	-	
QA/QC RPD%			3	3	-	-	-	3	-	8	-	-	1	8	0	11	-	-	-	-	-	-	-	-	5	-	-		
GL9-2-20131113		2013 11 13	-	7,950	-	-	-	40,900	-	-	485	< 500	< 100	1,250	3,100	25,500	950	-	-	-	-	-	-	-	-	64	-	-	
GL9-2-20140605		2014 06 05	-	9,100	-	-	-	39,300	-	-	11.9	730	-	1,230	3,240	26,100	1,030	-	-	-	-	-	-	-	-	7.8	-	0.0054	
GL9-2-20141125		2014 11 25	-	7,700	-	-	-	40,800	-	-	54.3	730	-	1,290	3,780	27,500	502	-	-	-	-	-	-	-	-	5.6	-	0.0054	
GL9-2-20150609	2015 06 09	8.05	7,650	-	-	-	38,700	-	-	92.3	< 600	< 100	1,270	2,400	27,100	1,080	-	-	-	-	-	-	-	-	64	-	0.0052		
GL9-2-20151104	2015 11 04	7.92	7,360	-	-	-	40,400	-	-	50.4	< 500	< 100	1,200	3,300	26,200	547	-	-	-	-	-	-	-	-	53	-	0.0057		

Associated CARO files available upon request.  
 Associated Exova file(s): 712940, 714233, 714243, 756693, 756810, 757047, 811364, 811710, 812030, 812741, 812985, 813438, 846260, 878316, 879073, 909346, 909448, 909654.  
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 \* RPDs are not calculated where one or more concentrations are less than five times RDL.  
 RDL Denotes reported detection limit.





Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics													
			pH	Total Hardness	pH (field)	Conductivity	Field Conductivity	Total Dissolved Solids	Dissolved Organic Carbon	Phosphate	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bromide	Hydrogen Sulfide	Sulfide	Chemical Oxygen Demand	Dissolved Phosphate	Ortho-Phosphate		
			mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	mg/L	µg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
GL12-1	GL12-1-20091112	2009 11 12	-	3,250	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	GL12-1-20100811	2010 08 11	-	3,080	-	-	-	-	7,420	-	-	< 10	-	-	174	-	3,890	558	-	-	-	-	-	-	-	-	50	-	0.004
	GL12-1-20110829	2011 08 29	-	3,310	-	-	-	-	7,330	-	-	20	-	-	151	-	4,240	544	-	-	-	-	-	-	-	30	-	0.095	
	GL30-1-20110629	Duplicate	-	3,400	-	-	-	-	7,270	-	-	30	-	-	151	-	4,190	542	-	-	-	-	-	-	-	20	-	0.052	
	QA/QC RPD%			-	3	-	-	-	1	-	-	*	-	-	0	-	0	-	-	-	-	-	-	-	-	*	-	3	
	GL12-1-20111218	2011 12 18	-	3,160	-	-	-	-	8,050	-	-	< 10	3,660	-	168	-	3,040	571	-	-	-	-	-	-	-	40	-	0.03	
	GL12-1-20120625	2012 06 25	-	3,520	-	-	-	-	7,750	-	-	< 10	-	-	173	-	4,400	589	-	-	-	-	-	-	-	70	-	0.003	
	GL12-1-20121204	2012 12 04	-	3,610	-	-	-	-	7,920	-	-	< 10	5,830	-	182	-	4,770	606	-	-	-	-	-	-	-	72	-	0.007	
	GL12-1-20130626	2013 06 26	-	3,720	-	-	-	-	8,440	-	-	5,4	8,300	-	222	2,200	4,980	767	-	-	-	-	< 2,5	-	-	63	-	-	
	GL12-1-20131113	2013 11 13	-	3,900	-	-	-	-	8,560	-	-	6,7	5,870	-	251	1,800	4,820	860	-	-	-	-	-	-	-	69	-	-	
	GL12-1-20140604	2014 06 04	-	4,090	-	-	-	-	9,790	-	-	69,6	2,640	-	467	2,900	5,550	1,170	-	-	-	-	< 2,5	-	-	258	-	0.357	
	GL12-1-20141118	2014 11 18	-	3,910	-	-	-	-	9,400	-	-	86,6	< 250	-	404	1,800	5,610	1,110	-	-	-	-	< 2,5	-	-	219	-	0.0076	
	GL12-1-20150609	2015 06 09	7,68	3,880	-	-	-	-	7,990	-	-	274	< 100	-	607	1,930	4,580	842	-	-	-	-	< 1,0	-	-	378	-	0.0016	
	DUPS-20150609	Duplicate	7,64	3,900	-	-	-	-	8,000	-	-	279	< 50	-	603	1,850	4,430	855	-	-	-	-	0,63	-	-	372	-	0.0011	
	QA/QC RPD%			-	1	-	-	-	0	-	-	10	-	-	2	-	2	-	-	-	-	-	*	-	-	2	-	-	
	GL12-1-20151104	2015 11 04	7,31	3,480	-	-	-	-	8,290	-	-	252	< 250	-	455	2,000	4,980	744	-	-	-	-	< 2,5	-	-	280	-	< 0.0010	
	GL12-1-20160524	2016 05 24	7,14	3,840	-	-	-	-	8,210	-	-	467	< 250	-	500	2,000	4,600	768	< 1,0	< 1,0	-	-	< 2,5	-	-	393	-	< 0.0010	
	GL12-1-20160921	2016 09 21	7,34	3,590	-	-	-	-	8,290	-	-	648	< 250	-	574	2,000	4,430	824	-	-	-	-	< 2,5	-	-	657	-	0.0062	
	GL12-1-20170529	2017 05 29	7,17	2,610	-	-	-	-	7,280	-	-	2,020	< 250	-	514	1,700	3,850	823	-	-	-	-	< 2,5	-	-	1,070	-	0.372	
	GL12-1-20170926	2017 09 26	7,39	3,240	-	-	-	-	6,500	-	-	1,720	< 100	-	556	1,750	3,540	877	-	-	-	-	< 1,0	-	-	751	-	0.157	
	GL12-1-180604	2018 06 04	7,31	3,390	6,73	-	-	58,741	6,950	382	0,0074	1,430	< 5,000a	< 10	1,050	1,220	9,180	865	865	< 1,0	< 1,0	< 1,0	< 50,0	-	-	542	0,0074	-	
	GL12-1-180919	2018 09 19	7,07	3,890	6,99	-	-	5,880	7,730	190	< 0,0050	1,840	< 100	< 100	495	1,840	3,660	882	882	< 1,0	< 1,0	< 1,0	< 1,00	-	-	513	< 0,0050	-	
	GL12-1-190527	2019 05 27	7,49	3,850	6,75	-	-	8,360	7,860	155	0,0125	1,750	59	24	480	1,560	3,800	907	907	< 1,0	< 1,0	< 1,0	0,33	-	-	485	0,0125	-	
	GL12-1-190919	2019 09 19	7,43	3,830	6,81	-	-	7,380	7,920	175	-	1,270	< 100	< 100	496	1,190	3,620	896	896	< 1,0	< 1,0	< 1,0	< 1,00	-	-	458	-	< 0,0500	
	GL12-1-200610	2020 06 10	7,39	4,490	6,78	-	-	6,947	8,040	203	-	4,260	< 100	< 100	610	1,200	3,890	997	997	< 1,0	< 1,0	< 1,0	< 1,00	-	-	544	-	< 0,0500	
	GL12-1-201102	2020 11 02	7,51	4,720	6,64	-	-	8,081	8,040	179	-	7,300	< 1,000	< 10	603	1,400	3,820	948	948	< 1,0	< 1,0	< 1,0	0,84	-	-	566	-	< 0,0050	
	GL12-1-210525	2021 05 25	7,89	4,090	6,69	-	-	7,982	7,150	156	-	4,360	< 1,000	< 10	568	1,430	3,850	915	915	< 1,0	< 1,0	< 1,0	< 10,0	-	-	563	-	< 0,0050	
	GL12-1-211005	2021 10 05	7,27	4,140	6,67	-	-	7,452	7,940	174	-	4,660	< 100	< 100	579	1,300	4,280	928	928	< 1,0	< 1,0	< 1,0	< 1,00	-	-	536	-	< 0,0500	
	GL13-1	GL13-1-20091117	2009 11 17	-	3,530	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		GL13-1-20100811	2010 08 11	-	3,550	-	-	-	-	11,200	-	-	< 10	-	-	178	-	5,870	640	-	-	-	-	-	-	10	-	0.005	
GL13-1-20110627		2011 06 27	-	3,950	-	-	-	-	10,800	-	-	< 10	-	-	196	-	6,580	666	-	-	-	-	-	-	30	-	0.007		
GL13-1-20111217		2011 12 17	-	3,500	-	-	-	-	10,900	-	-	40	220	-	183	-	5,900	682	-	-	-	-	-	-	30	-	0.03		
DUPC-20111217		Duplicate	-	113	-	-	-	-	1,570	-	-	410	< 50	-	72,6	-	2,3	1,420	-	-	-	-	-	-	< 10	-	0.02		
QA/QC RPD%			-	187	-	-	-	-	150	-	-	*	-	-	86	-	200	70	-	-	-	-	-	-	*	-	40		
GL13-1-20120625	2012 06 25	-	3,580	-	-	-	-	9,930	-	-	< 10	-	-	170	-	5,900	647	-	-	-	-	-	-	-	30	-	0.007		
GL13-1-20121204	2012 12 04	-	3,440	-	-	-	-	9,990	-	-	< 10	< 1,000	-	174	-	5,750	672	-	-	-	-	-	-	-	41	-	0.006		

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Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics													
			pH	Total Hardness	pH (field)	Conductivity	Field Conductivity	Total Dissolved Solids	Dissolved Organic Carbon	Phosphate	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bromide	Hydrogen Sulfide	Sulfide	Chemical Oxygen Demand	Dissolved Phosphate	Ortho-Phosphate		
			mg/L	mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
GL17-1 (cont'd)	GL17-1-190527	2019 05 27	8.11	124	7.56	-	2558	1,490	2.02	< 0.0050	445	< 10	< 10	75.7	1,960	14.4	1,380	1,380	< 1.0	< 1.0	< 1.0	0.18	-	-	-	< 20	< 0.0050	-	
	DUP1-190527	Duplicate	8.13	120	7.56	-	2558	1,470	1.76	< 0.0050	481	< 10	< 10	75.5	1,940	13.8	1,400	1,400	< 1.0	< 1.0	< 1.0	0.20	-	-	-	< 20	< 0.0050	-	
	QA/QC RPD%			0	3	-	-	-	-	-	8	-	-	0	1	4	1	1	-	-	-	-	-	-	-	-	-	-	-
	GL17-1-190923	2019 09 23	8.11	128	7.67	-	2421	1,550	1.92	-	351	< 10	< 10	78.7	1,940	14.3	1,360	1,360	< 1.0	< 1.0	< 1.0	0.42	-	-	-	< 20	-	0.0715	
	GL17-1-200608	2020 06 08	8.20	121	7.35	-	2,138	1,590	2.32	-	349	< 10	< 10	62.6	1,820	3.9	1,400	1,400	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	0.0500	
	GL17-1-201020	2020 10 20	8.01	132	7.43	-	2,457	1,530	2.22	-	402	< 10	< 10	69.6	1,990	4.4	1,300	1,300	< 1.0	< 1.0	< 1.0	0.33	-	-	-	< 20	-	0.0103	
	GL17-1-210604	2021 06 04	8.14	135	-	-	-	1,220	1.36	-	315	< 10	< 10	71.0	2,030	3.9	1,410	1,410	< 1.0	< 1.0	< 1.0	0.34	-	-	-	< 20	-	< 0.0050	
	GL17-1-211006	2021 10 06	7.98	127	7.33	-	2,153	1,660	1.24	-	399	< 10	< 10	64.2	1,970	< 10.0	1,460	1,460	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0050	
	GL17-2-20091112	2009 11 12	-	128	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL30-2-20091112	Duplicate	-	119	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
QA/QC RPD%			-	7	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL17-2	GL17-2-20100811	2010 08 11	-	110	-	-	-	1,630	-	350	-	-	65.2	-	6.2	1,480	-	-	-	-	-	-	-	-	-	10	-	0.058	
	GL17-2-20110628	2011 06 28	-	109	-	-	-	1,510	-	220	-	-	68	-	60	135	-	-	-	-	-	-	-	-	-	10	-	0.109	
	GL17-2-20120625	2012 06 25	-	3,440	-	-	-	9,700	-	190	-	-	204	-	5,740	606	-	-	-	-	-	-	-	-	-	40	-	< 0.002	
	GL17-2-20121204	2012 12 04	-	3,920	-	-	-	10,000	-	110	2,600	-	180	-	6,120	652	-	-	-	-	-	-	-	-	-	33	-	< 0.002	
	GL17-2-20130626	2013 06 26	-	4,000	-	-	-	10,800	-	< 5.0	2,610	-	191	2,300	6,330	780	-	-	-	-	-	< 2.5	-	-	-	33	-	-	
	GL17-2-20131113	2013 11 13	-	4,190	-	-	-	10,800	-	-	1,840	-	22.6	1,700	6,380	864	-	-	-	-	-	-	-	-	-	24	-	-	
	GL17-2-20140605	2014 06 05	-	3,650	-	-	-	10,500	-	32.4	1,490	-	226	1,300	6,290	822	-	-	-	-	-	< 2.5	-	-	-	29	-	0.0025	
	GL17-2-20141118	2014 11 18	-	3,860	-	-	-	11,300	-	47	1,330	-	247	1,400	6,820	966	-	-	-	-	-	< 2.5	-	-	-	40	-	0.0014	
	GL17-2-20150608	2015 06 08	7.5	4,010	-	-	-	10,300	-	33.2	1,680	-	241	1,700	6,660	870	-	-	-	-	-	< 2.5	-	-	-	32	-	0.0025	
	GL17-2-20151104	2015 11 04	7.65	3,760	-	-	-	11,100	-	9.3	1,970	-	257	1,700	7,000	705	-	-	-	-	-	< 2.5	-	-	-	26	-	0.0033	
	GL18-2-20091110	2009 11 10	-	1,060	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL18-2-20100811	2010 08 11	-	1,380	-	-	-	6,930	-	1,400	-	-	568	-	3,800	154	-	-	-	-	-	-	-	-	-	40	-	0.005	
	GL18-2-20110629	2011 06 29	-	1,510	-	-	-	6,440	-	710	-	-	572	-	3,770	260	-	-	-	-	-	-	-	-	-	40	-	0.078	
	GL18-2-20120626	2012 06 26	-	1,480	-	-	-	8,820	-	1,020	-	-	572	-	3,620	156	-	-	-	-	-	-	-	-	-	40	-	0.004	
	DUP-A-20120626	Duplicate	-	1,520	-	-	-	6,670	-	1,280	-	-	585	-	3,670	167	-	-	-	-	-	-	-	-	-	60	-	0.004	
	QA/QC RPD%			-	3	-	-	-	2	-	23	-	-	3	7	2	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL18-2-20121205	2012 12 05	-	1,380	-	-	-	6,600	-	1,450	< 10,000a	-	785	-	8,090	165	-	-	-	-	-	-	-	-	-	22	-	0.005	
	GL18-2-20130627	2013 06 27	-	1,400	-	-	-	6,660	-	1,330	< 250	-	611	< 1,000	3,900	177	-	-	-	-	-	3.7	-	-	-	47	-	-	
	GL18-2-20131114	2013 11 14	-	1,380	-	-	-	6,670	-	1,370	< 250	-	618	< 1,000	3,870	181	-	-	-	-	-	3.7	-	-	-	32	-	-	
GL18-2-20140609	2014 06 09	-	1,380	-	-	-	6,260	-	1,440	< 250	-	608	< 1,000	3,820	180	-	-	-	-	-	3.4	-	-	-	150	-	0.0043		
GL18-2-20141126	2014 11 26	-	1,380	-	-	-	6,330	-	1,370	760	-	613	< 1,000	3,780	680	-	-	-	-	-	3.5	-	-	-	38	-	0.0042		
DUP3-20141126	Duplicate	-	1,390	-	-	-	6,080	-	1,440	420	-	627	< 1,000	3,860	170	-	-	-	-	-	3.8	-	-	-	40	-	0.0033		
QA/QC RPD%			-	1	-	-	4	-	5	58	-	2	*	2	120	-	-	-	-	-	8	-	-	-	*	*	*		
GL18-2-20150615	2015 06 15	7.98	1,340	-	-	-	6,410	-	1,330	< 250	-	608	< 1,000	3,780	170	-	-	-	-	-	3.7	-	-	-	35	-	0.0043		
GL18-2-20170529	2017 05 29	7.95	1,370	-	-	-	6,310	-	1,390	< 250	-	619	< 1,000	3,820	141	-	-	-	-	-	3.2	-	-	-	< 20	-	0.0027		
GL18-2-180604	2018 06 04	7.38	1,410	7,797.8	8,140	7,172	8,140	2,92	0.0231	1,520	< 5,000a	< 10	1,130	230	8,810	138	138	< 1.0	< 1.0	< 1.0	< 50.0	< 0.01a	< 0.020	38	0.0231	-	-		
DUP-180604	Duplicate	7.43	1,430	7.79	-	7,172	6,310	2,91	0.0216	1,530	< 5,000a	< 10	1,130	250	8,740	139	139	< 1.0	< 1.0	< 1.0	< 50.0	< 0.01a	< 0.020	36	0.0216	-	-		
QA/QC RPD%			-	1	-	-	3	0	-	1	-	-	0	*	1	1	1	*	*	*	*	-	-	-	*	*	*	-	

Associated CARO files available upon request.  
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Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics													
			pH	Total Hardness	pH (field)	Conductivity	Field Conductivity	Total Dissolved Solids	Dissolved Organic Carbon	Phosphate	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bromide	Hydrogen Sulfide	Sulfide	Chemical Oxygen Demand	Dissolved Phosphate	Ortho-Phosphate		
			mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
GL23-1 (cont'd)	GL23-1-180529	2018 05 29	7.86	1,260	7.22	-	2,014	1,560	14.3	0.0062	36	< 10	66	34.2	710	341	1,090	1,090	< 1.0	< 1.0	< 1.0	0.27	-	-	-	39	0.0062	-	
	GL23-1-180523	2019 05 23	8.01	1,170	7.7	-	2,332	1,590	14.8	< 0.0050	33	72	< 10	34.0	660	384	1,120	1,120	< 1.0	< 1.0	< 1.0	0.27	-	-	-	30	< 0.0050	-	
	GL23-1-180917	2019 09 17	7.78	1,130	-	-	-	1,610	16.4	-	60	< 10	< 10	35.0	750	394	1,090	1,090	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	-	-	< 0.0050	
	GL23-1-200617	2020 06 17	7.97	1,000	6.95	-	-	2,150	15.30	14.6	-	< 50	134	< 100	32.3	< 1,000	405	964	964	< 1.0	< 1.0	< 1.0	< 1.00	-	-	33	-	< 0.0050	
	GL23-1-200910	2020 09 10	7.98	1,130	-	-	-	1,660	14.8	-	< 50	28	< 10	33.1	780	402	1,110	1,110	< 1.0	< 1.0	< 1.0	0.32	-	-	-	-	-	< 0.0050	
	GL23-1-210513	2021 05 13	7.85	1,080	7.06	-	2,319	1,370	13.9	-	< 50	10	< 10	33.2	760	376	1,180	1,180	< 1.0	< 1.0	< 1.0	0.33	-	-	22	-	< 0.0050		
	DUP 1-210513	Duplicate	7.73	1,090	7.06	-	2,319	1,490	14.7	-	< 50	< 10	< 10	34.4	720	356	1,170	1,170	< 1.0	< 1.0	< 1.0	0.30	-	-	43	-	< 0.0050		
	QA/QC RPD%		2	1	0	-	0	8	6	-	-	-	-	4	5	5	1	1	-	-	-	-	-	-	-	-	-	-	-
GL24-1	GL24-1-20100811	2010 08 11	-	1,200	-	-	-	2,110	-	-	< 10	-	-	91.4	-	762	852	-	-	-	-	-	-	-	-	20	-	0.034	
	GL24-1-20160531	2016 05 31	7.64	-	-	-	-	1,570	-	-	< 20	11,700	-	188	1,270	349	778	-	-	-	-	-	-	-	-	-	-	0.1	
	GL24-1-20180927	2018 09 27	-	1,760	-	-	-	-	-	-	31	61,600	-	99.1	1,140	1,450	-	-	-	-	-	< 0.10	-	-	-	-	-	< 0.0050	
	GL24-1-180612	2018 06 12	7.63	1,300	-	-	-	2,380	-	0.0083	60	13,100	29	216	1,090	742	1,060	1,060	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	0.0083	-		
	GL24-1-180917	2019 09 17	7.92	1,100	-	-	-	1,870	9.09	-	47	6,540	< 100	163	1,200	591	921	921	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	-	-	< 0.0050	
GL25-1	GL25-1-20091117	2009 11 17	-	8.04	-	-	-	1,750	6.56	-	< 50	1,690	< 10	123	1,390	418	930	930	< 1.0	< 1.0	< 1.0	0.30	-	-	-	-	-	< 0.0050	
	GL25-1-20100812	2010 08 12	-	1,540	-	-	-	2,630	-	-	< 10	-	-	67	-	1,350	455	-	-	-	-	-	-	-	-	-	-	0.016	
GL26-1	GL26-1-20091112	2009 11 12	-	654	-	-	-	-	-	-	< 10	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	GL26-1-20100812	2010 08 12	-	527	-	-	-	1,230	-	-	30	-	-	8.9	-	309	706	-	-	-	-	-	-	-	-	10	-	0.005	
	GL30-5-20100812	Duplicate	-	575	-	-	-	1,250	-	-	50	-	-	8.8	-	306	705	-	-	-	-	-	-	-	-	10	-	0.005	
	QA/QC RPD%		-	9	-	-	-	2	-	-	50	-	-	1	-	1	0	-	-	-	-	-	-	-	-	-	-	0	
GL26-2	GL26-2-20091116	2009 11 16	-	629	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	GL26-2-20100812	2010 08 12	-	491	-	-	-	1,210	-	-	< 10	-	-	15.5	-	346	655	-	-	-	-	-	-	-	-	20	-	0.013	
	GL26-2-20110629	2011 06 29	-	634	-	-	-	1,160	-	-	< 10	-	-	14.8	-	357	644	-	-	-	-	-	-	-	< 10	-	-	0.108	
	GL26-2-20120625	2012 06 25	-	670	-	-	-	1,210	-	-	30	-	-	18.3	-	367	644	-	-	-	-	-	-	-	20	-	-	0.006	
	GL26-2-20121204	2012 12 04	-	572	-	-	-	1,200	-	-	100	< 100	-	14.9	-	357	643	-	-	-	-	-	-	-	23	-	-	< 0.002	
	GL26-2-20130626	2013 06 26	-	673	-	-	-	1,170	-	-	62.7	120	-	15	1,380	410	666	-	-	-	-	< 1.0	-	-	< 20	-	-	-	
	GL26-2-20131114	2013 11 14	-	659	-	-	-	1,160	-	-	68.3	< 50	-	19.3	1,320	417	818	-	-	-	-	< 0.50	-	-	< 20	-	-	-	
	GL26-2-20140605	2014 06 05	-	665	-	-	-	1,130	-	-	52	< 50	-	14.3	1,170	400	762	-	-	-	-	< 0.50	-	-	< 20	-	-	0.0021	
	DUP2-20140605	Duplicate	-	668	-	-	-	1,130	-	-	58.7	< 50	-	14.2	1,170	396	816	-	-	-	-	< 0.50	-	-	< 20	-	-	0.0014	
		QA/QC RPD%		-	0	-	-	-	0	-	-	12	-	-	1	0	1	4	-	-	-	-	-	-	-	-	-	-	-
	GL26-2-20141117	2014 11 17	-	638	-	-	-	1,120	-	-	50.8	< 100	-	20	1,160	403	830	-	-	-	-	< 1.0	-	-	< 20	-	-	-	0.0023
	GL26-2-20150608	2015 06 08	7.58	643	-	-	-	1,120	-	-	80.2	99	-	19.1	1,170	406	735	-	-	-	-	< 0.50	-	-	< 20	-	-	-	0.0096
	GL26-2-20151104	2015 11 04	7.73	617	-	-	-	1,170	-	-	62.4	< 50	-	13.6	1,170	388	613	-	-	-	-	< 0.50	-	-	< 20	-	-	-	< 0.0010
GL26-3	GL26-3-20091111	2009 11 11	-	682	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	GL26-3-20100812	2010 08 12	-	538	-	-	-	1,500	-	-	< 10	-	-	62	-	499	604	-	-	-	-	-	-	-	20	-	-	0.03	

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			mg/L	mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	mg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
GL27-1	GL27-1-20091116	2009 11 16	94	-	-	-	-	1,650	-	210	-	68	-	57	1,580	-	-	-	-	-	-	-	-	-	-	-	-	10	0.041
GL27-1	GL27-1-20100812	2010 08 12	67	-	-	-	-	1,600	-	70	-	44	-	70	161	-	-	-	-	-	-	-	-	-	-	-	-	10	0.165
GL27-1	GL27-1-20110629	2011 06 29	88	-	-	-	-	1,600	-	70	-	44	-	70	161	-	-	-	-	-	-	-	-	-	-	-	10	0.165	
GL27-1	GL27-1-20120626	2012 06 26	94	-	-	-	-	1,660	-	70	-	36,5	-	8	1,600	-	-	-	-	-	-	-	-	-	-	-	20	-	
GL27-1	GL27-1-20120704	2012 07 04	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.121	
GL27-1	GL27-1-20121204	2012 12 04	73	-	-	-	-	1,670	-	100	< 100	39,8	-	6,3	1,570	-	-	-	-	-	-	-	-	-	-	18	0.128		
GL27-1	GL27-1-20130626	2013 06 26	88,4	-	-	-	-	1,730	-	126	< 100	37	3,540	< 10	1,550	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	-	
GL27-1	GL27-1-20131113	2013 11 13	93,5	-	-	-	-	1,630	-	107	< 100	41	3,400	< 10	1,500	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	-	
GL27-1	GL27-1-20140605	2014 06 05	94,4	-	-	-	-	1,630	-	126	< 100	38	3,420	< 10	1,560	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.12	
GL27-1	GL27-1-20141118	2014 11 18	86,8	-	-	-	-	1,640	-	171	< 100	39	3,280	< 10	1,640	-	-	-	-	< 1,0	-	-	-	-	-	38	-	0.115	
GL27-1	GL27-1-20150610	2015 06 10	8,41	87,1	-	-	-	1,470	-	122	< 100	38	3,250	< 6,0	1,590	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.102	
GL27-1	GL27-1-20151104	2015 11 04	8,19	86,8	-	-	-	1,610	-	180	< 100	36	3,080	< 6,0	1,500	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.0954	
GL27-1	GL27-1-20160526	2016 05 26	8,27	91,8	-	-	-	1,620	-	116	< 100	38	3,450	< 6,0	1,500	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.0886	
DUP-1	DUP-1-20160526	Duplicate	8,31	85,7	-	-	-	1,690	-	111	< 100	38	3,490	< 6,0	1,480	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.0902	
QA/QC RPD%			0	7	-	-	-	4	-	4	-	0	1	-	1	-	-	-	-	-	-	-	-	-	-	-	-	2	
GL27-1	GL27-1-20160919	2016 09 19	8,34	90,8	-	-	-	1,630	-	152	< 100	36	3,000	< 6,0	1,530	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.112	
GL27-1	GL27-1-20170525	2017 05 25	8,83	95,2	-	-	-	1,640	-	70,1	< 100	38	3,310	6	1,560	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.0674	
GL27-1	GL27-1-20170925	2017 09 25	8,14	92	-	-	-	1,650	-	155	< 100	32	3,260	6,6	1,450	-	-	-	-	< 1,0	-	-	-	-	-	< 20	-	0.0553	
GL27-1	GL27-1-180815	2018 08 15	7,98	89,6	7,63	-	1,870	1,680	2,57	0,0407	276	18	< 10	33,6	3,100	27,5	1,500	1,500	< 1,0	< 1,0	< 1,0	< 0,10	-	-	< 20	0,0407	-	-	
GL27-1	GL27-1-180919	2018 09 19	7,91	99,9	7,62	-	2,388	1,620	3,45	0,0445	220	< 10	< 10	35,1	3,210	19,2	1,450	1,450	< 1,0	< 1,0	< 1,0	< 0,10	-	-	< 20	0,0445	-	-	
GL27-1	GL27-1-190527	2019 05 27	8,20	90,6	7,67	-	2,620	1,430	2,89	0,0794	272	< 10	< 10	36,2	3,020	21,8	1,480	1,480	< 1,0	< 1,0	< 1,0	< 0,10	-	-	< 20	0,0794	-	-	
GL27-1	GL27-1-190919	2019 09 19	8,22	92,8	7,48	-	2,471	1,610	2,84	-	242	< 10	< 10	35,6	3,290	19,9	1,490	1,490	< 1,0	< 1,0	< 1,0	< 0,10	-	-	< 20	-	0,0424	-	
GL27-1	GL27-1-200698	2020 06 08	8,31	93,2	7,5	-	2,216	1,530	2,12	-	230	< 10	< 10	35,5	3,060	17,0	1,500	1,480	22,8	< 1,0	11,3	< 0,10	-	-	< 20	-	< 0,0950	-	
GL27-1	GL27-1-201022	2020 10 22	8,10	85,2	7,63	-	2,525	1,600	2,79	-	243	< 10	< 10	37,7	3,330	7,8	1,420	1,420	< 1,0	< 1,0	< 1,0	< 0,10	-	-	< 20	-	0,0567	-	
GL27-1	GL27-1-210602	2021 06 02	8,16	103	7,47	-	2,633	1,260	2,04	-	186	< 10	< 10	36,8	3,190	11,7	1,510	1,510	< 1,0	< 1,0	< 1,0	0,16	-	-	< 20	-	0,0558	-	
GL27-1	GL27-1-210924	2021 09 24	8,21	107	7,47	-	2,544	1,810	1,06	-	318	< 10	< 10	36,7	3,320	11,8	1,550	1,550	< 1,0	< 1,0	< 1,0	0,12	-	-	< 20	-	0,0391	-	
GL27-2	GL27-2-20111217	2011 12 17	83	-	-	-	-	1,630	-	80	< 50	40,1	-	20,4	1,500	-	-	-	-	-	-	-	-	-	10	-	0,08	-	
GL27-2	GL27-2-20091116	2009 11 16	3,760	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL27-2	GL27-2-20100812	2010 08 12	3,540	-	-	-	-	14,300	-	290	-	740	-	6,590	708	-	-	-	-	-	-	-	-	-	130	-	0,057	-	
GL27-3	GL27-3-20091112	2009 11 12	5,800	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL27-3	GL27-3-20100812	2010 08 12	4,700	-	-	-	-	17,800	-	500	-	800	-	8,490	645	-	-	-	-	-	-	-	-	-	60	-	0,007	-	
GL27-3	GL27-3-20110629	2011 06 29	5,170	-	-	-	-	16,700	-	470	-	610	-	9,700	639	-	-	-	-	-	-	-	-	-	30	-	0,268	-	
GL27-3	GL27-3-20111217	2011 12 17	4,500	-	-	-	-	17,100	-	410	< 200	582	-	10,900	653	-	-	-	-	-	-	-	-	-	40	-	0,04	-	
GL27-3	GL27-3-20120525	2012 06 25	5,050	-	-	-	-	16,400	-	520	-	543	-	9,620	638	-	-	-	-	-	-	-	-	-	70	-	0,003	-	
GL27-3	GL27-3-20121204	2012 12 04	4,480	-	-	-	-	15,900	-	650	< 1,000	502	-	9,230	626	-	-	-	-	-	-	-	-	-	62	-	0,002	-	
GL27-3	GL27-3-20130626	2013 06 26	5,280	-	-	-	-	17,200	-	730	< 600	589	1,300	11,100	864	-	-	-	-	-	-	< 5,0	-	-	63	-	-	-	
GL27-3	GL27-3-20131113	2013 11 13	4,880	-	-	-	-	16,200	-	552	< 500	577	1,390	9,840	876	-	-	-	-	-	-	-	-	-	31	-	-	-	
GL27-3	GL27-3-20140605	2014 06 05	5,120	-	-	-	-	16,300	-	564	< 250	586	< 1,000	10,600	967	-	-	-	-	-	-	4	-	-	47	-	0,0024	-	
GL27-3	GL27-3-20141118	2014 11 18	4,560	-	-	-	-	13,300	-	416	< 600	545	1,200	9,930	947	-	-	-	-	< 5,0	-	-	-	-	38	-	0,0055	-	

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			pH	Total Hardness mg/L	pH (field)	Conductivity µS/cm	Field Conductivity µS/cm	Total Dissolved Solids mg/L	Dissolved Organic Carbon mg/L	Phosphate mg/L	Ammonia, Total (as N) µg/L	Nitrate (as N) µg/L	Nitrite (as N) µg/L	Chloride mg/L	Fluoride µg/L	Sulfate mg/L	Total Alkalinity mg/L	Alkalinity, Bicarbonate (as CaCO3) mg/L	Alkalinity, Carbonate (as CaCO3) mg/L	Alkalinity, Hydroxide (as CaCO3) mg/L	Alkalinity, Phenolphthalein (as CaCO3) mg/L	Bromide mg/L	Hydrogen Sulfide mg/L	Sulfide mg/L	Chemical Oxygen Demand mg/L	Dissolved Phosphate mg/L	Ortho-Phosphate mg/L			
GL28-1 (cont'd)	GL28-1-201104	2020 11 04	7.62	1,850	7.14	-	4,062	3,840	6.24	-	128	< 1,000	< 10	46.9	1,020	2,240	516	516	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	< 20	-	< 0.0050		
	DUP3-201104	Duplicate	7.80	1,850	-	-	-	3,450	6.09	-	127	< 1,000	< 10	46.3	1,000	2,190	515	515	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	< 20	-	< 0.0050		
	QA/QC RPD%			0	0	-	-	-	11	2	-	-	-	-	2	2	0	0	-	-	-	-	-	-	-	-	-	-	-	
	GL28-1-210609	2021 06 09	7.83	1,720	6.99	-	3,969	3,130	7.14	-	82	< 100	< 100	57.4	1,270	1,910	542	542	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	25	-	< 0.0500		
	GL28-1-211007	2021 10 07	7.80	1,860	7.04	-	3,843	3,550	8.00	-	119	< 100	< 100	65.4	< 1,000	1,940	550	550	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	20	-	< 0.0500		
	DUP 3-211007	Duplicate	7.78	1,840	7.04	-	3,843	3,620	8.06	-	124	< 100	< 100	63.3	< 1,000	1,930	549	549	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	26	-	< 0.0500		
QA/QC RPD%			0	1	0	-	0	2	1	-	-	-	-	3	-	1	0	0	-	-	-	-	-	-	-	-	-	-	-	
GL28-2	GL28-2-20091116	2009 11 16	-	1,530	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	GL28-2-20160524	2016 05 24	7.72	1,840	-	-	-	4,530	-	-	-	11,200	-	46	< 1,000	2,870	696	696	< 1.0	< 1.0	-	< 2.5	-	-	-	< 20	-	0.0082	-	
	GL28-2-20160920	2016 09 20	7.5	1,810	-	-	-	4,760	-	-	< 5.0	12,100	-	49	< 1,000	2,760	693	693	< 1.0	< 1.0	-	< 2.5	-	-	-	< 20	-	0.0097	-	
	DUP1-20160920	Duplicate	7.51	3,610	-	-	-	4,750	-	-	< 5.0	12,000	-	48	< 1,000	2,740	693	693	< 1.0	< 1.0	-	< 2.5	-	-	-	< 20	-	0.0089	-	
	QA/QC RPD%			0	66	-	-	-	0	-	-	-	-	2	-	1	0	0	-	-	-	-	-	-	-	-	-	-	-	-
	GL28-2-20170711	2017 07 11	8.03	1,680	-	-	-	4,400	-	-	< 5.0	13,100	-	47	< 400	2,590	671	671	-	-	-	< 1.0	-	-	-	< 20	-	0.0093	-	
	GL28-2-20170926	2017 09 26	7.48	1,920	-	-	-	4,640	-	-	< 5.0	12,100	-	50	< 400	2,840	670	670	-	-	-	< 1.0	-	-	-	< 20	-	0.0095	-	
	GL28-2-180528	2018 05 28	7.42	1,900	6.77	-	4,680	4,730	6.09	< 0.0050	24	8,440	< 10	44.0	110	2,690	686	686	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	< 20	< 0.0050	-	-	
	DUP1-180528	Duplicate	7.51	1,860	6.77	-	4,680	4,960	6.55	< 0.0050	27	8,560	< 1,000	44.5	100	2,690	709	709	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	< 20	< 0.0050	-	-	
	QA/QC RPD%			1	2	-	-	5	7	-	5	1	-	-	1	-	3	3	-	-	-	-	-	-	-	-	-	-	-	-
	GL28-2-180925	2018 09 25	7.60	2,280	6.97	-	5,093	5,370	8.34	< 0.0050	63	9,480	< 10	44.2	140	3,160	700	700	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	24	< 0.0050	-	-	
	GL28-2-190528	2019 05 28	7.70	2,170	6.97	-	5,200	5,280	6.36	< 0.0500	24	11,600	< 100	48.6	< 1,000	2,830	723	723	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	< 0.0500	-	-	
	GL28-2-190919	2019 09 19	7.64	2,030	7.24	-	5,225	5,380	5.96	-	48	10,600	< 100	51.7	< 1,000	2,790	700	700	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	-	
	GL28-2-200610	2020 06 10	7.66	1,730	6.95	-	3,882	4,250	4.99	-	< 5.0	9,190	< 100	32.0	< 1,000	2,490	587	587	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	-	
	GL28-2-201104	2020 11 04	7.70	2,200	6.9	-	5,499	4,790	6.26	-	< 5.0	9,400	< 10	42.9	130	3,020	677	677	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	< 20	-	< 0.0050	-	
GL28-2-210609	2021 06 09	7.76	1,910	6.86	-	6,361	4,610	6.84	-	< 5.0	11,400	< 100	46.3	< 1,000	2,670	675	675	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	39	-	< 0.0500	-		
GL28-2-211007	2021 10 07	7.66	2,460	6.84	-	5,591	5,450	6.29	-	< 5.0	10,000	< 100	53.0	< 1,000	3,050	728	728	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	-		
QA/QC RPD%			-	1,760	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GL28-3	GL28-3-20100812	2010 08 12	-	1,580	-	-	-	4,230	-	-	< 10	-	-	60	-	1,950	702	702	-	-	-	-	-	-	-	-	-	-	0.038	
	GL28-3-20160524	2016 05 24	7.52	2,740	-	-	-	6,310	-	< 5.0	2,380	-	48	< 1,000	4,070	782	782	< 1.0	< 1.0	-	< 2.5	-	-	-	< 20	-	0.018	-		
	GL28-3-20160920	2016 09 20	7.57	1,280	-	-	-	6,550	-	< 5.0	< 250	-	49	< 1,000	4,140	858	858	-	-	-	< 2.5	-	-	-	< 20	-	0.0332	-		
	GL28-3-20170711	2017 07 11	8.13	2,480	-	-	-	6,160	-	< 5.0	690	-	48	< 1,000	4,000	840	840	-	-	-	< 2.5	-	-	-	< 20	-	0.0373	-		
	GL28-3-20170926	2017 09 26	7.6	2,520	-	-	-	6,150	-	< 5.0	1,120	-	49	< 400	4,100	807	807	-	-	-	< 1.0	-	-	-	< 20	-	0.0358	-		
	GL28-3-180528	2018 05 28	7.51	2,770	6.8	-	6,392	7,280	10.3	< 0.0050	29	5,640	< 10	45.9	230	3,780	870	870	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	23	< 0.0050	-		
	GL28-3-180925	2018 09 25	7.60	3,080	7	-	6,777	7,490	12.1	< 0.0050	76	7,780	47	49.6	280	4,350	827	827	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	35	< 0.0050	-		
	GL28-3-190528	2019 05 28	7.78	2,880	7	-	6,743	6,780	8.29	< 0.0500	40	5,880	< 100	49.4	< 1,000	4,040	846	846	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	< 0.0500	-		
	DUP2-190528	Duplicate	7.63	2,830	7	-	6,743	7,120	7.97	< 0.0500	44	6,130	< 100	62.1	< 1,000	4,170	855	855	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	< 0.0500	-		
	QA/QC RPD%			2	2	-	-	5	4	-	10	-	-	-	23	-	3	1	-	-	-	-	-	-	-	-	-	-	-	-
	GL28-3-190919	2019 09 19	7.65	2,790	7.19	-	6,895	7,490	8.62	-	26	4,180	< 100	51.7	< 1,000	4,100	865	865	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	-	
	DUP1-190919	Duplicate	7.78	2,830	7.19	-	6,895	7,330	8.84	-	37	4,000	< 100	48.8	< 1,000	3,900	844	844	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	-	
	QA/QC RPD%			2	1	-	-	2	3	-	35	-	-	6	-	5	2	2	-	-	-	-	-	-	-	-	-	-	-	-
	GL28-3-200610	2020 06 10	7.67	2,890	6.92	-	6,303	7,680	9.25	-	< 5.0	5,160	< 100	56.6	< 1,000	4,550	864	864	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	26	-	< 0.0500	-	
	GL28-3-201105	2020 11 05	7.75	2,870	6.96	-	277.6	7,810	9.33	-	< 5.0	5,150	18	49.4	280	4,500	839	839	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	< 20	-	< 0.0050	-	
GL28-3-210609	2021 06 09	7.80	2,820	7.00	-	7,674	7,260	11.2	-	< 5.0	5,900	< 100	57.1	< 1,000	4,120	872	872	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	< 20	-	< 0.0500	-		
GL28-3-211007	2021 10 07	7.69	3,090	6.87	-	7,571	7,450	8.42	-	< 5.0	4,890	< 100	56.5	< 1,000	4,210	888	888	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	20	-	< 0.0500	-		

Associated CARO files available upon request.  
 Associated Enova file(s): 712940, 714233, 714243, 756693, 756810, 757047, 811364, 811710, 812030, 812741, 812985, 813438, 846260, 878316, 879073, 909346, 909448, 909654.  
 All terms defined within the body of Kelltech's report.  
 < Denotes concentration less than indicated detection limit or RPD less than indicated value.  
 - Denotes analysis not conducted.  
 n/a Denotes no applicable standard/guideline.  
 QA/QC RPD Denotes quality assurance/quality control relative percent difference  
 \* RPDs are not calculated where one or more concentrations are less than five times RDL.  
 RDL Denotes reported detection limit.



Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics													
			pH	Total Hardness	pH (field)	Conductivity	Field Conductivity	Total Dissolved Solids	Dissolved Organic Carbon	Phosphate	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bromide	Hydrogen Sulfide	Sulfide	Chemical Oxygen Demand	Dissolved Phosphate	Ortho-Phosphate		
			mg/L	mg/L	µS/cm	µS/cm	mg/L	mg/L	mg/L	mg/L	µg/L	µg/L	µg/L	µg/L	µg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
GL35-3	BH11-31C-20111217	2011 12 17	1.100	-	-	-	37,000	-	57,300	< 500	-	4,000	-	10,800	17,000	-	-	-	-	-	-	-	-	-	-	-	2,400	0.16	
	DUPB-20111217	Duplicate	1.090	-	-	-	37,900	-	56,800	< 500	-	4,110	-	10,900	15,600	-	-	-	-	-	-	-	-	-	-	-	2,500	0.17	
	QA/QC RPD%			-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	6
	BH11-31C-20120625	2012 06 25	2.740	-	-	-	10,900	-	2,740	-	-	546	-	5,150	2,620	-	-	-	-	-	-	-	-	-	-	-	50	0.008	
	GL35-3-20121205	2012 12 05	2.680	-	-	-	10,900	-	2,590	< 10,000a	-	520	-	5,330	2,290	-	-	-	-	-	-	-	-	-	-	-	48	0.004	
	DUP-C-20121205	Duplicate	2.720	-	-	-	10,800	-	2,720	< 10,000a	-	503	-	5,150	2,300	-	-	-	-	-	-	-	-	-	-	-	41	0.004	
	QA/QC RPD%			-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL35-3-20130627	2013 06 27	2.220	-	-	-	8,910	-	2,330	< 250	-	475	2,200	4,630	2,400	-	-	-	-	-	-	2.6	-	-	-	-	38	-	
	DUP3-20130627	Duplicate	2.240	-	-	-	8,910	-	2,350	270	-	483	2,400	4,650	2,380	-	-	-	-	-	-	2.5	-	-	-	-	36	-	
	QA/QC RPD%			-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	GL35-3-20131113	2013 11 13	2.280	-	-	-	9,430	-	1,310	< 250	-	482	1,400	4,250	2,380	-	-	-	-	-	-	-	-	-	-	-	46	-	
	GL35-3-20140609	2014 06 09	2.220	-	-	-	8,650	-	2,420	< 250	-	460	1,500	4,300	2,270	-	-	-	-	-	-	< 2.5	-	-	-	-	43	< 0.0010	
	GL35-3-20141125	2014 11 25	2.050	-	-	-	8,850	-	3,210	270	-	478	1,600	4,280	2,680	-	-	-	-	-	-	2.9	-	-	-	-	33	0.0078	
	GL35-3-20150811	2015 08 11	7.63	2.170	-	-	8,690	-	2,490	< 250	-	447	1,500	4,170	2,340	-	-	-	-	-	-	< 2.5	-	-	-	-	50	0.0037	
	GL35-3-20151109	2015 11 09	7.67	2.030	-	-	12,000	-	6,870	< 500	-	676	< 2,000a	5,210	3,610	-	-	-	-	-	-	< 5.0	-	-	-	-	198	1.36	
	GL35-3-20160526	2016 05 26	7.59	2.200	-	-	8,300	-	2,590	< 250	-	500	1,900	4,690	2,050	-	-	-	-	-	-	2.6	-	-	-	-	32	0.0291	
	GL35-3-20170926	2017 09 26	7.45	2.010	-	-	7,480	-	1,870	< 250	-	403	1,400	3,750	1,990	-	-	-	-	-	-	2.6	-	-	-	-	21	< 0.0010	
	GL35-3-180815	2018 08 15	7.29	2.070	6.98	-	6,480	8,230	7.93	< 0.0050	1,720	< 10	279	341	1,720	3,320	2,070	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	-	< 20	< 0.0050	-	
	GL35-3-190530	2019 05 30	7.58	2,000	6.85	-	9,132	7,760	4.72	< 0.0500	1,220	< 100	< 100	351	1,730	3,510	2,000	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	-	26	< 0.0500	-	
	GL35-3-200608	2020 06 08	7.73	2,180	6.73	-	7,916	7,520	3.66	-	1,490	< 1,000	< 1,000a	325	1,410	3,410	1,920	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	-	< 20	< 0.500	-	
DUPA-200608	Duplicate	7.73	2,080	6.73	-	7,916	7,520	4.14	-	1,470	< 100	< 100	365	1,130	3,280	1,910	< 1.0	< 1.0	< 1.0	1.78	-	-	-	-	< 20	< 0.0500	-		
QA/QC RPD%			0	5	*	-	*	0	12	-	1	*	*	12	22	4	1	1	*	*	*	*	*	*	*	*	*	*	*
GL35-3-210610	2021 06 10	7.49	1,860	6.67	-	8,182	6,380	3.60	-	1,200	< 100	< 100	343	1,600	3,050	1,810	< 1.0	< 1.0	< 1.0	1.40	-	-	-	-	< 20	< 0.500	-		
DUP3-210610	Duplicate	7.47	1,870	6.67	-	8,182	6,440	3.54	-	1,210	< 100	< 100	337	1,630	3,050	1,790	< 1.0	< 1.0	< 1.0	1.48	-	-	-	-	< 20	< 0.500	-		
QA/QC RPD%			0	1	0	-	0	1	2	-	1	*	2	2	0	1	1	*	*	*	6	-	-	-	-	*	*	*	*
GL37	GL37-20130708	2013 07 08	-	5,860	-	-	35,900	-	1,660	< 500	-	783	410	14,500	1,590	-	-	-	-	-	6	-	-	-	-	109	-		
	GL37-20131114	2013 11 14	-	5,970	-	-	28,600	-	1,370	< 500	-	1,030	343	18,800	1,580	-	-	-	-	-	6.3	-	-	-	-	44	-		
GL39-1	GL39-1-191205	2019 12 05	7.86	1,790	-	-	3,610	8.17	-	116	1,640	25	98.1	1,240	1,910	576	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	-	179	< 0.0050			
	GL39-1-200609	2020 06 09	7.81	2,120	7.02	-	3,724	3,710	6.40	-	56	4,470	< 1,000a	102	< 10,000a	2,110	598	598	< 1.0	< 1.0	< 1.0	< 1.0	-	-	22	< 0.500			
	GL39-1-201019	2020 10 19	7.85	1,970	7.03	-	4,547	4,140	8.10	-	< 50	5,840	< 10	134	1,230	2,120	574	574	< 1.0	< 1.0	< 1.0	< 0.10	-	-	29	< 0.0050			
	GL39-1-210526	2021 05 26	7.71	3,300	6.92	-	5,480	4,660	8.82	-	< 50	6,500	< 10	144	1,140	460	659	659	< 1.0	< 1.0	< 1.0	< 2.50	-	-	< 20	< 0.0050			
	GL39-1-210914	2021 09 14	-	2,630	6.96	-	5,187	5,370	9.04	-	< 50	5,300	< 10	149	1,290	2,790	677	677	< 1.0	< 1.0	< 1.0	< 1.00	-	-	22	< 0.0050			
GL39-2	GL39-2-191205	2019 12 05	7.93	1,940	-	-	5,110	7.99	-	121	1,140	12	176	470	2,790	407	407	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	152	< 0.0050			
	GL39-2-200609	2020 06 09	7.85	1,910	7.29	-	4,140	4,110	6.23	-	< 50	1,820	< 1,000a	174	< 10,000a	2,400	401	401	< 1.0	< 1.0	< 1.0	< 1.00	-	-	26	< 0.500			
	GL39-2-201016	2020 10 16	7.88	1,240	7.35	-	3,324	2,960	6.14	-	< 50	1,400	< 10	180	500	1,540	374	374	< 1.0	< 1.0	< 1.0	< 1.00	-	-	21	< 0.0050			
	DUP1-201016	Duplicate	7.90	1,260	7.69	-	1,562	3,090	5.89	-	< 50	1,440	< 10	181	< 2,500a	1,570	397	397	< 1.0	< 1.0	< 1.0	< 1.00	-	-	23	< 0.0050			
	QA/QC RPD%			0	2	-	-	3	4	-	*	3	*	1	*	2	8	*	*	*	*	*	*	*	*	*	*	*	*
	GL39-2-210526	2021 05 26	7.98	1,090	7.31	-	3,323	2,350	5.28	-	< 50	588	< 10	154	510	1,250	436	436	< 1.0	< 1.0	< 1.0	< 2.50	-	-	< 20	< 0.0050			
	DUP 2-210526	Duplicate	7.98	1,100	7.31	-	3,323	2,090	5.32	-	< 50	700	< 10	159	500	1,240	435	435	< 1.0	< 1.0	< 1.0	< 2.50	-	-	< 20	< 0.0050			
	QA/QC RPD%			0	1	0	-	0	12	1	-	17	*	3	2	1	0	0	*	*	*	*	*	*	*	*	*	*	*
	GL39-2-210914	2021 09 14	-	1,800	7.27	-	4,281	3,820	5.79	-	< 50	1,940	< 10	130	410	2,140	472	472	< 1.0	< 1.0	< 1.0	< 2.50	-	-	30	< 0.0050			
	GL40-3	GL40-3-201117	2021 11 17	8.09	311	7.31	-	4,621	3,000	66.4	-	11,400	< 100	< 100	201	< 1,000	375	2,190	2,190	< 1.0	< 1.0	< 1.0	< 1.00	-	-	2,430	< 0.0500		
GL41-1	GL40-3-210610	2021 06 10	7.95	323	7.31	-	4,453	2,710	3.79	-	5,950	< 100	< 100	162	< 1,000	518	2,040	2,040	< 1.0	< 1.0	< 1.0	< 1.00	-	-	1,050	< 0.0500			
	GL41-1-200616	2020 06 16	8.03	661	7.43	-	2,257	1,400	6.70	-	54	1,060	< 100	399	< 1,000	185	497	497	< 1.0	< 1.0	< 1.0	< 1.00	-	-	28	< 0.0500			
	GL41-1-201102	2020 11 02	8.03	735	7.56	-	248	1,530	5.81	-	< 50	1,570	< 10	371	720	138	592	592	< 1.0	< 1.0	< 1.0	< 1.00	-	-	23	0.0142			
	GL41-1-210525	2021 05 25	8.09	755	7.27	-	2,558	2,000	6.50	-	< 50	1,300	< 10	399	660	163	596	596	< 1.0	< 1.0	< 1.0	< 1							



Table 1: Historical Summary of Analytical Results For Groundwater - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters													Dissolved Inorganics																
			pH	Total Hardness mg/L	pH (field)	Conductivity µS/cm	Field Conductivity µS/cm	Total Dissolved Solids mg/L	Dissolved Organic Carbon mg/L	Phosphate mg/L	Ammonia, Total (as N) µg/L	Nitrate (as N) µg/L	Nitrite (as N) µg/L	Chloride mg/L	Fluoride µg/L	Sulfate mg/L	Total Alkalinity mg/L	Alkalinity, Bicarbonate (as CaCO3) mg/L	Alkalinity, Carbonate (as CaCO3) mg/L	Alkalinity, Hydroxide (as CaCO3) mg/L	Alkalinity, Phenolphthalein (as CaCO3) mg/L	Bromide mg/L	Hydrogen Sulfide mg/L	Sulfide mg/L	Chemical Oxygen Demand mg/L	Dissolved Phosphate mg/L	Ortho-Phosphate mg/L					
GL41-2	GL41-2-191205	2019 12 05	8.05	530	-	-	-	1,230	6.32	-	174	1,550	50	301	700	138	558	558	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	-	-	-	-	-	-	< 0.0050
	GL41-2-200612	2020 06 12	7.44	728	7.24	-	-	2,073	1,390	6.13	-	< 50	1,500	< 100	387	< 1,000	168	563	-	-	-	-	< 1.00	-	-	-	-	-	-	-	< 0.0500	
	DUPD-200612	Duplicate	7.50	743	7.24	-	-	2,073	1,370	6.38	-	< 50	1,450	< 100	404	< 1,000	164	559	-	-	-	-	< 1.00	-	-	-	-	-	-	-	< 0.0500	
	QA/QC RPD%		1	2	*	-	*	1	4	-	*	3	*	4	*	1	1	1	-	-	-	-	*	-	-	-	-	-	-	-	*	-
	GL41-2-201022	2020 10 22	7.83	684	7.31	-	-	2,562	1,410	6.58	-	< 50	1,960	< 10	402	640	175	559	559	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	-	-	-	-	< 0.0050	
GL41-3	GL41-2-210525	2021 05 25	8.05	753	7.17	-	-	2,498	1,400	6.37	-	< 50	1,780	< 10	423	670	151	595	595	< 1.0	< 1.0	< 1.0	< 2.50	-	-	-	-	-	-	-	< 0.0050	
	GL41-2-210907	2021 09 07	7.91	711	7.21	-	-	2,442	1,320	5.28	-	< 50	2,140	< 10	383	580	138	608	608	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	-	-	-	-	< 0.0050	
	GL41-3-200612	2020 06 12	7.40	755	7.26	-	-	2,133	1,580	6.68	-	141	1,180	< 100	423	< 1,000	159	575	-	-	-	-	< 1.00	-	-	-	-	-	-	-	< 0.0500	
	GL41-3-201022	2020 10 22	7.86	696	7.31	-	-	2,621	1,400	6.93	-	< 50	1,380	< 10	423	650	160	570	570	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	-	-	-	-	< 0.0050	
	GL41-3-210525	2021 05 25	8.05	792	7.20	-	-	2,646	1,340	6.71	-	< 50	1,510	< 10	471	660	160	618	618	< 1.0	< 1.0	< 1.0	< 2.50	-	-	-	-	-	-	-	< 0.0050	
GL42-1	GL41-3-210907	2021 09 07	7.87	723	7.22	-	-	2,545	1,400	5.94	-	< 50	1,780	< 10	406	590	143	622	622	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	-	-	-	-	< 0.0050	
	DUP 1-210907	Duplicate	7.88	715	7.22	-	-	2,545	1,390	5.91	-	< 50	1,780	< 10	412	600	145	610	610	< 1.0	< 1.0	< 1.0	< 0.10	-	-	-	-	-	-	-	< 0.0050	
	QA/QC RPD%		0	1	0	-	-	0	1	-	*	0	*	1	2	1	2	2	*	*	*	*	*	-	-	-	-	-	-	-	*	-
GL42-2	GL42-1-200612	2020 06 12	7.12	184	7.28	-	-	2,332	2,360	2.39	-	703	< 100	< 100	36.7	< 1,000	20.8	2,050	-	-	-	-	< 1.00	-	-	-	-	-	-	-	0.0580	
	GL42-1-201106	2020 11 06	7.80	171	7.27	-	-	5,266	3,620	2.95	-	743	< 10	< 10	47.6	560	1.3	3,030	3,030	< 1.0	< 1.0	< 1.0	0.34	-	-	-	-	-	-	-	< 0.0050	
	GL42-1-210603	2021 06 03	8.05	187	7.35	-	-	5,277	3,170	2.14	-	698	< 10	< 10	49.7	650	< 10.0	3,560	3,560	< 1.0	< 1.0	< 1.0	0.28	-	-	-	-	-	-	-	< 0.0050	
	GL42-2-200616	2020 06 16	8.08	855	7.45	-	-	4,649	3,910	6.51	-	461	1,760	232	64.3	< 1,000	2,050	928	928	< 1.0	< 1.0	< 1.0	< 1.00	-	-	-	-	-	-	-	< 0.0050	
GL42-2	GL42-2-201109	2020 11 09	7.76	1,270	7.34	-	-	5,360	4,220	7.70	-	83	883	153	63.6	590	2,250	918	918	< 1.0	< 1.0	< 1.0	< 10.0	-	-	-	-	-	-	-	89	< 0.0050
	GL42-2-210607	2021 06 07	8.02	1,230	7.34	-	-	5,808	4,340	7.36	-	80	8,820	< 250	70.9	< 2,500a	2,220	1,020	1,020	< 1.0	< 1.0	< 1.0	< 2.50	-	-	-	-	-	-	-	< 0.125	

Associated CARO files available upon request.  
 Associated Exova file(s): 712940, 714233, 756663, 756810, 757047, 811364, 811710, 812030, 812741, 812985, 813438, 846260, 878316, 879073, 909346, 909448, 909654.  
 All terms defined within the body of KelTech's report.  
 < Denotes concentration less than indicated detection limit or RPD less than indicated value.  
 - Denotes analysis not conducted.  
 n/a Denotes no applicable standard/guideline.  
 QA/QC RPD Denotes quality assurance/quality control relative percent difference  
 \* RPDs are not calculated where one or more concentrations are less than five times RDL.  
 RDL Denotes reported detection limit.









Table 2: Historical Summary of Analytical Results For Groundwater - Metals

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters										Dissolved Metals																																		
			pH	Total Hardness mg/L	pH (field)	Conductivity µS/cm	Field Conductivity µS/cm	Total Dissolved Solids mg/L	Dissolved Organic Carbon mg/L	Phosphate mg/L	Dissolved Aluminum mg/L	Dissolved Calcium mg/L	Dissolved Iron mg/L	Dissolved Magnesium mg/L	Dissolved Manganese mg/L	Dissolved Potassium mg/L	Dissolved Sodium mg/L	Antimony µg/L	Arsenic µg/L	Barium µg/L	Beryllium µg/L	Boron µg/L	Cadmium µg/L	Chromium µg/L	Cobalt µg/L	Copper µg/L	Lead µg/L	Lithium µg/L	Mercury µg/L	Molybdenum µg/L	Nickel µg/L	Selenium µg/L	Silver µg/L	Strontium µg/L	Thallium µg/L	Tin µg/L	Titanium µg/L	Tungsten µg/L	Uranium µg/L	Vanadium µg/L	Zinc µg/L						
GL&1 (2011)	GL&1 (2011)-190603	2019 08 03	7.80	1,270	7.42	11,200	11903	6,100	175	1.15	86.19	507	192	412	421	1,490	1.10	5.96	321	<0.10	2,860	<0.010	16.7	21.7	11.8	<0.20	41.5	<0.010	1.44	15.3	0.50	<0.050	3.160	<0.020	4.82	11.2	1.8	18.2	3.1	<4.0							
	DUP3-190603	Duplicate	7.72	1,240	7.42	-	11903	6,100	180	0.560	87.1	191	467	185	402	1,420	1.09	5.93	320	<0.10	2,710	<0.010	16.8	21.6	<0.40	<0.20	39.3	<0.010	1.27	15.1	0.60	<0.050	3.140	<0.020	4.80	11.3	1.9	18.6	3.1	<4.0							
GL7-1	GL&1-200611	2020 08 11	7.82	962	7.1	6,440	6,871	28	3	69	0	4	2	5	1	0	73.8	151	181	142	285	382	1,200	1.70	6.48	367	0.025	2,180	0.0081	18.1	23.2	0.88	0.151	28.1	<0.010	1.31	23.7	0.86	<0.010	2,850	<0.004	4.82	15.2	2.04	1.95	3.81	1.8
	GL&1-210610	2021 08 10	7.07,72	1,230	6.99	-	-	-	-	-	79.0	229	1,180	160	439	356	988	0.810	4.88	398	0.029	3,510	0.0069	14.2	20.3	0.50	0.237	41.4	<0.010	1.02	17.0	1.22	<0.010	2,850	<0.004	3.19	11.2	1.67	0.228	2.89	2.3						
	GL7-1-20110704	2011 07 04	-	1,190	-	-	2,560	-	-	-	<5	176	5,590	182	1,060	21.4	492	<0.2	36.4	15	2.2	148	0.02	62.9	1.75	1	0.4	266	-	56.3	9	19.8	<0.01	4,680	<0.01	<0.1	<10	-	80.8	17.8	11						
	GL7-1-20120625	2012 06 25	-	1,150	-	-	2,590	-	-	-	<50a	164	12,800	180	1,260	20	509	<2	13	10	1.8	180	<0.1	7	1.9	<10a	<1	280	-	42	<10	<6	<0.10	4,580	<0.1	<1	<100	-	74	2	20						
	GL7-1-20121205	2012 12 05	-	1,120	-	-	2,500	-	-	-	54	159	5,360	176	871	18.7	496	<2.0	22.5	20	2.84	160	<0.10	12.2	4.91	<10a	<1.0	300	-	60.2	<10	<6.0	<0.10	4,440	<0.10	<1	<100	-	85.6	3.27	10						
	GL7-1-20130626	2013 06 26	-	1,110	-	-	2,500	-	-	-	<10a	162	4,850	172	1,350	21	526	<0.50	19.8	<20	<5.0a	120	<0.10	<1.0	1.88	<1.0a	3.5	292	<0.20	56.7	7.5	<2.0	<0.050	3,860	<0.20	<30	<50	-	79.4	<30	33.3						
	GL7-1-20131114	2013 11 14	-	1,140	-	-	2,530	-	-	-	<10a	160	5,290	179	922	20	509	<0.50	22.3	<20	<5.0a	110	<0.10	<1.0	1.38	<1.0a	<1.0	263	<0.20	60.6	7	<2.0	<0.050	4,150	<0.20	<30	<50	-	79.5	<30	88.8						
	DUP1-20131114	Duplicate	-	1,130	-	-	2,500	-	-	-	<10a	159	5,200	179	918	19.8	503	<0.50	22.6	<20	<5.0a	120	<0.10	<1.0	1.4	<1.0a	<1.0	260	<0.20	61.3	6.9	<2.0	<0.050	4,080	<0.20	<30	<50	-	78.1	<30	86.7						
	QA/QC RPD:																																														
	GL7-1-20140604	2014 06 04	-	1,190	-	-	2,560	-	-	-	<10a	164	7,030	190	1,130	20.6	502	<0.50	21.7	<20	<5.0a	120	<0.10	<1.0	1.83	<1.0a	<1.0	342	<0.20	38.6	7.8	<2.0	<0.050	4,190	<0.20	<30	<50	-	62.4	<30	55.8						
GL7-1-20141125	2014 11 25	-	1,110	-	-	2,480	-	-	-	<10a	144	5,600	183	861	18.8	471	<0.50	22.8	<20	<5.0a	110	<0.10	<1.0	1.44	<1.0a	<1.0	273	<0.20	50.4	6.6	<2.0	<0.050	4,030	<0.20	<30	<50	-	68.8	<30	36.1							
GL7-1-20150609	2015 06 09	7.32	1,090	-	-	2,430	-	-	-	<10	151	7,710	173	963	19.5	478	<0.50	26.7	<20	<5.0a	110	<0.050	<0.50	1.72	<1.0a	1	284	<0.20	40.7	7.3	<1.0	<0.050	4,050	<0.020	<30	<50	-	65.4	<30	61.6							
GL7-1-20151109	2015 11 09	6.61	1,090	-	-	2,470	-	-	-	<10	155	3,030	169	904	18.7	464	<0.50	13	<20	<5.0a	<100	<0.050	<0.50	1.33	<1.0a	<1.0	291	<0.20	44.8	7.3	<1.0	<0.050	3,540	<0.020	<30	<50	-	65.1	<30	45.4							
GL&1-20080529	2008 05 29	-	-	-	-	-	-	-	-	70	93	200	144	625	15.2	832	<2	6	10	<1	40	0.7	<5	<1	<10a	2	150	-	40	<5	<2	<0.1	12,300	<0.5	<10	52	-	12	3	10							
GL&1-20081104	2008 11 04	-	-	-	-	-	-	-	-	210	86.9	180	139	494	14.9	746	<2	5	20	<1	70	0.1	<5	<1	<10a	<1	160	-	40	6	<2	<0.1	11,900	<0.5	<10	43	-	10	2	10							
GL&1-20091110	2009 11 10	-	80	-	-	-	-	-	-	86	20.4	<100	2.2	421	2.4	19.6	<2	8	10	<0.4	40	0.32	4.4	0.8	<10a	<1	140	-	40	<10	<6	<0.10	10,900	<0.1	<1	92	-	7	<1	10							
GL&1-20100810	2010 08 10	-	630	-	-	2,710	-	-	-	158	74	120	109	536	14	822	<2	3	10	<0.4	40	<0.1	4.4	0.4	<10a	<1	140	-	44	<10	<6	<0.1	11,200	<0.1	<1	<100	-	11	<1	<10							
GL&2-20080529	2008 05 29	-	-	-	-	-	-	-	-	<50a	63.5	660	316	525	32.2	3,100	<2	23	20	<1	130	0.4	9	3	10	2	180	-	160	27	14	<0.1	7,890	<0.5	<10	127	-	172	25	10							
GL30-1-20080529	Duplicate	-	-	-	-	-	-	-	-	<50a	63.4	620	316	518	32.1	3,120	<2	23	20	<1	130	0.4	10	2	10	2	180	-	160	27	15	<0.1	7,680	<0.5	<10	122	-	166	22	<10							
QA/QC RPD:																																															
GL&2-20081104	2008 11 04	-	-	-	-	-	-	-	-	<50a	40.6	160	309	291	34.6	3,410	<2	23	30	<1	200	<0.10a	63	14	10	<1	180	-	280	34	9	0.19	7,210	<0.5	<10	98	-	152	152	<10							
GL&2-20091110	2009 11 10	-	1,190	-	-	-	-	-	-	<50a	32.5	190	270	280	34	150	<2	16	20	<0.4	170	0.39	26	1.2	<10a	<1	140	-	284	30	<6	<0.10	5,390	<0.1	<1	<10	-	119	26	110							
GL&2-20100810	2010 08 10	-	828	-	-	8,530	-	-	-	<50a	33	340	205	86	30	2,340	<2	13	20	<0.4	160	<0.1	5	0.8	20	<1	120	-	227	20	10	<0.1	5,360	<0.1	<1	<100	-	131	28	<10							
GL&2-20110627	2011 06 27	-	1,040	-	-	7,520	-	-	-	<50a	40.9	322	228	406	23	2,330	<2	7	20	<0.4	140	0.51	6	2	<10a	<1	140	-	191	20	<6	<0.1	5,310	<0.1	<1	<10	-	111	10	<10							
GL&2-20111217	2011 12 17	-	652	-	-	7,360	-	-	-	<50a	26.4	74	142	110	19.8	2,120	<2	13	20	<0.4	150	0.58	18	0.4	20	<1	130	-	300	20	<6	<0.10	4,460	0.43	<1	<10	-	134	20	<10							
GL&2-20120626	2012 06 26	-	800	-	-	5,610	-	-	-	<50a	42.2	2,420	169	400	38	1,330	<2	6	30	<0.4	200	0.27	10	1	10	<1	70	-	104	20	7	0.71	3,930	<0.1	<1	<100	-	74	16	<10							
DUP B-20120626	Duplicate	-	800	-	-	7,250	-	-	-	<50a	41	2,540	169	390	38	1,340	<2	5	30	<0.4	180	0.23	10	0.9	<10a	<1	70	-	94	20	<6	<0.1	3,900	<0.1	<1	<100	-	73	16	<10							
QA/QC RPD:																																															
GL&2-20121204	2012 12 04	-	561	-	-	7,350	-	-	-	<50a	22.4	86	128	95	19.6	2,170	<2.0	6.3	30	<0.40	150	0.18	22.5	2.37	<10a	<1.0	100	-	228	20	8.2	<0.10	4,670	<0.10	<10	19	-	126									





















Table 2: Historical Summary of Analytical Results For Groundwater - Metals

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters										Dissolved Metals																												
			pH	Total Hardness	Conductivity	Field Conductivity	Total Dissolved Solids	Total Organic Carbon	Phosphate	Dissolved Aluminum	Dissolved Calcium	Dissolved Iron	Dissolved Magnesium	Dissolved Manganese	Dissolved Potassium	Dissolved Sodium	Ammonia	Antimony	Arsenic	Beryllium	Boron	Cadmium	Chromium	Cobalt	Copper	Lead	Lithium	Mercury	Molybdenum	Nickel	Selenium	Silver	Strontium	Tellurium	Tin	Titanium	Tungsten	Uranium	Zinc		
GL28-3	GL28-3-200610	2020 10 10	7.67	2,890	6.92	-	630.3	7,680	9.25	-	< 1.0	395	< 2.0	462	130	12.7	1,190	0.110	0.893	19.9	0.012	6.0	0.180	0.35	0.356	1.45	< 0.050	40.5	< 0.010	13.1	8.14	0.23	< 0.010	9,460	0.0300	< 0.050	0.22	< 0.20	273	1.68	1.8
	GL28-3-201105	2020 11 05	7.75	2,870	6.96	-	277.6	7,810	8.33	-	< 1.0	408	4.2	448	281	12.3	1,170	0.142	0.815	19.2	0.010	5.0	0.227	0.28	0.484	1.69	< 0.050	46.5	< 0.010	16.5	11.6	0.17	< 0.010	8,710	0.0416	0.087	0.34	< 0.20	289	2.02	3.0
	GL28-3-201009	2020 09 09	7.80	2,820	7.00	-	-	-	-	-	1.7	339	< 2.0	479	270	12.6	1,170	0.157	0.684	18.5	0.010	6.6	0.0836	0.34	0.118	1.82	< 0.050	51.5	< 0.010	12.9	4.96	0.13	< 0.010	8,070	0.0194	< 0.050	0.20	< 0.20	295	1.22	4.3
GL28-1	GL28-1-201007	2021 10 07	7.69	3,090	6.87	-	-	-	-	1.2	351	2.2	537	186	15.2	1,230	0.139	0.260	21.5	< 0.010	4.5	0.208	0.34	0.191	1.42	< 0.050	32.7	< 0.010	17.3	3.09	0.29	< 0.010	8,300	0.0409	< 0.050	0.20	< 0.20	306	1.46	2.0	
	GL28-1-20130708	2013 07 08	-	-	-	-	-	-	-	< 1.0	625	217	57.8	658	10.5	272	< 0.50	3	60	< 5.0	< 100	< 0.050	< 0.50	1.25	< 1.0	< 1.0	114	< 0.20	8.8	< 5.0	< 1.0	< 0.050	2,530	< 0.20	< 30	< 50	< 1.0	< 3.0	< 30	< 5.0	
	GL28-1-20131113	2013 11 13	-	493	-	-	1,280	-	-	< 1.0	83.7	597	69	1,130	9.8	315	< 0.50	5.1	98	< 5.0	< 100	< 0.050	< 0.50	2.91	< 1.0	< 1.0	82	< 0.20	15.8	8.3	< 1.0	< 0.050	2,580	< 0.20	< 30	< 50	< 1.0	< 2.7	< 30	< 5.0	
GL28-1-20140903	DUP3-20131113	Duplicate	-	495	-	-	1,240	-	-	< 1.0	84	593	69.3	1,130	9.7	311	< 0.50	5.1	96	< 5.0	< 100	< 0.10	< 1.0	2.97	< 1.0	< 1.0	79	< 0.20	15.8	8.5	< 2.0	< 0.050	2,570	< 0.20	< 30	< 50	< 1.0	< 23.7	< 30	< 5.0	
	QA/QC RPD%		0	0	-	-	3	-	-	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
	GL28-1-20140603	2014 06 03	-	516	-	-	1,430	-	-	< 1.0	84.6	438	73.9	946	8.6	320	< 0.50	3.8	108	< 5.0	< 100	< 0.050	< 0.50	7.65	< 1.0	< 1.0	63	< 0.20	16.5	8.2	< 1.0	< 0.050	2,520	< 0.20	< 30	< 50	< 1.0	< 27.9	< 30	< 5.0	
GL28-1-20141118	GL28-1-20141118	2014 11 18	-	899	-	-	1,950	-	-	< 1.0	106	1,980	105	1,530	9.8	411	< 0.50	6.5	194	< 5.0	< 100	< 0.10	< 1.0	14.4	< 1.0	< 1.0	61	< 0.20	21	8.8	< 2.0	< 0.050	3,480	< 0.20	< 30	< 50	< 1.0	< 30.4	< 30	< 5.0	
	GL28-1-20150609	2015 06 09	8.12	629	-	-	1,900	-	-	< 1.0	99.5	823	92.4	1,250	9.3	391	< 0.50	4.5	111	< 5.0	< 100	< 0.050	< 0.50	8.07	< 1.0	< 1.0	51	< 0.20	20.2	8.8	< 1.0	< 0.050	3,370	< 0.020	< 30	< 50	< 1.0	< 31.6	< 30	< 5.0	
	GL28-1-20151105	2015 11 05	7.85	671	-	-	1,780	-	-	< 1.0	116	176	82.5	1,070	9.6	347	< 0.50	1.9	93	< 5.0	< 100	0.057	< 0.50	12.6	5.3	< 1.0	< 50	< 0.20	23.3	18.7	< 1.0	< 0.050	3,100	< 0.020	< 30	< 50	< 1.0	< 36	< 30	< 5.0	
GL28-1-20160524	GL28-1-20160524	2016 05 24	7.84	682	-	-	1,650	-	-	< 1.0	128	94	87.9	861	10.2	306	< 0.50	2.4	83	< 5.0	< 100	0.097	5.68	5.88	13.5	< 1.0	< 50	< 0.20	29.9	30.1	< 1.0	< 0.050	2,880	< 0.020	< 30	< 50	< 1.0	< 46.9	< 30	< 5.0	
	GL28-1-20160921	2016 09 21	8.08	639	-	-	1,590	-	-	< 1.0	118	47	83.6	885	9.7	312	0.5	2.3	86	< 5.0	< 100	0.2	< 0.50	14.5	13.5	< 1.0	< 50	< 0.20	29.9	30.1	< 1.0	< 0.050	3,050	< 0.020	< 30	< 50	< 1.0	< 46.9	< 30	< 5.0	
	GL28-1-20170529	2017 05 29	8.1	696	-	-	1,300	-	-	< 1.0	115	< 30	72.8	< 10	10.2	272	0.54	2.1	69	< 5.0	< 100	0.07	< 0.50	1.64	1.34	< 1.0	51	< 0.20	23.8	19.0	< 1.0	< 0.050	2,770	< 0.010	< 30	< 50	< 1.0	< 41.1	< 30	< 5.0	
GL28-1-20170926	GL28-1-20170926	2017 09 26	7.88	542	-	-	1,290	-	-	< 1.0	101	< 30	70.2	312	9.8	262	0.52	2.1	69	< 5.0	< 100	0.297	< 0.50	12.6	8.8	< 1.0	52	< 0.20	21.4	21.2	< 1.0	< 0.050	2,730	< 0.010	< 30	< 50	< 1.0	< 38.2	< 30	< 5.0	
	DUP1-20170926	Duplicate	7.88	539	-	-	1,330	-	-	< 1.0	99.6	< 30	70.8	307	9.8	258	0.53	2.2	68	< 5.0	< 100	0.305	< 0.50	13	9.1	< 1.0	53	< 0.20	21.6	22.3	< 1.0	< 0.050	2,690	< 0.010	< 30	< 50	< 1.0	< 38.6	< 30	< 5.0	
	QA/QC RPD%		0	1	-	-	3	-	-	1	1	2	0	2	2	5	1	2	0	3	3	3	3	3	2	2	1	5	1	5	1	1	1	1	1	1	1	1	1		
GL28-2	GL28-2-180904	2018 09 04	7.71	699	7.24	-	1,240	1,220	118	0.0343	6.1	191	73	437	39.8	160	70.9	1.30	3.64	51.9	< 0.10	512	2.67	2.08	2.15	84.0	< 0.20	16.4	< 0.010	40.1	30.8	0.69	< 0.050	1,570	0.039	< 0.20	< 5.0	1.7	21.5	5.5	6.1
	GL28-2-180919	2018 09 19	7.70	693	7.38	-	1,389	1,190	83.7	< 0.0058	< 5.0	193	49.2	437	15.8	83.2	1.70	3.88	83.4	< 0.10	518	0.371	1.97	53.0	84.5	< 0.20	16.6	< 0.010	45.0	36.2	0.79	< 0.050	1,720	0.054	< 0.20	< 5.0	5.1	27.3	5.2	7.7	
	GL28-2-190803	2019 08 03	7.76	467	7.06	-	1,715	1,160	12.8	< 0.0050	38.8	67.4	65	60.3	55.7	11.1	284	0.80	1.67	52.4	0.20	92.0	0.053	< 0.50	20.1	1.92	< 0.20	118	< 0.010	9.71	6.47	0.60	< 0.050	3,190	< 0.020	< 0.20	< 5.0	1.0	19.0	< 1.0	< 4.0
GL28-1-20190924	GL28-1-20190924	2019 09 24	7.89	448	7	-	1,731	1,160	11.1	-	8.3	79.6	584	60.8	70.4	9.74	267	0.33	2.08	68.5	< 0.10	75.2	< 0.010	0.71	3.33	< 0.10	< 0.20	89.8	< 0.010	1.67	2.82	0.68	< 0.050	2,880	< 0.020	< 0.20	< 5.0	5.2	31.4	1.2	< 4.0
	GL28-1-2020012	2020 01 12	7.04	421	7.01	-	1,380	1,110	6.25	-	1.9	74.4	1,030	57	67.4	93.2	263	0.478	4.78	68.4	0.089	59.8	0.0043	0.19	33.0	< 0.10	< 0.050	99.1	< 0.010	8.96	2.52	0.11	< 0.010	2,880	< 0.004	0.051	0.29	4.51	25.2	0.30	< 1.0
	GL28-1-2020120	2020 12 20	7.84	442	7.07	-	1,723	1,050	3.16	-	1.1	84.5	898	56.1	532	10.3	276	< 0.058	3.89	56.0	0.122	43.4	< 0.0020	0.15	47.8	< 0.10	< 0.050	95.0	< 0.010	8.94	1.39	< 0.10	< 0.004	0.050	< 0.20	3.08	2.11	< 0.20	< 1.0		
GL28-1-20210811	GL28-1-20210811	2021 08 11	7.90	460	7.00	-	-	-	-	2.6	84.1	1,170	60.7	717	11.9	285	< 0.050	4.80	64.2	0.124	48.4	< 0.0020	0.16	124	< 0.10	< 0.050	101	< 0.010	8.20	1.84	< 0.10	< 0.010	2,640	< 0.004	< 0.050	< 0.20	6.33	16.3	< 0.20	< 1.0	
	GL28-1-20210006	2021 10 06	7.89	436	7.37	-	-	-	-	2.9	75.9	1,740	59.9	875	9.71	259	0.074	4.36	78.3	0.068	63.8	< 0.0020	0.31	73.1	< 0.10	< 0.050	72.2	< 0.010	8.47	1.30	0.15	< 0.010	2,760	< 0.004	< 0.050	0.31	7.38	26.5	0.20	< 1.0	
	GL28-2-20130627	2013 06 27	-	2,830	-	-	7,910	-	-	< 1.5	333	276	486	3,310	20.2	1,230	< 0.50	4.1	55	< 1.0	< 200	< 0.25	< 2.5	17.7	< 2.5	< 1.0	53	< 0.20	46.3	60.5	< 5.0	< 0.050	7,280	< 0.20	< 30	< 50	< 1.0	< 106	< 60	< 10	
GL28-2-20131113	GL28-2-20131113	2013 11 13	-	2,910	-	-	7,890	-	-	< 3.0	346	1,080	496	3,410	20.4	1,260	< 1.0	4.5																							





Table 3: Historical Summary of Analytical Results For Surface Water - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters														Dissolved Inorganics																				
			pH	pH	Hardness	pH (field)	C Temperature	Conductivity	Field Conductivity	Total Dissolved Solids	Total Suspended Solids	Dissolved Organic Carbon	Total Nitrogen-N	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Nitrate+Nitrite Nitrogen	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bicarbonate	Kjeldahl Nitrogen-N	Bromide	Chemical Oxygen Demand	Phosphate	Ortho-Phosphate	Total Organic Carbon	Total Phosphorus as P				
NORTHEAST POND (Cont'd)	NE Pond-20150311	2015 03 11	-	8.10	-	2,240	-	2,240	-	1,510	8.8	-	180	< 100	-	143	1,390	413	791	660	131	< 1.0	-	1.59	< 1.0	44	-	0.199	12.8	-	-	-	-	-	-		
	NE Pond-20150816	2015 06 16	-	8.70	-	2,240	-	1,670	3.4	-	15.1	< 100	-	155	1,540	496	888	727	161	< 1.0	-	1.28	< 1.0	49	-	0.307	14.1	-	-	-	-	-	-				
	NE Pond-20151029	2015 10 29	9.08	941	-	2,780	-	2,060	3.6	-	50.3	< 100	-	183	1,540	551	949	690	258	< 1.0	-	1.58	< 1.0	55	-	0.146	16.9	-	-	-	-	-	-	-			
	NE POND-20160914	2016 09 14	-	1.060	-	3,160	-	2,310	14.1	-	26.4	< 100	-	212	1,820	744	1,090	871	217	< 1.0	-	2.71	< 1.0	74	-	0.125	20.6	-	-	-	-	-	-	-			
	NE POND-20161116	2016 11 16	8.47	1,010	-	2,960	-	2,130	4.5	-	2,090	< 100	-	185	1,560	644	992	939	53	< 1.0	-	3.17	< 1.0	52	-	0.357	15.9	-	-	-	-	-	-	-			
	NE POND-20170418	2017 04 18	8.62	944	-	2,460	-	1,630	3.6	-	73.4	< 100	-	146	1,320	539	862	766	85.4	< 1.0	-	1.11	< 1.0	33	-	0.085	13	-	-	-	-	-	-	-	-		
	NE POND-20170607	2017 06 07	8.56	967	-	2,500	-	1,730	6.9	-	11.2	< 100	-	155	1,560	586	876	719	157	< 1.0	-	1.05	< 1.0	35	-	0.3	16	-	-	-	-	-	-	-	-		
	NE POND-20170907	2017 09 07	8.31	1,050	-	2,790	-	2,070	4.2	-	71.8	< 100	-	192	1,570	685	933	530	403	< 1.0	-	2.13	< 1.0	57	-	0.15	20.7	-	-	-	-	-	-	-	-		
	NE POND-20171101	2017 11 01	8.11	1,060	-	2,740	-	1,980	3.6	-	122	< 100	-	207	1,790	676	945	651	294	< 1.0	-	1.32	< 1.0	53	-	0.226	15.6	-	-	-	-	-	-	-	-		
	NE SAMPLE-20160518	2016 05 18	-	913	-	2,760	-	1,950	< 3.0	-	21.9	< 100	-	167	1,440	598	943	747	196	< 1.0	-	1.29	< 1.0	47	-	0.172	17.2	-	-	-	-	-	-	-	-		
	NORTHEAST POND-180404	2018 04 04	8.81	961	8.95	8.8	2,400	1,965	1,670	6.4	0.955	40	17	< 10	16.8	13.2	1,210	483	757	568	189	< 1.0	94.3	-	0.938	0.48	59	0.133	-	-	-	-	-	-	-	-	
	NORTHEAST POND-180523	2018 05 23	8.80	937	8.72	24.1	2,440	2,436	1,740	< 2.5	0.968	67	< 10	< 10	< 10.0	133	920	431	717	542	175	< 1.0	87.6	-	0.988	< 0.10	< 20	0.0154	-	-	-	-	-	-	-	-	
	NORTHEAST POND-180906	2018 09 06	8.52	1,180	8.84	17.91	3,100	385	2,210	106	-	3.40	154	< 100	< 100	176	2,260	518	1,120	1,020	99.6	< 1.0	49.8	-	3.40	< 1.00	116	0.0660	-	-	-	-	-	-	-	-	
	NORTHEAST POND-181107	2018 11 07	8.45	1,030	8.61	7.7	2,170	2,050	1,570	41.5	2.37	133	< 10	< 10	< 10.0	164	1,360	456	787	725	61.8	< 1.0	30.9	-	2.37	< 1.00	67	0.0951	-	-	-	-	-	-	-	-	
	Northeast Pond	2019 03 29	8.49	724	8.72	10.9	1,910	1,577	1,080	28.5	1.36	24	< 10	< 10	< 10.0	113	1,010	349	603	-	46.7	< 1.0	23.4	556	1.36	0.23	49	0.109	-	-	-	-	-	-	-	-	
	Northeast Pond	2019 06 05	8.60	1,010	8.33	22.4	2,570	2,267	1,800	17.2	1.33	195	< 10	< 10	< 10.0	161	1,260	596	858	712	146	< 1.0	72.9	-	1.33	< 0.10	32	< 0.0050	-	-	-	-	-	-	-	-	
	Northeast Pond	2019 09 04	8.98	1,040	9.62	19.8	2,620	2,484	1,710	8.7	14.0	1.22	60	< 10	< 10	< 10.0	180	1,670	546	907	584	323	< 1.0	161	-	1.22	< 0.10	40	-	-	-	-	-	-	-	-	
	NE Pond	2019 10 23	8.52	1,040	9.04	9	2,710	2,659	1,850	3.8	11.2	1.25	225	224	< 10	224	1,940	1,600	523	987	987	< 1.0	< 1.0	< 1.0	1.02	< 0.10	35	-	-	-	-	-	-	-	-	-	
	NEPOND-200407	2020 04 07	8.46	1,000	9	9.3	2,470	2,264	1,810	2.4	11.0	0.863	< 50	< 10	< 10	< 10.0	167	1,370	543	821	753	68.3	< 1.0	34.2	-	0.863	< 0.10	34	-	-	-	-	-	-	-	-	
	NEPOND-200605	2020 06 05	8.72	1,050	8.67	20.2	2,460	2,311	1,820	3.2	14.5	1.33	199	< 10	< 10	< 10.0	160	1,310	488	870	662	208	< 1.0	104	-	1.33	< 0.10	48	-	-	-	-	-	-	-	-	
	NEPOND-200918	2020 09 18	8.82	1,030	8.85	18.4	2,750	2,514	2,380	10.2	25.8	3.66	422	< 10	< 10	-	194	1,660	541	992	703	289	< 1.0	144	-	3.66	0.26	93	-	-	-	-	-	-	-	-	
	NEPOND-201028	2020 10 28	8.50	1,030	8.69	4.5	2,660	2,758	1,580	12.4	18.4	2.33	180	31	< 10	31.1	139	1,220	397	907	798	109	< 1.0	54.5	-	2.30	< 0.10	69	-	-	-	-	-	-	-	-	
	NE POND-210323	2021 03 23	8.42	963	8.5	6.5	2,200	2,392.0	1,640	6.0	12.4	0.965	< 50	< 10	< 10	< 10.0	143	1,380	424	851	801	50.0	< 1.0	25.0	-	0.965	< 1.00	42	-	-	-	-	-	-	-	-	
	NE POND-210616	2021 06 16	8.59	1,060	8.63	23.8	2,420	2,729	1,800	9.2	13.4	1.43	112	< 10	< 10	< 10.0	186	1,860	541	990	724	266	< 1.0	133	-	1.43	< 0.10	45	-	-	-	-	-	-	-	-	
	NE POND-211019	2021 10 19	8.60	1,220	8.70	10.8	2,950	2,960.8	2,040	-	14.8	1.95	735	< 10	25	25.0	201	1,840	569	1,020	846	172	< 1.0	86.2	-	1.92	< 1.00	41	-	-	-	-	-	-	-	-	
SLOUGH	Alki Lake-20080506	2008 05 06	9.49	-	-	-	20,000	-	-	-	17,500	-	-	490	23	-	1,050	-	-	4,680	7,420	-	-	-	-	13.1	-	556	-	-	-	-	-	-	-		
	Alki Lake-20080507	2008 05 07	-	-	-	-	-	-	-	242	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	Alki Lake-20080520	2008 05 20	9.43	1,070	-	-	22,000	-	18,400	88	-	1,770	25	-	-	1,130	-	4,980	8,220	-	-	-	-	-	-	20.8	-	440	-	-	-	-	-	-	-		
	Alki Lake-20091119	2009 11 19	-	1,120	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	Slough-20010619	2001 06 19	-	-	-	-	-	-	24,200	-	-	-	-	-	-	-	-	6,850	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	Slough-20010815	2001 08 15	-	-	-	-	-	-	53,500	-	-	-	-	-	-	-	-	17,800	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	Slough-20010920	2001 09 20	-	-	-	-	-	-	91,500	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	Slough-20090521	2009 05 21	-	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	Slough-20130429	2013 04 29	9.51	715	-	-	20,000	-	18,000	154	-	1,330	< 500	-	-	-	1,260	2,700	5,110	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
	Slough-20130528	2013 05 28	9.46	789	-	-	22,400	-	20,100	72.7	-	428	< 500	-	-	-	1,480	831	6,030	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	Slough-20130718	2013 07 18	9.65	803	-	-	27,200	-	25,900	366	-	364	< 500	-	-	-	1,780	996	7,630	9,320	4,000	5,320	< 5.0	-	-	36.9	17.2	920	-	-	-	-	-	-	-	-	
	Slough-20131016	2013 10 16	9.73	567	-	-	36,900	-	37,600	142	-	998	< 500	-	-	-	2,740	< 2,000a	12,100	15,200	6,010	9,190	< 100	-	-	24.4	20.1	1,050	-	-	-	-	-	-	-	-	
	Slough-20140331	2014 03 31	9.46	531	-	-	9,940	-	7,580	34.8	-	1,310	< 250	-	-	-	621	< 1,000	2,760	1,560	1,200	< 1.0	-														





Table 3: Historical Summary of Analytical Results For Surface Water - Inorganics

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters														Dissolved Inorganics																
			pH	pH (field)	Hardness	Temperature	Conductivity	Field Conductivity	Total Dissolved Solids	Total Suspended Solids	Dissolved Organic Carbon	Total Nitrogen-N	Ammonia, Total (as N)	Nitrate (as N)	Nitrite (as N)	Nitrate+Nitrite Nitrogen	Chloride	Fluoride	Sulfate	Total Alkalinity	Alkalinity, Bicarbonate (as CaCO3)	Alkalinity, Carbonate (as CaCO3)	Alkalinity, Hydroxide (as CaCO3)	Alkalinity, Phenolphthalein (as CaCO3)	Bicarbonate	Kjeldahl Nitrogen-N	Bromide	Chemical Oxygen Demand	Phosphate	Ortho-Phosphate	Total Organic Carbon	Total Phosphorus as P	
LITTLE ROBERT LK Cont'	Little Robert Lk	2019 06 05	9.02	987	8,84	22.3	2,690	2,335	2,010	3.8	-	1.32	84	< 100	< 100	< 100	181	< 1,000	749	637	384	253	< 1.0	127	-	1.32	< 1.00	36	0.209	-	12.7	0.787	
	Little Robert Lk	2019 09 04	8.98	1,110	8,19	25	3,100	3,090	2,160	4.4	23.7	1.82	45	< 100	< 100	< 100	165	< 1,000	972	745	478	267	< 1.0	133	-	1.82	< 1.00	49	-	0.387	25.5	1.16	
	LITTLE ROBERT LAKE-200928	2020 09 28	8.72	1,330	8,76	14.2	4,350	4,285	3,490	153	24.0	2.85	211	< 100	< 100	-	115	< 1,000	1,720	675	520	155	< 1.0	77.7	-	2.85	< 1.00	93	-	0.564	27.2	1.50	
	LITTLE ROBERT LAKE-201029	2020 10 29	8.50	1,300	8,71	5	4,150	4,187	3,210	6.4	19.5	2.65	440	309	< 100	309	103	< 1,000	1,540	697	621	75.8	< 1.0	37.9	-	2.34	< 1.00	52	-	0.618	23.3	1.58	
	LITTLE ROBERT LAKE-200605	2020 06 05	8.86	1,240	8,97	20.5	3,520	3,393	3,040	8.8	23.5	1.78	< 50	< 10	< 10	< 10	116	430	1,630	648	414	234	< 1.0	117	-	1.78	< 1.00	50	-	0.604	25.7	0.592	
	LITTLE ROBERT LAKE-210412	2021 04 12	8.42	1,560	8,59	10.8	4,200	4,486.0	3,740	23.0	24.4	1.58	110	< 100	< 100	< 100	< 1,000	1,840	749	701	47.4	< 1.0	23.7	-	1.58	< 1.00	51	-	0.953	28.3	1.67		
	Little Robert Lake	2021 08 17	9.08	1,620	9,29	20.6	4,220	4,945	4,320	30.4	16.6	1.90	< 50	< 100	< 100	110	< 1,000	2,210	861	349	312	< 1.0	156	-	1.90	< 1.00	67	-	0.600	22.7	1.09		
	LITTLE ROBERT LAKE-210922	2021 09 22	8.61	1,630	8,81	15.0	5,370	5,225	4,310	-	24.1	1.96	340	< 100	< 100	< 100	123	< 1,000	2,500	772	629	142	< 1.0	71.1	-	1.96	< 1.00	66	-	0.440	24.7	1.44	
	LITTLE ROBERT LAKE-211021	2021 10 21	8.47	1,520	8,47	8.3	5,020	4,527.0	4,110	-	22.1	2.45	488	< 100	< 100	< 100	110	< 1,000	2,320	770	699	70.9	< 1.0	35.5	-	2.45	< 1.00	58	-	0.442	24.4	1.35	
	ROBERT LK	Robert Lake-20150616	2015 06 16	-	1,150	-	-	12,500	-	13,700	31.1	-	82	< 500	-	-	346	< 2,000a	8,420	1,760	1,230	530	< 1.0	-	-	5.85	< 5.0	233	-	4.85	82.3	-	
ROBERT'S LAKE 1-20160921	2016 09 21	9.67	1,450	-	-	21,800	-	21,300	19.7	-	-	-	< 500	-	-	524	< 2,000a	12,800	2,010	-	-	-	-	-	< 5.0	-	-	-	110	-			
ROBERT LAKE - NORTH-20161117	2016 11 17	-	1,150	-	-	15,600	-	13,300	188	-	-	510	< 500	-	-	358	< 2,000a	8,640	1,410	821	592	< 1.0	-	-	7.85	< 5.0	252	-	2.94	81.7	-		
ROBERT LAKE - SOUTH-20161117	2016 11 17	-	1,070	-	-	16,300	-	13,700	67.3	-	-	83.9	< 500	-	-	387	< 2,000a	9,250	1,440	783	661	< 1.0	-	-	8.09	< 5.0	258	-	2.6	82.1	-		
ROBERT LK-180417	2018 04 17	8.98	1,040	8,92	11	9,100	3,334	7,730	18.0	-	3.59	47	< 10	< 10	< 10.0	161	450	3,840	1,010	714	297	< 1.0	148	-	3.59	0.80	127	1.79	-	74.0	2.21		
ROBERT LK-180503	2018 05 03	8.98	1,090	8,58	19.3	8,740	7,684	7,330	17.0	-	4.71	119	< 100	< 100	< 100	135	145	520	3,850	1,010	713	296	< 1.0	148	-	3.36	< 10.0	109	1.61	-	39.7	2.45	
ROBERT LK-180614	2018 06 14	8.97	1,200	9,19	19.1	8,000	6,915	6,690	12.8	-	3.56	98	< 100	< 100	< 100	198	< 1,000	3,490	1,020	706	316	< 1.0	158	-	3.56	< 1.00	113	1.24	-	39.9	1.99		
ROBERT LK-180712	2018 07 12	9.02	1,120	9,22	27.2	8,110	7,162	6,820	12.6	-	3.98	66	< 10	< 10	< 10.0	205	710	3,280	1,110	766	347	< 1.0	173	-	3.98	< 1.0	115	1.02	-	49.9	2.14		
Robert Lk	2019 03 29	9.02	885	9,25	8	5,660	636.7	3,900	17.7	-	3.72	105	< 100	< 100	< 100	140	< 1,000	2,280	763	-	231	< 1.0	115	532	3.72	< 1.00	110	0.735	-	29.2	1.44		
Robert Lk	2019 05 06	8.92	1,060	8.6	20.9	7,900	6,464	6,200	34.7	-	5.44	139	< 10	< 10	< 10.0	209	660	3,310	1,180	859	321	< 1.0	160	-	5.44	0.94	165	1.59	-	48.4	2.22		
Robert Lk	2019 06 05	8.85	1,130	8,62	22	8,000	6,741	6,520	27.4	-	5.64	733	< 100	< 100	< 100	212	< 1,000	3,160	1,210	898	313	< 1.0	156	-	5.64	< 1.00	143	0.888	-	45.3	2.55		
Robert Lk	2019 09 04	8.91	1,490	8,61	26.6	10,300	10,048	8,440	42.3	53.4	5.52	372	< 100	< 100	< 100	127	127	279	< 1,000	4,350	1,660	1,210	459	< 1.0	229	-	5.40	1.14	154	-	1.61	59.8	3.71
ROBERT LAKE-200407	2020 04 07	8.87	1,190	9.4	14	7,620	6,679	6,240	21.7	38.2	3.64	68	< 10	< 10	< 10.0	203	590	3,350	1,170	873	294	< 1.0	147	-	3.64	< 0.10	117	-	1.26	39.3	2.95		
ROBERT LAKE-200605	2020 06 05	8.61	1,220	8,86	21.1	7,520	735.8	7,100	147	53.5	7.34	438	< 1,000	< 1,000	193	630	3,560	1,440	1,090	349	< 1.0	175	-	7.34	< 10.0	245	-	2.70	57.5	4.98			
ROBERT LAKE-200928	2020 09 28	8.97	1,450	8,92	15.4	10,400	10,262	8,580	32.0	60.3	6.86	1,160	< 1,000	107	-	262	< 1,000	4,160	1,560	1,050	516	< 1.0	268	-	6.56	< 1.00	179	-	1.88	64.1	3.47		
ROBERT LAKE-201028	2020 10 28	8.94	1,360	9,18	4	9,890	9,840	7,960	44.7	58.4	6.80	129	< 250	79	< 250	245	630	4,160	1,580	1,100	477	< 1.0	239	-	6.72	0.98	153	-	0.869	68.3	3.47		
ROBERT LAKE-210412	2021 04 12	8.73	1,330	9.12	11.0	7,810	8,577	7,290	60.0	38.4	6.14	204	< 100	< 100	< 100	190	< 1,000	3,200	1,440	1,050	393	< 1.0	196	-	6.14	< 1.00	213	-	1.75	46.7	3.28		
ROBERT LAKE-210616	2021 06 16	8.96	1,510	9.02	17.9	8,560	9,489	8,250	44.0	47.4	7.32	118	< 100	< 100	< 100	242	< 1,000	4,110	1,690	1,150	541	< 1.0	270	-	7.32	< 1.00	234	-	1.12	57.0	3.46		
ROBERT LAKE-210922	2021 09 22	9.12	1,980	9.12	15.7	12,800	12,687.0	9,700	-	65.8	8.96	143	< 100	< 100	< 100	365	< 1,000	6,060	2,110	1,300	810	< 1.0	405	-	8.96	1.33	271	-	1.68	77.7	3.80		
ROBERT LAKE-211021	2021 10 21	9.08	1,530	9.29	7.9	12,600	11,012.0	9,700	-	61.8	12.7	173	< 100	< 100	< 100	336	< 1,000	5,790	2,020	1,290	731	< 1.0	365	-	12.7	1.22	255	-	1.37	76.1	3.82		
DIFFUSER	DIFFUSER-180417	2018 04 17	8.98	1,090	9.26	12	9,030	8,592	7,570	19.3	-	2.69	56	< 10	< 10	< 10.0	168	460	3,890	1,010	720	294	< 1.0	147	-	2.69	0.80	132	1.86	-	61.0	5.73	
DIFFUSER-180503	2018 05 03	8.98	1,110	8,67	19.7	8,740	7,700	7,710	15.0	-	3.39	135	< 1,000	< 1,000	145	520	3,890	1,020	726	299	< 1.0	149	-	3.39	< 10.0	112	1.38	-	42.7	2.51			
DIFFUSER-180614	2018 06 14	8.99	1,230	9.29	19.5	7,940	6,818	10,400	10.8	-	3.86	48	< 10	< 10	< 10.0	182	970	3,350	1,050	691	363	< 1.0	181	-	3.86	0.91	99	0.710	-	41.5	1.97		
JH Outfall	JH OUTFALL-180417	2018 04 17	8.68	861	8.89	10.3	2,100	2,089	1,580	28.0	-	1.53	23	486	< 10	486	150	650	485	520	441	78.8	< 1.0	39.4	-	1.04	0.20	30	< 0.0050	-	12.4	0.0576	
JH Outfall	JH OUTFALL-180503	2018 05 03	8.63	710	8.31	16.1	1,830	1,586	1,150	< 3.3	-	2.56	469	1,090	21	1,110	148	670	241	476	411	65.4	< 1.0	32.7	-	1.45	< 0.10	31	0.0090	-	10.1	0.0528	
QUAIL RIDGE	Treated Leachate Feb 02/00-20000202	2000 02 02	-	-	-	-	-	0.043	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Quail Ridge-20081104	2008 11 04	7.18	-	-	-	7,040	-	-	-	-	-	106,000	63,500	-	-	-	-	-	3,580	-	-	-	-	-	-	-	430	-	-	-	-		
Qu																																	





Table 4: Historical Summary of Analytical Results For Surface Water Metals

Sample Location	Sample ID	Sample Date (yy/mm/dd)	Physical Parameters													Total Metals																										
			pH	Total Hardness (mg/L)	Total Phosphate (mg/L)	Aluminum (µg/L)	Antimony (µg/L)	Arsenic (µg/L)	Barium (µg/L)	Beryllium (µg/L)	Bismuth (µg/L)	Boron (µg/L)	Cadmium (µg/L)	Calcium (mg/L)	Chromium (µg/L)	Cobalt (µg/L)	Copper (µg/L)	Iron (µg/L)	Lead (µg/L)	Lithium (µg/L)	Magnesium (µg/L)	Manganese (µg/L)	Mercury (µg/L)	Molybdenum (µg/L)	Nickel (µg/L)	Phosphorus (µg/L)	Selenium (µg/L)	Silicon (µg/L)	Silver (µg/L)	Sodium (µg/L)	Strontium (µg/L)	Sulfur (µg/L)	Tellurium (µg/L)	Thallium (µg/L)	Thorium (µg/L)	Tin (µg/L)	Titanium (µg/L)	Uranium (µg/L)	Vanadium (µg/L)	Zinc (µg/L)	Zirconium (µg/L)	
NORTHEAST POND (Cont'd)	NORTHEAST POND-181107	2018 11 07	8.45	1,030	0.61	588	0.21	3.25	117	< 0.10	< 0.10	102	0.019	67,000	1.60	0.93	5.35	842	0.58	40.3	211,000	180	< 0.0404	21.3	3.78	578	19,200	< 0.50	13,200	< 0.050	288,000	3,880	169,000	< 0.020	< 0.10	< 0.20	< 30.0	< 10.0	36.8	3.6	4.4	0.68
	Northeast Pond	2019 03 29	8.49	724	0.72	331	< 0.20	2.59	64.8	< 0.10	< 0.10	56.9	0.024	53,900	0.90	0.62	1.54	555	0.51	27.7	143,000	180	< 0.0404	11.9	3.11	345	11,500	< 0.50	8,100	< 0.050	192,000	2,780	135,000	< 0.020	< 0.10	< 0.20	16.0	< 10.0	25.1	2.7	4.2	0.52
	Northeast Pond	2019 06 05	8.60	1,010	0.33	140	0.25	3.77	93.4	< 0.10	< 0.10	102	0.026	52,700	< 0.50	0.58	1.92	194	0.21	44.9	214,000	119	< 0.0404	27.3	3.54	325	16,000	< 0.50	3,300	< 0.050	317,000	3,840	197,000	< 0.020	< 0.10	< 0.20	7.8	< 10.0	41.0	4.6	< 4.0	0.55
	Northeast Pond	2019 09 04	8.98	1,040	0.62	142	0.28	4.42	84.7	< 0.10	< 0.10	34.2	< 0.010	24,300	0.92	0.37	0.72	202	< 0.20	53.6	237,000	81.1	< 0.010	30.0	3.87	149	15,800	< 0.50	2,000	< 0.050	325,000	4,120	206,000	< 0.020	< 0.10	< 0.20	7.8	< 10.0	40.8	2.2	< 4.0	0.23
	NE Pond	2019 10 20	8.62	1,040	0.04	35.1	0.20	3.48	64.8	< 0.10	< 0.10	48.7	0.013	33,200	< 0.50	0.53	0.68	62	< 0.20	45.4	232,000	220	< 0.010	32.9	4.34	246	16,100	< 0.50	3,000	< 0.050	304,000	4,160	202,000	< 0.020	< 0.10	< 0.20	< 5.0	< 10.0	54.4	1.6	< 4.0	0.26
	NEPOND-200407	2020 04 07	8.46	1,000	9	27.2	0.178	3.37	39.2	< 0.010	< 0.010	81.0	0.0058	53,000	0.68	0.324	0.67	55.4	0.060	44.1	211,000	176	< 0.010	22.2	2.94	350	15,900	< 0.38	5,480	< 0.010	296,000	3,890	198,000	< 0.040	0.011	< 0.050	2.04	< 0.20	40.9	2.12	< 4.0	0.572
	NEPOND-200626	2020 06 05	8.72	1,050	0.67	17.6	0.219	3.05	15.4	0.010	0.010	87.1	0.0089	52,800	0.14	0.245	0.32	36.8	< 0.050	40.2	223,000	132	< 0.010	18.6	2.45	343	17,800	< 0.38	2,780	< 0.010	338,000	4,210	211,000	< 0.040	0.016	< 0.050	1.32	< 0.20	33.8	2.50	< 1.0	0.345
	NEPOND-200918	2020 09 18	8.82	1,030	0.85	73.4	0.345	6.45	115	< 0.010	< 0.010	78.0	0.0081	39,400	0.36	0.545	0.66	149	0.117	34.8	226,000	381	< 0.010	18.6	3.01	555	22,100	< 0.33	10,400	< 0.010	322,000	3,670	176,000	< 0.040	0.016	< 0.050	5.71	< 0.20	26.6	4.09	3.0	0.716
	NEPOND-201028	2020 10 28	8.50	1,030	0.69	77.9	0.220	3.76	105	0.196	< 0.10	85.7	0.0084	40,500	0.27	0.621	0.66	151	0.157	48.2	225,000	216	< 0.010	22.0	3.28	344	14,700	< 0.22	10,200	< 0.010	323,000	4,230	194,000	< 0.040	0.028	< 0.050	6.83	< 0.20	32.6	3.41	2.4	0.948
	NEPOND-210323	2021 03 23	8.62	963	8.5	117	0.201	2.53	60.5	< 0.010	< 0.010	92.7	0.0087	57,300	0.49	0.492	1.15	187	0.122	33.8	199,000	112	< 0.010	24.3	3.41	297	15,100	< 0.25	5,270	< 0.010	278,000	7,330	165,000	< 0.040	0.013	0.097	6.88	< 0.20	35.8	2.90	1.7	0.82
NE POND-210616	2021 06 16	8.89	1,080	0.83	398	0.214	3.31	55.1	< 0.010	< 0.010	65.5	0.0087	38,300	< 0.2	0.495	0.86	328	0.227	47.7	238,000	105	< 0.010	31.9	3.81	292	15,700	< 0.21	6,100	< 0.010	381,000	4,000	198,000	< 0.040	0.024	< 0.050	1.32	< 0.20	40.1	3.12	2.3	0.892	
SLOUGH	NE POND-210719	2021 07 19	8.60	1,220	0.70	79.9	0.187	2.65	129	< 0.010	< 0.010	48.8	0.0117	40,400	0.36	0.392	0.48	160	0.084	54.6	272,000	118	< 0.010	46.7	3.69	260	19,700	< 0.28	4,040	< 0.010	379,000	4,770	220,000	< 0.040	0.010	0.055	5.75	0.25	51.0	1.4	1.0	0.840
	Skough-20010619	2001 06 19	-	-	-	190	< 50a	140	< 40a	< 50a	< 20	2,470	< 8a	32	10	240	22	106	139,000	8	-	37	59	1,700	447,000	< 40a	< 10a	< 8,930,000	532	2,600,000	-	< 40a	-	< 30	5	-	< 10	< 25	-	-		
	Skough-20010711	2001 07 11	-	-	-	260	< 100a	< 200a	108	< 10a	< 200	3,840	< 10a	< 50a	65	30	400	63	210	124,000	7.5	-	60	70	1,600	729,000	< 100a	< 4,340	< 30a	< 12,700,000	525	4,640,000	-	< 100a	-	< 80	63	-	< 53	< 20a	-	
	2001 08 15	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	Skough-20010816	2001 08 16	-	-	-	< 200a	< 500a	95	< 30a	< 40a	8,480	< 30a	< 10,000a	< 40a	< 30a	< 50a	310	140	320	135,000	< 10	-	50	85	3,200	1,000,000	< 200a	< 4,050	< 50a	< 19,100,000	595	5,760,000	-	< 200a	-	< 200	70	-	< 50	< 30a	-	
	Skough-20010920	2001 09 20	-	-	-	< 200a	< 530	255	< 30a	< 40a	8,110	< 30a	< 10,000a	< 40a	< 130	< 50a	420	< 100a	310	194,000	< 20	-	55	220	8,600	1,570,000	< 200a	< 2,860	< 50a	< 29,700,000	848	9,400,000	-	< 200a	-	< 200	295	-	< 90	85	-	
	Sk Lake-20080520	2008 05 06	9.49	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	Sk Lake-20080507	2008 05 07	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	Sk Lake-20080520	2008 05 20	9.43	1,070	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
	Skough-20090521	2009 05 21	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Sk Lake-20091119	2009 11 19	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Skough-20130429	2013 04 29	9.51	715	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Skough-20130528	2013 05 28	9.47	789	-	2,530	13.5	81.7	< 100	< 50a	-	1,400	< 2.5a	14,200	< 2.5a	< 5.0a	< 2.5a	3,580	4.8	< 100	183,000	68	< 0.20a	60.3	34	-	-	-	< 5.0a	< 0.5a	8,760,000	-	-	< 5.0a	-	< 140	< 195	< 300a	< 50	-	-		
Skough-20130718	2013 07 18	9.36	787	-	1,530	8.2	39.8	< 100	< 50a	-	1,400	< 2.5a	14,200	< 2.5a	< 5.0a	< 2.5a	3,580	4.8	< 100	183,000	68	< 0.20a	60.3	34	-	-	-	< 5.0a	< 0.5a	8,760,000	-	-	< 5.0a	-	< 140	< 195	< 300a	< 50	-	-		
Skough-20131016	2013 10 16	9.73	567	-	< 1.50	< 20.0	< 162	< 200	< 100a	-	2,100	< 2.5a	6,400	< 2.5a	< 5.0a	< 2.5a	< 600	< 2.5	< 200	134,000	< 100	< 0.20a	89.3	37	-	-	-	< 5.0a	< 0.87	< 12,100,000	-	-	< 5.0a	-	< 100	< 200	< 436	< 600a	< 100	-		
Skough-20140331	2014 03 31	9.46	531	-	1,750	4.5	35.5	< 50	< 2.5a	-	820	< 0.50a	24,700	6.5	2.8	9.2	2,360	1.2	< 50	114,000	73	< 0.20a	27.6	38	-	-	-	< 1.0a	< 0.12	2,480,000	-	-	< 1.0a	-	< 104	< 81.8	< 150a	< 25	-			
Skough-20140528	2014 05 28	9.37	665	-	3,080	11.2	80.4	< 100	< 50a	-	1,000	< 1.0a	12,500	< 10a	4.3	10	4,520	1.7	< 100	154,000	84	< 0.20a	41	27	-	-	-	< 2.0a	< 0.3	2,480,000	-	-	< 2.0a	-	< 180	< 158	< 300a	< 50	-			
Skough-20140528	2014 05 28	9.58	911	-	2,330	7.2	198	< 200	< 100a																																	



Table 4: Historical Summary of Analytical Results For Surface Water Metals

Sample Location	Sample ID	Sample Date (yyyy mm dd)	Physical Parameters														Total Metals																										
			pH	Total Hardness	pH (field)	Aluminum	Antimony	Arsenic	Barium	Beryllium	Bismuth	Boron	Cadmium	Calcium	Chromium	Cobalt	Copper	Iron	Lead	Lithium	Magnesium	Manganese	Mercury	Molybdenum	Nickel	Phosphorus	Potassium	Selenium	Silicon	Silver	Sodium	Strontium	Sulphur	Tellurium	Thallium	Thorium	Tin	Titanium	Tungsten	Vanadium	Zinc	Zirconium	
ROBERT LK (Cont'd)	ROBERT LAKE - SOUTH-20161117	2016 11 17	-	1,070	-	2,790	4.20	11	< 5.0	< 25u	< 1,000	< 500	< 0.10	33,100	5.3	2.2	< 10a	3,410	1.6	< 50	241,000	123	< 0.20a	90.3	< 10	3,390	90,000	< 1.0	0.460	< 0.20	4,500,000	3,630	-	-	< 0.20	< 150	147	-	< 131	< 150a	< 25	-	
	ROBERT LK-180417	2018 04 17	6.98	1,040	6.92	150	0.91	9.89	31.0	< 0.10	< 0.10	22.3	0.025	55,600	1.19	0.82	2.20	198	0.20	6.81	220,000	345	< 0.010	61.1	4.42	2,750	58,600	0.59	17,000	< 0.050	2,710,000	3,190	1,780,000	< 0.50	< 0.020	< 0.10	< 0.20	10.8	1.4	89.9	6.0	< 4.0	2.31
	ROBERT LK-180503	2018 05 03	8.99	1,090	6.58	35.8	0.65	10.2	32.8	< 0.10	< 0.10	31.7	0.033	63,000	< 0.50	0.74	1.83	77	< 0.20	11.3	225,000	242	-	35.5	4.05	2,610	57,100	0.59	15,800	< 0.050	2,460,000	3,540	1,700,000	< 0.50	< 0.020	< 0.10	< 0.20	5.0	1.0	82.2	6.2	4.8	1.86
	ROBERT LK-180614	2018 06 14	6.97	1,200	6.19	47.0	0.80	11.1	33.8	< 0.10	< 0.10	29.3	0.033	78,900	< 0.50	0.29	1.06	70	< 0.20	21.0	244,000	238	< 0.010	45.2	2.85	2,390	57,500	< 0.50	14,400	< 0.050	2,020,000	4,080	1,570,000	< 0.50	< 0.020	< 0.10	< 0.20	< 5.0	< 1.0	74.1	3.1	4.3	1.19
	ROBERT LK-180712	2018 07 12	9.02	1,120	6.22	110	0.57	9.51	23.8	< 0.10	< 0.10	44.8	0.029	71,300	0.52	0.31	1.18	101	< 0.20	19.8	229,000	95.7	< 0.010	47.5	2.92	2,270	51,700	< 0.50	17,000	< 0.050	1,840,000	4,050	1,310,000	< 0.50	< 0.020	< 0.10	< 0.20	5.5	< 1.0	73.3	2.4	< 4.0	0.85
	Robert Lk	2019 03 29	9.02	685	6.25	118	0.29	5.21	25.9	< 0.10	< 0.10	17.2	0.021	36,000	< 0.50	0.50	1.56	165	0.23	10.7	144,000	206	< 0.040a	36.8	2.70	1,530	31,100	< 0.50	4,600	< 0.050	1,240,000	2,170	890,000	< 0.50	< 0.020	< 0.10	< 0.20	7.5	< 1.0	54.1	3.1	< 4.0	1.30
	Robert Lk	2019 05 06	6.92	1,060	6.5	691	0.53	7.39	42.9	< 0.10	< 0.10	32.0	0.061	59,300	1.49	0.58	2.42	777	0.59	17.0	221,000	172	< 0.040a	47.5	4.42	2,400	46,600	0.51	8,300	< 0.050	1,960,000	3,550	1,360,000	< 0.50	< 0.020	< 0.10	< 0.20	40.1	< 1.0	75.9	5.0	7.1	2.33
	Robert Lk	2019 06 05	6.85	1,130	6.52	831	0.68	8.69	51.9	< 0.10	< 0.10	48.1	0.030	68,200	1.37	0.50	1.95	721	0.83	20.5	234,000	236	< 0.040a	39.2	4.41	2,700	47,700	0.71	6,900	< 0.050	2,020,000	3,750	1,290,000	< 0.50	< 0.020	< 0.10	< 0.20	34.2	< 1.0	71.7	5.0	7.1	1.64
	Robert Lk	2019 09 04	6.91	1,490	6.61	1,040	0.78	13.8	55.8	< 0.10	< 0.10	81.9	0.027	92,800	2.51	1.15	3.00	1,230	0.81	28.5	305,000	153	< 0.010	45.2	5.87	4,280	68,500	0.85	8,500	0.072	2,630,000	5,420	1,750,000	< 0.50	< 0.020	0.15	< 0.20	61.5	1.2	90.9	8.1	6.7	2.93
	ROBERT LAKE-200407	2020 04 07	8.87	1,190	6.4	420	0.495	8.04	42.6	0.016	< 0.010	51.1	0.0189	63,900	0.68	1.22	2.24	515	0.399	18.4	250,000	192	< 0.010	53.2	4.58	3,000	48,700	0.58	8,020	< 0.010	1,740,000	3,380	1,350,000	0.050	0.040a	0.080	< 0.050	26.5	0.85	91.5	10.2	3.2	3.68
	ROBERT LAKE-200505	2020 05 05	6.81	1,220	6.35	850	0.553	8.20	58.7	0.038	0.014	43.1	0.0434	96,800	2.19	1.64	2.24	1,150	0.660	15.1	239,000	373	< 0.010	56.6	5.80	4,250	51,100	0.49	4,780	< 0.010	1,800,000	4,530	1,230,000	0.052	0.080	0.124	0.075	17.8	1.00	94.6	10.0	5.3	4.69
	ROBERT LAKE-200528	2020 05 28	6.97	1,450	6.92	1,430	0.611	11.9	58.8	0.046	0.019	63.4	0.0379	93,200	2.70	1.23	3.38	1,330	0.864	24.0	296,000	168	< 0.010	52.9	6.02	3,770	63,200	0.79	9,630	< 0.010	2,410,000	4,650	1,740,000	0.054	0.0113	0.212	0.066	17.4	1.29	90.7	7.73	7.7	3.48
ROBERT LAKE-201028	2020 10 28	6.94	1,380	6.18	1,790	0.621	12.1	61.6	0.077	0.021	65.9	0.0484	66,400	3.08	1.48	3.97	1,770	1.24	27.4	295,000	145	< 0.010	56.6	6.68	3,920	62,600	1.08	13,100	0.018	2,280,000	4,100	1,680,000	0.050	0.0169	0.228	0.071	104	1.48	90.0	11.3	9.2	3.72	
ROBERT LAKE-210412	2021 04 12	8.13	1,330	6.12	1,630	0.548	10.1	67.3	0.058	0.025	48.6	0.0478	62,200	3.28	1.85	4.79	1,950	1.33	22.6	286,000	261	< 0.010	66.3	7.22	3,620	54,100	0.61	15,100	0.012	2,070,000	3,700	1,410,000	0.054	0.0147	0.190	0.080	102	1.16	96.4	13.8	8.8	3.25	
ROBERT LAKE-210616	2021 06 16	6.96	1,510	6.02	1,450	0.485	9.71	69.5	0.051	0.027	54.5	0.0425	93,500	2.74	1.51	5.88	1,730	1.18	25.2	311,000	291	< 0.010	59.0	6.38	3,840	63,100	0.50	15,000	< 0.010	2,300,000	4,080	1,550,000	0.050	0.0148	0.184	0.053	63.5	1.09	105	7.99	7.7	3.10	
ROBERT LAKE-210922	2021 09 22	6.12	1,980	6.12	1,150	0.649	15.4	81.5	0.029	0.017	62.6	0.0383	44,500	2.47	1.29	3.63	1,210	1.20	22.6	453,000	127	< 0.010	76.2	7.53	4,120	90,200	1.25	13,500	< 0.010	3,460,000	4,990	2,270,000	0.050	0.0101	0.138	< 0.050	63.2	1.88	127	7.83	7.5	3.23	
ROBERT LAKE-211021	2021 10 21	9.08	1,530	6.29	1,290	< 0.002	12.7	58.5	< 1.00a	< 1.00	27.8	< 0.200	42,800	< 10.0a	1.13	< 10.0	1,450	< 5.00	26.9	345,000	105	< 0.010	60.1	4.95	4,110	68,200	< 10.0a	11,500	< 1.00	2,740,000	4,530	1,910,000	< 5.00	< 0.400	< 1.00	< 5.00	73.1	< 5.00	95.5	< 20.0	< 100	2.51	
DIPFUSER	DIPFUSER-180417	2018 04 17	6.98	1,090	6.28	176	0.59	10.1	31.2	< 0.10	< 0.10	20.8	0.017	57,400	0.97	1.28	2.44	248	0.27	6.99	230,000	355	< 0.010	60.8	4.72	2,900	60,800	0.57	7,400	< 0.050	2,440,000	3,170	1,840,000	< 0.50	< 0.020	< 0.10	< 0.20	12.7	1.2	90.2	6.2	4.5	2.90
	DIPFUSER-180503	2018 05 03	6.98	1,110	6.67	51.5	0.67	10.5	33.2	< 0.10	< 0.10	30.0	0.033	64,700	< 0.50	0.74	1.54	89	< 0.20	12.5	230,000	290	-	99.4	4.08	2,710	58,700	0.57	5,900	< 0.050	2,540,000	3,610	1,740,000	< 0.50	< 0.020	< 0.10	< 0.20	< 5.0	< 1.0	83.9	6.4	6.5	1.90
JH Outfall	DIPFUSER-180615	2018 06 15	6.99	1,230	6.29	70.1	0.75	11.1	33.3	< 0.10	< 0.10	28.2	0.032	82,100	< 0.50	0.41	0.99	109	< 0.20	20.3	249,000	243	< 0.010	44.9	4.99	2,410	59,400	< 0.50	3,600	< 0.050	2,000,000	4,130	1,600,000	< 0.50	< 0.020	< 0.10	< 0.20	5.3	< 1.0	73.0	3.2	5.3	1.15
	JH OUTFALL-180417	2018 04 17	6.89	861	6.89	312	< 0.20	1.92	59.3	< 0.10	< 0.10	41.8	< 0.010	76,100	1.13	0.65	2.13	492	0.30	27.2	163,000	84.2	< 0.010	14.9	2.72	96	13,700	1.22	< 1.00a	< 0.050	272,000	3,630	201,000	< 0.50	< 0.020	< 0.10	< 0.20	17.7	< 1.0	38.4	4.1	5.4	0.45
QUAL RIDGE	JH OUTFALL-180503	2018 05 03	6.93	710	6.31	29.1	0.20	2.05	70.0	< 0.10	< 0.10	42.1	0.014	63,500	0.76	0.31	2.24	47	< 0.20	32.0	134,000	27.3	-	16.8	1.67	84	15,200	1.58	2,300	< 0.050	212,000	3,320	113,000	< 0.50	< 0.020	< 0.10	< 0.20	< 5.0	< 1.0	29.3	4.5	6.1	0.24
	Treated Leachate Feb 02-00-20000202	2000 02 02	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
	Qual Ridge Leachate-20011115	2000 11 15	-	-	-	244	< 10a	< 20	245	< 1a	< 10	2,350	< 1a	102,000	18.6	16.2	56	476	< 4a	39	287,000	468	-	< 2	25	4,220	327,000	< 8a	18,500	< 2a	1,980,000	2,550	-	-	< 8a	-	< 6	86.6	-	< 15	22.4	-	
	Qual Ridge Leachate-20010223	2001 02 23	-	-	-	740	-	-	-	-	-	-	-	148,000	-	-	-	1,750	-	-	325,000	1,120	-	-	-	-	262,000	-	-	19,000	-	-	-	-	-								

Table 5: Historical Summary of Analytical Results For Leachate

Sample Location		N Pumphouse MH											Sample Location		N Pumphouse MH							
Sample ID	LEACHATE- MANHOLE- 20130312	N Pumphouse MH-20080205	N Pumphouse MH-20080219	N Pumphouse MH-20080304	N Pumphouse MH-20080325	N Pumphouse MH-20080408	N Pumphouse MH-20080424	N Pumphouse MH-20080507	N Pumphouse MH-20080521	N Pumphouse MH-20080617	N Pumphouse MH-20080626	N Pumphouse MH-20080708	Sample ID	N Pumphouse MH-20131211	N Pumphouse MH-20140408	N Pumphouse MH-20140610	N Pumphouse MH-20150122	N Pumphouse MH-20150815	N Pumphouse MH-20150915	N Pumphouse MH-20151203		
Sample Date (yyyy mm dd)	2013 03 12	2008 02 05	2008 02 19	2008 03 04	2008 03 25	2008 04 08	2008 04 24	2008 05 07	2008 05 21	2008 06 17	2008 06 26	2008 07 08	Sample Date (yyyy mm dd)	2013 12 11	2014 04 08	2014 06 10	2015 01 22	2015 08 15	2015 09 15	2015 12 03		
Parameter	Units	Analytical Results											Parameter	Units	Analytical Results							
<b>Dissolved Inorganics</b>																						
Ammonia, Total (as N)	µg/L	118,000	-	-	-	-	-	-	-	-	-	-	Ammonia, Total (as N)	µg/L	108,000	64,800	65,300	40,600	95,000	99,700	111,000	
Nitrate (as N)	µg/L	< 250	-	-	-	-	-	-	-	-	-	-	Nitrate (as N)	µg/L	< 250	< 250	350	< 250	< 250	< 250	350	
Nitrite (as N)	µg/L	-	-	-	-	-	-	-	-	-	-	-	Nitrite (as N)	µg/L	-	-	-	-	-	-	-	
Chloride	mg/L	490	-	-	-	-	-	-	-	-	-	-	Chloride	mg/L	380	506	553	368	377	416	441	
Fluoride	µg/L	5,200	-	-	-	-	-	-	-	-	-	-	Fluoride	µg/L	2,200	< 1,000	778	< 1,000	1,600	< 1,000	< 1,000	
Sulfate	mg/L	503	-	-	-	-	-	-	-	-	-	-	Sulfate	mg/L	376	1,130	860	299	545	545	688	
Total Alkalinity	mg/L	-	-	-	-	-	-	-	-	-	-	-	Total Alkalinity	mg/L	-	3,440	4,930	2,100	3,470	3,640	3,640	
Alkalinity, Bicarbonate (as CaCO3)	mg/L	-	-	-	-	-	-	-	-	-	-	-	Alkalinity, Bicarbonate (as CaCO3)	mg/L	-	-	-	2,100	-	3,640	3,640	
Alkalinity, Carbonate (as CaCO3)	mg/L	-	-	-	-	-	-	-	-	-	-	-	Alkalinity, Carbonate (as CaCO3)	mg/L	-	-	-	< 1.0	-	< 1.0	< 1.0	
Alkalinity, Hydroxide (as CaCO3)	mg/L	-	-	-	-	-	-	-	-	-	-	-	Alkalinity, Hydroxide (as CaCO3)	mg/L	-	-	-	< 1.0	-	< 1.0	< 1.0	
Alkalinity, Phenolphthalein (as CaCO3)	mg/L	-	-	-	-	-	-	-	-	-	-	-	Alkalinity, Phenolphthalein (as CaCO3)	mg/L	-	-	-	-	-	-	-	
Bromide	mg/L	3.3	-	-	-	-	-	-	-	-	-	-	Bromide	mg/L	2.6	4.2	4.7	< 2.5	2.6	3.3	2.9	
Sulfide	mg/L	-	-	-	-	-	-	-	-	-	-	-	Sulfide	mg/L	-	-	-	-	-	-	-	
Biochemical Oxygen Demand	mg/L	-	-	-	-	-	-	-	-	-	-	-	Biochemical Oxygen Demand	mg/L	-	-	-	-	-	-	-	
Chemical Oxygen Demand	mg/L	454	-	-	-	-	-	-	-	-	-	-	Chemical Oxygen Demand	mg/L	381	628	660	205	357	421	415	
Phosphate	mg/L	-	-	-	-	-	-	-	-	-	-	-	Phosphate	mg/L	-	-	-	-	-	-	-	
Ortho-Phosphate	mg/L	2.6	-	-	-	-	-	-	-	-	-	-	Ortho-Phosphate	mg/L	2.2	3.07	4.55	0.8	2.3	2.46	2.63	
Total Organic Carbon	mg/L	120	-	-	-	-	-	-	-	-	-	-	Total Organic Carbon	mg/L	106	-	-	-	-	-	-	
Total Phosphorous as P	mg/L	-	-	-	-	-	-	-	-	-	-	-	Total Phosphorous as P	mg/L	-	-	-	-	-	-	-	
<b>Dissolved Metals</b>																						
Dissolved Aluminum	µg/L	-	-	-	-	-	-	-	-	-	-	-	Dissolved Aluminum	µg/L	-	94	82	20	36	42	46	
Dissolved Calcium	mg/L	-	-	-	-	-	-	-	-	-	-	-	Dissolved Calcium	mg/L	-	662	644	115	104	95	96.2	
Dissolved Iron	µg/L	-	-	-	-	-	-	-	-	-	-	-	Dissolved Iron	µg/L	-	261	144	1,060	116	108	76	
Dissolved Magnesium	mg/L	-	-	-	-	-	-	-	-	-	-	-	Dissolved Magnesium	mg/L	-	185	257	214	250	265	286	
Dissolved Manganese	µg/L	-	-	-	-	-	-	-	-	-	-	-	Dissolved Manganese	µg/L	-	283	299	841	423	377	395	
Dissolved Potassium	mg/L	-	-	-	-	-	-	-	-	-	-	-	Dissolved Potassium	mg/L	-	-	-	-	-	-	169	
Dissolved Sodium	mg/L	-	-	-	-	-	-	-	-	-	-	-	Dissolved Sodium	mg/L	-	1,770	2,260	698	1,140	1,370	1,520	
Antimony	µg/L	-	-	-	-	-	-	-	-	-	-	-	Antimony	µg/L	-	3.8	11.8	< 0.50	3.3	7.69	8	
Arsenic	µg/L	-	-	-	-	-	-	-	-	-	-	-	Arsenic	µg/L	-	16.5	33.9	1.7	9.6	14.1	16	
Barium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Barium	µg/L	-	100	148	201	238	247	256	
Beryllium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Beryllium	µg/L	-	< 1.0	< 1.5	< 1.0	< 1.0	< 1.0	< 1.0	
Boron	µg/L	-	-	-	-	-	-	-	-	-	-	-	Boron	µg/L	-	1,590	1,640	890	1,390	1,490	1,520	
Cadmium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Cadmium	µg/L	-	< 0.50	< 0.50	< 0.25	< 0.050	< 0.050	< 0.050	
Chromium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Chromium	µg/L	-	16.1	22.3	5.2	11.1	13.4	15	
Cobalt	µg/L	-	-	-	-	-	-	-	-	-	-	-	Cobalt	µg/L	-	6.6	6.1	3.27	7.03	6.92	7.7	
Copper	µg/L	-	-	-	-	-	-	-	-	-	-	-	Copper	µg/L	-	< 5.0	< 5.0	< 2.5	< 1.0	< 1.0	< 2.0	
Lead	µg/L	-	-	-	-	-	-	-	-	-	-	-	Lead	µg/L	-	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	
Lithium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Lithium	µg/L	-	< 50	59	< 50	< 50	< 50	< 50	
Mercury	µg/L	-	-	-	-	-	-	-	-	-	-	-	Mercury	µg/L	-	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	
Molybdenum	µg/L	-	-	-	-	-	-	-	-	-	-	-	Molybdenum	µg/L	-	3	4.6	< 1.0	1.4	2.3	1.3	
Nickel	µg/L	-	-	-	-	-	-	-	-	-	-	-	Nickel	µg/L	-	25.8	26	8.5	14.1	16.1	17.8	
Selenium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Selenium	µg/L	-	< 10	< 10	< 5.0	< 1.0	1.7	< 1.0	
Silver	µg/L	-	-	-	-	-	-	-	-	-	-	-	Silver	µg/L	-	< 0.10	< 0.10	< 0.050	< 0.050	< 0.050	< 0.10	
Thallium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Thallium	µg/L	-	< 1.0	< 1.0	< 0.50	< 0.050	< 0.20	< 0.10	
Titanium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Titanium	µg/L	-	59	73	< 50	< 50	55	55	
Tungsten	µg/L	-	-	-	-	-	-	-	-	-	-	-	Tungsten	µg/L	-	-	-	-	-	-	-	
Uranium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Uranium	µg/L	-	22.5	16.2	3.61	5.43	5.09	4.55	
Vanadium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Vanadium	µg/L	-	< 60	< 90	< 30	< 60	< 60	< 60	
Zinc	µg/L	-	-	-	-	-	-	-	-	-	-	-	Zinc	µg/L	-	< 10	< 15	< 5.0	< 10	< 10	< 10	
Bismuth	µg/L	-	-	-	-	-	-	-	-	-	-	-	Bismuth	µg/L	-	-	-	-	-	< 400	< 400	
Phosphorous	µg/L	-	-	-	-	-	-	-	-	-	-	-	Phosphorous	µg/L	-	-	-	-	-	7,640	3,180	
Silicon	µg/L	-	-	-	-	-	-	-	-	-	-	-	Silicon	µg/L	-	-	-	-	-	15,700	15,400	
Strontium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Strontium	µg/L	-	-	-	-	-	3,610	3,440	
Sulfur	µg/L	-	-	-	-	-	-	-	-	-	-	-	Sulfur	µg/L	-	-	-	-	-	179,000	720,000	
Tellurium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Tellurium	µg/L	-	-	-	-	-	< 1.0	< 1.0	
Thorium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Thorium	µg/L	-	-	-	-	-	< 0.50	< 0.50	
Tin	µg/L	-	-	-	-	-	-	-	-	-	-	-	Tin	µg/L	-	-	-	-	-	< 60	< 60	
Zirconium	µg/L	-	-	-	-	-	-	-	-	-	-	-	Zirconium	µg/L	-	-	-	-	-	17.8	19.2	
<b>Monocyclic Aromatic Hydrocarbons</b>																						
Benzene	µg/L	3.13	16	11	14	13	11	7	9	8	11	12	8	Benzene	µg/L	3.74	2.05	4.75	-	2.86	3.08	2.98
Ethylbenzene	µg/L	19.3	63	46	64	60	56	47	56	44	49	38	38	Ethylbenzene	µg/L	11.9	22.1	45.9	-	9.41	11	13.4
Toluene	µg/L	1.03	2	2	3	3	2	2	2	2	3	3	3	Toluene	µg/L	0.79	3.8	4.01	-	0.76	0.88	0.72
Xylenes	µg/L	8.35	9	9	13	12	10	12	7	11	8	9	9	Xylenes	µg/L	9.62	19.8	40.3	-	5.25	3.49	7.9
Styrene	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	Styrene	µg/L	-	-	-	-	-	-	
<b>Polycyclic Aromatic Hydrocarbons</b>																						
Naphthalene	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	Naphthalene	µg/L	-	3.19	3.09	0.36	1.45	2.11	2.76
Methylanthracene, 1-	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	Methylanthracene, 1-	µg/L	-	-	-	-	-	-	
Methylanthracene, 2-	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	Methylanthracene, 2-	µg/L	-	-	-	-	-	-	
Acenaphthylene	µg/L	-	-	-	-	-</																

Table 5: Historical Summary of Analytical Results For Leachate

Sample Location					N Pumphouse MH														Sample Location								
N PUMPHOUSE MH-20160315	N PUMPHOUSE MH-20160623	N PUMPHOUSE MH-20160915	N PUMPHOUSE MH-20161117	N PUMPHOUSE MH-20170914	Sample ID	N PUMPHOUSE MH-20171204	N Pumphouse MH	N Pumphouse MH	N Pumphouse MH-20180524	N Pumphouse MH	N Pumphouse MH-20181108	N Pumphouse MH	N Pumphouse MH-20190315	N Pumphouse MH	N Pumphouse MH-20190603	N Pumphouse MH	N Pumphouse MH-20190903	N Pumphouse MH-20190903	Sample ID	N Pumphouse MH	N Pumphouse MH-20191031	N Pumphouse MH	N Pumphouse MH	N Pumphouse MH			
Sample Date (yyyy mm dd)					Sample Date (yyyy mm dd)	2017 12 04	2018 03 15	2018 05 24	2018 05 24	2018 11 08	2018 11 08	2019 03 15	2019 03 15	2019 06 03	2019 06 03	2019 09 03	2019 09 03	2019 09 03	2019 09 03	Sample Date (yyyy mm dd)	2019 10 31	2019 10 31	2020 03 05	2020 06 03			
Parameter Units					Analytical Results														Parameter Units								
<b>Dissolved Inorganics</b>																											
76,800	11,400	99,000	140,000	87,000	Ammonia, Total (a)	µg/L	85,800	171	52,900	52,900	50,200	50,200	14,600	14,600	39,500	39,500	33,800	33,800	Ammonia, Total (a)	µg/L	52,300	52,300	55,100	35,000			
< 250	5,710	< 250	< 250	< 250	Nitrate (as N)	µg/L	< 100	< 100	< 100	< 100	< 250	< 250	3,530	3,530	< 100	< 100	< 10	< 10	Nitrate (as N)	µg/L	< 100	< 100	< 10	< 100			
420	217	502	671	503	Chloride	mg/L	554	531	437	437	936	936	501	410	410	89.9	89.9	Chloride	mg/L	401	401	337	530				
< 1,000	1,280	< 1,000	< 1,000	1,100	Fluoride	mg/L	< 1,000	< 1,000	< 1,000	< 1,000	< 2,500	< 2,500	< 1,000	< 1,000	< 1,100	< 1,100	Fluoride	mg/L	< 1,000	< 1,000	810	< 1,000					
573	347	893	996	954	Sulfate	mg/L	1,180	236	1,010	1,010	2,660	2,660	1,340	1,340	1,120	1,120	240	240	Sulfate	mg/L	1,180	1,180	859	1,350			
3,190	934	3,920	4,980	3,760	Total Alkalinity	mg/L	5,390	575	2,740	2,740	8,350	8,350	2,890	3,310	3,310	6,780	6,780	Total Alkalinity	mg/L	3,440	3,440	2,900	3,310				
< 1.0	-	-	-	-	Alkalinity, Bicarb	mg/L	-	575	2,740	2,740	6,350	6,350	2,790	3,310	3,310	6,780	6,780	Alkalinity, Bicarb	mg/L	3,440	3,440	2,900	3,310				
< 1.0	-	-	-	-	Alkalinity, Carbon	mg/L	-	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Alkalinity, Carbon	mg/L	< 1.0	< 1.0	< 1.0	< 1.0				
< 1.0	-	-	-	-	Alkalinity, Hydrox	mg/L	-	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Alkalinity, Hydrox	mg/L	< 1.0	< 1.0	< 1.0	< 1.0				
2.8	< 1.0	3.7	5.3	3.4	Bromide	mg/L	3.9	< 1.0	< 1.0	< 1.0	< 2.50	< 2.50	2.37	2.37	< 1.00	< 1.00	< 1.00	< 1.00	Bromide	mg/L	2.80	2.8	1.98	2.59			
-	-	-	-	-	Sulfide	mg/L	-	< 0.020	31.7	-	102	-	26.7	-	46.1	-	129	-	Sulfide	mg/L	75.3	-	46.3	38.4			
518	46	482	681	508	Biochemical Oxy	mg/L	-	< 5.5	63.7	-	301	-	111	-	58.3	-	275	-	Biochemical Oxy	mg/L	60.2	-	79.4	113			
-	-	-	-	-	Chemical Oxygen	mg/L	529	< 20	382	382	925	925	436	436	430	430	947	947	Chemical Oxygen	mg/L	310	310	385	548			
2.29	0.222	3.01	0.392	3.33	Phosphate	mg/L	4.5	< 0.0860	3.02	-	6.51	-	6.51	-	2.90	-	2.90	-	Phosphate	mg/L	1.00	1.0	2.01	3.42			
-	-	-	-	-	Ortho-Phosphate	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	Ortho-Phosphate	mg/L	-	-	-	-			
-	-	-	-	-	Total Organic Car	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	Total Organic Car	mg/L	-	-	-	-			
-	-	-	-	-	Total Phosphor	mg/L	-	0.143	4.00	-	8.08	-	4.30	-	3.99	-	10.1	-	Total Phosphor	mg/L	2.90	-	2.80	5.01			
<b>Dissolved Metals</b>																											
59	< 1.0	< 5.0	49	58	Dissolved Alumin	µg/L	156	< 5.0	78.3	78.3	180	180	81.6	81.6	72.4	72.4	168	168	Dissolved Alumin	µg/L	40.7	40.7	32.7	105			
84.6	58.7	113	89.8	96.8	Dissolved Calc	mg/L	66.2	69.3	83.0	83	54.6	54.6	57.9	57.9	83.1	83.1	50.6	50.6	Dissolved Calc	mg/L	95.4	95.4	104	7.95			
59	130	122	84	< 90	Dissolved Iron	µg/L	53	61	97	97	63	63	48	48	53	53	62	62	Dissolved Iron	µg/L	78.3	78.3	153	58.3			
236	149	291	262	270	Dissolved Magn	mg/L	305	136	205	205	257	257	204	204	232	232	215	215	Dissolved Magn	mg/L	272	272	293	157			
494	90	493	355	411	Dissolved Mangan	µg/L	317	157	316	305	196	196	157	157	316	316	154	154	Dissolved Mangan	µg/L	369	369	580	157			
182	31.6	177	243	177	Dissolved Potas	mg/L	253	16.7	151	151	307	307	134	134	158	158	251	251	Dissolved Potas	mg/L	146	146	138	166			
1,580	308	1,760	2,020	1,700	Dissolved Soda	mg/L	1,700	3,250	1,300	1,300	4,180	4,180	1,860	1,860	1,720	1,720	4,200	4,200	Dissolved Soda	mg/L	1,660	1,660	1,410	510			
7.85	0.73	12.3	9.3	8.5	Antimony	µg/L	4.66	< 0.20	9.61	9.61	25.1	25.1	6.91	6.91	6.92	6.92	11.2	11.2	Antimony	µg/L	9.63	9.63	7.85	10.8			
21.8	2.8	17.2	23.4	23.2	Arsenic	µg/L	15.8	1.15	25.8	25.8	89.9	89.9	20.8	20.8	19.8	19.8	34.5	34.5	Arsenic	µg/L	35.4	35.4	21.3	46.1			
151	97	308	234	233	Barium	mg/L	172	78.9	205	205	142	142	85.7	85.7	159	159	156	156	Barium	mg/L	232	232	228	86.6			
< 1.0	< 0.20	< 1.0	< 1.0	< 1.0	Beryllium	µg/L	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	Beryllium	µg/L	0.024	0.024	0.017	< 0.010			
1.650	330	1.680	2.080	1.520	Boron	µg/L	1,930	28.0	1,350	1,350	1,740	1,740	978	978	1,240	1,240	2,280	2,280	Boron	µg/L	1,180	1,180	1,290	135			
< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	Cadmium	µg/L	< 0.025	0.015	0.011	0.011	0.012	0.012	0.013	0.013	< 0.010	< 0.010	0.014	0.014	Cadmium	µg/L	0.0053	0.0053	0.0036	0.0088			
16.1	3.14	17	22.5	12.8	Chromium	µg/L	26.5	2.83	15.7	15.7	45.7	45.7	14.3	14.3	15.3	15.3	47.8	47.8	Chromium	µg/L	18.0	18	13.8	18.6			
6.57	0.84	8.5	11.5	9.2	Cobalt	µg/L	5	0.12	3.88	3.88	5.46	5.46	2.14	2.14	4.59	4.59	5.77	5.77	Cobalt	µg/L	6.60	6.6	7.21	2.56			
< 1.0	< 1.0	< 2.0	< 2.0	< 2.0	Copper	µg/L	2	1.09	< 0.40	< 0.40	< 0.40	< 0.40	0.88	0.88	0.43	0.43	0.41	0.41	Copper	µg/L	0.22	0.22	0.33	0.97			
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Lead	µg/L	< 0.25	< 0.20	< 0.20	< 0.20	< 0.22	< 0.22	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	Lead	µg/L	< 0.050	< 0.050	< 0.050	< 0.050			
< 50	< 50	52	< 50	52	Lithium	µg/L	65.8	36.9	54.6	54.6	49.2	49.2	55.4	55.4	48.8	48.8	64.5	64.5	Lithium	µg/L	53.7	53.7	45.4	4.24			
< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	Mercury	µg/L	< 0.25	< 0.010	< 0.010	< 0.010	< 0.200	< 0.200	< 0.100	< 0.100	< 0.010	< 0.010	< 0.010	< 0.010	Mercury	µg/L	< 0.010	< 0.010	< 0.010	< 0.010			
2.5	13.4	3.190	3.160	1.8	Molybdenum	µg/L	2.33	19.8	2	2	5.33	5.33	7.18	7.18	3.32	3.32	5.48	5.48	Molybdenum	µg/L	4.49	4.49	1.82	3.68			
21.8	< 5.0	19.7	25.5	18	Nickel	µg/L	21.5	1.02	21.8	21.8	33.8	33.8	13.2	13.2	16.6	16.6	33.1	33.1	Nickel	µg/L	18.7	18.7	19.3	16.1			
11.4	5	< 1.0	3.64	11.8	Selenium	µg/L	14.4	7.41	2.58	2.58	1.35	1.35	2.42	2.42	0.96	0.96	20.7	20.7	Selenium	µg/L	0.83	0.83	0.66	1.29			
< 0.050	< 0.050	< 0.10	< 0.10	< 0.10	Silver	µg/L	< 0.078	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	Silver	µg/L	< 0.078	< 0.050	< 0.050	< 0.050			
< 0.050	< 0.010	< 0.10	< 0.10	< 0.10	Thallium	µg/L	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	< 0.020	Thallium	µg/L	< 0.040	< 0.040	< 0.040	< 0.040			
< 50	< 50	< 50	40.4	59	Titanium	µg/L	60.1	< 1.0	40.4	40.4	116	116	30.4	30.4	45.2	45.2	118	118	Titanium	µg/L	52.0	52	46.6	44.1			
8.59	33.3	54.3	67	-	Tungsten	µg/L	< 1.0	2.3	-	-	4.8	-	1.8	-	2.4	-	4.9	-	Tungsten	µg/L	2.19	-	1.78	0.39			
< 60	< 30	< 60	< 60	< 60	Uranium	µg/L	14.2	39.5	25	25	37.2	37.2	33.3	33.3	16.8	16.8	26.2	26.2	Uranium	µg/L	13.7	13.7	8.87	2.15			
< 10	< 5.0	< 10	< 10	< 10	Zinc	µg/L	19.1	3.3	13.0	13	27.6	27.6	8.5	8.5	11.8	11.8	24.1	24.1	Zinc	µg/L	12.0	12	9.97	14.9			
< 400	< 200	< 400	< 400	< 600	Bismuth	µg/L	< 0.25	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	< 0.10	Bismuth	µg/L	< 0.010	< 0.010	< 0.010	< 0.010			
3,180	300	3,190	3,160	3,410	Phosphorus	µg/L	8,100	158	4,380	4,380	9,460	9,460	4,530	4,530	4,100	4,100	9,920	9,920	Phosphorus	µg/L	18,500	18,500	16,500	12,600			
12,700	10,100	16,700	16,200	14,500	Silicon	µg/L	13,100	10,700	14,200	14,200	14,700	14,700	10,300	10,300	13,500	13,500	15,600	15,600	Silicon	µg/L	18,500	18,500	16,500	12,600			
2,660	2,670	3,960	3,100	3,400	Strontium	µg/L	2,800	3,160	3,480	3,480	2,510	2,510	2,320	2,320	3,410	3,410	2,440	2,440	Strontium	µg/L	4,220	4,220	4,120	2,250			

Table 5: Historical Summary of Analytical Results For Leachate

N Pumphouse MH						P1 Leachate MH					Sample Location					P1 Leachate MH					
N Pumphouse MH	N Pumphouse MH	N Pumphouse MH	N Pumphouse MH	N Pumphouse MH	N Pumphouse MH	Landfill Leachate 20061109	Landfill Leachate 20061116	Landfill Leachate 20061122	P1 LEACHATE MH-20130911	P1 LEACHATE MH-20140408	P1 LEACHATE MH-20140610	P1 LEACHATE MH-20150122	P1 LEACHATE MH-20150615	Sample ID	P1 LEACHATE MH-20150915	P1 LEACHATE MH-20151203	P1 LEACHATE MH-20160315	P1 LEACHATE MH-20160623	P1 LEACHATE MH-20160915	P1 LEACHATE MH-20161117	P1 LEACHATE MH-20170914
2020 09 30	2020 11 16	2021 03 18	2021 06 17	2021 09 16	2021 10 22	2006 11 09	2006 11 16	2006 11 22	2013 09 11	2014 04 08	2014 06 10	2015 01 22	2015 06 15	Sample Date (yyyy mm dd)	2015 09 15	2015 12 03	2016 03 15	2016 06 23	2016 09 15	2016 11 17	2017 09 14
Analytical Results																					
Parameter													Units								
Dissolved Inorganics													Analytical Results								
101,000	29,800	37,300	56,500	70,600	32,000	-	-	-	102,000	82,000	73,700	23,900	78,300	Ammonia Total (d)	91,500	78,200	58,300	17,300	18,400	71,100	74,300
< 100	1,240	1,950	< 100	< 100	< 100	-	-	-	< 250	< 250	< 250	< 100	< 250	Nitrate (as N)	< 250	< 250	< 250	4,060	170	< 250	< 250
< 100	< 100	5,110	< 100	< 100	< 100	-	-	-	-	-	-	-	-	Nitrite (as N)	µg/L	-	-	-	-	-	-
605	369	548	518	704	362	-	-	-	445	319	304	355	350	Chloride	mg/L	389	306	435	219	246	392
< 1,000	< 1,000	< 1,000	< 1,000	< 1,000	< 1,000	-	-	-	1,000	1,400	1,530	1,000	1,600	Fluoride	µg/L	1,200	1,200	< 1,000	1,100	1,230	1,400
1,200	813	1,430	1,360	1,620	834	-	-	-	448	878	784	374	899	Sulfate	mg/L	1,170	890	753	443	404	882
4,280	3,350	4,080	4,540	5,950	2,530	-	-	-	-	4,020	4,950	1,510	4,270	Total Alkalinity	mg/L	4,410	3,910	3,030	1,070	1,300	3,690
< 1.0	8.7	< 1.0	< 1.0	292	< 1.0	-	-	-	-	-	-	< 1.0	-	Alkalinity, Bicarb	mg/L	4,410	3,910	3,030	-	-	-
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	-	-	-	-	-	-	< 1.0	-	Alkalinity, Carbon	mg/L	< 1.0	< 1.0	< 1.0	-	-	-
< 1.0	4.3	< 1.0	< 1.0	166	< 1.0	-	-	-	-	-	-	< 1.0	-	Alkalinity, Hydroxi	mg/L	< 1.0	< 1.0	< 1.0	-	-	-
< 10.0	2.56	< 10.0	1.16	< 10.0	< 10.0	-	-	-	2.8	3.4	3.1	< 1.0	2.8	Alkalinity, Phenol	mg/L	3.9	< 2.5	2.6	< 1.0	1	3.3
73.3	82.3	70.5	51.7	89.2	11.6	-	-	-	-	-	-	-	-	Bromide	mg/L	-	-	-	-	-	-
289	334	88.0	64.0	200	34.0	-	-	-	-	-	-	-	-	Sulfide	mg/L	-	-	-	-	-	-
789	490	472	562	653	198	-	-	-	413	433	353	117	336	Biochemical Oxy	mg/L	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-	-	-	-	-	Chemical Oxygen	mg/L	405	288	411	71	100	319
2.96	2.67	2.04	0.847	4.00	0.923	-	-	-	2.34	3.27	3.94	0.43	3.32	Phosphate	mg/L	3.26	3.32	0.503	0.27	0.502	0.319
-	-	-	-	-	-	-	-	-	114	-	-	-	-	Ortho-Phosphate	mg/L	-	-	-	-	-	-
5.27	3.73	4.39	4.53	5.39	2.12	-	-	-	-	-	-	-	-	Total Organic Car	mg/L	-	-	-	-	-	-
-	-	-	-	-	-	-	-	-	-	-	-	-	-	Total Phosphoru	mg/L	-	-	-	-	-	-
Dissolved Metals													Analytical Results								
60.7	116	70.1	160	68.1	61.3	-	-	-	41	22	13	29	29	Dissolved Alumin	µg/L	659	32	55	< 10	16	47
103	43.8	77.4	125	92.6	103	-	-	-	89.4	107	99.9	100	107	Dissolved Calcium	µg/L	102	97.9	124	83.2	85	84.3
33.8	< 200	69.4	< 200	119	51.8	-	-	-	665	65	1,630	< 90	1,630	Dissolved Calcium	µg/L	100	156	224	92	278	90
334	135	197	209	183	302	-	-	-	301	389	186	304	304	Dissolved Magnesi	mg/L	389	384	203	156	172	336
490	101	211	253	313	273	-	-	-	442	475	636	440	440	Dissolved Mangan	µg/L	419	505	860	215	650	473
161	132	138	222	120	129	-	-	-	-	-	-	-	-	Dissolved Potassi	mg/L	160	113	125	43.9	51.4	125
1,810	1,950	1,860	2,170	1,680	1,620	-	-	-	1,580	1,730	541	1,530	1,530	Dissolved Sodium	µg/L	1,890	1,500	1,090	419	490	1,670
11.1	17.3	14.0	12.8	15.8	18.8	-	-	-	2.43	1.35	< 0.50	1.4	1.4	Antimony	µg/L	< 0.50	1.52	2.84	< 0.50	1.9	5.2
31.2	41.8	53.8	33.8	43.8	43.4	-	-	-	10.1	6.7	1.4	7	7	Arsenic	µg/L	1.1	6.8	12.6	2.1	2.4	4.2
204	79.5	111	127	134	176	-	-	-	316	401	130	261	261	Barium	µg/L	304	330	145	92	108	254
0.024	< 1.00	0.024	< 1.00	0.023	0.024	-	-	-	< 10	< 10	< 5.0	< 15	< 15	Beryllium	µg/L	< 15	< 10	< 10	< 5.0	< 10	< 15
1.510	1.140	1.300	1.990	1.230	1.290	-	-	-	1.480	1.400	540	1.360	1.360	Boron	µg/L	1.370	1.040	1.170	360	460	1.390
0.0038	< 0.200	0.0056	< 0.200	0.0075	0.0068	-	-	-	< 0.25	< 0.25	< 0.10	< 0.050	< 0.050	Cadmium	µg/L	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050	< 0.050
21.4	18.7	16.7	17.8	19.0	17.1	-	-	-	12.3	10.3	2.9	11.3	11.3	Chromium	µg/L	1.33	9.24	11.1	1.73	2.02	9.5
6.72	2.56	2.82	4.39	3.35	5.49	-	-	-	6.82	6.66	1.54	6.2	6.2	Cobalt	µg/L	1.21	4.68	4.62	1.5	1.98	6.6
0.60	< 10.0	0.48	< 10.0	0.27	0.39	-	-	-	< 2.5	< 2.5	< 1.0	< 2.0	< 2.0	Copper	µg/L	6	< 1.0	< 1.0	3.5	1.4	< 2.0
< 0.050	< 5.00	< 0.050	< 5.00	< 0.050	< 0.050	-	-	-	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Lead	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0
57.8	35.5	54.3	69.5	52.9	75.5	-	-	-	< 50	< 50	< 50	< 50	< 50	Lithium	µg/L	< 50	< 50	< 50	< 50	< 50	< 50
< 0.010	< 0.010	< 0.020	< 0.010	< 0.040	< 0.030	-	-	-	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	Mercury	µg/L	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20	< 0.20
3.24	5.48	8.35	2.88	10.4	6.88	-	-	-	2.7	2.1	< 1.0	1.6	1.6	Molybdenum	µg/L	11.1	1.5	1.8	15.3	3.6	2.1
20.2	15.9	15.4	21.2	14.1	16.8	-	-	-	15.6	10.3	6.9	12.7	12.7	Nickel	µg/L	< 5.0	11.7	14.8	9	12.8	11.3
1.63	< 10.0	2.12	< 10.0	2.12	2.61	-	-	-	< 5.0	< 5.0	< 2.0	< 1.0	< 1.0	Selenium	µg/L	< 1.0	4.4	6.6	3.3	< 1.0	< 0.50-1.0
< 0.010	< 1.00	< 0.010	< 1.00	< 0.010	0.086	-	-	-	< 0.02	< 0.02	< 0.02	< 0.02	< 0.02	Silver	µg/L	< 0.050	0.096	< 0.050	< 0.050	< 0.050	< 0.10
< 0.0040	< 0.400	< 0.0040	< 0.400	< 0.0040	< 0.0040	-	-	-	< 0.50	< 0.50	< 0.20	< 0.10	< 0.10	Thallium	µg/L	< 0.050	< 0.050	< 0.020	< 0.020	< 0.10	< 0.10
48.0	49.6	37.8	64.0	50.7	38.9	-	-	-	61	57	< 50	< 50	< 50	Titanium	µg/L	58	< 50	< 50	< 50	< 50	< 50
2.24	< 20.0	1.68	< 20.0	2.03	1.69	-	-	-	-	-	-	-	-	Tungsten	µg/L	-	-	-	-	-	-
14.2	13.3	25.2	16.8	24.5	19.7	-	-	-	11.5	3.9	5.86	6.22	6.22	Uranium	µg/L	1.71	10.1	29.1	81.3	8.91	6.64
9.96	< 20.0	9.46	< 20.0	10.2	10.0	-	-	-	< 60	< 60	< 30	< 90	< 90	Vanadium	µg/L	< 60	< 60	< 30	< 30	< 60	< 90
1.3	< 100	< 1.0	< 100	< 1.0	1.6	-	-	-	< 10	< 10	< 15	< 10	< 10	Zinc	µg/L	< 10	< 10	< 5.0	< 5.0	< 10	25
< 0.010	< 1.00	< 0.010	< 1.00	< 0.010	< 0.010	-	-	-	-	-	-	-	-	Bismuth	µg/L	< 600	< 400	< 400	< 200	< 400	< 600
4,110	4,070	4,720	4,380	4,740	4,740	-	-	-	-	-	-	-	-	Phosphorous	µg/L	3,710	3,610	2,050	< 300	580	3,570
16,500	5,810	13,800	5,880	12,400	16,700	-	-	-	-	-	-	-	-	Silicon	µg/L	17,500	16,800	13,800	13,000	14,200	16,800
3,540	1,600	3,120	2,870	2,860	4,350	-	-	-	-	-	-	-	-	Strontium	µg/L	4,220	3,900	2,640	2,500	4,050	3,910
407,000	519,000	444,000	631,000	344,000	462,000	-	-	-	-	-	-	-	308,000	Sulfur	µg/L	377,000	840,000	247,000	142,000	134,000	280,000
0.067	< 0.00	0.065	7.03	0.090	0.145	-	-	-	-	-	-	-	-	Tellurium	µg/L	< 0.20	< 1.0	< 1.0	< 0.40	-	< 2.0
0.019	< 1.00	0.020	< 1.00	0.015	0.017	-	-	-	-	-	-	-	< 1.0	Thorium	µg/L	0.16	< 0.50	< 0.50	< 0.20	-	< 1.0
6.33	41.8	27.5	38.7	26.3	20.1	-	-	-	-	-	-	-	-	Tin	µg/L	< 60	< 60	< 30	< 30	< 60	< 90
22.5	11.2	15.0	15.6	17.9	23.3	-	-	-	-	-	-	-	32.9	Zincium	µg/L	3	36.9	13.1	4	-	31
Monocyclic Aromatic Hydrocarbons													Analytical Results								
4.6	3.7	4.6	6.9	8.4	1.6	4	4	4	3.08	1.76	1.69	-	1.29	Benzene	µg/L	1.88	1.28	2.4	-	-	1.3
42.7	43.1	53.5	48.1	64.1	11.7	42	48	40	9.49	9.32	3.15	-	1.7	Ethylbenzene	µg/L	3.84	3.73	11.9	-	-	1.65
2.2	1.4	2.6	1.8	< 1.0	1.8	1	1	1	1	1.8	0.66	-	12.8	Toluene	µg/L	< 0.50	< 0.50	0.69	-	-	0.9







Table 5: Historical Summary of Analytical Results For Leachate

Sample Location					P2 A2 Leachate MH					
S Leachate Wet Well	S Leachate Wet Well	S Leachate Wet Well	S Leachate Wet Well	S Leachate Wet Well	Sample ID	P2 A2 Leachate MH	P2 A2 Leachate MH	P2 A2 Leachate MH	P2 A2 Leachate MH	
2020 11 16	2021 03 18	2021 06 17	2021 09 15	2021 10 22	Sample Date (yyyy mm dd)	2021 03 19	2021 06 18	2021 09 16	2021 10 21	
Parameter					Units					
Analytical Results					Analytical Results					
<b>Dissolved Inorganics</b>										
66,400	35,500	50,300	59,900	71,800	Ammonia, Total (d	µg/L	81,400	127,000	161,000	155,000
< 100	3,260	16,600	21,400	< 100	Nitrate (as N)	µg/L	< 100	221	< 100	388
< 100	961	7,970	20,000	10,300	Nitrite (as N)	µg/L	< 100	< 100	< 1,000	< 100
834	620	995	788	792	Chloride	mg/L	1,030	830	1,150	1,310
< 1,000	< 1,000	< 1,000	< 1,000	< 1,000	Fluoride	µg/L	< 1,000	< 1,000	< 1,000	< 1,000
1,800	1,540	1,410	1,730	1,710	Sulfate	mg/L	345	305	115	145
5,940	4,250	4,880	6,670	7,230	Total Alkalinity	mg/L	2,940	3,390	4,450	4,470
5,680	3,910	4,380	5,770	6,070	Alkalinity, Bicarbonate	mg/L	2,940	3,390	4,450	4,470
263	321	306	893	1,220	Alkalinity, Carbonate	mg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Alkalinity, Hydroxide	mg/L	< 1.0	< 1.0	< 1.0	< 1.0
131	161	153	446	612	Alkalinity, Phenolic	mg/L	< 1.0	< 1.0	< 1.0	< 1.0
5.60	< 10.0	1.31	< 1.00	< 10.0	Bromide	mg/L	13.6	73.4	70.5	< 10.0
250	114	71.1	85.5	219	Sulfide	mg/L	0.114	1.80	3.41	2.49
469	178	123	351	605	Biochemical Oxygen Demand	mg/L	1,270	3,260	3,160	< 34268.8
859	564	642	856	794	Chemical Oxygen Demand	mg/L	1,870	6,460	4,690	844
+	+	+	+	+	Phosphate	mg/L	+	+	+	+
6.14	2.19	1.25	5.13	5.19	Ortho-Phosphate	mg/L	< 0.0500	< 0.0500	< 0.0500	< 0.0500
+	+	+	+	+	Total Organic Carbon	mg/L	+	+	+	+
7.84	5.03	6.07	6.66	7.70	Total Phosphorus	mg/L	3.19	5.79	4.42	1.66
<b>Dissolved Metals</b>										
196	114	160	298	126	Dissolved Aluminum	µg/L	42.8	56.8	34.6	153
80.3	56.6	141	120	129	Dissolved Calcium	mg/L	280	675	525	163
< 200	36.4	< 200	< 200	29.3	Dissolved Iron	µg/L	8,890	37,900	85,300	9,300
229	195	235	262	249	Dissolved Magnesium	mg/L	401	322	421	410
200	137	382	206	204	Dissolved Manganese	µg/L	4,990	20,800	21,900	671
271	208	222	283	221	Dissolved Potassium	mg/L	228	186	205	222
4,000	2,810	2,100	4,010	4,370	Dissolved Sodium	mg/L	1,270	927	1,070	1,380
37.3	14.2	13.4	39.2	32.9	Antimony	µg/L	4.20	9.73	4.10	< 5.00
81.4	79.4	32.7	95.5	95.0	Arsenic	µg/L	20.7	16.8	55.8	64.1
145	90.8	153	175	156	Barium	µg/L	380	924	1,240	1,830
< 1.00	0.031	1.72	< 1.00	0.053	Beryllium	µg/L	0.017	0.013	0.016	< 1.00
2,340	1,660	1,930	2,420	2,040	Boron	µg/L	5,170	7,330	6,100	4,710
< 0.200	0.0046	< 0.200	< 0.200	0.0082	Cadmium	µg/L	0.116	0.0198	0.0253	< 0.200
41.7	24.7	18.1	46.7	42.1	Chromium	µg/L	25.9	51.0	23.5	15.0
5.11	3.14	5.29	6.37	6.88	Cobalt	µg/L	61.9	157	31.6	15.8
< 10.0	0.42	27.1	< 10.0	0.68	Copper	µg/L	3.66	0.64	1.13	< 10.0
< 5.00	0.092	< 5.00	< 5.00	0.087	Lead	µg/L	0.370	< 0.050	0.130	< 5.00
85.9	64.6	68.1	74.6	82.8	Lithium	µg/L	38.9	65.0	37.7	29.5
< 0.010	< 0.040	< 0.040	< 0.040	0.020	Mercury	µg/L	< 0.010	< 0.040	< 0.040	< 0.020
5.63	4.27	3.78	5.92	4.09	Molybdenum	µg/L	60.7	4.43	6.46	5.25
31.0	17.6	23.0	25.3	27.1	Nickel	µg/L	305	356	149	183
122	1.07	< 10.0	< 10.0	1.13	Selenium	µg/L	3.97	2.37	2.12	< 10.0
< 1.00	< 0.010	< 1.00	< 1.00	0.010	Silver	µg/L	0.012	< 0.010	0.013	< 1.00
< 0.400	< 0.0040	< 0.400	< 0.400	< 0.0040	Thallium	µg/L	< 0.0040	< 0.0040	< 0.0040	< 0.400
98.8	52.3	38.0	75.2	67.3	Titanium	µg/L	19.1	5.49	22.8	30.3
< 20.0	2.54	< 20.0	< 20.0	4.65	Tungsten	µg/L	2.23	0.96	2.86	< 20.0
17.8	15.7	18.3	12.0	8.94	Uranium	µg/L	12.6	3.07	2.73	3.58
< 20.0	13.9	< 20.0	< 20.0	17.1	Vanadium	µg/L	18.3	7.39	36.0	39.7
< 100	1.1	< 100	< 100	1.2	Zinc	µg/L	15.7	15.1	13.2	< 100
< 1.00	0.013	< 1.00	< 1.00	0.010	Bismuth	µg/L	< 0.010	< 0.010	< 0.010	< 1.00
8,340	7,230	5,280	9,840	8,750	Phosphorus	µg/L	791	655	7,560	1,600
13,700	12,100	< 5,000	14,100	15,200	Silicon	µg/L	28,600	51,600	38,400	36,000
2,420	2,130	3,030	2,950	3,320	Strontium	µg/L	7,100	6,710	7,670	7,600
882,000	892,000	555,000	792,000	1,010,000	Sulfur	µg/L	140,000	121,000	49,600	58,000
< 5.00	< 0.050	13.7	< 5.00	0.169	Tellurium	µg/L	0.258	0.265	0.271	< 5.00
< 1.00	0.024	< 1.00	< 1.00	0.020	Thorium	µg/L	0.018	< 0.010	0.018	< 1.00
83.6	34.6	17.5	127	80.1	Tin	µg/L	1.89	1.41	2.00	< 5.00
30.9	20.3	17.6	37.4	43.9	Zirconium	µg/L	81.8	5.82	77.5	95.2
<b>Monocyclic Aromatic Hydrocarbons</b>										
7.9	6.3	8.0	9.5	7.4	Benzene	µg/L	0.8	1.2	3.1	0.7
103	56.3	56.0	114	97.3	Ethylbenzene	µg/L	< 1.0	3.1	9.1	2.1
2.4	1.9	1.5	2.1	1.1	Toluene	µg/L	17.4	64.6	61.5	6.3
77.8	51.4	44.0	80.2	66.7	Xylenes	µg/L	5.5	11.4	20.3	2.8
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Styrene	µg/L	2.3	3.5	2.3	< 1.0
<b>Polycyclic Aromatic Hydrocarbons</b>										
5.43	3.06	2.47	6.43	3.57	Naphthalene	µg/L	< 0.200	0.525	< 2.09	< 1.97
0.838	0.549	0.598	1.19	< 1.09	Methyl-naphthalene	µg/L	< 0.100	< 0.100	1.05	< 0.883
0.471	0.247	< 0.458	0.439	< 1.09	Methyl-naphthalene	µg/L	< 0.100	0.109	< 1.05	< 0.583
< 0.200	< 0.200	< 0.895	< 0.200	< 2.18	Acenaphthylene	µg/L	< 0.200	< 0.200	< 2.09	< 1.97
0.354	0.229	0.265	0.503	< 0.545	Acenaphthene	µg/L	< 0.050	< 0.050	< 0.524	< 0.491
0.229	0.179	< 0.249	0.324	< 0.545	Fluorene	µg/L	< 0.050	< 0.050	< 0.524	< 0.491
0.340	0.266	< 0.458	0.422	< 1.09	Phenanthrene	µg/L	< 0.100	< 0.100	< 1.05	< 0.883
0.037	0.019	< 0.050	0.026	< 0.109	Anthracene	µg/L	< 0.010	< 0.038	< 0.105	< 0.058
< 0.050	< 0.050	< 0.249	< 0.050	< 0.545	Acridine	µg/L	< 0.050	0.539	< 0.524	< 0.491
0.110	0.077	< 0.149	0.111	< 0.227	Fluoranthene	µg/L	< 0.050	< 0.050	< 0.514	< 0.295
0.091	0.071	< 0.100	0.079	< 0.218	Pyrene	µg/L	< 0.020	0.045	< 0.208	< 0.197
0.021	< 0.010	< 0.050	< 0.010	< 0.109	Benzo(a)anthracene	µg/L	< 0.010	< 0.039	< 0.105	< 0.058
< 0.050	< 0.050	< 0.249	< 0.050	< 0.545	Chrysene	µg/L	< 0.050	0.057	< 0.524	< 0.491
0.057	< 0.050	< 0.249	< 0.050	< 0.545	Benzo(b)fluoranthene	µg/L	< 0.050	< 0.150	< 0.524	< 0.491
< 0.050	< 0.050	< 0.249	< 0.050	< 0.545	Benzo(k)fluoranthene	µg/L	< 0.050	0.076	< 0.524	< 0.491
< 0.010	< 0.010	< 0.050	< 0.010	< 0.109	Benzo(a)pyrene	µg/L	< 0.010	0.064	< 0.105	< 0.098
< 0.050	< 0.050	< 0.249	< 0.050	< 0.545	Indeno(1,2,3-cd)pyrene	µg/L	< 0.050	0.105	< 0.524	< 0.491
< 0.010	< 0.010	< 0.050	< 0.010	< 0.109	Dibenz(a,h)anthracene	µg/L	< 0.010	0.095	< 0.105	< 0.098
< 0.050	< 0.050	< 0.249	< 0.050	< 0.545	Benzo(g,h,i)perylene	µg/L	< 0.050	0.116	< 0.524	< 0.491
< 0.100	< 0.100	< 0.498	< 0.100	< 1.09	Chloronaphthalene	µg/L	< 0.100	< 0.100	< 1.05	< 0.983
< 0.050	< 0.050	< 0.249	< 0.050	< 0.545	Quinoline	µg/L	< 0.264	< 0.778	1.19	< 0.491
<b>Volatile Organic Compounds</b>										
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Bromodichloromethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Bromoform	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	Carbon Tetrachloride	µg/L	< 0.5	< 0.5	< 0.5	< 0.5
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Chlorobenzene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0

Table 5: Historical Summary of Analytical Results For Leachate

Sample Location		N Pumphouse MH												Sample Location		N Pumphouse MH					
Sample ID	LEACHATE- MANNHOLE- 20130312	N Pumphouse MH-20080205	N Pumphouse MH-20080219	N Pumphouse MH-20080304	N Pumphouse MH-20080325	N Pumphouse MH-20080408	N Pumphouse MH-20080424	N Pumphouse MH-20080507	N Pumphouse MH-20080521	N Pumphouse MH-20080617	N Pumphouse MH-20080626	N Pumphouse MH-20080708	Sample ID	N Pumphouse MH-20131211	N Pumphouse MH-20140408	N Pumphouse MH-20140610	N Pumphouse MH-20150122	N Pumphouse MH-20150615	N Pumphouse MH-20150915	N Pumphouse MH-20151203	
Parameter	Sample Date (yyyy mm dd)	2013 02 05	2008 02 19	2008 03 04	2008 03 25	2008 04 08	2008 04 24	2008 05 07	2008 05 21	2008 06 17	2008 06 26	2008 07 08	Parameter	Sample Date (yyyy mm dd)	2013 12 11	2014 04 08	2014 06 10	2015 01 22	2015 06 15	2015 09 15	2015 12 03
Units													Units								
<b>Volatiles Organic Compounds Cont.</b>																					
Chloroethane	µg/L	9.7	20	10	30	20	< 10	20	20	20	20	10	Chloroethane	µg/L	6.3	1.3	-	-	6	6	4.3
Chloroform	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Chloroform	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Chloromethane	µg/L	< 5.0	< 10	< 10	< 10	< 10	< 10	< 10	< 10	< 10	< 10	< 10	Chloromethane	µg/L	< 5.0	< 5.0	-	-	< 5.0	< 5.0	< 5.0
Dibromochloromethane [DBCM]	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dibromochloromethane [DBCM]	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dibromoethane, 1,2-	µg/L	-	-	-	-	-	-	-	-	-	-	-	Dibromoethane, 1,2-	µg/L	-	-	-	-	-	-	-
Dibromomethane	µg/L	-	-	-	-	-	-	-	-	-	-	-	Dibromomethane	µg/L	-	-	-	-	-	-	-
Dichlorobenzene, 1,2-	µg/L	< 0.70	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichlorobenzene, 1,2-	µg/L	< 0.70	< 0.70	-	-	< 0.70	< 0.70	< 0.70
Dichlorobenzene, 1,3-	µg/L	< 1.0	1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichlorobenzene, 1,3-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dichlorobenzene, 1,4-	µg/L	1.1	< 1	1	1	1	1	< 1	< 1	1	1	1	Dichlorobenzene, 1,4-	µg/L	1.5	< 1.0	-	-	1.1	1.2	1.1
Dichloroethane, 1,1-	µg/L	17.6	13	12	13	12	11	11	15	15	19	21	Dichloroethane, 1,1-	µg/L	16.2	1.5	-	-	12.4	3.4	8.4
Dichloroethane, 1,2-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichloroethane, 1,2-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dichloroethylene, 1,1-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichloroethylene, 1,1-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dichloroethylene, 1,2-cis-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichloroethylene, 1,2-cis-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dichloroethylene, 1,2-trans-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichloroethylene, 1,2-trans-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dichloromethane	µg/L	< 5.0	< 5	< 5	< 5	< 5	< 5	< 5	< 5	< 5	< 5	< 5	Dichloromethane	µg/L	< 5.0	< 5.0	-	-	< 5.0	< 5.0	< 5.0
Dichloropropane, 1,2-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichloropropane, 1,2-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dichloropropane, 1,3- (cis+trans)	µg/L	< 1.4	-	-	-	-	-	-	-	-	-	-	Dichloropropane, 1,3- (cis+trans)	µg/L	< 1.4	< 1.4	-	-	< 1.4	< 1.4	< 1.4
Dichloropropane, 1,3-cis-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichloropropane, 1,3-cis-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Dichloropropane, 1,3-trans-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Dichloropropane, 1,3-trans-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Tetrachloroethane, 1,1,1,2-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Tetrachloroethane, 1,1,1,2-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Tetrachloroethane, 1,1,2,2-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Tetrachloroethane, 1,1,2,2-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Tetrachloroethylene	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Tetrachloroethylene	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Trichloroethane, 1,1,1-	µg/L	< 1.0	8	5	5	5	5	5	5	5	5	5	Trichloroethane, 1,1,1-	µg/L	1.6	< 1.0	-	-	1.6	1.1	< 1.0
Trichloroethane, 1,1,2-	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Trichloroethane, 1,1,2-	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Trichloroethylene	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Trichloroethylene	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Trichlorofluoromethane	µg/L	< 1.0	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	< 1	Trichlorofluoromethane	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
Vinyl Chloride	µg/L	< 1.0	< 2	< 2	< 2	< 2	< 2	< 2	< 2	< 2	< 2	< 2	Vinyl Chloride	µg/L	< 1.0	< 1.0	-	-	< 1.0	< 1.0	< 1.0
<b>Gross Parameters</b>																					
VH (C6-C10)	µg/L	-	-	-	-	-	-	-	-	-	-	-	VH (C6-C10)	µg/L	-	< 100	< 100	-	< 100	< 100	< 100
VPH (C6-C10)	µg/L	-	-	-	-	-	-	-	-	-	-	-	VPH (C6-C10)	µg/L	-	< 100	< 100	-	< 100	< 100	< 100
EPH (C10-C19)	µg/L	-	-	-	-	-	-	-	-	-	-	-	EPH (C10-C19)	µg/L	-	1,110	1,160	850	< 250	260	310
LEPH (C10-C19)	µg/L	-	-	-	-	-	-	-	-	-	-	-	LEPH (C10-C19)	µg/L	-	1,110	1,170	850	< 250	250	310
EPH (C18-C32)	µg/L	-	-	-	-	-	-	-	-	-	-	-	EPH (C18-C32)	µg/L	-	640	850	720	< 250	< 250	< 250
HEPH (C18-C32)	µg/L	-	-	-	-	-	-	-	-	-	-	-	HEPH (C18-C32)	µg/L	-	640	850	720	< 250	< 250	< 250
<b>MTBE</b>																					
Methyl Tert-butyl Ether [MTBE]	µg/L	-	-	-	-	-	-	-	-	-	-	-	Methyl Tert-butyl Ether [MTBE]	µg/L	-	-	-	-	-	-	-
<b>Resin and Fatty Acids</b>																					
Acetic Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Acetic Acid	mg/L	-	-	-	-	-	-	-
Butyric Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Butyric Acid	mg/L	-	-	-	-	-	-	-
Caproic Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Caproic Acid	mg/L	-	-	-	-	-	-	-
Heptanoic Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Heptanoic Acid	mg/L	-	-	-	-	-	-	-
Isobutyric Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Isobutyric Acid	mg/L	-	-	-	-	-	-	-
Isocaproic Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Isocaproic Acid	mg/L	-	-	-	-	-	-	-
Isovaleric Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Isovaleric Acid	mg/L	-	-	-	-	-	-	-
Propionic Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Propionic Acid	mg/L	-	-	-	-	-	-	-
Valeric Acid	mg/L	-	-	-	-	-	-	-	-	-	-	-	Valeric Acid	mg/L	-	-	-	-	-	-	-

Associated CARO file(s): 8031228, 8052345, 8081555, 8110837, 9031248, 9060275, 9090105, mg/L, N000833, up/L.  
 Associated Exova file(s): 506479, 507801, 509233, 600276, 602695, 605369, 608922, 611891, 614770, 617175, 619614, 625680, 627511, 629501.  
 All terms defined within the body of Keltech's report.  
 - Denotes concentration less than indicated detection limit or RPD less than indicated value.  
 - Denotes analysis not conducted.  
 n/a Denotes no applicable standard/guideline.  
 QA/QC RPD Denotes quality assurance/quality control relative percent difference.  
 \* RPDs are not calculated where one or more concentrations are less than five times RDL.  
 RDL Denotes reported detection limit.

Table 5: Historical Summary of Analytical Results For Leachate

Sample Location					N Pumphouse MH										Sample Location											
N PUMPHOUSE MH-20160315	N PUMPHOUSE MH-20160623	N PUMPHOUSE MH-20160915	N PUMPHOUSE MH-20161117	N PUMPHOUSE MH-20170914	Sample ID	N PUMPHOUSE MH-20171204	N Pumphouse MH	N Pumphouse MH	N Pumphouse MH-20180524	N Pumphouse MH	N Pumphouse MH-20181108	N Pumphouse MH	N Pumphouse MH-20190315	N Pumphouse MH	N Pumphouse MH-20190603	N Pumphouse MH	N Pumphouse MH-20190903	Sample ID	N Pumphouse MH	N Pumphouse MH-20191031	N Pumphouse MH	N Pumphouse MH				
Sample Date (yyyy mm dd)					Sample Date (yyyy mm dd)																					
Parameter					Parameter																		Units			
Volatiles Organic Compounds					Analytical Results																		Volatiles Organic Compounds			
5.2	-	-	3.7	9	Chloroethane	µg/L	< 3.0	< 2.0	< 2.0	< 2.0	< 2.0	< 2.0	< 2.0	< 2.0	< 2.0	2.0	2	< 2.0	< 2.0	Chloroethane	µg/L	< 2.2	< 2.2	< 2.0	< 2.0	
< 1.0	-	-	< 1.0	< 1.0	Chloroform	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Chloroform	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	
< 5.0	-	-	< 5.0	< 5.0	Chloromethane	µg/L	< 5.0	-	-	-	-	-	-	-	-	-	-	-	-	Chloromethane	µg/L	-	-	-	-	
< 1.0	-	-	< 1.0	< 1.0	Dibromochloromethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dibromochloromethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	
-	-	-	-	-	Dibromoethane, 1	µg/L	-	< 0.3	-	-	< 0.3	-	< 0.3	-	< 0.3	-	< 0.3	-	< 0.3	-	Dibromoethane, 1	µg/L	< 0.3	-	< 0.3	< 0.3
< 0.70	-	-	< 0.70	< 0.50	Dibromomethane	µg/L	< 1.0	< 1.0	-	-	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	Dibromomethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.0	-	-	< 1.0	< 1.0	Dichlorobenzene	µg/L	< 0.50	< 0.5	< 0.5	< 0.5	0.6	0.6	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5		
< 1.0	-	-	< 1.0	< 1.0	Dichlorobenzene	µg/L	1.6	< 1.0	< 2.3	3.0	3	< 1.0	< 1.0	2.1	2.1	3.0	< 1.0	< 1.0	< 1.0	< 1.0	1.6	1.6	< 1.0	< 1.0		
12.5	-	-	13.3	10.1	Dichloroethane, 1	µg/L	3.2	< 1.0	1.8	1.8	10.8	10.8	2.6	2.6	3.6	3.6	9.0	9	Dichloroethane, 1	µg/L	5.8	5.8	4.3	2.9		
< 1.0	-	-	< 1.0	< 1.0	Dichloroethane, 1	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 1.0	Dichloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 1.0	Dichloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 1.0	Dichloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 1.0	Dichloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 5.0	-	-	< 5.0	< 5.0	Dichloromethane	µg/L	< 5.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	< 3.0		
< 1.0	-	-	< 1.0	< 1.0	Dichloropropane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.4	-	-	< 1.4	< 1.0	Dichloropropene	µg/L	< 1.0	< 1.0	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	Dichloropropene	µg/L	< 1.0	-	< 1.0	< 1.0
< 1.0	-	-	< 1.0	< 0.50	Dichloropropene	µg/L	< 0.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
< 1.0	-	-	< 1.0	< 0.50	Dichloropropene	µg/L	< 0.50	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
< 1.0	-	-	< 1.0	< 1.0	Tetrachloroethane	µg/L	< 1.0	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
< 1.0	-	-	< 1.0	< 0.20	Tetrachloroethane	µg/L	< 0.20	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5		
< 1.0	-	-	< 1.0	< 1.0	Tetrachloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 0.50	Trichloroethane, 1	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 0.50	Trichloroethane, 1	µg/L	< 0.50	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 1.0	Trichloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 1.0	Trichloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 1.0	Trichlorobromomethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
< 1.0	-	-	< 1.0	< 0.40	Vinyl Chloride	µg/L	< 0.40	< 1.0	< 1.0	< 1.0	1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	< 1.0		
Gross Parameters					Gross Parameters																					
< 100	-	-	< 100	-	VH (C6-C10)	µg/L	-	< 100	147	147	181	181	< 100	< 100	< 100	< 100	< 100	224	224	VH (C6-C10)	µg/L	< 100	< 100	104	< 100	
< 100	-	-	< 100	-	VPH (C6-C10)	µg/L	-	< 100	< 100	< 100	< 100	< 100	< 100	< 100	< 100	< 100	< 100	< 100	< 100	< 100	VPH (C6-C10)	µg/L	< 100	< 100	< 100	< 100
750	< 250	< 250	400	< 250	EPH (C10-C19)	µg/L	250	< 250	766	766	346	346	661	661	724	724	953	953	EPH (C10-C19)	µg/L	330	330	< 250	< 250		
260	< 250	< 250	400	< 250	LEPH (C10-C19)	µg/L	250	< 250	763	763	342	342	675	675	719	719	945	945	LEPH (C10-C19)	µg/L	325	-	< 250	< 250		
< 250	< 250	< 250	< 250	< 250	EPH (C19-C32)	µg/L	< 250	< 250	660	660	< 250	< 250	429	429	474	474	858	858	EPH (C19-C32)	µg/L	< 250	< 250	< 250	426		
< 250	< 250	< 250	< 250	< 250	HEPH (C19-C32)	µg/L	< 250	< 250	660	660	< 250	< 250	429	429	474	474	858	858	HEPH (C19-C32)	µg/L	< 250	-	< 250	426		
MTBE					MTBE																					
-	-	-	-	-	Methyl Tert-butyl Ether	µg/L	-	< 1.0	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	< 1.0	-	Methyl Tert-butyl Ether	µg/L	< 1.0	-	< 1.0	< 1.0
Resin and Fatty Acids					Resin and Fatty Acids																					
-	-	-	-	-	Acetic Acid	mg/L	-	-	-	-	-	-	< 3.0	-	< 3.0	-	< 3.0	-	< 3.0	-	Acetic Acid	mg/L	< 3.0	-	23.4	< 3.0
-	-	-	-	-	Butyric Acid	mg/L	-	-	-	-	-	-	< 2.0	-	< 2.0	-	< 2.0	-	< 2.0	-	Butyric Acid	mg/L	< 2.0	-	7.2	< 2.0
-	-	-	-	-	Caproic Acid	mg/L	-	-	-	-	-	-	< 2.0	-	2.4	-	< 2.0	-	< 2.0	-	Caproic Acid	mg/L	< 2.0	-	3.5	< 2.0
-	-	-	-	-	Heptanoic Acid	mg/L	-	-	-	-	-	-	< 2.0	-	< 2.0	-	< 2.0	-	< 2.0	-	Heptanoic Acid	mg/L	< 2.0	-	< 2.0	< 2.0
-	-	-	-	-	Isobutyric Acid	mg/L	-	-	-	-	-	-	< 2.0	-	< 2.0	-	< 2.0	-	< 2.0	-	Isobutyric Acid	mg/L	< 2.0	-	< 2.0	< 2.0
-	-	-	-	-	Isocaproic Acid	mg/L	-	-	-	-	-	-	< 2.0	-	< 2.0	-	< 2.0	-	< 2.0	-	Isocaproic Acid	mg/L	< 2.0	-	< 2.0	< 2.0
-	-	-	-	-	Isovaleric Acid	mg/L	-	-	-	-	-	-	< 2.0	-	< 2.0	-	< 2.0	-	< 2.0	-	Isovaleric Acid	mg/L	< 2.0	-	< 2.0	< 2.0
-	-	-	-	-	Propionic Acid	mg/L	-	-	-	-	-	-	< 2.0	-	< 2.0	-	< 2.0	-	< 2.0	-	Propionic Acid	mg/L	< 2.0	-	3.8	< 2.0
-	-	-	-	-	Valeric Acid	mg/L	-	-	-	-	-	-	< 2.0	-	< 2.0	-	< 2.0	-	< 2.0	-	Valeric Acid	mg/L	< 2.0	-	2.0	< 2.0

Associated CARO file(s): 8031228, 8052345, 8081555, 8110837, 9031248, 9060275, 9090105, mg/L, N000833, ug/L.  
 Associated Exova file(s): 506479, 507801, 509233, 600276, 602695, 605363, 608922, 611891, 614770, 617175, 619614, 625660, 627511, 629501.  
 All terms defined within the body of Keltech's report.  
 < Denotes concentration less than indicated detection limit or RPD less than indicated value.  
 - Denotes analysis not conducted.  
 n/a Denotes no applicable standard/guideline.  
 QA/QC RPD Denotes quality assurance/quality control relative percent difference.  
 \* RPDs are not calculated where one or more concentrations are less than five times RDL.  
 RDL Denotes reported detection limit.



Table 5: Historical Summary of Analytical Results For Leachate

P1 LEACHATE MH-20171204	P1 Leachate MH 2018 03 15	P1 Leachate MH 2018 05 24	P1 Leachate MH-20180524	P1 Leachate MH 2018 08 16	Sample Location		P1 Leachate MH				P1 Leachate MH 2				S Leachate Wet Well						Sample Date				
					Sample ID	P1 Leachate MH 20180816		P1 Leachate MH 201811 08		P1 Leachate MH 2019 03 15		P1 Leachate MH 2019 03 15		2020 09 29		2021 10 22		S LEACHATE WET WELL-20131211	S LEACHATE WET WELL-20140408	S LEACHATE WET WELL-20140610		S LEACHATE WET WELL-20150615	S LEACHATE WET WELL-20150915	S LEACHATE WET WELL-20151203	S LEACHATE WET WELL-20160315
						Parameter	Units	2018 08 16	2018 11 08	2019 03 15	2019 03 15	2020 09 29	2021 10 22	2013 12 11	2014 04 08	2014 06 10	2015 06 15	2015 09 15	2015 12 03	2016 03 15					
<b>Analytical Results</b>																									
<b>Volatile Organic Compounds</b>																									
6.9	8.9	<2.0	<2.0	<2.0	Chloroethane	µg/L	<2.0	<2.0	<2.0	<2.0	<8.0	9.9	17.4	4.7	<6.8	<3.0	<2.0	<1.0	-	1.4	1.1	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Chloroform	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<5.0	-	-	-	-	Chlorobenzene	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
<1.0	<1.0	<1.0	<1.0	<1.0	Dibromochloromethane	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0		
-	<0.3	<0.3	-	<0.3	Dibromoethane, 1	µg/L	-	<0.3	<0.3	-	<0.3	<0.3	<0.3	<0.3	<0.3	<0.3	-	-	-	-	-	-	-		
<0.50	<1.0	<1.0	<1.0	<1.0	Dibromomethane	µg/L	-	<1.0	<1.0	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	-	-	-	-	-	-	-		
<1.0	<0.5	<0.5	<0.5	<0.5	Dichlorobenzene	µg/L	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<1.4	<0.70	<0.70	<0.70	<0.70	<0.70	<0.70		
<1.0	<1.0	<1.0	<1.0	<1.0	Dichlorobenzene	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
1.1	<1.0	<1.0	<1.0	<1.2	Dichlorobenzene	µg/L	<1.2	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	2.9	<1.0	-	2	2.2	1.3	1.1		
3.2	2.3	<1.0	<1.0	1.0	Dichloroethane, 1	µg/L	1	<1.0	<1.0	<1.0	6.8	5.0	5.4	1.2	3.7	1.5	5.2	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Dichloroethane, 1	µg/L	<1.0	<1.0	<1.0	<1.0	80.9	65.7	53.8	19.5	69.4	21.8	<2.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Dichloroethylene	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Dichloroethylene	µg/L	<1.0	<1.0	<1.0	<1.0	5.0	6.3	12.8	1.4	9.0	3.3	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Dichloroethylene	µg/L	<1.0	<1.0	<1.0	<1.0	15.2	19.0	14.8	4.0	11.1	14.3	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<5.0	<3.0	<3.0	<3.0	<3.0	Dichloromethane	µg/L	<3.0	<3.0	<3.0	<3.0	264	234	174	54.1	12.4	<3.0	<1.0	<5.0	-	<5.0	<5.0	<5.0	<5.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Dichloropropane	µg/L	<1.0	<1.0	<1.0	<1.0	<2.5	1.8	<1.6	<1.0	1.7	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	-	<1.0	Dichloropropene	µg/L	-	<1.0	<1.0	-	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<2.8	<1.4	-	<1.4	<1.4	<1.4	<1.4		
<0.50	-	-	-	-	Dichloropropene	µg/L	-	-	-	-	-	-	-	-	-	-	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<0.50	-	-	-	-	Dichloropropene	µg/L	-	-	-	-	-	-	-	-	-	-	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	-	-	-	-	Tetrachloroethane	µg/L	-	-	-	-	-	-	-	-	-	-	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<0.20	<0.5	<0.5	<0.5	<0.5	Tetrachloroethane	µg/L	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Tetrachloroethylene	µg/L	<1.0	<1.0	<1.0	<1.0	<3.3	1.8	1.0	1.1	<1.0	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Trichloroethane, 1	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<0.50	<1.0	<1.0	<1.0	<1.0	Trichloroethane, 1	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Trichloroethylene	µg/L	<1.0	<1.0	<1.0	<1.0	<2.4	2.7	7.0	<1.0	3.9	1.8	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<1.0	<1.0	<1.0	<1.0	<1.0	Trichlorofluoromethane	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.1	<1.0	<1.0	1.4	<1.0	<2.0	<1.0	-	<1.0	<1.0	<1.0		
<0.40	<1.0	<1.0	<1.0	<1.0	Vinyl Chloride	µg/L	<1.0	<1.0	<1.0	<1.0	<1.0	<3.0	<4.1	<1.0	<1.0	6.8	<2.0	<1.0	-	<1.0	<1.0	<1.0	<1.0		
<b>Gross Parameters</b>																									
-	<100	<100	<100	<100	VH (C6-C10)	µg/L	<100	<100	<100	<100	1,430	889	1,570	287	1,240	481	-	<100	120	130	140	<100	<100		
-	<100	<100	<100	<100	VPH (C6-C10)	µg/L	<100	<100	<100	<100	1,050	425	1,100	194	818	270	-	<100	<100	<100	<100	<100	<100		
<250	714	616	616	616	EPH (C10-C19)	µg/L	<250	<250	<250	<250	615	1,250	1,600	384	7,600	3,930	-	1,230	1,950	750	250	620	370		
<250	609	480	480	480	EPH (C19-C32)	µg/L	<250	<250	<250	<250	405	352	430	<250	13,800	259	-	710	1,340	<250	<250	<250	<250		
<250	609	480	480	480	HEPH (C19-C32)	µg/L	<250	<250	<250	<250	405	352	430	<250	13,800	259	-	710	1,340	<250	<250	<250	<250		
<b>MTBE</b>																									
-	<1.0	<1.0	-	<1.0	Methyl Tert-butyl	µg/L	-	<1.0	<1.0	-	<1.3	7.2	9.6	1.9	<8.6	<4.2	-	-	-	-	-	-	-		
<b>Resin and Fatty Acids</b>																									
-	-	-	-	-	Acetic Acid	mg/L	-	-	<3.0	-	3,610	848	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Butyric Acid	mg/L	-	-	<2.0	-	1,730	169	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Caproic Acid	mg/L	-	-	<2.0	-	771	86.7	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Heptanoic Acid	mg/L	-	-	<2.0	-	124	11.6	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Isobutyric Acid	mg/L	-	-	<2.0	-	2,540	102	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Isocaproic Acid	mg/L	-	-	<2.0	-	19.0	6.6	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Isovaleric Acid	mg/L	-	-	<2.0	-	359	53.6	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Propionic Acid	mg/L	-	-	<2.0	-	445	468	-	-	-	-	-	-	-	-	-	-	-		
-	-	-	-	-	Valeric Acid	mg/L	-	-	<2.0	-	870	89.9	-	-	-	-	-	-	-	-	-	-	-		

Associated CARO file(s): 8031228, 8052345, 8081555, 8110837, 9031248, 9060275, 9090105, mg/L, N000833, up/L.  
 Associated Exova file(s): 506479, 507801, 509233, 600276, 602695, 605369, 608922, 611891, 614770, 617175, 619614, 625680, 627511, 629501.  
 All terms defined within the body of Keltech's report.  
 < Denotes concentration less than indicated detection limit or RPD less than indicated value.  
 - Denotes analysis not conducted.  
 n/a Denotes no applicable standard/guideline.  
 QA/QC RPD Denotes quality assurance/quality control relative percent difference  
 \* RPDs are not calculated where one or more concentrations are less than five times RDL.  
 RDL Denotes reported detection limit.





Table 5: Historical Summary of Analytical Results For Leachate

					Sample Location	P2 A2 Leachate MH				
S Leachate Wet Well	S Leachate Wet Well	S Leachate Wet Well	S Leachate Wet Well	S Leachate Wet Well	Sample ID	P2 A2 Leachate MH	P2 A2 Leachate MH	P2 A2 Leachate MH	P2 A2 Leachate MH	
2020 11 16	2021 03 18	2021 06 17	2021 09 15	2021 10 22	Sample Date (yyyy mm dd)	2021 03 19	2021 06 18	2021 09 16	2021 10 21	
					Parameter	Analytical Results				
					Units					
<b>Volatile Organic Compounds</b>										
< 2.0	< 2.0	< 2.0	2.0	< 2.0	Chloroethane	µg/L	< 2.0	< 2.0	< 5.2	< 2.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Chloroform	µg/L	< 1.0	1.2	< 1.0	< 1.0
-	-	-	-	-	Chloromethane	µg/L	-	-	-	-
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dibromochloroethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 0.3	< 0.3	< 0.3	< 0.3	< 0.3	Dibromomethane, 1	µg/L	< 0.3	< 0.3	< 0.3	< 0.3
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dibromomethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
0.5	< 0.5	< 0.5	< 0.5	< 0.5	Dichlorobenzene	µg/L	< 0.5	< 0.5	< 0.5	< 0.5
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dichlorobenzene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
3.6	3.4	3.1	2.8	2.7	Dichlorobenzene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
3.5	3.6	3.6	6.0	4.3	Dichloroethane, 1	µg/L	< 1.0	< 1.0	2.2	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dichloroethane, 1	µg/L	2.0	7.6	10.5	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dichloroethylene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dichloroethylene	µg/L	< 1.0	2.0	6.7	5.7
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dichloroethylene	µg/L	1.8	2.0	2.8	< 1.0
< 3.0	< 3.0	< 3.0	< 3.0	< 3.0	Dichloromethane	µg/L	38.3	58.1	32.4	< 3.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dichloropropane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Dichloropropene	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
-	-	-	-	-	Dichloropropene	µg/L	-	-	-	-
-	-	-	-	-	Dichloropropene	µg/L	-	-	-	-
-	-	-	-	-	Tetrachloroethane	µg/L	-	-	-	-
< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	Tetrachloroethane	µg/L	< 0.5	< 0.5	< 0.5	< 0.5
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Tetrachloroethylene	µg/L	2.3	2.2	1.7	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Trichloroethane, 1	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Trichloroethane, 1	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Trichloroethylene	µg/L	< 1.0	< 1.0	1.6	< 1.0
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Trichlorofluoromethane	µg/L	< 1.0	< 1.0	< 1.0	< 1.0
< 1.3	< 1.0	< 1.0	3.2	< 1.0	Vinyl Chloride	µg/L	< 1.0	< 1.0	< 2.8	1.9
<b>Gross Parameters</b>										
215	235	179	114	< 100	VH (C6-C10)	µg/L	284	496	439	< 100
< 100	120	< 100	< 100	< 100	VPH (C6-C10)	µg/L	258	413	343	< 100
424	< 250	483	544	< 2,500	EPH (C10-C19)	µg/L	299	1,150	< 2,500	< 2,500
417	< 250	480	536	< 2,500	LEPH (C10-C19)	µg/L	299	1,140	< 2,500	< 2,500
322	< 250	685	313	< 2,500	EPH (C19-C32)	µg/L	< 250	859	< 2,500	< 2,500
322	< 250	685	313	< 2,500	HEPH (C19-C32)	µg/L	< 250	859	< 2,500	< 2,500
<b>MTBE</b>										
< 1.0	< 1.0	< 1.0	< 1.0	< 1.0	Methyl Tert-butyl Ether	µg/L	4.0	3.5	< 9.0	< 5.0
<b>Resin and Fatty Acids</b>										
5.2	-	-	-	-	Acetic Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Butyric Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Caproic Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Heptanoic Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Isobutyric Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Isocaproic Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Isovaleric Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Propionic Acid	mg/L	-	-	-	-
< 2.0	-	-	-	-	Valeric Acid	mg/L	-	-	-	-

Associated CARO file(s): 8031228, 8052345, 8081555, 8110837, 9031248, 9060275, 9090105, mg/L, N000833, up/L.  
 Associated Exova file(s): 506479, 507801, 509233, 600276, 602695, 605369, 608922, 611891, 614770, 617175, 619614, 625680, 627511, 629501.  
 All terms defined within the body of Keltech's report.  
 - Denotes concentration less than indicated detection limit or RPD less than indicated value.  
 - Denotes analysis not conducted.  
 n/a Denotes no applicable standard/guideline.  
 QA/QC RPD Denotes quality assurance/quality control relative percent difference.  
 \* RPDs are not calculated where one or more concentrations are less than five times RD.L.  
 RD.L Denotes reported detection limit.

# **Appendix G**

## **Background Water Quality Assessment**



# Technical Memorandum

07 December 2023

<b>To</b>	Mr. Scott Hoekstra (City)	<b>Contact No.</b>	250-469-8588
<b>Copy to</b>	Roxy Hasiar (GHD)	<b>Email</b>	shoekstra@kelowna.ca
<b>From</b>	David R. Barton/tw/1	<b>Project No.</b>	12605725
<b>Project Name</b>	Glenmore Landfill Engineering Reports		
<b>Subject</b>	Glenmore Landfill Site Specific Background and Compliance Water Quality Review		

## 1. Introduction

GHD Limited (GHD) has prepared this technical memorandum (memo) for the City of Kelowna (City) to determine Site-specific background groundwater and surface water concentrations and assess water quality compliance at the Glenmore Landfill (Landfill). The Landfill is located at 2710 John Hindle Drive (Site). This assessment has been completed to satisfy the requirements of Section 3.7(b) of the Site Operational Certificate (OC) 12218, issued by the Ministry of Environment and Climate Change Strategy (the Ministry) on December 8, 2000, and most recently amended on May 30, 2023. The assessment has been completed using the guidance provided in *Protocol 9 for Contaminated Sites, Establishing Local Background Concentrations in Groundwater*, Version 2, published by the Ministry on February 1, 2021 (Protocol 9). The Site, Landfill, and monitoring locations are shown on Figure 1.

## 2. Background

In 2019, following an inspection of the Landfill, the Ministry issued a warning letter (Attachment 1) describing potential non-compliance issues. The Ministry determined that the Landfill was out of compliance with Section 2.8 of OC 12218 (Groundwater and Surface Water Quality Impairment). Groundwater concentrations were noted to exceed the applicable water quality criteria and background concentrations at downgradient compliance wells GL28-1, GL28-2, and GL28-3. Surface water concentrations were noted to exceed the applicable water quality criteria in Little Robert Lake. No background surface water quality data was available for comparison. In response to the warning letter, the City engaged GHD to complete a background water quality assessment for the Site.

GHD completed a background water quality assessment for the Site in 2020 (GHD Limited, 2020) to establish local background groundwater and surface water concentrations and to compare these concentrations to groundwater and surface water quality at the compliance monitoring locations. The assessment is included in Attachment 2. In the assessment, it was determined that insufficient monitoring wells and upstream surface water monitoring locations were present at the Site to characterize background groundwater and surface water quality in the hydrostratigraphic units underlying the Site. Additionally, most of the statistical analyses completed indicated that logarithmic distributions or multiple populations existed for the available data and therefore background concentrations could not be determined.

Following the 2019 warning letter, new groundwater monitoring wells GL41-1, GL41-2, and GL41-3 were installed upgradient of the Landfill at the northwest corner of the property boundary to characterize background groundwater. Additional groundwater monitoring wells GL39-1, GL39-2, GL39-3, GL42-1, and GL42-2 were installed downgradient of the Landfill adjacent to the south property boundary to assess groundwater compliance. Additionally, surface water quality monitoring was initiated at Bubna Slough and Slough 2, the closest upstream surface water bodies to the Site, to support the characterization of background surface water quality.

Since the initial background groundwater and surface water quality assessment was completed in 2020, a sufficient number of groundwater and surface water samples have been collected to assess local background groundwater and surface water quality in accordance with Protocol 9. Samples have been collected from the GL41 (background), GL39, and GL42 (compliance) series groundwater monitoring wells as well as from Slough 2 and Bubna Slough (background).

Background groundwater quality for the Site was assessed using the Protocol 9 options (2a and 2b) for establishing local background concentration in groundwater. Option 2a was also applied to estimate background concentrations in surface water based on surface water quality data from Bubna Slough and Slough 2.

In the 2021 revision of Protocol 9, a table was added that presents regional background concentrations for inorganic substances in groundwater for the Thompson Okanagan Region. The concentrations listed in Table 1 of Protocol 9 are considered representative of background groundwater quality and are applicable at the Site.

On May 30, 2023, the Ministry issued a revised version of OC 12218. In the revised OC, Section 2.8 has been removed and replaced with Section 3.7.

### **3. Assessment Methodology**

#### **Groundwater**

Background concentrations and groundwater quality exceedances at compliance wells were determined following the below steps:

- Compliance groundwater analytical results from 2022 were compared to the applicable water quality criteria to establish a preliminary list of potential water quality exceedances.
- The water quality exceedances identified in step 1 were then compared to the regional background concentrations for the Thompson Okanagan Region listed in Table 1 of Protocol 9.
- Background concentrations were determined for the parameters that exceeded both the CSR standards and regional background concentrations as well as parameters that are not included in Table 1 of Protocol 9. Background concentrations for the selected parameters were determined using the statistical methods described in Options 2a and 2b of Protocol 9.

As illustrated on Figure 3.1, the substances that were found to exceed the applicable water quality criteria, the regional background concentrations (where applicable), and the Site-specific 95<sup>th</sup> percentile background concentrations are considered to be exceedances. After identifying exceedances, concentrations of the exceeding parameters at the compliance wells were compared to landfill leachate concentrations to assess whether the exceedances are likely leachate derived.

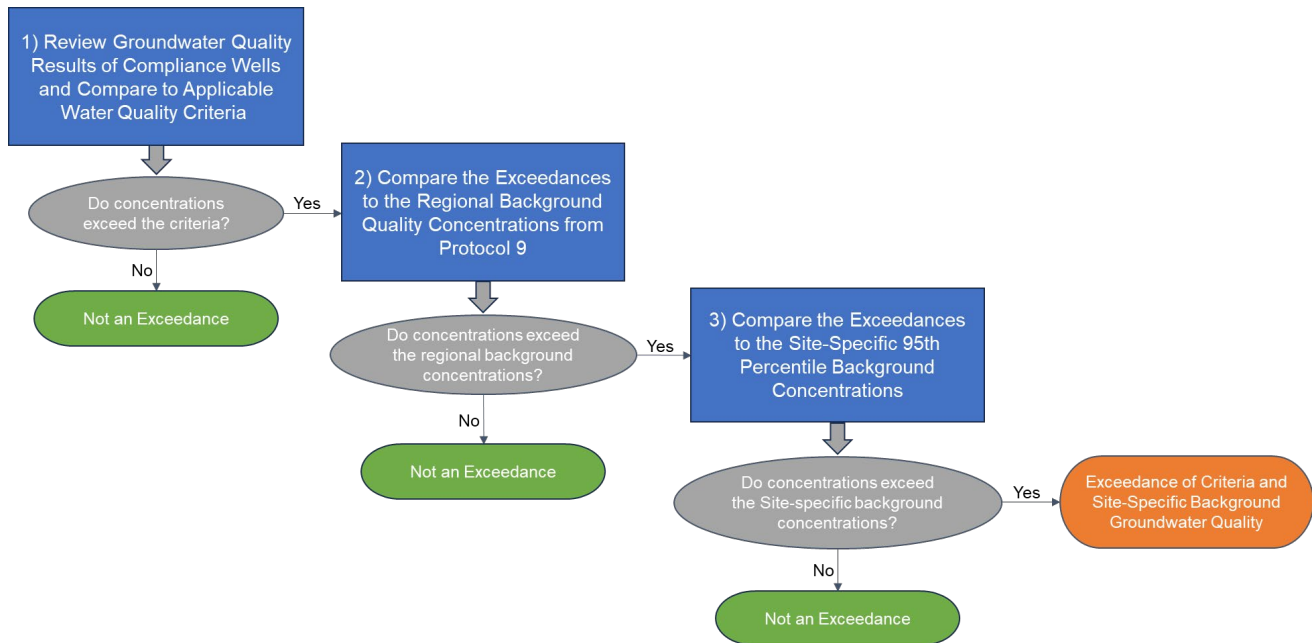


Figure 3.1 Groundwater Quality Exceedance Assessment Methodology

### Surface Water

To establish Site-specific background concentrations for surface water at the Site, GHD applied the methodology described in Option 2a of Protocol 9. Under this option, background concentrations in surface water were established through the collection of samples from representative background locations (Slough 2 and Bubna Slough) located upstream of the Site.

## 4. Hydrogeologic Site Setting

This section provides a summary overview of the Site hydrogeologic setting. A detailed characterization of the Site hydrogeologic setting is provided in the 2023 Hydrology and Hydrogeology Characterization Report (HHCR).

### 4.1.1 Site Geology and Hydrogeology

Geology underlying the Site consists of overburden sediments of variable thickness which overlie volcanic and sedimentary bedrock. The overburden sediments consist of glaciolacustrine silt and clay deposits which overlie glaciofluvial sands and gravels, which overlie a glacial till unit. Overburden material is primarily found in the valley floor and pinches out towards the sides of the Glenmore Valley. Bedrock underlies the glacial till unit.

GHD's review of the Site's stratigraphy logs indicates that the glaciofluvial sand and gravel deposits range in thickness from 0 to 10.0 meters in thickness, with the thickest sand and gravel deposits at the north end of the Site and the thinnest deposits around the slough area. The sand and gravel deposits did not appear in every borehole log, suggesting that the sand and gravel layer forms a discontinuous deposit across the Site. Bedrock at the Site is inferred to have an undulating surface with a depression directly underlying the slough, causing groundwater in the bedrock aquifer to flow preferentially towards the slough.

The BC aquifer classification system indicates Aquifer 469<sup>1</sup> and Aquifer 470<sup>2</sup> are present at the Site. Aquifer 469 is an overburden aquifer composed of sands and gravels with moderate productivity, low vulnerability, and low demand. Aquifer 470 is a bedrock aquifer composed of volcanic rocks belonging to the Pentiction Group or Harper Ranch Group.

In general, the geologic units described above may be grouped into the following hydrogeologic units identified in brackets:

1. Shallow silt and clay deposits (act as a leaky aquitard)
2. Glaciofluvial sand and gravel deposits (Aquifer 469)
3. Glacial till unit (act as a leaky aquitard)
4. Bedrock (Aquifer 470)

Horizontal groundwater flow at the Site occurs primarily in the glaciofluvial sand and gravel unit and the underlying bedrock unit. Groundwater flow is interpreted to be generally flowing from north to south, through the Landfill, the slough and the Compost Facility towards the mouth of the valley. It is likely that during periods of high precipitation, precipitation falling on the valley walls and small mountains to the east and west of the valley follow bedrock topography and flow towards the centre of the Site. Once flow reaches the centre of the Site, it joins the primary flow path to the south.

The glacial till unit has a wide range of hydraulic conductivities and is inferred to vary in composition laterally across the Site. The till unit is considered a leaky aquitard, a confining unit with areas that transmits water at a very slow rate. The till unit partially separates the sand and gravel unit from the bedrock unit below it. Flow within the glacial till may be a combination of horizontal and vertical flow depending on the composition.

A portion of groundwater/leachate recharges the slough, which acts as a hydraulic sink. From the slough, groundwater/leachate slowly infiltrates the underlying silt and clay deposits and the sand and gravel unit. A review of the 2022 inferred direction of groundwater flow figures indicate a portion of groundwater that does not recharge the slough also flows south toward the Site boundary.

A review of the 2022 vertical hydraulic gradients on Site indicates that vertical groundwater flows upwards in the northern area of the Site, as well as near the eastern and western Site boundaries. Slight downward vertical gradients occur in the slough and compost facility areas, specifically monitoring well nests GL28, GL29, GL34, GL35 and GL39.

## **5. Site Groundwater Monitoring Locations**

### **5.1 Compliance/Downgradient Groundwater Monitoring Wells**

The groundwater compliance wells for the Site are located along the south property boundary. The compliance wells and the hydrogeologic units they are screened in are listed below:

- GL28-3 (silt and clay)
- GL28-1 (sand and gravel unit)
- GL28-2 (sand and gravel unit)
- GL39-2 (sand and gravel unit)
- GL42-2 (glacial till unit)
- GL39-1 (glacial till unit)
- GL42-1 (glacial till unit)

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<sup>1</sup> British Columbia Groundwater Wells and Aquifers, Aquifer 469 Summary. <https://apps.nrs.gov.bc.ca/gwells/aquifers/469>

<sup>2</sup> British Columbia Groundwater Wells and Aquifers, Aquifer 470 Summary. <https://apps.nrs.gov.bc.ca/gwells/aquifers/470>



Groundwater quality data from the compliance wells reported from 2022 was compared to the applicable water quality criteria listed in Section 6 and to the regional background concentrations for the Thompson Okanagan Region listed in Table 1 of Protocol 9. Parameters that were reported at concentrations exceeding the applicable water quality criteria and the regional background concentrations, as well as parameters that are not included in Protocol 9 Table 1 (i.e., chloride, nitrate, sulphate, and TDS) are presented in Table 7.2.

It should be noted that GL28-1 is drilled 10 m into bedrock but is screened in the overlying sand and gravel unit.

## 5.2 Background Groundwater Monitoring Locations

Table 5.1 lists the background groundwater monitoring locations selected for the Site. Selection criteria included:

- Hydraulically upgradient or cross-gradient of the Landfill footprint and Site activities.
- Historically used as a background location.
- Stable water quality with no clear indication of impacts from the Landfill or Site activities.
- Screened within a hydrogeologic unit present upgradient and downgradient of the Landfill footprint.

Wells that met these criteria are screened in the sand and gravel unit and the glacial till unit. There are no background wells screened in the silt and clay deposits.

*Table 5.1 Background Groundwater Monitoring Locations*

Well ID	Hydrogeologic Units	Location
GL41-3	Sand and gravel unit	Northwest property boundary
GL23-1	Sand and gravel unit	Northeast of Landfill footprint
GL0-3	Sand and gravel unit	North of Landfill footprint (decommissioned in 2021)
Site ID 12082 (off-Site)*	Sand and gravel unit	275 m southeast of the Site boundary (cross gradient)
GL41-2	Glacial till unit	Northwest property boundary
GL15-2	Glacial till unit	Southwest, off-Site
GL0-2	Glacial till unit	North of Landfill footprint (decommissioned in 2021)

\* Source: BC Groundwater Database

## 6. Applicable Groundwater Quality Criteria

The BC Contaminated Site Regulation (CSR) standards are the applicable water quality criteria for the Site (refer to OC Condition 3.7) and supersede previously used Site criteria. A detailed rationale on the applicability of BCs groundwater quality classes is provided in the 2023 DOCP.

The water quality criteria applicable to the Site include:

- BC CSR drinking water use (DW)
- BC CSR irrigation water use (IW)

## 7. Determination of Groundwater Quality Exceedances at the Property Boundary

### 7.1 Application of Protocol 9

Protocol 9 states that for background concentrations that fall within a single statistical population, the representative local background concentration for a substance in groundwater is the 95<sup>th</sup> percentile concentration of the data set. To establish local, Site-specific, background concentrations for the parameters listed in Table 7.2 (column 3), GHD calculated the 95<sup>th</sup> percentile concentrations for background groundwater in accordance with the methodology described in Options 2a and 2b of Protocol 9. Specifically, Protocol 9 specifies a two-step process in which first the 95<sup>th</sup> percentile concentration is determined for each of a minimum of three background wells, and then the local background value is set across the background wells as the 95<sup>th</sup> percentile of the individual well 95<sup>th</sup> percentile values. This process accounts for spatial variability in groundwater conditions within a unit by selecting an upper (95<sup>th</sup>) percentile of the individual well background estimates.

The 95<sup>th</sup> percentile concentrations were calculated using ProUCL Version 5.2. ProUCL is statistical software developed by the United States Environmental Protection Agency (US EPA) for environmental applications<sup>3</sup>. The 95<sup>th</sup> percentile represents the value below which 95 percent of the data points in the dataset are found. That is, 95 of 100 random samples from the background population (or 19 out of 20) are expected to have a concentration at or below the calculated 95<sup>th</sup> percentile.

The following steps were conducted in calculating the 95<sup>th</sup> percentile background concentrations for the Site:

1. Compiling and tabulating analytical data from the most recent six monitoring events for each of the site's background monitoring wells, as well as from Site 12082 of the Ministry's background groundwater database.
2. Establishing that the concentration data for each parameter occur collectively within a single statistical population. Specifically, that the groundwater monitored at each location has similar aquifer characteristics (depths, spatial proximity, upgradient of potential local anthropogenic impacts, etc.)
3. Determining the statistical data distribution for each data set (e.g., if the concentrations for a parameter in groundwater from each monitoring location fall within a normal, gamma or lognormal distribution).
4. Checking each data set for any statistical outliers. Statistical outliers were determined using ProUCL, taking into account the observed data distribution.
5. Calculating the 95<sup>th</sup> percentile concentration for each parameter for each background monitoring location.
6. Calculating the overall background value as the 95<sup>th</sup> percentile of the individual-well values calculated in step 5. Note that if fewer than three data points were available, the maximum reported concentration was used (this occurred for only two data sets – sulphate and uranium in groundwater from the till wells).

The methodologies employed by ProUCL in calculating percentile values for a data set is described in Section 3.3 of the ProUCL Technical Guide (USEPA, 2022)<sup>4</sup>. Other required test methods within ProUCL used in the data evaluation include goodness-of-fit tests to determine data distributions (Section 2.2 in USEPA, 2022) and testing for outliers (Sections 7.3 and 7.4 of USEPA, 2022). Due to the relatively small sample sizes available (i.e., up to 6 observations per background well), the following notes specify how the statistical calculations were applied:

- Many of the data sets were found to fit all three of the data distributions tested by ProUCL (i.e., normal, gamma and lognormal). The data distributions selected were therefore based on inspection of the probability plots (Q-Q plots) produced by ProUCL, as well as considering the diagnostic statistics provided in the goodness of fit tests.

<sup>3</sup> <https://www.epa.gov/land-research/proucl-software>

<sup>4</sup> USEPA, June 2022. ProUCL Version 5.2.0 Technical Guide. United States Environmental Protection Agency, Office of Research and Development, Washington DC.

- In some cases, potential outlier values were identified. Each of these was reviewed and considered for applicability in the background calculations. Upon review, a small number of outliers were excluded from the background value calculations.
- Data distribution-based 95<sup>th</sup> percentile calculations were required, as rank-based (nonparametric) percentile estimates do not provide 95<sup>th</sup> percentile coverage for small data sets (see Section 3.3.1 of USEPA, 2022).

The analytical results used in step 5 of the statistical analysis are summarized in Table 1 for the sand and gravel unit and Table 2 for the glacial till unit. The 95<sup>th</sup> percentile concentrations for each monitoring well calculated in step 5 of the statistical analysis are presented in Table 3.

The overall 95<sup>th</sup> percentile background concentrations are presented in Table 7.1, below. These are considered the background concentrations for the Site.

**Table 7.1 Overall 95<sup>th</sup> Percentile Background Concentrations in Groundwater**

Exceedance Parameter	Units	Sand and Gravel Unit 95 <sup>th</sup> Percentile Concentration	Glacial Till Unit 95 <sup>th</sup> Percentile Concentration
Chloride	mg/L	556.4	717.4
Nitrate (as N)	mg/L	2.5	n/a
Sulphate	mg/L	763.7	347.6 (maximum*)
Sodium	mg/L	n/a	1423
Lithium	ug/L	62.2	76.61
Strontium	ug/L	n/a	18,282
Alkalinity, total (as CaCO <sub>3</sub> )	mg/L	1401.0	n/a
Total Dissolved Solids	mg/L	2250.0	n/a
Uranium	µg/L	227.7	30.0 (maximum*)

Notes:  
n/a – not applicable; parameter not assessed as there were no exceedances.  
\* Only two values remained after removing outliers from the sulphate and uranium datasets for the glacial till wells. Therefore, it was not possible to calculate 95<sup>th</sup> percentile concentrations and the maximum of the remaining values was used.

## 7.2 Groundwater Quality Impact Assessment

Based on the results of this assessment, several parameters exceeded the applicable groundwater quality criteria, the regional background concentrations, and the Site-Specific background concentrations (i.e., 95<sup>th</sup> percentile concentration) at the Site compliance locations. The exceedances are presented in Table 7.2.

**Table 7.2 Groundwater Quality Exceedances at Site Compliance Wells**

Compliance Location	Exceedances of Water Quality Criteria (2022)	Exceedances also above Regional Background Concentrations	Exceedances also above Site-Specific Background Concentrations
<b>Sand and Gravel Unit</b>			
GL28-1	<ul style="list-style-type: none"> <li>– Lithium<sup>(DW)</sup></li> <li>– Molybdenum<sup>(IW)</sup></li> <li>– Sodium<sup>(DW)</sup></li> <li>– Strontium<sup>(DW)</sup></li> <li>– Uranium<sup>(DW)(IW)</sup></li> <li>– Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>– Uranium<sup>(DW)(IW)</sup></li> <li>– Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>– Sulphate<sup>(DW)</sup></li> </ul>

Compliance Location	Exceedances of Water Quality Criteria (2022)	Exceedances also above Regional Background Concentrations	Exceedances also above Site-Specific Background Concentrations
GL28-2	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Nitrate (as N)<sup>(DW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Nitrate (as N)<sup>(DW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Nitrate (as N)<sup>(DW)(MAC)</sup></li> <li>- Sulphate<sup>(DW)(AO)</sup></li> </ul>
GL39-2	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(DW)</sup></li> </ul>
<b>Glacial Till Unit</b>			
GL42-2	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>
GL39-1	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)</sup></li> <li>- Chloride<sup>(IW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(DW)(AO)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> </ul>
GL42-1	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> </ul>
<b>Silt and Clay</b>			
GL28-3	<ul style="list-style-type: none"> <li>- Arsenic<sup>(DW)</sup></li> <li>- Cobalt<sup>(DW)</sup></li> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Nickel<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Strontium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)(AW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Nickel<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)(AW)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Lithium<sup>(DW)</sup></li> <li>- Molybdenum<sup>(IW)</sup></li> <li>- Nickel<sup>(DW)</sup></li> <li>- Sodium<sup>(DW)</sup></li> <li>- Uranium<sup>(DW)(IW)</sup></li> <li>- Sulphate<sup>(DW)(AW)</sup></li> </ul>
<p>Notes:</p> <p>DW: Schedule 3.2 Generic Numerical Water Standards Column 6 for the protection of Drinking Water.</p> <p>IW: Schedule 3.2 Generic Numerical Water Standards Column 4 for the protection of Irrigation Water.</p> <p>AO: Aesthetic Objective</p> <p>MAC: Maximum Acceptable Concentration</p>			

Concentrations of the exceeding parameters at the compliance wells were compared to landfill leachate concentrations to assess whether the exceedances are likely leachate derived or not. The following conclusions were made:

- The concentration of nitrate, lithium, and uranium reported at GL28-2, GL39-1, GL41-1, and GL42-2 are greater than the concentrations reported in Landfill leachate from Phase 1 and 2 indicating that landfill leachate is not solely the cause of nitrate, lithium, and uranium exceedances in groundwater at the property boundary:
  - The concentration of nitrate in Landfill leachate ranged from non-detect to 7.7 mg/L in 2022, which is below the CSR DW criteria of 10 mg/L. Nitrate in landfill leachate is protective of drinking water, and so the nitrate exceedance at GL28-2 is not resulting from leachate.
  - The concentration of lithium in landfill leachate ranged from 31.9 to 290 ug/L in 2022, which is lower than the concentration reported at GL41-1 (861 ug/L) and GL42-2 (861 ug/L). As such, landfill leachate cannot solely be the cause of the lithium exceedance at GL42-2.
  - The concentration of uranium in leachate ranged from 1.75 to 32.2 ug/L in 2022, which is well below the concentrations measured at GL39-1 (244 ug/L) and GL42-2 (122 ug/L). As such, landfill leachate cannot solely be the cause of the uranium exceedance at GL39-1 and GL42-2.
- Sulphate concentrations in landfill leachate (<10 mg/L to 1,880 mg/L) are similar to groundwater at the property boundary (28.2 mg/L to 4,640 mg/L), indicating that the source of sulphate in groundwater may be landfill derived.
- Monitoring well GL28-3 is a shallow well screened in silt and clay. The concentrations of dissolved metals reported at GL28-3 are substantially higher than the concentrations measured at nested wells GL28-2 and GL28-1, which are screened deeper within the sand and gravel unit. The elevated concentrations of dissolved metals at GL28-3 may be related to elevated turbidity of groundwater at GL28-3 due to the presence of silt and clay in groundwater samples.

## 8. Hydrology Site Setting

Surface water features on and off-Site are presented on Figure 1.

Two sloughs located north of the Site serve as the surface water background locations for the EMP. Slough 2 is 3.5 km and Bubna Slough is 1.5 km north of the Site.

Within the Site boundary, stormwater is directed to and contained in the three constructed ponds (Northeast Pond, Bredin Pond, and Tutt Pond) with no overland flow off the Site property under normal operating conditions. Stormwater from the Northeast Pond flows to Bredin Pond, which flows into Tutt Pond. Local farmers use water from Tutt Pond to irrigate their lands.

Additionally, Tutt Pond is equipped with an emergency by-pass system that allows water to be pumped from Tutt Pond via temporary pumps and hoses into the drainage system at the south end of the Site. Throughout the Site's history, emergency pumping from Tutt Pond has only occurred twice, between April 15 and July 10, 2018, and April 29 to May 28, 2019. During large storm events, run-off from the southeastern portion of the Site (i.e., from the administrative building area) can also enter the drainage system at the south end of the Site. This drainage system discharges to Little Robert Lake via a drainage culvert located at the south Site property boundary. The flow meter installed within the culvert shows that stormwater occasionally discharges from the Site.

The Slough, located at the centre of the Site, is the remnant of Alki Lake, a former lake, which was partially infilled with waste when landfilling began at the Site. The Slough does not have any overland outlet drainages. Water in the Slough is partially drained by the Landfill leachate collection system and is reduced through evaporation. A portion of water in the Slough also infiltrates into the underlying groundwater system.

There are two sloughs located south of the Site (downstream). Little Robert Lake is 250 m and Robert Lake is 650 m from the Site south boundary. Each of these surface water bodies are natural alkaline lakes and are considered potential off-Site aquatic receptors to the Landfill.

## **9. Surface Water Locations**

For the purposes of this memo, surface water quality is characterized/assessed as follows:

- Background surface water quality is characterized by Slough 2 and Bubna Slough, which are located hydraulically upgradient, north of the Site boundary.
- Potential Site derived impact was assessed at Little Robert Lake and Robert Lake, which are located downstream of the Site.

Little Robert Lake is being assessed for Site derived impacts resulting from Site stormwater discharge and potential groundwater recharge. Robert Lake is being assessed for Site derived impacts resulting from groundwater recharge.

It should be noted that Little Robert and Robert Lake are not monitored as compliance locations under the 2022 Environmental Monitoring Program developed for the Site. Instead, these lakes are monitored as background locations. The surface water impact assessment presented herein is being completed as a voluntary and proactive measure, and is not required under the Landfill OC.

## **10. Applicable Surface Water Quality Criteria**

The BC water quality guidelines (WQGs) were used in this assessment as the most applicable water quality criteria for Little Robert Lake and Robert Lake. As mentioned in Section 8, these surface water bodies are natural alkaline lakes and so are unique environments that aren't necessarily applicable to freshwater aquatic life criteria. However, in the absence of Site-specific criteria, BC WQGs were applied. Additional rationale for the selection of the applicable water quality criteria is included in the DOCP.

The water quality criteria used for this assessment include:

- – BC Water Quality Guidelines (WQG) Aquatic Life Long-Term Chronic (AW LT)
- – BC WQG Aquatic Life Short-Term Acute (AW ST)
- – BC WQG Irrigation Long-Term Chronic (IW LT)
- – BC WQG Irrigation Short-Term Acute (IW ST)

The short-term chronic WQGs are the primary criteria. Where short-term chronic criteria are not available, long-term chronic WQGs were used.

## **11. Determination of Surface Water Quality Exceedances**

To identify surface water quality exceedances, the 2022 water quality dataset for Little Robert Lake was reviewed. Parameters that were reported at concentrations greater than the applicable criteria at Little Robert Lake are presented in Table 11.2.

### **11.1 Application of Protocol 9**

To determine Site-specific background surface water concentrations, Protocol 9 was applied following the steps described in Section 3. As there are only two background surface water monitoring locations at the Site, data

from the six most recent monitoring events at Slough 2 and Bubna Slough were treated as a single dataset from which 95<sup>th</sup> percentile concentrations were calculated. The analytical results used in the statistical analysis are presented in the attached Table 4. The 95<sup>th</sup> percentile results are summarized in Table 11.1.

**Table 11.1 95<sup>th</sup> Percentile Concentrations in Background Surface Water**

Parameter	Units	95 <sup>th</sup> Percentile Concentration in Background Surface Water
Chloride	mg/L	812.1
Sulphate	mg/L	1520
Ammonia, Total (as N)	mg/L	1.22
Aluminium	mg/L	0.0411
Arsenic	mg/L	0.00618
Chromium	mg/L	3.45 x 10 <sup>-4</sup>
Iron	mg/L	0.0785
Uranium	mg/L	0.0329
Molybdenum*	mg/L	0.00733*
Field Conductivity	uS/cm	6438
Alkalinity, Total (as CaCO <sub>3</sub> )	mg/L	1037
Phosphorus, Total (as P)	mg/L	0.0733
Notes: * Molybdenum concentrations in background surface water do not fall within a normal, lognormal, or gamma distribution. The maximum concentration in background surface water from the most recent 6 samples at Slough 2 and Bubna Slough was used.		

## 11.2 Surface Water Impact Assessment

Based on the results of this assessment, several parameters were determined to exceed the applicable surface water quality criteria and the local 95<sup>th</sup> percentile background surface water concentrations at Little Robert Lake. The parameters that exceeded the applicable water quality criteria and Site-specific background concentrations are summarized in Table 11.2.

**Table 11.2 Surface Water Quality Exceedances at Little Robert Lake**

Monitoring Location	Exceedances of Applicable Water Quality Criteria (2022)	Exceedances also above Site-Specific Background Concentrations
Little Robert Lake	<ul style="list-style-type: none"> <li>- Chloride<sup>(IW-ST)</sup></li> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Aluminium<sup>(AW-ST, IW-ST)</sup></li> <li>- Arsenic<sup>(AW-ST)</sup></li> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Field Conductivity<sup>(IW-LT)</sup></li> <li>- Total Alkalinity (as CaCO<sub>3</sub>)<sup>(IW-LT)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Aluminium<sup>(AW-ST, IW-ST)</sup></li> <li>- Arsenic<sup>(AW-ST)</sup></li> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> </ul>
Robert Lake	<ul style="list-style-type: none"> <li>- Chloride<sup>(IW-ST, AW-LT)</sup></li> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Ammonia<sup>(AW-ST)</sup></li> <li>- Aluminium<sup>(AW-ST)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Sulphate<sup>(AW-LT)</sup></li> <li>- Total Alkalinity (as CaCO<sub>3</sub>)<sup>(IW-LT)</sup></li> <li>- Aluminium<sup>(AW-ST)</sup></li> <li>- Arsenic<sup>(AW-ST)</sup></li> </ul>



Monitoring Location	Exceedances of Applicable Water Quality Criteria (2022)	Exceedances also above Site-Specific Background Concentrations
	<ul style="list-style-type: none"> <li>- Arsenic<sup>(AW-ST)</sup></li> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Molybdenum<sup>(IW-ST)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Total Alkalinity (as CaCO<sub>3</sub>)<sup>(IW-LT)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> <li>- Field Conductivity<sup>(IW-LT)</sup></li> </ul>	<ul style="list-style-type: none"> <li>- Chromium<sup>(IW-LT)</sup></li> <li>- Iron<sup>(AW-ST)</sup></li> <li>- Uranium<sup>(AW-LT, IW-LT)</sup></li> <li>- Molybdenum<sup>(IW-ST)</sup></li> <li>- Total Phosphorus (as P)<sup>(AW-ST)</sup></li> <li>- Field Conductivity<sup>(IW-LT)</sup></li> </ul>
<p>Notes:</p> <p>AW-ST: BCWQG Aquatic Life Short-Term Maximum guideline.  AW-LT: BCWQG Aquatic Life Long-Term Average guideline.  IW-ST: BCWQG Irrigation Water Short-Term Maximum guideline.  IW-LT: BCWQG Irrigation Water Long-Term Average guideline.</p>		

Concentrations of the exceeding parameters at the compliance wells were compared to landfill leachate concentrations to assess whether the exceedances are potentially leachate derived or not. The following conclusions were made:

- The concentration of sulphate in Landfill leachate ranged from non-detect to 1,880 mg/L in 2022, which is lower or similar in concentration to surface water in Little Robert Lake and Robert Lake (1,810-6,280 mg/L) indicating that leachate is not solely the source of sulphate exceedances. The presence of Landfill-related sulphate impacts in groundwater at the Site boundary and an increasing sulphate trend at each lake suggests that sulphate impacts may be related to the Landfill. Additional monitoring is needed to further assess sources of sulphate, as described in the HHCR.
- Aluminium, uranium, and molybdenum are lower in concentration within Landfill leachate than compared to surface water collected from Little Robert and Robert Lake. Additionally, these metals and arsenic, chromium, and iron are not in high concentrations within the sand and gravel groundwater, which recharges Robert Lake, indicating that these exceedances may not be Landfill derived. As presented in the HHCR, higher concentrations of metals in the surface water bodies may be attributable to the evaporative condition of the lakes. Over time, the cumulative effects of evaporation cycles can cause metal concentrations in surface water to increase over time.

## 12. Summary

The available groundwater and surface water quality data for the Site from 2022 was assessed to determine Site-specific background water quality concentrations and water quality exceedances at groundwater compliance wells and at downstream surface water locations at Little Robert Lake and Robert Lake.

This assessment was completed by comparing compliance and downstream surface water concentrations to regional and Site-specific background concentrations and applicable water quality criteria. Site-specific background concentrations were determined using the guidance provided in Protocol 9. Exceedances are listed below.

### Groundwater – Sand and Gravel Unit:

- GL28-1 (sulphate)
- GL28-2 (nitrate, sulphate)
- GL39-2 (sulphate)

**Groundwater – Glacial Till Unit:**

- GL42-2 (sulphate, lithium, uranium)
- GL39-1 (sulphate, uranium)
- GL42-1 (lithium)

**Groundwater – Silt and Clay**

- GL28-3: (lithium, molybdenum, nickel, sodium, uranium, sulphate)

**Surface Water**

- Little Robert Lake (sulphate, aluminium, arsenic, chromium, iron, uranium, total phosphorus)
- Robert Lake (sulphate, aluminium, arsenic, chromium, iron, uranium, total phosphorus, total alkalinity, molybdenum, and field conductivity)

Based on a comparison of concentrations in Landfill leachate, compliance groundwater, and surface water, only sulphate cannot be ruled out as being Landfill derived.

**Recommendations**

- Apply Protocol 9 to future annual reports to determine local background concentrations.

Regards



**David R Barton, GIT**  
Hydrogeologist in Training



**Rose Marie Rocca, P.Ge.**  
Hydrogeologist

# Tables

**Table 1**  
**Background Groundwater Quality Data Summary**  
**Sand and Gravel Aquifer**  
**Glenmore Landfill**  
**City of Kelowna**

<b>Sample Location</b>		GL41-3	GL41-3	GL41-3	GL41-3	GL41-3	GL41-3	GL23-1	GL23-1	GL23-1	GL23-1	GL23-1	GL23-1
<b>Sample Date</b>		20-Jun-20	22-Oct-20	25-May-21	7-Sep-21	6/15/2022	9/23/2022	5/23/2019	8/17/2019	6/17/2020	10-Sep-20	13-May-21	6/6/2022
Parameter	Units												
Chloride	mg/L	423	423	471	406	250	337	34	35	32.3	33.1	33.2	31.9
Nitrate (as N)	mg/L	1.18	1.38	1.51	1.78	1.32	1.75	0.072	ND (0.01)	0.134	0.028	0.01	0.041
Sulphate	mg/L	159	160	160	143	108	133	384	394	405	402	376	416
Alkalinity, total (as CaCO <sub>3</sub> )	mg/L	575	570	618	622	533	587	1120	1090	964	1110	1180	962
Total Dissolved Solids	mg/L	1580	1400	1340	1400	1010	1230	1,590	1,610	1530	1660	1370	1610
Uranium	ug/L	27.7	26.9	26.3	24.6	14.1	19.3	80.5	75.6	68.9	74.7	68.5	73.5
Lithium	ug/L	47.5	41.3	45.3	43.4	31.1	37	42.5	39.8	36.7	41.7	36.7	39.6

## Notes:

mg/L - milligrams per litre

uS/cm - microSiemens per centimetre

ND (50) - Not detected at the associated reporting limit

**Table 1**  
**Background Groundwater Quality Data Summary**  
**Sand and Gravel Aquifer**  
**Glenmore Landfill**  
**City of Kelowna**

<b>Sample Location</b>		GL0-3	GL0-3	GL0-3	GL0-3	GL0-3	GL0-3	09BH03	09BH03	09BH03	09BH03	09BH03	09BH03
<b>Sample Date</b>		11/3/2015	5/24/2016	5/24/2017	5/29/2018	5/29/2019	3/10/2020	6/1/2017	6/4/2018	5/30/2019	6/9/2020	6/9/2021	6/6/2022
Parameter	Units												
Chloride	mg/L	121	127	131	121	154	139	15	26.2	27.9	25.3	11.1	9.43
Nitrate (as N)	mg/L	47.6	49.1	48.7	44.7	67	55.8	0.69	ND (0.01)	1.88	1.75	1.01	0.931
Sulphate	mg/L	382	401	368	293	613	505	1024	1,500	1,090	1540	939	1070
Alkalinity, total (as CaCO <sub>3</sub> )	mg/L	422	442	396	481	525	491	698	788	780	776	713	644
Total Dissolved Solids	mg/L	1460	1450	1420	1480	2060	1970	2270	2,800	2,460	3020	1,800	2200
Uranium	ug/L	111	124	130	198	178	122	124	168	161	207	115	140
Lithium	ug/L	ND (50)	ND (50)	ND (50)	41.1	52.3	50.1	ND (50)	29.9	33.3	31	22	20.2

Notes:  
 mg/L - milligrams per litre  
 uS/cm - microSiemens per centimetre  
 ND (50) - Not detected at the associated reporting limit

**Table 2**  
**Background Groundwater Quality Data Summary**  
**Till Unit**  
**Glenmore Landfill**  
**City of Kelowna**

Sample Location		GL41-2	GL41-2	GL41-2	GL41-2	GL41-2	GL41-2	GL15-2	GL15-2	GL15-2	GL15-2	GL15-2	GL15-2	GL0-2	GL0-2	GL0-2	GL0-2	GL0-2	GL0-2	
Sample Date		6/12/2020	10/22/2020	5/25/2021	9/7/2021	15-Jun-22	9/23/2022	9/25/2017	9/28/2018	9/24/2019	11/4/2020	10/7/2021	10/5/2022	11/3/2015	5/24/2016	5/24/2017	5/29/2018	5/29/2019	3/10/2020	
Parameter	Units																			
Chloride	mg/L	387	402	423	383	232	286	181	214	246	360	346	361	12.1	6.8	7.1	9.63	71.6*	7.88	
Sulphate	mg/L	166	175	151	138	109	122	4560	3730	4060	7190	5260	4080	317	310	325	296	349	303	
Sodium	mg/L	279	256	286	266	195	199	1070	992	794	1630*	ND (0.5)	786	92.7	56.7	60.4	63.2	116	58.3	
Lithium	ug/L	45.2	41.7	42.5	41.5	29.7	32.9	55	49.2	52.8	64.9	36.1	39.6	ND (25)	ND (25)	ND (25)	32	27	32	
Strontium	ug/L	3120	2840	2990	2960	2140	2440	8810	6020	8810	14900	ND (5)	6830	1650	1420	1670	1360	2020	1500	
Uranium	ug/L	26.3	25.8	24.5	24.6	15.4	18	423	318	355	549	453	329	19.5*	1.92	2.05	3.1	55.3*	3.01	

Notes:  
 mg/L - milligrams per litre  
 uS/cm - microSiemens per centimetre  
 ND (5) - Not detected at the associated reporting limit  
 \* Value identified as outlier and removed from the dataset

**Table 3**  
**Background Groundwater Quality Data Summary**  
**95th Percentile Concentrations -**  
**Sand and Gravel Aquifer and Glacial Till Unit**  
**Glenmore Landfill**  
**City of Kelowna**

Hydrogeologic Unit Monitoring Location	Units	Sand and Gravel Aquifer					Till Unit		
		GL41-3	GL23-1	GL0-3	09BH03	12082 <sup>(1)</sup>	GL41-2	GL15-2	GL0-2
Chloride	mg/L	515*	35.11	153*	32.73	54.6	476.3	417.3	12.31
Nitrate (as N)	mg/L	1.9	0.1	65.54*	2.1	1.0	n/a	n/a	n/a
Sulphate	mg/L	178	420.2	614.3	1619	2446.4	185.4	6919*	347.6
Alkalinity, total (as CaCO <sub>3</sub> )	mg/L	638.7	1217	538.3	828	-	n/a	n/a	n/a
Total Dissolved Solids	mg/L	1643	1731	2121	3146	-	n/a	n/a	n/a
Uranium	ug/L	32.0	81.0	201.9	207.8	122.6	561.9	550.2	3.5*
Lithium	ug/L	50.8	43.5	57.6	36.8	185	49.0	66.9	35.1
Sodium	mg/L	n/a	n/a	n/a	n/a	n/a	312.6	1145	114.6
Strontium	ug/L	n/a	n/a	n/a	n/a	n/a	3370	14798	1995

## Notes:

mg/L - milligrams per litre

uS/cm - microSiemens per centimetre

ND (50) - Not detected at the associated reporting limit

\* Value identified as outlier and removed from the dataset

n/a - not applicable; parameter not assessed as there were no exceedances

(1) - 95th percentile concentrations from Site ID 12082 (BC Groundwater Database)

- Alkalinity and total dissolved solids data not available from Site ID 12082



**Table 4**  
**Background Surface Water Data Summary**  
**Slough 2 and Bubna Slough**  
**Glenmore Landfill**  
**City of Kelowna**

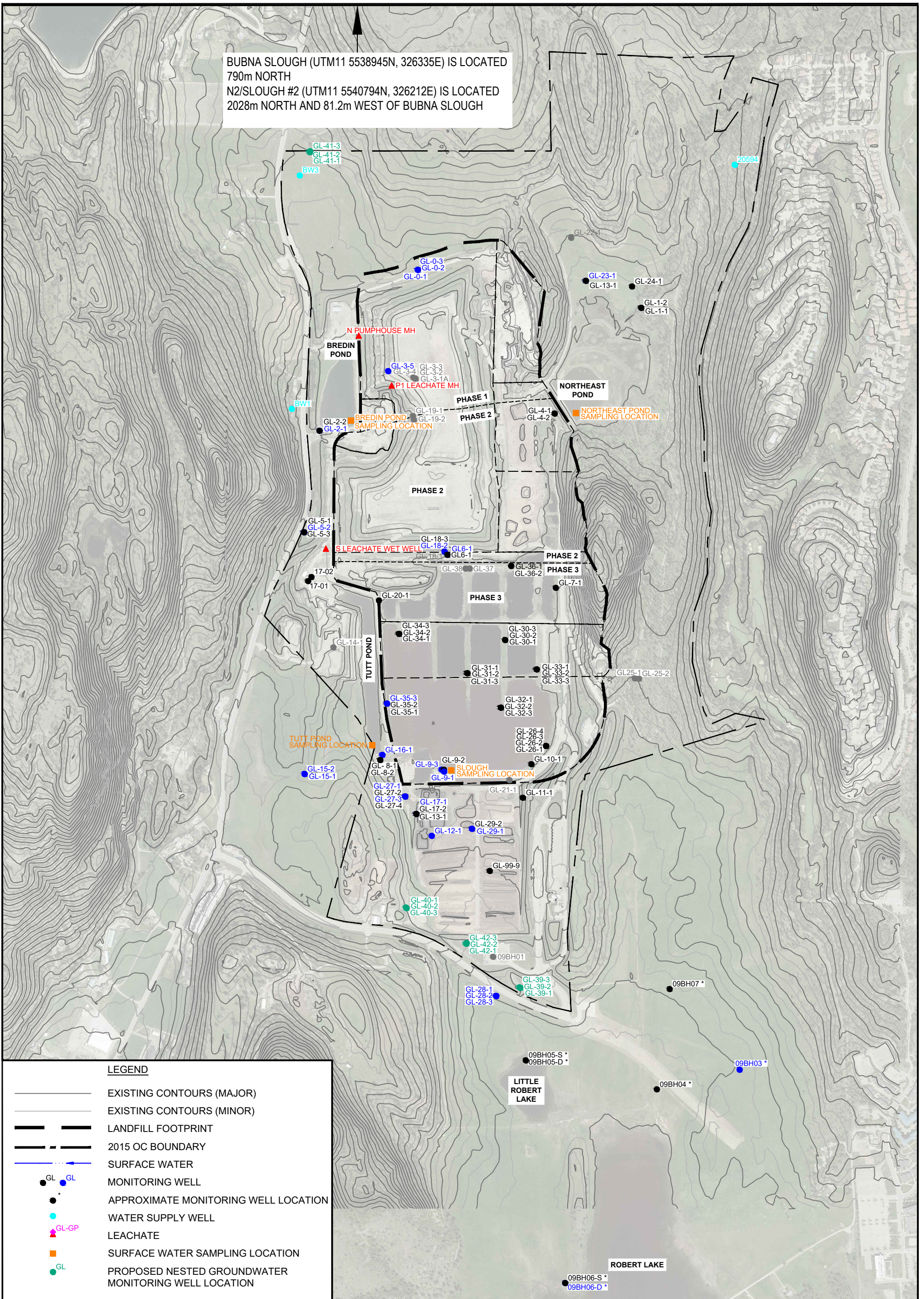
Sample Location		Slough #2	Slough #2	Slough #2	Slough #2	Slough #2	Slough #2	Bubna Slough	Bubna Slough	Bubna Slough	Bubna Slough	Bubna Slough	Bubna Slough
Sample Date		6/16/2021	10/20/2021	3/23/2022	6/21/2022	9/12/2022	10/19/2022	6/16/2021	10/20/2021	3/23/2022	6/21/2022	9/12/2022	10/19/2022
Parameter	Units												
Conductivity, field	uS/cm	4,926	5,874	3548	5057	5889	5950	3018	3587	1427	3023	3371	3403
Ammonia, Total (as N)	mg/L	0.118	1.28	0.189	0.622	0.535	1.28	0.153	0.297	ND (0.050)	ND (0.050)	0.233	0.384
Chloride	mg/L	558	568	363	643	778	759	498	581	301	552	668	665
Sulphate	mg/L	1050	1100	661	1160	1380	1410	184	219	97.7	185	217	220
Alkalinity, Total (as CaCO3)	mg/L	875	974	651	904	973	910	688	792	442	687	744	708
Phosphorus, Total (as P)	mg/L	0.0374	0.0553	0.0566	0.0582	0.148*	0.0799	0.014	0.0169	0.023	0.0235	0.02	0.0185
Aluminium	mg/L	0.0063	0.0126	0.0537	0.0179	0.0282	0.027	ND (0.002)	0.0033	0.0078	0.0039	0.0032	0.0053
Arsenic	mg/L	0.00557	0.00521	0.00337	0.00427	0.0055	0.00505	0.00179	0.00158	0.00108	0.00154	0.0016	0.0015
Chromium	mg/L	0.00026	0.00036	0.00033	0.00026	0.00022	ND (0.00025)	0.00014	0.00013	0.00018	0.00013	0.00018	0.00015
Iron	mg/L	0.0288	0.0404	0.0929	0.0343	0.0686	0.0567	0.0083	0.0067	0.0149	0.0072	0.0037	0.0067
Uranium	mg/L	0.0197	0.0302	0.0183	0.0249	0.0255	0.0305	0.00484	0.00563	0.00615	0.00493	0.00353	0.00466
Molybdenum	mg/L	0.00473	0.00733	0.00362	0.00528	0.00598	0.00658	0.00154	0.00128	0.00128	0.00138	0.00115	0.00126

Notes:  
mg/L - milligrams per litre  
uS/cm - microSiemens per centimetre  
ND (0.025) - Not detected at the associated reporting limit  
\* Value identified as outlier and removed from the dataset

# Figures



BUBNA SLOUGH (UTM11 5538945N, 326335E) IS LOCATED 790m NORTH  
 N2/SLOUGH #2 (UTM11 5540794N, 326212E) IS LOCATED 2028m NORTH AND 81.2m WEST OF BUBNA SLOUGH



**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- LEACHATE
- SURFACE WATER SAMPLING LOCATION
- PROPOSED NESTED GROUNDWATER MONITORING WELL LOCATION



CITY OF KELOWNA - GLENMORE LANDFILL  
 BACKGROUND WATER QUALITY REVIEW

**MONITORING LOCATIONS**

12605725  
 Oct 5, 2023

**FIGURE 1**



# Attachments

# **Attachment 1**



January 24, 2020

Reference No. 084612-24

Mr. Scott Hoekstra  
Solid Waste Supervisor  
City of Kelowna  
1435 Water Street  
Kelowna, BC V1Y 1J4

Dear Mr. Hoekstra:

**Re: Background Water Quality Review  
Glenmore Landfill, City of Kelowna**

## **1. Introduction**

GHD Limited (GHD) has prepared this letter report for the City of Kelowna (City) to provide a background water quality review for the Glenmore Landfill (Site). This background water quality review has been conducted as part of the action plan to address a non-compliance identified in a July 23, 2019 inspection letter *Re: Warning Letter, Operational Certificate, 12218*, from the Ministry of Environment and Climate Change Strategy (ENV).

## **2. Site Setting**

This section provides an overview of the physical Site setting.

### **2.1 Site Location and Physical Setting**

The Site is located at 2720 John Hindle Drive in Kelowna, British Columbia (BC). The Site is approximately 1.5 kilometres (km) east of Okanagan Lake and 9 km northeast of downtown Kelowna. The Site is situated in a narrow-flat bottomed valley known as Glenmore Valley surrounded by two ridges. The eastern ridge of Glenmore Valley includes Bredin Hill, located to the northeast, and Tutt Mountain, located to the southeast of the Site. Glenmore Valley trends north-south, generally parallel with Okanagan Lake, and the valley floor gradually slopes towards the south. The adjacent land uses are a combination of roads, rural developments, agricultural lands, and natural forested land.

#### **2.1.1 Site Geology and Hydrogeology**

Based on previous investigations and data interpretations, volcanic bedrock and sedimentary bedrock are encountered in the vicinity of the Site. There are bedrock outcrops in ridges along the western and eastern



sides of the valley. Overburden material is primarily found in the valley floor and pinches out towards the sides of the valley. There are three stratigraphic layers within the overburden:

- A glacial till overlying the bedrock.
- A glaciofluvial sands and gravels overlying the till.
- Glaciolacustrine silt and clay deposits overlying the glaciofluvial sands and gravels.

Although groundwater is encountered in all the stratigraphic units identified above, groundwater at the Site is interpreted to primarily flow horizontally through the sand and gravel and bedrock aquifers. Groundwater within these two aquifers is interpreted to flow towards the centre of the Site from the walls of the valley located to the east and west of the Site, however an unquantified portion of groundwater is also inferred to flow north to south along the floor of the valley. Additional monitoring wells have been installed at the Site to assist in quantifying the inferred north to south groundwater flow. The results of this investigation/analysis will be presented under separate cover.

Figure 1 presents a Site plan with the inferred groundwater flow directions.

### **2.1.2 Site Surface Water and Surface Water Drainage**

Prior to the existence of the landfill at the Site, an alkaline lake known as Alki Lake occupied the area. A surface water outlet is inferred to have been historically present at the southwest corner of Alki Lake, which flowed towards Little Robert Lake and then Robert Lake (Golder, 2012). Alki Lake was infilled by the waste and what remains of Alki Lake is currently known as the Slough. The Slough does not have any overland outlet drainages. A leachate collection pipe is located between Phase 2 and Phase 3 of the landfill footprint, which does collect water from the Slough as well as Phase 2 of the landfill.

At present-day, surface water that flows on to the Site is contained and/or managed within the Site's surface water ponds. Site surface water run-off is managed in three constructed ponds, Northeast Pond, Bredin Pond, and Tutt Pond. Surface water from the Northeast Pond flows to Bredin Pond, which flows into Tutt Pond. An overflow pipe links Tutt Pond to the Slough. The water level in Tutt Pond is managed such that flow is directed towards the Slough. Surface water from Tutt Pond is also periodically used to irrigate the agricultural lands southwest of the Site.

Within the Landfill footprint, surface water runoff is managed as leachate through infiltration into the waste mass or collection in the Slough. As mentioned, the Slough was formerly used as a waste disposal area, therefore water drained from this area is managed as leachate.

Figure 2 illustrates the Site location and surface water features near the Site.

More details regarding the Site setting, geology, hydrogeology and surface water information can be found in 2018 Design, Operations, and Closure Plan (2018 DOCP) (GHD, 2018).





### 3. Current Groundwater and Surface Water Quality Monitoring Program

#### 3.1 Current Groundwater and Surface Water Quality Monitoring Program

A groundwater and surface water monitoring program has been implemented at the Site as a part of the Site's Environmental Monitoring Program (EMP). The objective of the EMP is to detect the extent and magnitude of potential impacts to groundwater and surface water quality associated with the landfilling activities, ensure regulatory compliance, and to mitigate potential environmental risks.

#### 3.2 Groundwater Monitoring Program

This section describes the EMP undertaken in 2018 as the 2019 EMP was in progress at the time of preparing this letter report. As of November 2019, there are 73 monitoring wells located onsite and offsite to be included in the Site's EMP.

There were 82 groundwater monitoring wells included in the Site's 2018 EMP. Hydraulic monitoring is conducted at each monitoring well on a quarterly basis. For the 2018 EMP, groundwater sample collection was conducted at 23 monitoring wells during the spring monitoring event and 9 monitoring wells during the fall event. Groundwater samples are collected for analysis of general chemistry parameters, nutrients, and dissolved metals. The wells sampled during the 2018 spring monitoring event and fall monitoring event are listed in Table 3.1 and Table 3.2, respectively. The wells are grouped based on their location relative to the landfill and screened hydrostratigraphic unit.

**Table 3.1 2018 EMP - Spring**

	Waste	Clay	Sand/Gravel	Till	Bedrock
North of Phase 1 (background)			GL0-3	GL0-2	GL0-1
Northeast of Phase 1 (background)			GL23-1		
Phase 1			GL3-5		
Phase 2	GL6-1 (2011)	GL2-1	GL5-2, GL18-2*		
Phase 3			GL35-3	GL9-3	GL9-1
South of Phase 3				GL12-1	GL29-1
Southwest of Phase 3		GL27-3			GL16-1, GL17-1, GL27-1
Downgradient of the Site (compliance)		GL28-3	GL28-2	GL28-1	



	Waste	Clay	Sand/Gravel	Till	Bedrock
Downgradient of the Site			09BH06D, 09BH03		
Notes:					
* GL18-2 was decommissioned in 2019					

**Table 3.2 2018 EMP - Fall**

	Waste	Clay	Sand/Gravel	Till	Bedrock
South of Phase 3				GL12-1	GL29-1
Southwest of Phase 3				GL15-2	GL17-1, GL27-1, GL15-1
Downgradient of the Site (compliance)		GL28-3	GL28-2	GL28-1	

Groundwater samples were collected and analyzed for general chemistry parameters, nutrients, and dissolved metals. The results of the groundwater water monitoring program are summarized in the annual monitoring reports prepared by a third party consultant.

Figure 2 illustrates the locations of the groundwater monitoring wells at the Site.

### 3.2.1 Additions to the Groundwater Monitoring Program

In the 2018 DOCP, GHD proposed to include 5 more of the existing monitoring wells in the Site's groundwater monitoring program for sample collection during the spring and fall monitoring events. It is anticipated that sampling at these locations will be included in the 2020 EMP. The additional monitoring wells are listed in Table 3.3 below.

**Table 3.3 Additional Monitoring Wells From 2018 DOCP**

	Waste	Clay	Sand/Gravel	Till	Bedrock
Area 1		GL2-2, GL4-2	GL2-1, GL4-1	GL20-1	

### 3.3 Surface Water Monitoring Program

There are four surface water sampling locations included in the Site's EMP. Surface water samples are analyzed for general chemistry parameters, nutrients, and total metals. In 2018, surface water collection was conducted in April, May, September, and November. All four surface water sampling locations are on-Site surface water management ponds, as follows:

- Northeast Pond – northeast corner of the Site
- Tutt Pond – west side of the Site



- Bredin Pond – northwest corner of the Site
- Slough – central area of the Site

As indicated in the 2018 Glenmore Landfill Annual Report (2019, City of Kelowna) (2018 Annual Report), significant quantities of surface water runoff from the upstream Bubna Slough and the Glenmore-Ellison Improvement District's McKinley Reservoir flowed onto the Site in the 2018 freshet season. To manage the excess surface water, surface water was pumped from Tutt Pond to Little Robert Lake as per the Surface Water Management Plan in the Comprehensive Site Development Plan (CH2MHILL, 2008) (CSDP). Surface water samples were collected from the Bubna Slough (Bubna Discharge), Little Robert Lake, and Robert Lake during four separate sampling events in 2018 to understand the potential impacts the excess surface water may have on Site and downstream surface water quality. These monitoring locations are not part of the "routine" surface water monitoring program, therefore there is a minimal historical dataset for surface water quality at these surface water bodies.

GHD proposed 3 additional surface water monitoring locations in the 2018 DOCP in anticipation of the construction of new surface water management infrastructure at the Site. The proposed additional surface water monitoring locations include:

- North surface water pond, located north of Landfill Gas (LFG) flare compound
- South surface water pond, located at southwest corner of the limit of waste
- Background ephemeral surface water locations north of the Site

The north surface water pond and the south surface water pond will be new lined ponds on Site. These ponds are scheduled constructed over the next 10 years.

## **4. Documentation Review**

To assist with the background water quality review for the Site, the City provided GHD with reference documentation. The reference documentation includes previous reports detailing investigations completed on the properties immediately to the southeast of the Site, which are owned by the University of British Columbia Okanagan (UBCO). The City also provided GHD with a work plan prepared by SNC Lavalin to install additional monitoring wells at the Site for reference and review.

### **4.1 UBCO Water Quality Summary**

UBCO retained EBA Engineering Consultants Ltd. (EBA) to complete a series of investigations on their lands adjacent to the Site from 2008 to 2010. UBCO owns nineteen property lots (UBCO Property) located to the southeast of the Site. The investigations and the BC Ministry of Environment's (BC MOE) response to the investigations are detailed in the following documents:

- *Baseline Groundwater Quality and Surface Water Quality Assessment*, November 2008. EBA.
- *Stage 1 Preliminary Site Investigation*, February 2010. EBA.



- *Stage 2 Preliminary Site Investigation*, February 2010. EBA.
- *Background Surface Water Investigation*, March 2010. EBA.
- *Application for Background Sulphate and Ammonia in Surface Water*, March 2010. BC MOE.

The key findings of each document, which are relevant to this letter report are summarized in the subsections below.

#### **4.1.1 Baseline Groundwater Quality and Surface Water Quality Assessment, 2008. EBA**

In 2008, UBCO retained EBA to conduct a baseline groundwater and surface water quality investigation on the UBCO Property. The following work was completed in the investigation:

- Two monitoring wells were scheduled for field monitoring and groundwater sample collection – 06BH01 and 06BH02. 06BH01 was located approximately 100 metres (m) north of Little Robert Lake and 06BH02 is located approximately 400 m southeast of the Slough. 06BH01 could not be sampled as it was destroyed prior to the field event.
- Groundwater monitoring and sample collection at one monitoring well (06BH02). Groundwater samples were analyzed for general chemistry parameters, dissolved metals, and volatile organic compounds (VOCs).
- Surface water monitoring and sample collection at two surface water sampling locations (Tutt Pond and Little Robert Lake). Surface water samples were collected for analysis of general chemistry parameters and total and dissolved metals.
- The groundwater sample analytical results were compared to the BC Contaminated Sites Regulation generic numerical water quality standards of the day for Aquatic Life, Irrigation, Livestock, and Drinking Water use. Groundwater analytical results were also compared to the BC Water Quality Guidelines for Freshwater Aquatic Life, Irrigation, Livestock, and Drinking Water use.
- Previous groundwater results from a monitoring well screened below the waste at the Glenmore Landfill was also included in the report for reference. The name of the monitoring well is not provided in this document.
- Data from a 'background' monitoring well is also included in the document, but the name of the monitoring well is not provided. The "background" monitoring well is described as being located up-gradient and cross gradient of the landfill footprint as leachate indicator parameter concentrations in groundwater sampled from this well were significantly lower than leachate concentrations measured in groundwater collected from wells located within the vicinity of the landfill. The range of concentrations recorded in the 'background well' for a number of water quality parameters between August 1993 and September 2003 are presented in the following table. In the document, the range of sodium concentrations between 1994 and 1996 were provided as a footnote in a table, the following table presents this data in the same format.



**Table 4.1 Summary of UBCO Background Groundwater Concentrations - EBA 2008**

Parameter	Range of concentrations (mg/L) in groundwater collected from the 'background' well August 1993 - September 2003
Sulphate	93 – 145
Sodium	63.4 – 71.4*
Hardness (CaCO <sub>3</sub> )	220 – 342
Dissolved calcium	50 – 75
Dissolved magnesium	34 – 49
Dissolved manganese	0.05 – 0.35
Dissolved chloride	5 - 30
* Between November 1996 and September 2003. Concentrations were between 299 mg/L and 658 mg/L in 1994, 1995, and 1996.	

- Surface water analytical results were compared to the BC Water Quality Guidelines for Freshwater Aquatic Life, Irrigation, and Livestock.
- Concentrations of sulphate, sodium, and hardness were elevated in groundwater samples beneath the UBCO Property.
- Volatile organic compounds (VOC) were not detected in groundwater collected from 06BH02 in 2008. EBA compared the 2008 results to previous results from 2006, and noted trace concentrations of VOCs in groundwater collected from 06BH01 and 06BH02.
- Available information at the time of the investigation and a lack of water observed in Robert Lake indicated that the aquifer most likely to be impacted by leachate is not hydraulically connected to Robert Lake or the small pond (Little Robert Lake) on the UBCO Property, however further testing was recommended to confirm this observation. EBA indicated the slightly elevated levels of calcium, magnesium, and manganese in groundwater beneath the UBCO Property may be naturally occurring, and derived from the igneous bedrock or highly mineralized sedimentary bedrock in the area.
- EBA noted that elevated levels of sulphate in groundwater beneath the UBCO Property may also be a naturally-occurring phenomenon or background concentration, and not due to the landfill. It was indicated that a detailed hydrogeological study is required to confirm this.
- EBA concluded landfill leachate has not migrated to the UBCO property according to the interpretation of the concentration of chloride.
- EBA recommended further assessment of surface water hydrology and groundwater hydrogeology around the small pond (Little Robert Lake) was required to understand the level of interaction between the small pond and the sand and gravel aquifer.



#### **4.1.2 Stage 1 Preliminary Site Investigation, 2010. EBA**

- In 2009 to 2010, EBA conducted a Stage 1 Preliminary Site Investigation (PSI) at the UBCO Property. The investigations were completed on behalf of UBCO.
- EBA indicated the groundwater standards for the protection of aquatic life are considered to apply as aquatic habitat is located within 1 km to the UBCO Property. EBA indicated the CSR groundwater standards for drinking water (DW), livestock watering (LW) and irrigation watering (IW) do not apply to the UBCO Property.
- EBA identified the Glenmore Landfill as an area of potential environmental concern (APEC) for the UBCO Property as the groundwater beneath the Glenmore Landfill may flow toward the UBCO Property thus potentially contaminating it.
- The identified potential contaminants of concern (PCOC) included chloride, nitrate, sulphate, manganese, iron, and sodium as parameters associated with landfilling activities.
- A Stage 2 environmental investigation was considered warranted by EBA.

#### **4.1.3 Background Surface Water Investigation, 2010. EBA**

- EBA sampled two off-site reference ponds, N1 (Bubna Slough) and N2 (unnamed pond). N1 and N2 are alkaline surface water bodies similar in physical nature and lie within the same geologic setting to an unnamed small pond (Little Robert Lake) and Robert Lake in UBCO Property.
- EBA characterized water quality in an unnamed small pond (Little Robert Lake), Robert Lake, and N1 and N2 reference ponds. There was a wide variation in concentrations of sulphate and ammonia nitrogen that were also greater than the CSR AW standards of the day.
- Based on the analytical results, EBA concluded the water chemistry of the alkaline ponds is naturally variable. The variable water chemistry is likely a result of naturally occurring biophysical and chemical processes found in alkaline environments and the natural mineral and salt constituents found in the Glenmore Clay in which these ponds lie.
- There were no anthropogenic sources of sulphate and ammonia identified by EBA on the UBCO Property.
- EBA conducted a statistical review of the collected surface water quality data for sulphate and ammonia using the methodology detailed in the document *Protocol 9; Determining Background Groundwater Quality* (BC MOE, 2004). EBA concluded the 95<sup>th</sup> percentile concentrations of sulphate and ammonia nitrogen using both parametric and non-parametric methodologies are likely to be in the range of 15,000 mg/L to 20,000 mg/L for sulphate and 10.9 mg/L to 14.7 mg/L for ammonia nitrogen.
- EBA concluded that water quality in an unnamed small pond (Little Robert Lake) and Robert Lake reflect naturally occurring conditions and were no evidence of anthropogenic contamination.



#### **4.1.4 Stage 2 Preliminary Site Investigation, 2010. EBA**

- Eight boreholes (09BH01 to 09BH07 and 06BH01) were advanced and completed as groundwater monitoring wells on the UBCO Property. Four of the eight wells were completed as nested shallow and deep pairs.
- Groundwater was encountered at various depths, ranging from near ground surface in southerly wells to approximately 6 m below ground surface at 09BH03. No significant difference in groundwater elevation was observed between the nested well pairs.
- Using the BC CSR standards of the day, EBA concluded that CSR Drinking Water, Irrigation and Livestock standards do not apply to groundwater quality at the UBCO Property. EBA also concluded that the CSR Aquatic Life standards do not apply to the UBCO Property as no hydraulic connection exists between confined groundwater potentially affected by the Site and the surface water bodies on UBCO Property, and groundwater travel time to UBCO Property and downgradient surface water bodies was in excess of 50 years.
- EBA consulted with the MOE and determined that the BC CSR AW standards were appropriate for the UBCO Property based on the following rationale:
  - Ponds at UBCO Property are saline and water chemistry is generally hostile to aquatic life.
  - Ponds do not support trout or other fish species of value.
  - Ponds do not discharge to fish bearing water courses or other surface water bodies.
  - Ponds dry up seasonally.
- EBA reviewed the groundwater analytical results and noted that concentrations of chloride, sulphate, calcium, chromium, magnesium, manganese, selenium and sodium were elevated.
- The analysis of surface water samples collected from an unnamed small pond (Little Robert Lake) and Robert Lake found concentrations of the PCOCs to be less than the CSR AW standard, with the exception of dissolved sulphate and ammonia nitrogen.

The MOE reviewed EBA's report entitled *Background Surface Water Investigation* dated January 2010 and a revised report entitled *Background Surface Water Investigation* dated March 3, 2010. Based on the review, MOE responded in a letter entitled *Re: Application for Determination of Background Sulphate and Ammonia Nitrogen in Surface Water* dated March 9, 2010 accepting the report's conclusion that the representative background concentration of sulphate in surface water, at the UBCO Property, was 20,200 mg/L and ammonia nitrogen in surface water was 14.7 mg/L.

#### **4.2 Planned Expansion of Monitoring Well Network in 2019**

In accordance to the 2018 DOCP, SNC-Lavalin Inc. (SNC) proposed to install three nested monitoring wells at three locations along the southern property line of the Site and one monitoring well nest at one upgradient background location (Figure 1).





Each of the monitoring well nests installed along the southern property line will target the clay, sand, and till hydrostratigraphic units. After developing the wells, single well response testing and sampling will be completed for the purpose of:

- Determining hydraulic conductivity and groundwater flow velocity through each hydrostratigraphic unit.
- Attempt to characterize the flux of groundwater flowing through the Slough.
- Model the potential geochemical impacts to groundwater quality at the southern property line and within the Slough as recommended in the DOCP.

Currently all the upgradient background monitoring are located northeast to the landfill footprint. Nested monitoring wells GL0-1/2/3 will be decommissioned in 2020 to make way for the landfill expansion. The background nested monitoring wells described above are intended to replace GL0-1/2/3. The new background monitoring wells will also assist in determining the background groundwater quality in the northwest portion of the Site.

## 5. Background Water Quality Characterization

To attempt to characterize the background groundwater and surface water quality for the Site, GHD prepared a piper plot and completed a statistical analysis of the groundwater and surface water data available to GHD.

### 5.1 Piper Plots

To understand the groundwater quality trends of major ions for Site groundwater, a piper plot was generated using summer 2018 groundwater and leachate analytical results. Groundwater data from monitoring wells located north, northwest, southwest, and southeast of the landfill footprint as well as leachate data was included in the piper plot. The symbols for each monitoring well plotted in the piper plot are colour coded based on the screened hydrostratigraphic unit as summarized in Table 5.1. The piper plot is presented in Figure 3.

**Table 5.1 Monitoring Wells Included in Piper Plots**

Monitoring Well	Location Relative to Landfill Footprint	Screened Hydrostratigraphic Unit	Symbol Colour
GL0-1	North	Till/Bedrock	Green
GL0-2	North	Till	Blue
GL0-3	North	Sand and Gravel	Orange
GL1-1	North	Till	Blue
GL1-2	North	Clay/Sand and Gravel	Orange
GL2-1	Northwest	Clay	Red
GL15-1	Southwest	Bedrock	Green



Monitoring Well	Location Relative to Landfill Footprint	Screened Hydrostratigraphic Unit	Symbol Colour
GL15-2	Southwest	Sand and Gravel	Blue
GL23-1	North	Sand	Blue
GL24-1	North	Sand and Gravel	Blue
GL28-1	South	Till	Blue
GL28-2	South	Sand and Gravel	Orange
GL28-3	South	Clay	Red
09BH03	Southeast	Sand	Orange
09BH06-D	Southeast	Sand and Gravel	Orange

From review of Figure 3, a majority of the groundwater wells plot in a similar area in the centre of the piper plot. This indicates the ratio of major ions in groundwater chemistry is similar for these locations, indicating groundwater at these monitoring locations appears to have a similar source. It also appears that the ratio of major ions for the monitoring well nests do not drastically vary between the different hydrostratigraphic units.

Conversely, the leachate data points all plot in the bottom end of the diamond opposite from the groundwater data points, indicating little to no similarities between the groundwater chemistry ratios of major ions and leachate chemistry ratios for major ions.

Where groundwater is impacted by landfill leachate, the impacted groundwater data point typically plots between the leachate data point and background groundwater data point on a piper plot. This illustrates a “mixing” trend between the background groundwater and landfill leachate in typical cases where groundwater is impacted by landfill leachate.

## 5.2 Statistical Review of Site Background Water Quality

To characterize background groundwater and surface water quality for the Site, GHD completed a statistical review of the available water quality data for the Site. The statistical analysis for the background groundwater and surface water characterization was completed in accordance with BC ENV documents *Protocol 9 Determining Background Groundwater Quality* (BC ENV, 2018) (Protocol 9).

As per Protocol 9, to characterize background water quality for a site, at least three monitoring locations that represent unimpacted (i.e. no anthropogenic influence) water quality should be used. In cases where the site takes up a large area, additional sampling locations may be required. Protocol 9 also states that at least two water samples per year (e.g. spring and fall) should be collected from the sampling locations to account for seasonal fluctuations in water quality.



## 5.2.1 Background Groundwater Quality

### *Inputs*

To complete the background groundwater quality characterization for the Site, GHD reviewed the available groundwater monitoring data for the Site. As indicated in Section 2.1.1, groundwater generally flows radially to the centre of the Site with a portion of groundwater flowing towards the south. Therefore to characterize background groundwater quality for the Site, groundwater quality from the north, east, and west should be considered. Furthermore, there are four hydrostratigraphic units at the Site, therefore background groundwater quality should be characterized for each hydrostratigraphic unit separately.

In recent years, most of the groundwater monitoring wells that are sampled at the Site are sampled once per year in the spring. GHD reviewed the analytical results for the Site from 1993 to 2001, which included spring and fall sampling events and found there were minimal seasonal fluctuations in Site groundwater quality.

The City also provided GHD with historical data from former water supply wells BW-1 and BW-3, both of which were located north of the landfill footprint.

Table 5.2 summarizes the monitoring wells that may be considered to be used to characterize background groundwater quality, the well's location relative to the landfill footprint, and screened hydrostratigraphic unit.

Waste disposal, composting and agricultural activities have occurred at and around the Site for many decades. As a result, it is difficult to quantify true "untouched" background groundwater conditions for the Site. The historical activities at and around the Site that have occurred in the vicinity of each monitoring well are also summarized in the Table 5.2 below.

**Table 5.2 Monitoring Wells Considered for Background Groundwater Characterization**

Monitoring Well	Location Relative to Landfill Footprint	Screened Hydrostratigraphic Unit	Historical Activities	Date of Activities
GL0-1	North	Till/Bedrock	-Composting and biosolids	-1993-2004, possibly earlier than 1993
GL0-2	North	Till	-Beverage manufacturing waste application as fertilizer replacement	-Beverage manufacturing waste application 2006-2008
GL0-3	North	Sand and Gravel	-Composting and leachate spill	-Composting 1978-1994
GL1-1	North	Till	-Beverage manufacturing waste application as fertilizer replacement	-Biosolids 1990-1994
GL1-2	North	Clay/Sand and Gravel		-Leachate spill 2016



Monitoring Well	Location Relative to Landfill Footprint	Screened Hydrostratigraphic Unit	Historical Activities	Date of Activities
				-Beverage manufacturing waste application 2006-2008
GL2-1	Northwest	Sand	Woodwaste and fill material in area	Unknown
GL15-1	Southwest	Bedrock	Agriculture	Since 1959, at least
GL15-2	Southwest	Sand and Gravel	Agriculture	
GL23-1	North	Sand	Composting and leachate spill	-Composting 1978-1994
GL24-1	North	Sand and Gravel	-Composting and leachate spill -Beverage manufacturing waste application as fertilizer replacement	-Biosolids 1990-1994 -Leachate spill 2016 -Beverage manufacturing waste application 2006-2008
09BH03	Southeast	Sand	Agriculture	Since 1959, at least
09BH06-D	Southeast	Sand and Gravel	Agriculture	Since 1959, at least

GL15-1 and GL15-2 are nested monitoring wells located to the southwest and upgradient of the landfill footprint, however surface water from Tutt Pond is at times used to irrigate the fields in the vicinity of these monitoring locations. As indicated in Section 2.1.2, surface water in Tutt Pond is sourced from stormwater run-off upstream of the landfill, therefore irrigating the fields in the vicinity of GL15-1/GL15-2 with water from Tutt Pond should not result in leachate impact to groundwater quality in this area. However, due to the perceived interference from using surface water from Tutt Pond for irrigation, GL15-1/GL15-2 have been excluded from the statistical analysis.

09BH06-D is located south of the landfill footprint adjacent to Little Robert Lake and may be located in the southerly flow path of groundwater from the landfill. For this statistical analysis 09BH06-D has also been excluded.

GL1-1/GL1-2, GL23-1, and GL24-1 are all located in the vicinity of a recent leachate spill, which occurred in 2016. Groundwater quality in these monitoring locations may not be representative of background conditions for the Site due to the recent leachate spill. As a result, these monitoring locations have been excluded from the statistical analysis.



Based on the identified historical activities in the potential background areas discussed above, and the exclusion of certain wells to be used for the statistical analysis, it appears there are a sufficient number of monitoring wells to only complete the statistical analysis for the sand and gravel unit.

The statistical analysis to determine the background conditions of selected parameters was completed for parameters greater than or similar to the applicable CSR groundwater standards at compliance location GL28-2 over the last three years. GHD notes that groundwater quality at the GL28-1/2/3 well series is also compared to the BC Water Quality Guidelines (WQGs) for Irrigation and Freshwater Aquatic Life as well as the Guidelines for Canadian Drinking Water Quality (GCDWQ). There have been exceedances for other parameters (e.g. fluoride, aluminum, and sodium) for the applicable WQGs and/or the GCDWQ over the past three years. Due to the limited quantity of suitable background groundwater monitoring locations for the Site, only the parameters exceeding the applicable CSR water quality standards were focused on in this letter report. Further statistical analyses for the parameters detected in concentrations greater than the applicable WQGs and/or the GCDWQ in groundwater at GL28-2 should be completed once additional background monitoring locations become available.

The analysis was completed for the following parameters:

- Conductivity
- Sulphate
- Nitrate
- Total dissolved solids (TDS)
- Manganese
- Molybdenum
- Uranium

The analytical results considered in the statistical analysis are summarized in the attached Table 1. The data presented in Table 1 includes annual groundwater analytical results for monitoring wells GL0-3, GL2-1, 09BH03 from 2016, 2017, and 2018. Table 1 also includes 1994 - 1999 groundwater analytical results for wells BW-1 and BW-3 provided by the City.

### ***Statistical Analysis***

The statistical analysis was completed in three trials for each parameter to include different groups of monitoring wells in the analysis. The well groups for each of the three trials are summarized in Table 5.3 below.



**Table 5.3 Statistical Analysis Trial Groups**

Trial Number	Trial Name	Wells Included
1	North Wells	GL0-3, GL2-1
2	North and East Wells	GL0-3, GL2-1, 09BH03
3	North and BW Wells	GL0-3, GL2-1, BW-1, BW-3

The North Wells were selected as they are all monitoring wells located north of the landfill footprint and hydraulically upgradient of the Site (Figure 1). The North Wells are interpreted to represent groundwater unimpacted by landfill activities. The North and East Wells trial group includes the same monitoring wells in the North Wells trial group plus 09BH03. 09BH03 is located southeast of the landfill footprint and is hydraulically upgradient/cross-gradient of the Site (Figure 1). 09BH03 is also interpreted to represent groundwater quality that is unimpacted by landfill activities. The North and BW Wells trial group includes the same monitoring wells as the North Wells plus BW-1 and BW-3. BW-1 and BW-3 are historic water wells that were located north or west of the landfill footprint (Figure 1). BW-1 and BW-3 are also interpreted to be hydraulically upgradient of the Site and represent unimpacted groundwater quality for the Site.

To complete the statistical analysis, the available dataset is processed to determine if the dataset creates a normal distribution. If the dataset is a normal distribution, the 95<sup>th</sup> percentile concentration may be used as the Site specific background concentration for a given parameter.

The results for each statistical analysis are summarized in Table 2, attached.

From review of Table 2, only four parameters have normal distributions under Trial 1, one parameter has a normal distribution under Trial 2, and two parameters have normal distributions under Trial 3. The results of the normal distribution datasets are summarized in Table 5.4 below.

**Table 5.4 Statistical Analysis Trial Groups**

Trial Number	Parameter	Units	95 <sup>th</sup> Percentile Result	GL28-2 Range*
1	Conductivity, field	uS/cm	2,492.7	3,974 - 5,093
1	Total dissolved solids	mg/L	1,776.2	4,400 - 5,370
1	Molybdenum	µg/L	17.5	3.9 - 5.5
1	Sulphate	mg/L	380.2	2,590 - 3,160
2	Uranium	mg/L	198.4	168 - 200
3	Conductivity, field	uS/cm	2,878.4	3,974 - 5,093
3	Molybdenum	µg/L	23.7	3.9 - 5.5

\*Concentration range for 2018 data collected by Kelowna

From review of Table 5.4, molybdenum is the only parameter from the statistical analysis that has 95<sup>th</sup> percentile values that are greater than the historical concentration range detected at compliance location GL28-2. Uranium's 95<sup>th</sup> percentile result in Trial 2 is slightly less than the upperbound limit for the historical concentrations range detected in groundwater at GL28-2.



For the parameters not included in Table 5.4, their datasets either had logarithmic distributions or appeared to have multiple populations. Groundwater quality for each area relative to the landfill footprint (i.e. north, east, and west) is only represented by one monitoring location, which appears to be insufficient for representing the variable groundwater conditions surrounding the Site.

## 5.2.2 Background Surface Water Quality

### *Inputs*

To complete the background surface water characterization for the Site, GHD reviewed the available dataset for surface water quality near the Site. The surface water sampling locations included in the routine EMP for the Site do not include an upstream sampling location. As a result, surface water analytical results from non-routine sampling locations and surface water samples collected by others were considered for this characterization.

Table 5.5 below summarizes the surface water sampling locations and their location relative to the landfill footprint.

**Table 5.5 Surface Water Locations Considered for Background Characterization**

Surface Water Sampling Location	Location Relative to Landfill Footprint
Bredin Pond	West - On site
Tutt Pond	West - On site
Northeast Pond	East - On site
Slough <sup>(1)</sup>	South - On site
Bubna Slough/N1	North
N2	North
Little Robert Lake <sup>(2)</sup>	South
Robert Lake	South
Notes:	
<sup>(1)</sup> Surface water from Slough managed as leachate due to historical waste disposal in the Slough.	
<sup>(2)</sup> Surface water was discharged from Tutt Pond to Little Robert Lake in spring 2018 due to high water levels experienced throughout the region.	

Figure 2 illustrates the locations of the surface water sampling locations. From review of Table 5.5, surface water sampling locations Bubna Slough/N1 and N2, are upstream relative to the Site. The ponds are alkaline surface water bodies similar in physical nature to the Little Robert Lake (EBA, 2010). The analytical results from these surface water sampling locations were used in the statistical analysis.

The statistical analysis to determine the background surface water conditions of selected parameters was completed for parameters greater than or similar to the BC CSR water quality standards for Irrigation and/or the BC WQGs for Irrigation in Little Robert Lake as noted in the July 23, 2019 ENV inspection letter.





The statistical analysis was completed for the following parameters:

- Sulphate
- Chloride
- Ammonia
- pH
- Conductivity

The analytical results considered in the statistical analysis are summarized in the attached Table 3. The data presented in Table 3 includes quarterly analytical results for upstream surface water monitoring locations Bubna Slough/N1 from 2018. Table 3 also includes 2009-2010 surface water analytical results for upstream surface water locations Bubna Slough/N1 and N2 collected by others.

### ***Statistical Analysis***

To complete the statistical analysis, the available dataset is processed to determine if the dataset creates a normal distribution. If the dataset is a normal distribution, the 95<sup>th</sup> percentile concentration may be used as the Site specific background concentration for a given parameter.

The results for statistical analyses completed for each parameter are summarized in Table 4, attached.

From review of Table 4, conductivity and pH are the only parameters from the statistical analysis that have 95<sup>th</sup> percentile values that are greater than the historical concentration range detected at compliance location Little Robert Lake.

For the other parameters in this analysis, their datasets appeared to have multiple populations. As presented in Table 4, a portion of the data used in this analysis is from 2009-2010 and the other portion is from 2018. It may be beneficial to collect additional data from the two background surface water bodies considered in this analysis to create a more recent dataset.

In the *Background Surface Water Investigation*, EBA estimated the background concentrations for ammonia and sulphate in surface water to be 14.7 mg/L and 20,200 mg/L, respectively. This result was not replicated in this analysis. This may be due to a change in background surface water quality conditions in 2018 compared to 2009-2010 when EBA's investigation was completed.



## 6. Limitations

Based on the results of the statistical analysis, it appears there are a number of limitations and/or data gaps that affected the results of the analysis. The limitations are summarized as follows.

### *Groundwater*

- At least three monitoring wells are required to complete a statistical analysis to characterize background groundwater quality as per BC ENV Protocol 9. There are four hydrostratigraphic units at the Site, however only one of the hydrostratigraphic units had at least three monitoring wells upgradient of the landfill footprint. As a result, the background groundwater characterization analysis was completed for the sand and gravel unit only in this letter report. The new monitoring well nest north of the landfill footprint will provide sufficient monitoring wells for analysis of the till unit. One more location is required for the bedrock and two more locations are required for the clay unit in order to complete a statistical analysis in accordance with BC ENV Protocol 9.
- A majority of the groundwater monitoring locations that were used in the analysis were north of the limit of waste, however groundwater is also interpreted to flow on to the Site from the east and west. Additional locations to the east and west (minimum one in each area) may assist in characterizing background groundwater quality for the Site.
- Groundwater quality in the surrounding areas of the Site may be impacted by numerous historical activities including composting, biosolids storage, fill storage, leachate spills, and agriculture. As a result, it is difficult to assess “untouched” water quality conditions for the Site. GL1-2, GL23-1, and GL24-1 were excluded from the statistical analysis due to a recent leachate spill in the vicinity of these monitoring wells.
- Groundwater quality at GL15-2 appears to have groundwater quality similar to GL28-2, however the area around GL15-2 is periodically irrigated using surface water from Tutt Pond. Surface water in Tutt Pond is sourced from surface water run-off upstream of the landfill footprint, therefore leachate impacts should not be apparent in groundwater at GL15-2. Nevertheless, GL15-2 was excluded from the statistical analysis due to the perceived interference from the irrigation activities.
- Some of the data included in the statistical analysis was from the late 1990s and may no longer be representative of current groundwater quality conditions.
- There are composting operations occurring in the southern portion of the Site between the landfill footprint and the compliance groundwater monitoring wells. This statistical analysis completed in this letter did not capture if groundwater quality is being influenced by the composting activities.



### *Surface Water*

- At this time, there are no upstream surface water monitoring locations regularly included in the Site's EMP.
- The surface water data used from EBA's 2009-2010 investigation may not be representative of current background surface water conditions.

## **7. Summary**

Based on the results of the background water quality characterization exercise, GHD summarizes the following:

- EBA conducted a statistical review for surface water quality for sulphate and ammonia at the UBCO Property in 2009. EBA concluded that the appropriate background concentration ranges for surface water quality were 15,000 mg/L to 20,000 mg/L for sulphate and 10.9 mg/L to 14.7 mg/L for ammonia nitrogen.
- In 2010, the BC MOE accepted EBA's conclusion that the representative background concentrations of sulphate in surface water was 20,200 mg/L and ammonia nitrogen in surface water was 14.7 mg/L at the UBCO Property.
- Groundwater quality for upgradient and compliance groundwater monitoring locations has a different proportional make-up of major ions compared to leachate data for the Site. A mixing trend between upgradient groundwater, leachate, and compliance locations groundwater is not apparent in the piper plot results.
- The statistical analysis to estimate the background concentration for certain groundwater parameters yielded mixed results. A majority of the statistical analyses completed indicated a logarithmic distributions or multiple populations existed for the available groundwater data and therefore a background concentration could not be determined.
- A majority of the groundwater monitoring wells used in the statistical analysis are located north of the landfill footprint, however groundwater is also interpreted to flow on to the Site from the east and west. Additional locations to the east and west (minimum one in each area) may assist in providing a more comprehensive data set for the statistical analysis.
- Background groundwater concentrations were estimated to be greater than the 2018 concentration range for groundwater quality at GL28-2 for two parameters:
  - Molybdenum: 23.7 mg/L or 24.6 mg/L
  - Uranium: 205 mg/L
- A majority of the statistical analyses completed indicated logarithmic distributions or multiple populations existed for the available surface water data.



- Background surface water concentrations were estimated to be greater than the 2018 concentration range for surface water quality at Little Robert Lake for two parameters:
  - Conductivity: 4,799.6 uS/cm
  - pH: 9.7

## 8. Recommendations

Based on the findings and limitations of this background water quality study, GHD provides the following recommendations to aid with determining representative background concentrations for the Site:

- Review the results of the one nested monitoring well installed north of the landfill footprint and the three nested monitoring wells installed in the southern area of the Site.
- Include an additional well located on the UBCO Property (09BH07) in the Site's EMP to further characterize groundwater quality southeast of the landfill footprint.
- Consider installing nested monitoring wells to the west of the Site away from the agricultural properties located west of the Site to characterize groundwater southwest of the landfill footprint.
- Collect surface water samples at least twice per year (spring and fall) from surface water bodies Bubna Slough/N1 and N2 to further characterize background surface water quality for the Site.
- Complete statistical analysis to establish background concentrations, using the data from the proposed background well locations.

Sincerely,

GHD

Michaela Dyck, G.I.T.

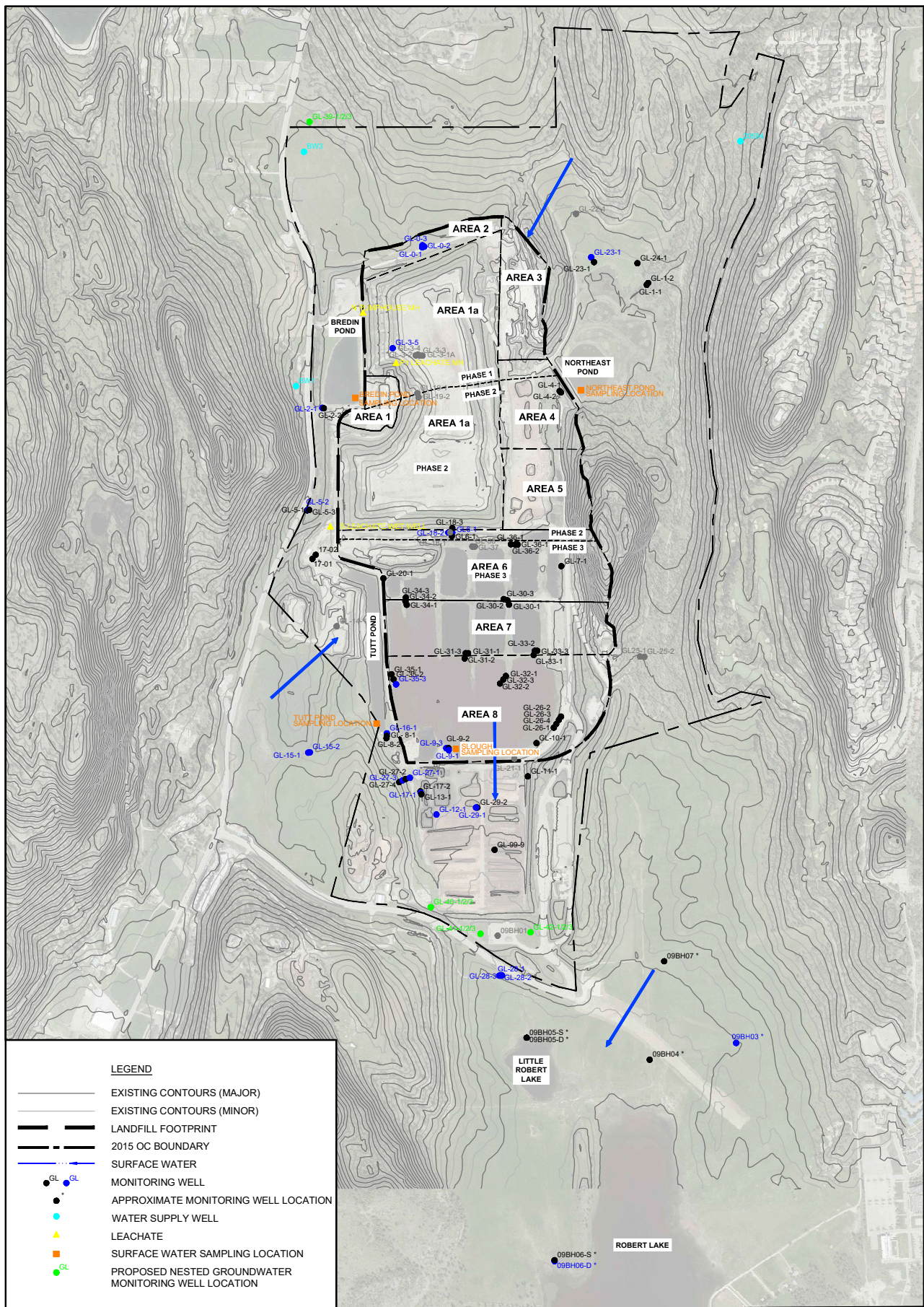
MND/cs/02

Encl.

cc: Deacon Liddy (GHD)  
Roxy Hasiar (GHD)

Michelle Uyeda, P.Eng., CSAP





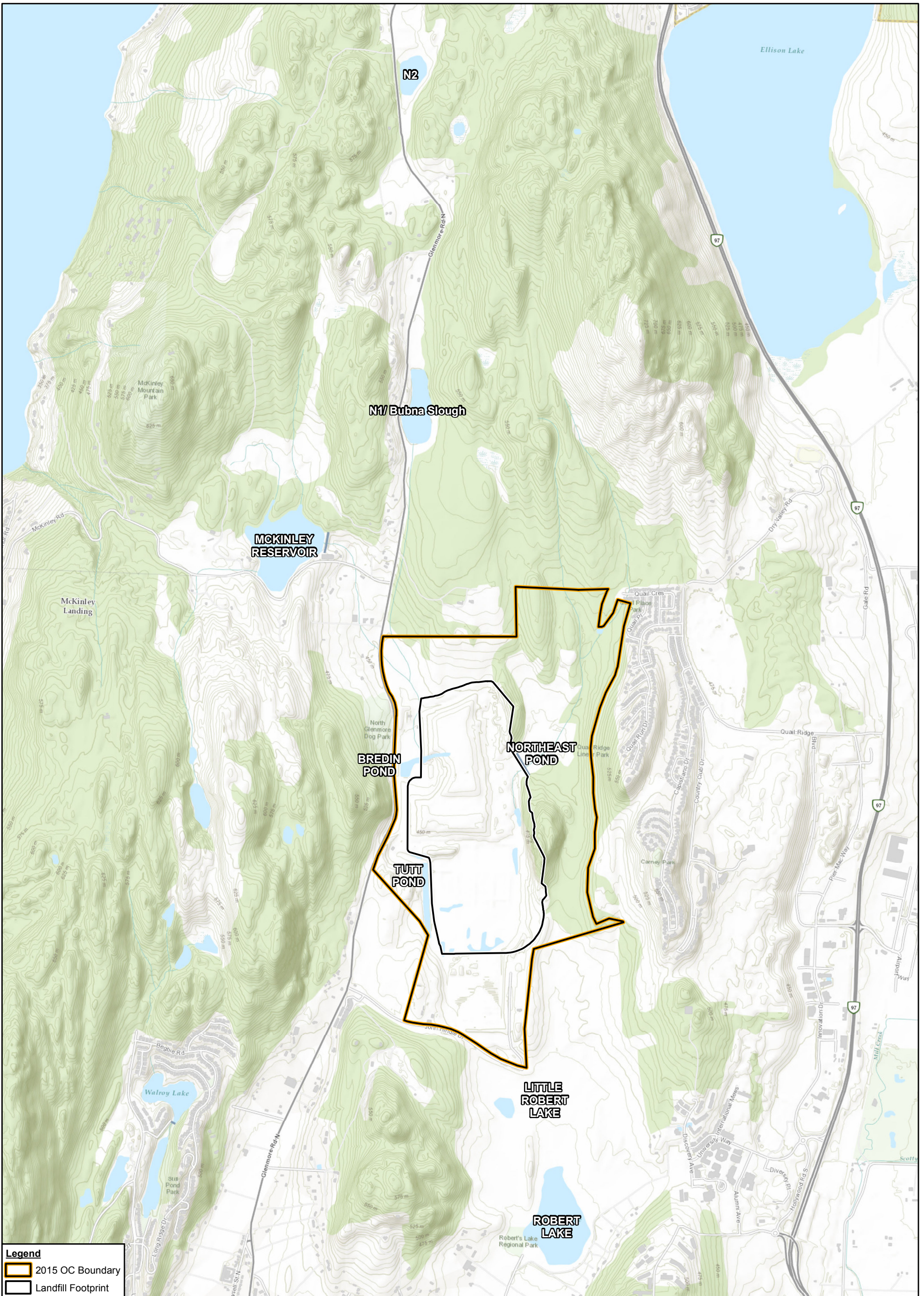
CITY OF KELOWNA - GLENMORE LANDFILL  
BACKGROUND WATER QUALITY REVIEW

MONITORING LOCATIONS

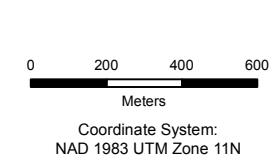
084612-22  
Dec 18, 2019

FIGURE 1





Source: ESRI Topographic Basemap - Accessed 2019



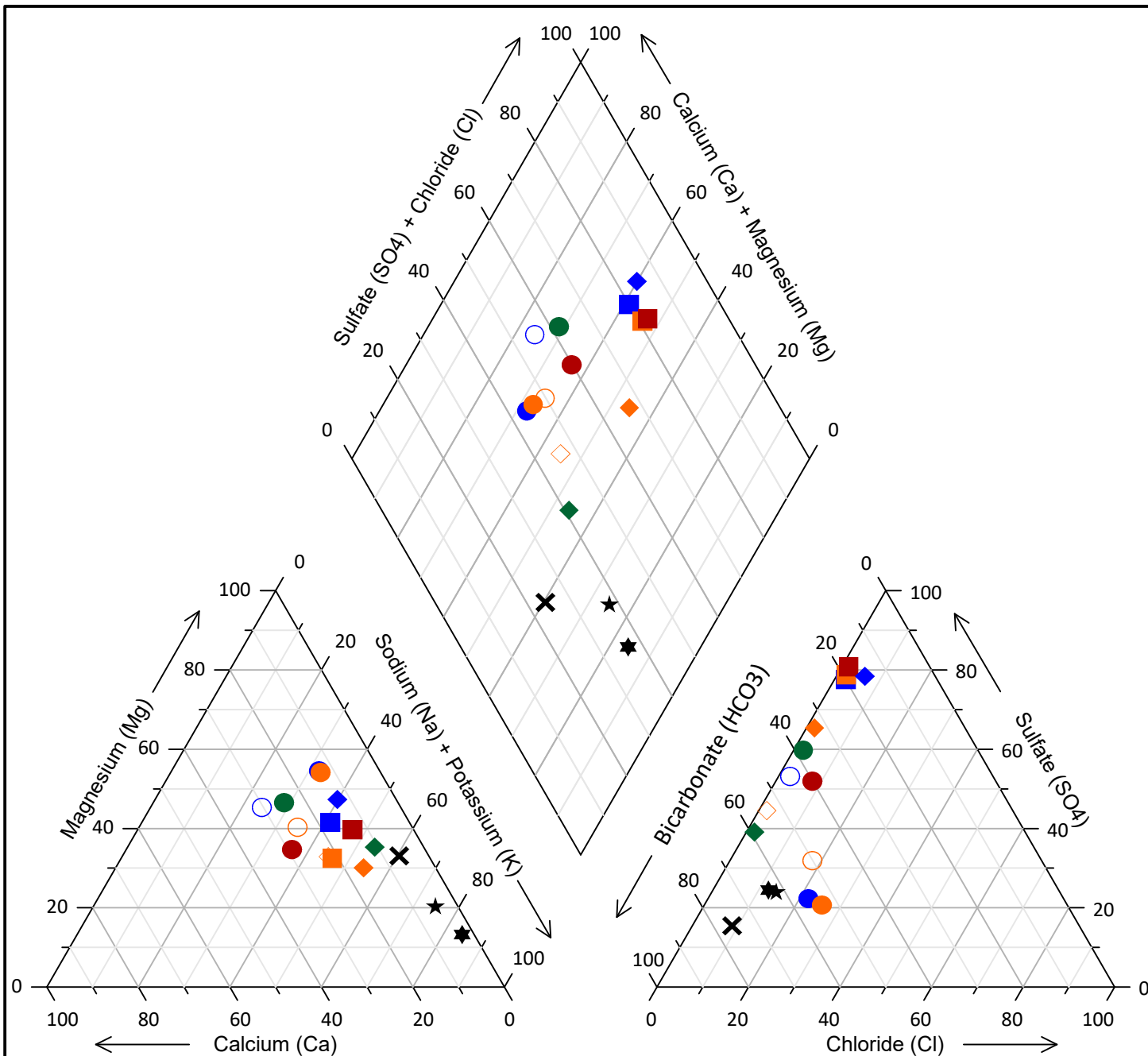
BACKGROUND WATER QUALITY REVIEW  
 GLENMORE LANDFILL  
 CITY OF KELOWNA

SURFACE WATER MONITORING LOCATIONS

084612  
 Oct 17, 2019

FIGURE 2





**LEGEND**

Background Wells	Downgradient Wells	Other Wells	Leachate
● GL1-1	■ GL28-1	◆ 09BH03	★ N Pumphouse MH
● GL1-2	■ GL28-2	◇ 09BH6-D	✕ P1 Leachate MH
● GL0-1	■ GL28-3	◆ GL15-1	★ S Leachate Wet Well
○ GL0-2		◆ GL15-2	
○ GL0-3			
● GL2-1			



GLENMORE LANDFILL  
CITY OF KELOWNA  
BACKGROUND WATER QUALITY REVIEW

**PIPER PLOT**

084612  
December 16, 2019

**FIGURE 3**



**Table 1**  
**Groundwater Data Summary**  
**Background Water Quality Review**  
**Glenmore Landfill**  
**City of Kelowna**

<b>Sample Location</b>		<b>GL0-3</b>	<b>GL0-3</b>	<b>GL0-3</b>	<b>GL2-1</b>	<b>GL2-1</b>	<b>GL2-1</b>	<b>GL2-1</b>	<b>09BH03</b>	<b>09BH03</b>	<b>09BH03</b>
<b>Sample Date</b>		<b>24-05-16</b>	<b>24-05-17</b>	<b>29-05-18</b>	<b>24-05-16</b>	<b>24-05-16</b>	<b>24-05-17</b>	<b>28-05-18</b>	<b>24-05-16</b>	<b>24-05-16</b>	<b>01-06-17</b>
<b>Sampled By:</b>		<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>
<b>Parameter</b>	<b>Units</b>										
Conductivity, field	uS/cm	1980	2066	1826	1080	1080	1222	-	2650	-	3010
Sulphate	mg/L	401	368	293	275	283	323	319	909	521	1240
Nitrate (as N)	mg/L	49.1	48.7	44.7	0.097	0.068	< 0.025	< 0.250	0.69	0.7	0.69
Total Dissolved Solids (TDS)	mg/L	1450	1420	1480	730	718	815	845	1980	1900	2270
Iron, dissolved	mg/L	< 0.030	< 0.030	< 0.010	0.085	0.062	0.651	0.796	<0.03	< 0.030	< 0.030
Manganese, dissolved	mg/L	< 0.010	< 0.010	0.00188	0.017	0.013	0.158	0.151	< 0.010	< 0.010	< 0.010
Molybdenum, dissolved	mg/L	0.0141	0.0159	0.0144	0.0087	0.009	0.0114	0.0111	0.0194	0.0191	0.0215
Uranium, dissolved	mg/L	0.111	0.124	0.13	0.00548	0.00572	0.00558	0.00511	0.117	0.115	0.124

Notes:  
uS/cm - micro Siemes per centimetre  
mg/L - miligrams per litre  
Kelowna - City of Kelowna

**Table 1**  
**Groundwater Data Summary**  
**Background Water Quality Review**  
**Glenmore Landfill**  
**City of Kelowna**

<b>Sample Location</b>		<b>09BH03</b>	<b>GL28-2</b>	<b>GL28-2</b>	<b>GL28-2</b>	<b>GL28-2</b>	<b>GL28-2</b>	<b>GL28-2</b>	<b>GL28-2</b>	<b>GL28-2</b>	<b>GL28-2</b>
<b>Sample Date</b>		<b>04-06-18</b>	<b>24-05-16</b>	<b>20-09-16</b>	<b>20-09-16</b>	<b>11-07-17</b>	<b>26-09-17</b>	<b>28-05-18</b>	<b>28-05-18</b>	<b>25-09-18</b>	<b>28-05-19</b>
<b>Sampled By:</b>		<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>
Parameter	Units										
Conductivity, field	uS/cm	3665	4200	4600	-	3986	3974	4680	4680	5093	
Sulphate	mg/L	1500	2870	2740	2760	2590	2840	2690	2690	3160	2830
Nitrate (as N)	mg/L	< 0.010	11.2	12	12.1	13.1	12.1	8.56	8.44	9.48	11.6
Total Dissolved Solids (TDS)	mg/L	2800	4530	4750	4760	4400	4640	4730	4960	5370	5280
Iron, dissolved	mg/L	0.153	<0.03	0.127	0.235	< 0.030	< 0.030	< 0.010	< 0.010	< 0.010	< 0.010
Manganese, dissolved	mg/L	< 0.00020	0.033	0.019	0.037	0.012	0.018	0.0176	0.0174	0.0204	0.0215
Molybdenum, dissolved	mg/L	0.0264	0.0055	0.0041	0.0039	0.0049	0.0043	0.00484	0.00481	0.00507	0.00541
Uranium, dissolved	mg/L	0.168	0.183	0.184	0.178	0.17	0.168	0.19	0.181	0.196	0.2

Notes:  
 uS/cm - micro Siemens per centimetre  
 mg/L - milligrams per litre  
 Kelowna - City of Kelowna

**Table 1**  
**Groundwater Data Summary**  
**Background Water Quality Review**  
**Glenmore Landfill**  
**City of Kelowna**

<b>Sample Location</b>		<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>	<b>BW-3</b>
<b>Sample Date</b>		<b>28-03-94</b>	<b>11-07-94</b>	<b>24-10-94</b>	<b>27-03-95</b>	<b>23-08-95</b>	<b>29-05-96</b>	<b>05-11-96</b>	<b>16-07-97</b>	<b>29-04-98</b>	<b>24-08-98</b>
<b>Sampled By:</b>		<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>
<b>Parameter</b>	<b>Units</b>										
Conductivity, field	uS/cm	1600	1600	2000	1600	1650	1950	1650	3100	2500	2800
Sulphate	mg/L										
Nitrate (as N)	mg/L										
Total Dissolved Solids (TDS)	mg/L										
Iron, dissolved	mg/L	<.005	<0.02	<0.02	-	<0.02	0.16	-	0.163	0.043	<0.003
Manganese, dissolved	mg/L	<0.005	<0.003	<0.003	-	0.002	0.007	-	0.0068	0.0061	0.074
Molybdenum, dissolved	mg/L	0.009	<0.02	<0.02	-	<0.02	0.007	-	0.01	<0.005	<0.005
Uranium, dissolved	mg/L	-	-	-	-	-	-	-	<0.06	<0.06	<0.06

Notes:  
uS/cm - micro Siemens per centimetre  
mg/L - milligrams per litre  
Kelowna - City of Kelowna

**Table 1**  
**Groundwater Data Summary**  
**Background Water Quality Review**  
**Glenmore Landfill**  
**City of Kelowna**

<b>Sample Location</b>		<b>BW-3</b>	<b>BW-1</b>	<b>BW-1</b>	<b>BW-1</b>	<b>BW-1</b>	<b>BW-1</b>	<b>BW-1</b>
<b>Sample Date</b>		<b>28-09-99</b>	<b>28-03-94</b>	<b>11-07-94</b>	<b>25-10-94</b>	<b>27-03-95</b>	<b>23-08-95</b>	<b>29-05-96</b>
<b>Sampled By:</b>		<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>	<b>Kelowna</b>
Parameter	Units							
Conductivity, field	uS/cm	2350	-	-	-	-	-	-
Sulphate	mg/L							
Nitrate (as N)	mg/L							
Total Dissolved Solids (TDS)	mg/L							
Iron, dissolved	mg/L	0.047	<0.005	<0.02	<0.02	0.02	<0.02	0.03
Manganese, dissolved	mg/L	0.0013	<0.005	0.008	0.015	0.03	<0.001	0.007
Molybdenum, dissolved	mg/L	0.003	<0.005	<0.02	<0.02	<0.02	<0.02	0.007
Uranium, dissolved	mg/L	-	-	-	-	-	-	-

Notes:  
 uS/cm - micro Siemens per centimetre  
 mg/L - milligrams per litre  
 Kelowna - City of Kelowna

**Table 2**  
**Groundwater Statistical Analysis Summary**  
**Background Water Quality Review**  
**Glenmore Landfill**  
**City of Kelowna**

Parameter	Units	Number of Samples	Sample Locations	Mean	Median	Standard Deviation	Coefficient of Variance	Distribution	95th Percentile	GL28-2
<b>Trial 1</b>										
Field Conductivity	uS/cm	5	GL0-3, GL2-1	1634.8	1826	452.7	0.28	Normal	2492.7	3,974 - 5,093
Sulphate	mg/L	5	GL0-3, GL2-1	315.6	319	35.3	0.11	Normal	380.2	2,590 - 3,160
Nitrate	mg/L	6	GL0-3, GL2-1	23.8	22.5	26	1.09	Two Populations	-	8.44 - 13.1
Total Dissolved Solid	mg/L	6	GL0-3, GL2-1	1123.3	1132.5	360.3	0.32	Normal	1776.2	4,400 - 5,370
Manganese	ug/L	6	GL0-3, GL2-1	58	13.5	74.9	1.29	Two Populations	-	12 - 37
Molybdenum	ug/L	6	GL0-3, GL2-1	12.6	12.8	2.7	0.21	Normal	17.5	3.9 - 5.5
Uranium	ug/L	6	GL0-3, GL2-1	63.5	58.3	64	1.01	Two Populations	-	168 - 200
<b>Trial 2</b>										
Field Conductivity	uS/cm	8	GL0-3, GL2-1, 09BH03	2218	2023	978	0.44	Log	-	3,974 - 5,093
Sulphate	mg/L	9	GL0-3, GL2-1, 09BH03	615	323	482	0.78	Log	-	2,590 - 3,160
Nitrate	mg/L	8	GL0-3, GL2-1, 09BH03	18	0.7	24.5	1.36	Two Populations	-	8.44 - 13.1
Total Dissolved Solid	mg/L	10	GL0-3, GL2-1, 09BH03	1470	1435	774	0.53	Log	-	4,400 - 5,370
Manganese	ug/L	10	GL0-3, GL2-1, 09BH03	38.1	10	61.6	1.62	Two Populations	-	12 - 37
Molybdenum	ug/L	10	GL0-3, GL2-1, 09BH03	15	14	6	0.38	Log	-	3.9 - 5.5
Uranium	ug/L	10	GL0-3, GL2-1, 09BH03	79.6	114	65.5	0.82	Normal	198.4	168 - 200
<b>Trial 3</b>										
Field Conductivity	uS/cm	16	GL0-3, GL2-1, BW3	1935.9	1888	539.8	0.28	Normal	2878.4	3,974 - 5,093
Manganese	ug/L	18	GL0-3, GL2-1, BW3, BW1	24.8	7.5	47.7	1.92	Two Populations	-	12 - 37
Molybdenum	ug/L	18	GL0-3, GL2-1, BW3, BW1	14	14.3	5.6	0.4	Normal	23.7	3.9 - 5.5

**Table 3**  
**Surface Water Data Summary**  
**Background Water Quality Review**  
**Glenmore Landfill**  
**City of Kelowna**

Sample Location		Bubna Slough/N1 Pond	Bubna Slough/N1 Pond	Bubna Slough/N1 Pond	Bubna Slough/N1 Pond	Bubna Slough/N1 Pond	Bubna Slough/N1 Pond	N2 Pond	N2 Pond	Little Robert Lake	Little Robert Lake	Little Robert Lake
Sample Date		12-11-09	10-02-10	20-04-18	03-05-18	15-06-18	08-11-18	12-11-09	10-02-10	17-04-18	03-05-18	15-06-18
Sampled By:		EBA	EBA	Kelowna	Kelowna	Kelowna	Kelowna	EBA	EBA	Kelowna	Kelowna	Kelowna
Parameter	Units											
Conductivity, field	uS/cm	-	-	-	2584	2484	3359	-	-	3334	1779	1940
Conductivity, lab	uS/cm	-	-	2810	2920	3950	3330	-	-	3780	2000	2140
pH, field	s.u.	-	-	-	8.08	9.06	8.43	-	-	8.92	8.34	9.19
pH, lab	s.u.	9.06	8.94	8.29	8.56	8.91	8.36	9.46	9.24	8.73	8.56	8.51
Ammonia	mg/L	0.24	4.43	0.03	0.056	0.023	0.038	0.27	3.98	0.054	0.173	0.053
Chloride	mg/L	1420	383	555	476	542	630	4610	569	76.5	151	172
Sulphate	mg/L	822	186	214	170	201	268	20200	1200	1490	400	403

## Notes:

mg/L - milligrams per litre

uS/cm - microSiemens per centimetre

Kelowna - City of Kelowna

EBA - EBA Engineering Consultants Ltd. Data sourced from *Background Surface Water Investigation Tutt Ranch*, 2010

**Table 4**  
**Surface Water Statistical Analysis Summary**  
**Background Water Quality Review**  
**Glenmore Landfill**  
**City of Kelowna**

Parameter	Units	Number of Samples	Sample Locations	Mean	Median	Standard Deviation	Coefficient of Variation	Distribution	95th Percentile	Little Robert Lake
Conductivity, field	uS/cm	4	Bubna Slough/N1	3252.5	3125	516	0.16	Normal	4799.6	2,000 - 3,780
Sulphate	mg/L	8	Bubna Slough/N1, N2	2907.6	241	6997.4	2.41	Two Populations	-	400 - 1,490
Chloride	mg/L	8	Bubna Slough/N1, N2	1148.1	562	1435.2	1.25	Two Populations	-	76.5 - 172
Ammonia	mg/L	8	Bubna Slough/N1, N2	1.1	0.1	1.9	1.68	Two Populations	-	0.053 - 0.173
pH, lab	s.u.	8	Bubna Slough/N1, N2	8.9	9.1	0.4	0.05	Normal	9.7	8.34 - 9.19



# **Attachment 2**



Report Date: July 23, 2019

File: 12218

Report Number: 129139

CITY OF KELOWNA

City Hall  
1435 Water Street  
Kelowna BC V1Y 1J4

Dear CITY OF KELOWNA

**Re: Warning Letter, Operational Certificate, 12218**

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On June 11, 2019, Ministry of Environment, Environmental Protection Division staff conducted an inspection under *Environmental Management Act (EMA)*, 12218. The inspection determined that CITY OF KELOWNA is out of compliance with its Operational Certificate 12218, and the section(s) listed below. This Warning Letter lists the compliance verification information contained below.

Failure to comply with the requirements set out in your Operational Certificate is an offence under the *Environmental Management Act (EMA)*. Section 120(6) of *EMA* states as follows:

*120(6) A person who, holding a permit or approval issued to the person under this Act to introduce waste into the environment, introduces waste into the environment without having complied with the requirements of the permit or approval commits an offence and is liable on conviction to a fine not exceeding \$1 000 000 or imprisonment for not more than 6 months, or both.*

It should also be noted that, as an alternative to prosecution of the offence referenced above, the Ministry may initiate action to impose an administrative penalty against CITY OF KELOWNA. *The Administrative Penalties Regulation (EMA)* (B.C. Reg. 133/2014) (APR) was brought into force in 2014. The APR describes the prescribed provisions of the *EMA* as well as that of specified regulations under which administrative penalties can be assigned. Section 12(5) of the APR states as follows:

*12(5) A person who fails to comply with a requirement of a permit or approval issued or given under the Act is liable to an administrative penalty not exceeding \$40 000, unless the requirement the person failed to comply with is also a prescribed provision of the EMA or the regulations that is subject to a different maximum administrative penalty.*

I request that CITY OF KELOWNA immediately implement the necessary changes or modifications to correct the non-compliance(s) listed above with the *Environmental Management Act*. Further, I request that CITY OF KELOWNA notify this office in writing, by email or letter within 30 days of this letter, advising what corrective measures have been taken, and what else is being done, to prevent similar non-compliances in the future.

Please submit your response to the Ministry's Compliance Mailbox at [EnvironmentalCompliance@gov.bc.ca](mailto:EnvironmentalCompliance@gov.bc.ca).

As a result of this Warning, this authorization will be prioritized for follow-up inspection. The corrective measures will be reviewed by an Officer as part of the next inspection.

Finally, if you fail to take the necessary actions to restore compliance, you may be subject to escalating enforcement action. This Warning Letter and the alleged violations and circumstances to which it refers, will form part of the compliance history of CITY OF KELOWNA and will be taken into account in the event of future violations.

---

**Ministry of Environment  
and Climate Change  
Strategy**

Compliance  
Environmental  
Protection Division

Mailing Address:  
102 Industrial PI  
Penticton BC V2A 7C8

Telephone: 250 490 8200  
Facsimile: 250 490 2231  
Website: [www.gov.bc.ca/env](http://www.gov.bc.ca/env)

**Inspection Details:**

Requirement Description:	<p><b>1. AUTHORIZED DISCHARGES, 1.1, 1.1.1</b></p> <p>1.1.1.: This section applies to the discharge of refuse from municipal, commercial and light industrial sources to a sanitary landfill known as the Glenmore Landfill. The site reference number for this discharge is E104956. 1.1.1 The maximum authorized rate of waste discharge is 170,000 tonnes annually. The maximum quantity of waste discharged must not exceed the design capacity of the landfill as specified in an approved Design and Operations Plan. The final footprint and profile of the discharged waste must be within that specified in the Design and Operations Plan and approximately as shown on the attached locations map.</p>
Details/Findings:	<p>An office review was conducted on June 11, 2019 by Officer Kaylee Garnett (Officer) from the Ministry of Environment and Climate Change Strategy (Ministry) to verify compliance with the Operational Certificate 12218. This was a follow up inspection from a warning letter issued September 17, 2018. The contact for this inspection was Scott Hoekstra an operator for the City of Kelowna.</p> <p>The inspection period is from September 18, 2018 to June 11, 2019.</p> <p>Reports reviewed during this inspection;</p> <ul style="list-style-type: none"> <li>- The 2018 Annual Report dated March 30, 2019 (2019, report) which included the 2018 Glenmore Landfill Annual Water Quality Report by SNC-Lavalin dated March 13, 2019 (2019, WQ)</li> <li>- 2018 Design, Operation and Closure Plan (DOCP) and Financial Security Plan (FSP) dated November 1, 2018 by GHD Limited.</li> </ul> <p>The 2018 Annual Report was submitted to the Ministry dated March 30, 2019 . The annual tonnage for the Glenmore landfill was 166,916 t.</p>
Compliance:	In
Requirement Description:	<p><b>2. OPERATING REQUIREMENTS, 2.1 Design, Operations and Closure Plans, 2.1.1</b></p> <p>2.1.1: The City must submit a Design, Operations and Closure Plan prepared by a suitably qualified professional for approval by the Director by June 30, 2016, and a Financial Security Plan by June 30, 2017. The Design, Operations and Closure Plan must address, but not be limited to, each of the subsections in the Landfill Criteria for Municipal Solid Waste unless otherwise approved by the Director, including performance, siting, design, operational, closure and post-closure criteria. The facilities must be developed, operated and closed in accordance with the Design, Operations and Closure Plan. Should there be any inconsistency between this Operation Certificate and the Design, Operations and Closure Plan, this Operational Certificate must take precedence.</p>
Details/Findings:	<p>The City of Kelowna submitted to the Ministry a Design, Operation and Closure Plan (DOCP) and a Financial Security Plan prepared by GHD Limited on March 27, 2019. This replaced the existing Plan from 2008 and rectified requirements from the June 2015 Permit Amendment. The Officer has now determined the Permittee is in compliance with this section.</p>

Compliance:	In
Requirement Description:	<p><b>2. OPERATING REQUIREMENTS, 2.1 Design, Operations and Closure Plans, 2.1.2</b></p> <p>2.1.2: The Design, Operations and Closure plans must be reviewed every 5 years throughout the operating life of the landfill and updated to encompass the next 10 years of landfill operation and/or post-closure activities. The updated landfill design, operating and closure plans must be prepared by a professional engineer or geoscientist licensed to practice in the province of British Columbia and knowledgeable in such matters. The updated plans must be submitted to the Director for approval and must include any information relevant to the design, operations, closure and post-closure care of the landfill.</p>
Details/Findings:	The City of Kelowna submitted to the Ministry a Design, Operation and Closure Plan (DOCP) and a Financial Security Plan prepared by GHD Limited on March 27, 2019. The signing authority was Deacon Liddy, Professional Engineer in good standing with the Association of Professional Engineers and Geoscientists of the Province of BC. This was an update to the existing Plan from 2008 that encompasses the next 10 years.
Compliance:	In
Actions to be taken:	Review the DOCP every five years.
Requirement Description:	<p><b>2. OPERATING REQUIREMENTS, 2.1 Design, Operations and Closure Plans, 2.1.3</b></p> <p>2.1.3: The landfill facility must be constructed and maintained in accordance with the approved Design, Operations and Closure plans and subject to the conditions set therein. A knowledgeable professional engineer must carry out field reviews of the landfill construction and installation of works. As-constructed drawings of the landfill and all works, including elevations relative to a common datum, must be submitted (or retained on site) to the Director. The as-constructed drawings must be sealed by a professional engineer or geoscientist who is licensed to practice in the province of British Columbia and knowledgeable in the appropriate field of study.</p>
Details/Findings:	The City of Kelowna submitted to the Ministry a Design, Operation and Closure Plan (DOCP) and a Financial Security Plan prepared by GHD Limited on March 27, 2019. This report and included drawings were signed and sealed by Deacon Liddy, Professional Engineer in good standing with the Association of Professional Engineers and Geoscientists of the Province of BC.

Compliance:	In
Requirement Description:	<b>2. OPERATING REQUIREMENTS, 2.1 Design, Operations and Closure Plans, 2.1.4</b> 2.1.4: Written authorization from the Director must be obtained prior to implementing any changes to the approved plans. Based on any information obtained in connection with this facility, the Director may require revision of, or addition to, the design, operations and closure plans.
Details/Findings:	The Officer noted the new DOCP 2019 is currently in review by a director from Authorizations. However as noted in the last IR85264 there has already been changes to the facility layout since the approved CSDP (2008), therefore the Permittee is out of compliance with this section.
Compliance:	Out
Actions to be taken:	Written authorization from the Director must be obtained prior to implementing any changes to the approved plans.
Requirement Description:	<b>2. OPERATING REQUIREMENTS, 2.2 Qualified Professionals, 2.2.1</b> 2.2.1: All information, including plans, drawings, assessments, investigations, surveys, programs and reports, must be certified by a qualified professional. As-built plans and drawings of the facilities and works must be certified by a qualified professional. 2.2.1 "qualified professional" means a person who: (a) is registered in British Columbia with his or her appropriate professional association, acts under that professional association's code of ethics, and is subject to disciplinary action by that professional association; and (b) through suitable education, experience, accreditation and knowledge may be reasonably relied on to provide advice within his or her area of expertise as it relates to this Operational Certificate.
Details/Findings:	The City of Kelowna submitted to the Ministry a Design, Operation and Closure Plan (DOCP) and a Financial Security Plan prepared by GHD Limited on March 27, 2019. This report and included drawings were signed and sealed by Deacon Liddy, Professional Engineer in good standing with the Association of Professional Engineers and Geoscientists of the Province of BC
Compliance:	In

Requirement Description:	<p><b>2. OPERATING REQUIREMENTS, 2.5 Landfill Site Development, 2.5.1</b></p> <p>2.5.1: In accordance with the approved Design, Operations and Closure Plan, surface water diversions and groundwater drainage works must be installed to prevent surface water run-off and groundwater seepage from entering the waste discharge area. The effect of sediment transport from areas upgradient and within the landfill site must be considered when designing, installing and maintaining the surface water diversion system. Diversion and drainage structures must be maintained by the Operational Certificate Holders on a regular basis to the satisfaction of the Director.</p>
Details/Findings:	<p>As this was an office review, the Officer did not inspect the facility and could not determine if the drainage structures are in good working order.</p>
Compliance:	<p>Not Determined</p>
Requirement Description:	<p><b>2. OPERATING REQUIREMENTS, 2.8 Ground and Surface Water Quality Impairment</b></p> <p>2.8: The quality of ground and surface water at the property boundary must not exceed the appropriate (e.g.freshwater aquatic life, drinking water, etc.) water quality criteria in the British Columbia Approved Water Quality Guidelines and A Compendium of Working Water Quality Guidelines for British Columbia, as amended from time to time, or their replacements approved by the Director in writing. Where natural background water quality exceeds the appropriate water quality criteria, the quality of ground and surface water at the property boundary must not exceed natural background water quality. Water quality criteria from other jurisdictions can only be used for contaminants which have not been dealt with in the British Columbia Guidelines. After considering existing and potential future uses of ground and surface water, a qualified professional may recommend the appropriate water quality criteria. The appropriate water quality criteria are subject to the approval of the Director in writing. If excursions result to the specified water quality criteria, the Director may require that leachate management control measures or works be undertaken. Terms of reference for any leachate management study and/or design work is subject to the authorization of the Director.</p>

<p>Details/Findings:</p>	<p>Groundwater quality  The 2018 Annual report from March 2019 states that well GL28- 1,2 and 3 is the best monitoring location for leachate migration offsite, as it is located downstream immediately off the permitted landfill boundary. Samples taken in May and September of 2018 for GL28-2 and 3 show levels exceeding the BCWQG aquatic life guidelines for nitrate and sulfate, exceeding drinking water standards for sulfates and irrigation guidelines for field conductivity. As did GL28-1 except with no elevated nitrate. Due to this, it was concluded that nitrate increase was “most likely the result of surface water contamination from local agriculture activity.” (2019, WQ)  These exceedances were not found in up gradient background data well G23-1.  GL28-1 – conductivity 3,761 µS/cm (Sept 25), sulfate 2,150 µg/L (Sept 25)  GL28-2 - conductivity 4,860 µS/cm, (May 28), Nitrate 8,440 µg/L (May 28) and 9480 µg/L (sept 25), Sulfate 2,690 mg/l (May 28) and 3,160 mg/l (Sept 25),  GL28-3 –conductivity 6,777 µS/cm (Sept 25), Nitrates 7,780 µg/L (Sep 25), sulfate 3,780 mg/l (May 28) and 4.350 mg/l (Sept 25)  Surface water quality  Little Robert Lake, outside the boundary, was used as an overflow for Tutt pond, within the boundary, in 2018. The BCWQG quality standards for Little Robert Lake showed exceedances in field conductivity and chloride for irrigation water and for aquatic life there was exceedances of pH, total ammonia (based on pH), chloride, and sulfate. There is no background data for Little Robert Lake.  Little Robert Lake – conductivity 3,340 µg/L (Apr 17), chloride 172 mg/l (Jun 15), pH 9.19, total ammonia 173 µg/L (May 3), sulfate 3,840 mg/l (Jun 15)  It should also be noted runoff collections ponds on the property, Tutt Pond, Northeast Pond and sometimes Bredin Pond are used to irrigate fields that are outside of the property boundary. There are few guidelines for irrigation water in the BCWQG; field conductivity, chloride, fluoride and, dependent on the crop, conductivity. Exceedance in chloride was observed in Tutt and Bredin pond, and the NE exceeded fluoride.  The Director has not approved alternate terms of reference for water quality.  These wells and surface waterbodies were found to exceed water quality standards at the property boundary, therefore the Permittee is out of compliance with this section.</p>
<p>Compliance:</p>	<p>Out</p>
<p>Actions to be taken:</p>	<p>Ensure that the quality of ground and surface water at the property boundary does not exceed the appropriate (e.g. freshwater aquatic life, drinking water, etc.) water quality criteria in the British Columbia Approved Water Quality Guidelines and A Compendium of Working Water Quality Guidelines for British Columbia, as amended from time to time, or their replacements approved by the Director in writing.</p>



Requirement Description:	<p><b>3. MONITORING, 3.2 Management of Leachate Collection System Fluid</b></p> <p>3.2: Leachate collection sump fluid levels must be monitored and fluid removed from the leachate collection system as specified in the approved design, operating and closure plans. A sample of fluid from each of the leachate collection sumps must be collected on a quarterly basis and laboratory analyses obtained for the leachate indicator parameters identified in the monitoring program. The Director may vary the location and frequency of sampling and analyses of leachate collection system fluid should conditions warrant. Fluid recovered from the leachate collection system may be used within the landfill footprint for irrigation, dust suppression and/or re-circulated within the buried waste as well as directed to the Kelowna Wastewater Treatment facility unless otherwise directed by the Director. Other methods of treatment and/or disposal of the leachate collection sump fluids must have the prior approval of the Director.</p>
Details/Findings:	<p>Leachate Collection Monitoring plan outlined in the updated DOCP 2019 in Appendix L. Samples are taken quarterly at three monitoring locations for parameters of general chemistry, nutrients, dissolved metals, and petroleum hydrocarbon constituents. Leachate is managed through a recirculation piolet program or discharged to the City of Kelowna sewer that goes to the Wastewater Treatment facility.</p>
Compliance:	In
Requirement Description:	<p><b>3. MONITORING, 3.3 Groundwater Contamination by Leachate</b></p> <p>3.3: Should it be determined that leachate is being generated and carried in the groundwater or surface water and, in the opinion of the Director, requires interception and treatment, appropriate remedial measures as approved by the Director must be implemented.</p>
Details/Findings:	<p>A detailed comparison of leachate quality and groundwater quality was not completed. The Water Quality report (2019, QW) stated in 7.2.4 that 'The results of the comparison are shown in Table 3d and suggest that groundwater quality in the GL28 well series is not impacted by leachate'. The table 3d does show that GL28 did exceed multiple water quality parameters and that the background up gradient well had no exceedances. This permit is currently under review and it has not yet been determined by a director if leachate has migrated.</p>
Compliance:	Not Determined

Actions to be taken:	The City of Kelowna is actively participating in a permit amendment. Water quality standards and leachate concerns should be addressed in the permit amendment and DCOP review. Should it be determined that leachate is being generated and carried in the groundwater or surface water and, in the opinion of the Director, requires interception and treatment, appropriate remedial measures as approved by the Director must be implemented.
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**Compliance History:**  
 IR85264 - 2018-09-17 - Warning - Section 2.1 - Failure to update DOCP, Section 2.5.1 - Failure to maintain ditches, Section 2.8- Not meeting water quality standards.

The Ministry of Environment Compliance and Enforcement Policy and Procedure prescribes common requirements and procedures for all Ministry staff to ensure consistent and risk based assessment and response to noncompliance. Using the Non-Compliance Decision Matrix, the compliance determination for this inspection has been assessed as a Level 3, Category A.

**General compliance information:**  
[www.gov.bc.ca/environmentalcompliance](http://www.gov.bc.ca/environmentalcompliance)  
**Non-Compliance Decision Matrix information:**  
[www.gov.bc.ca/environment/how-compliance-is-assessed](http://www.gov.bc.ca/environment/how-compliance-is-assessed)  
**Reporting and data submission requirements (to be sent to EnvAuthorizationsReporting@gov.bc.ca):**  
[www.gov.bc.ca/submit-waste-authorization-reports](http://www.gov.bc.ca/submit-waste-authorization-reports)

Please be advised that this inspection report may be published on the provincial government website within 7 days.

If you have any questions about this warning, please contact the undersigned.

Yours truly,

Kaylee Garnett  
 Environmental Protection Officer

cc:

**Attachments:**

**Deliver via:**  
 Email:  Fax:  Mail:   
 Registered Mail:  Hand Delivery:

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**Ministry of Environment  
and Climate Change  
Strategy**

Compliance  
Environmental  
Protection Division

Mailing Address:  
102 Industrial Pl  
Penticton BC V2A 7C8

Telephone: 250 490 8200  
Facsimile: 250 490 2231  
Website: [www.gov.bc.ca/env](http://www.gov.bc.ca/env)

**DISCLAIMER:**

Please note that sections of the permit, regulation or code of practice referenced in this inspection record are for guidance and are not the official version. Please refer to the original permit, regulation or code of practice.

To see the most up to date version of the regulations and codes of practices please visit  
<http://www.bclaws.ca>

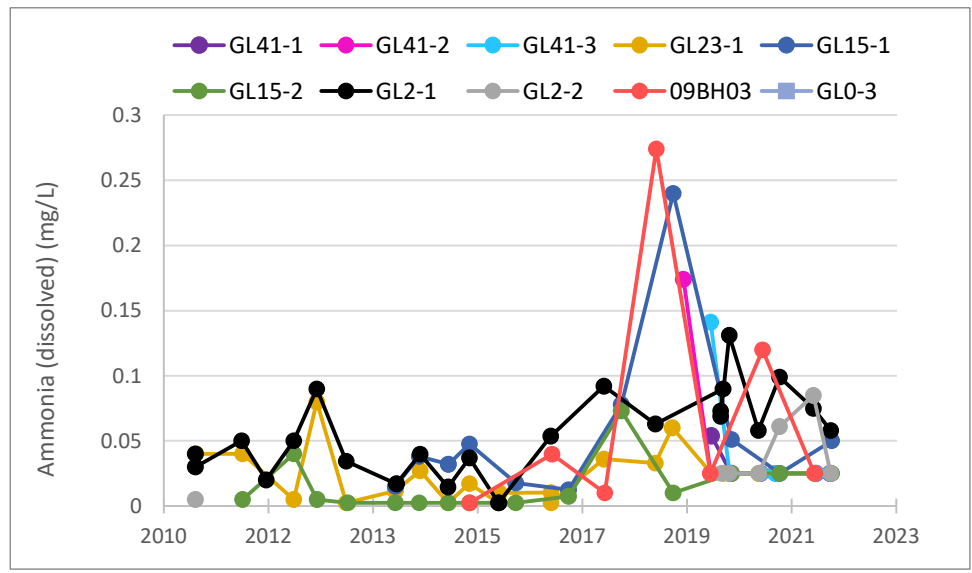
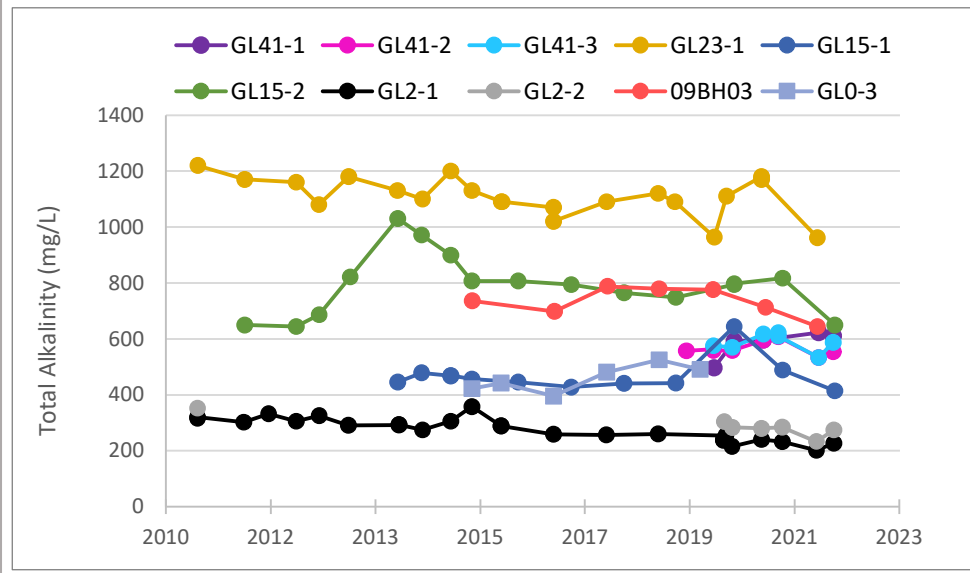
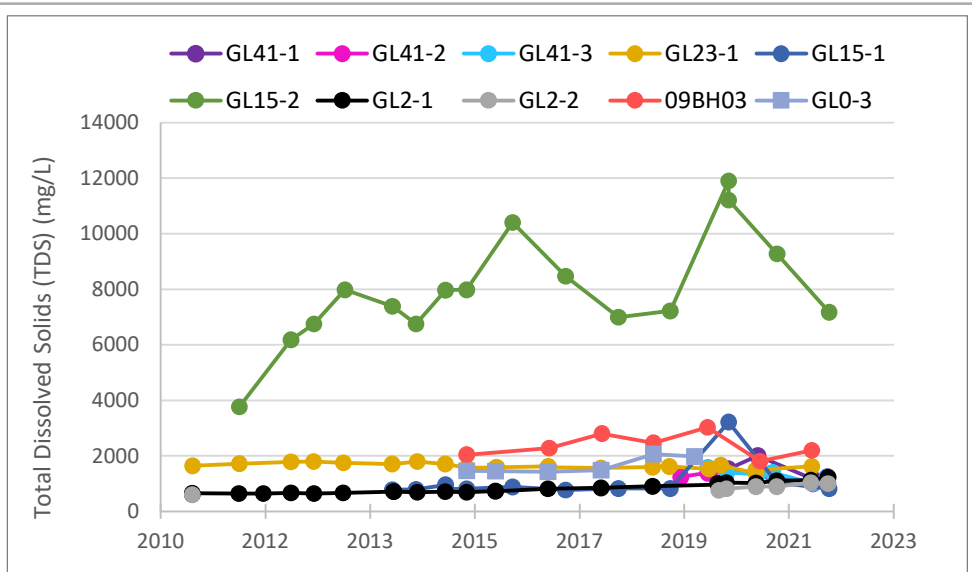
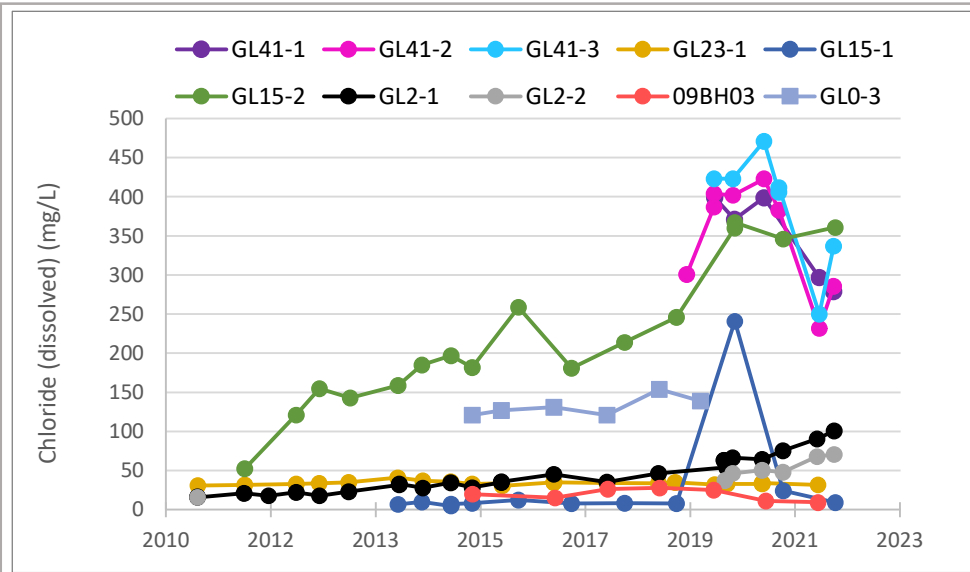
If you require a copy of the original permit, please contact the inspector noted on this inspection record.

It is also important to note that this inspection record does not necessarily reflect each requirement or condition of the authorization therefore compliance is noted only for the requirements or conditions listed in the inspection record.



# Appendix H

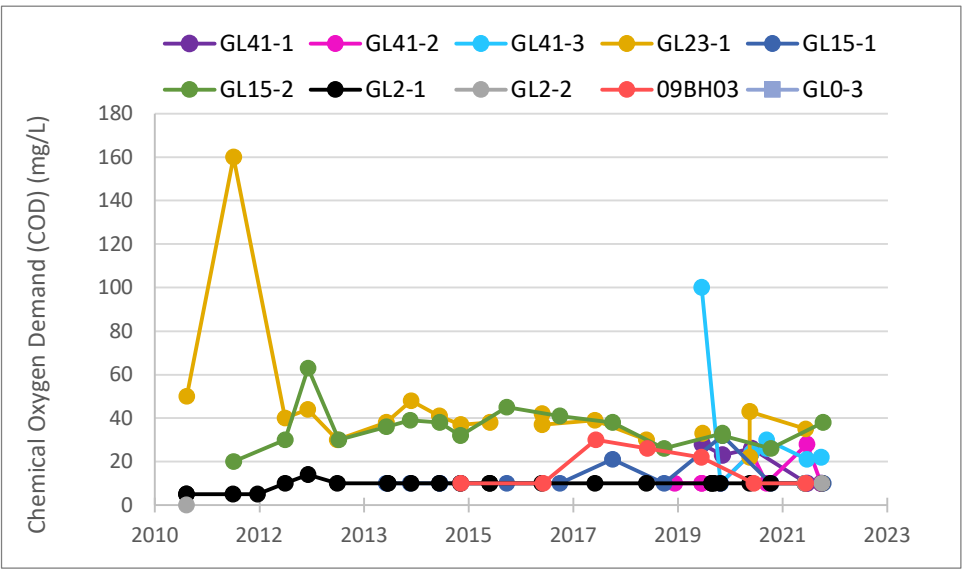
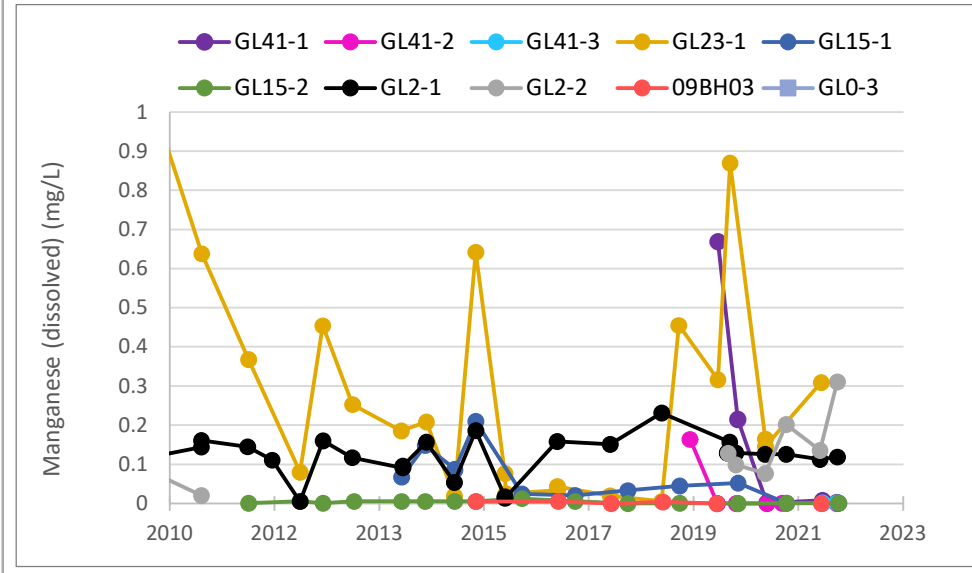
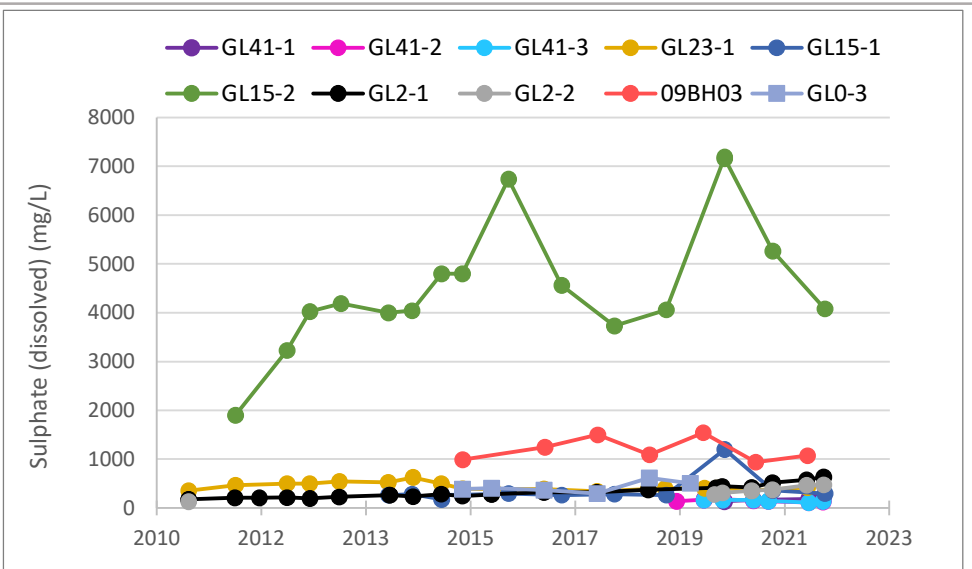
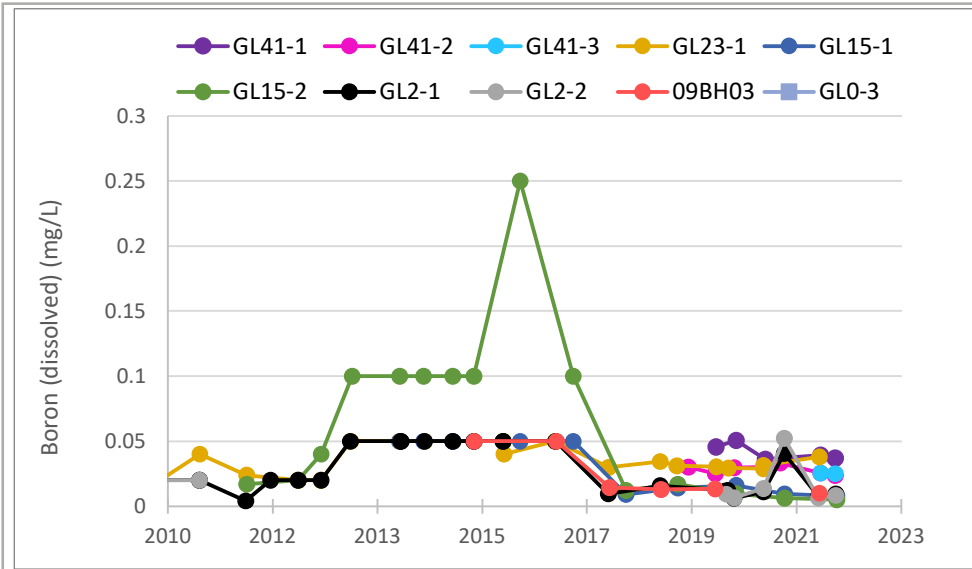
## Concentration vs Time Plots



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 UPGRADIENT WELLS

Project No. 12605725  
 Date October 2023

FIGURE H-1

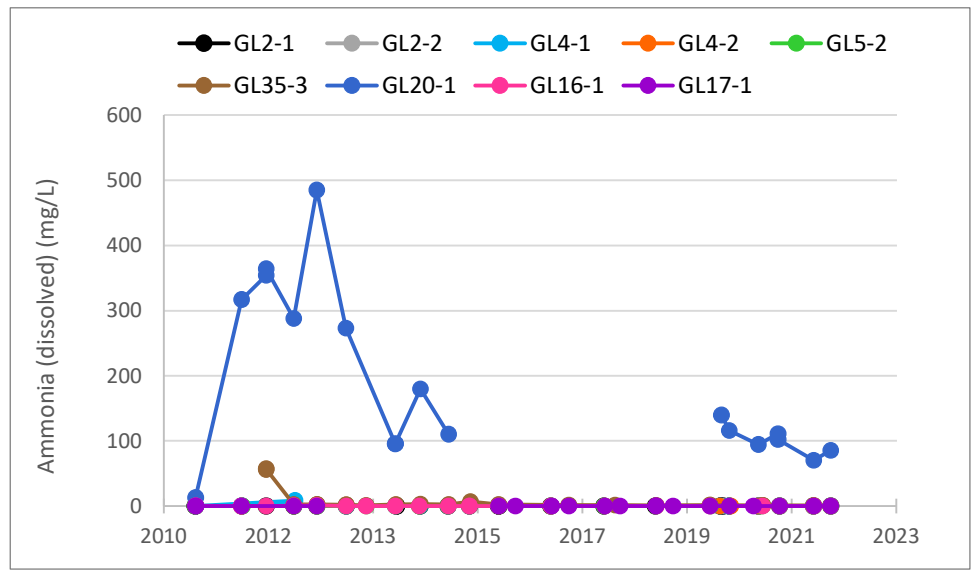
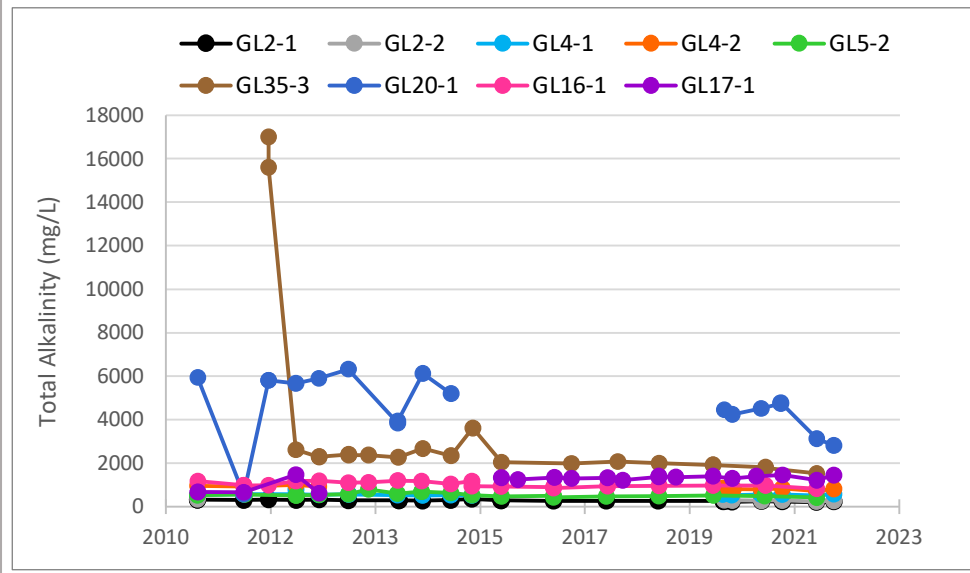
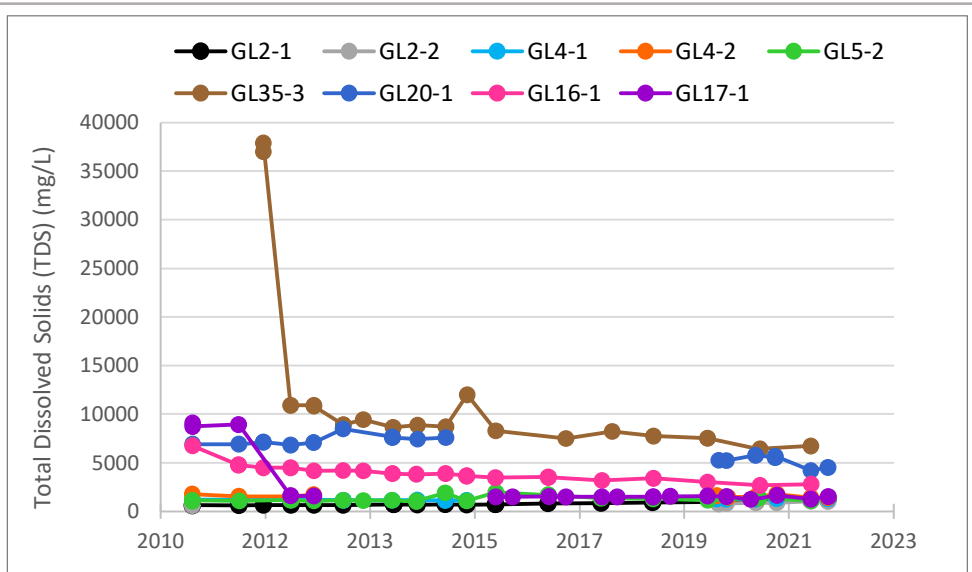
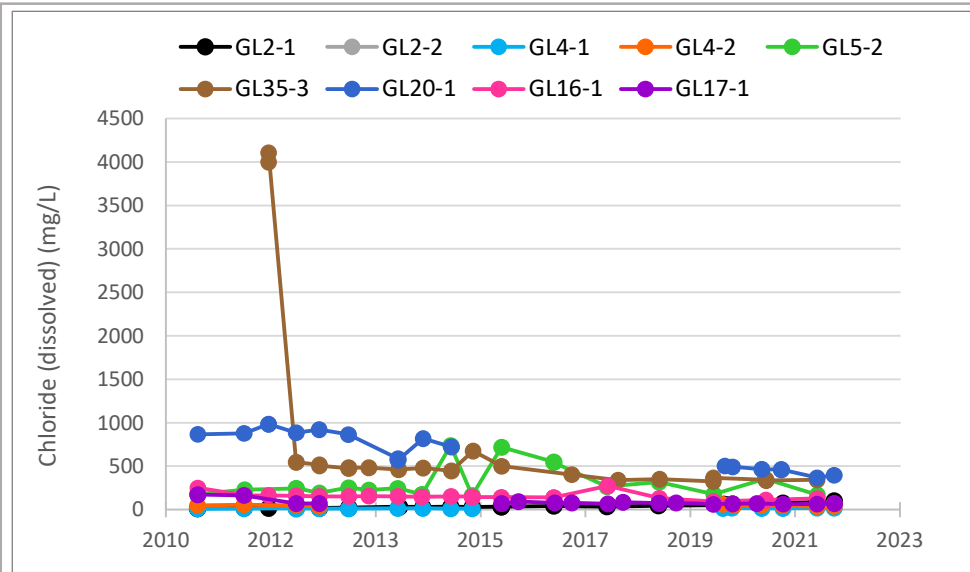


CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 UPGRADIENT WELLS

Project No. 12605725  
 Date October 2023

FIGURE H-2

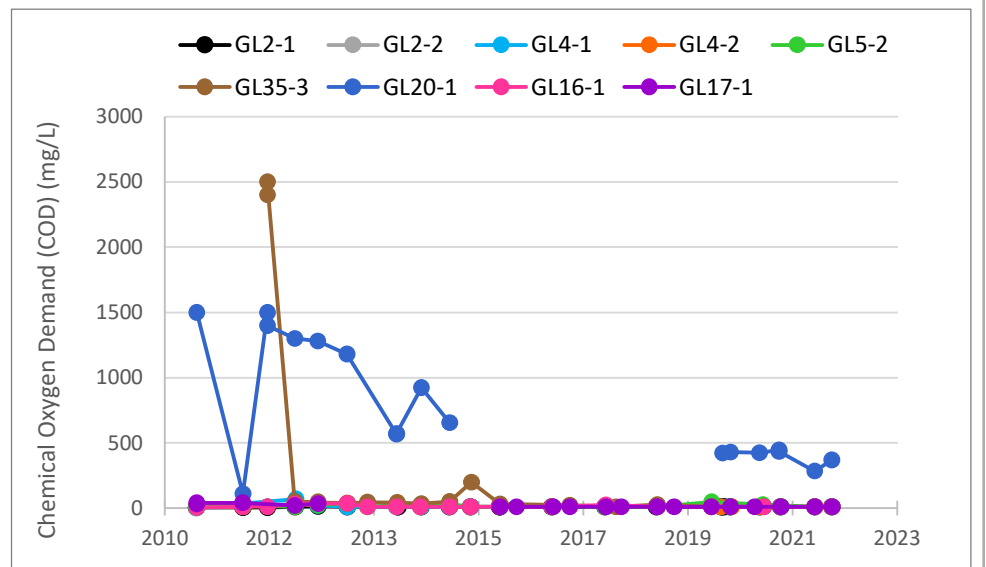
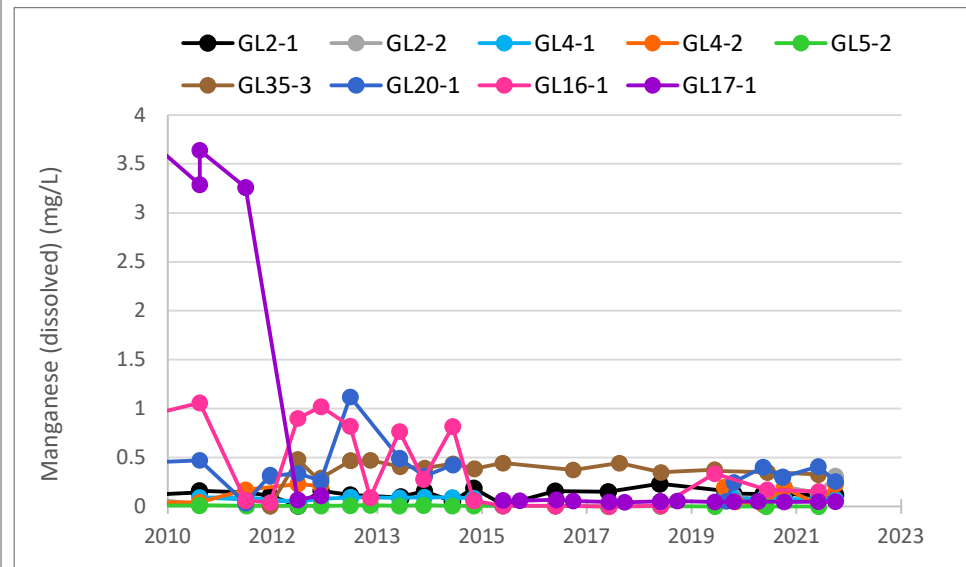
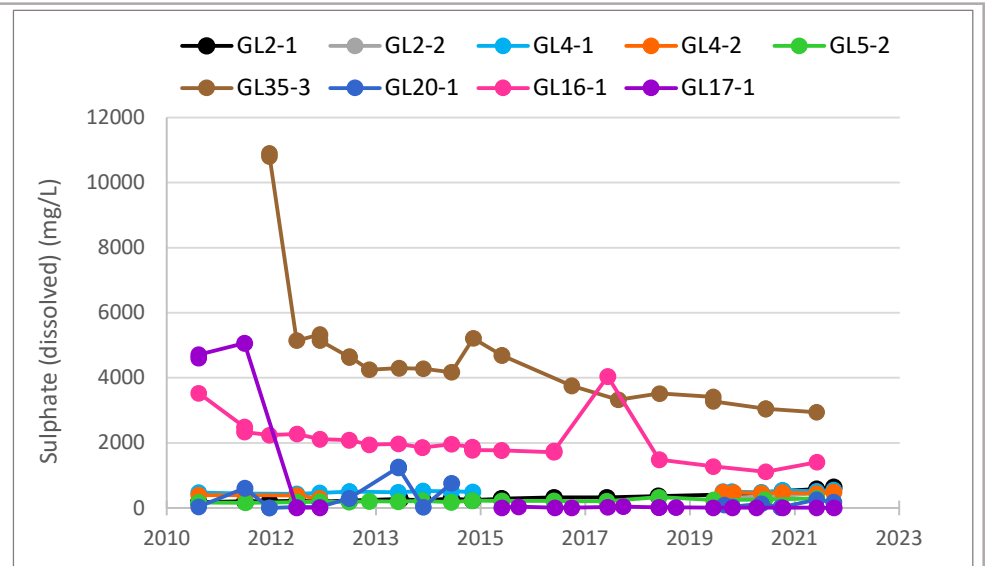
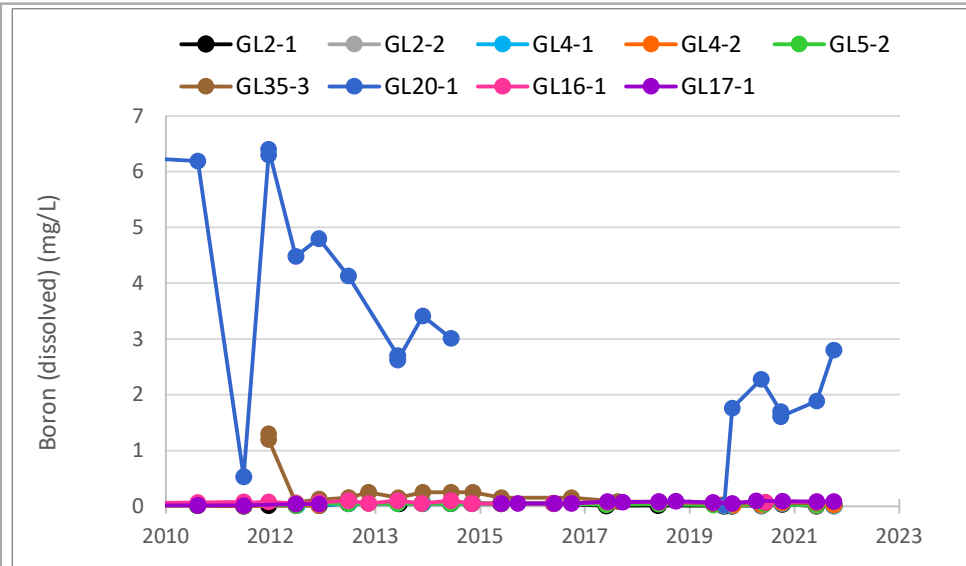




CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 LANDFILL VICINITY WELLS

Project No. 12605725  
 Date October 2023

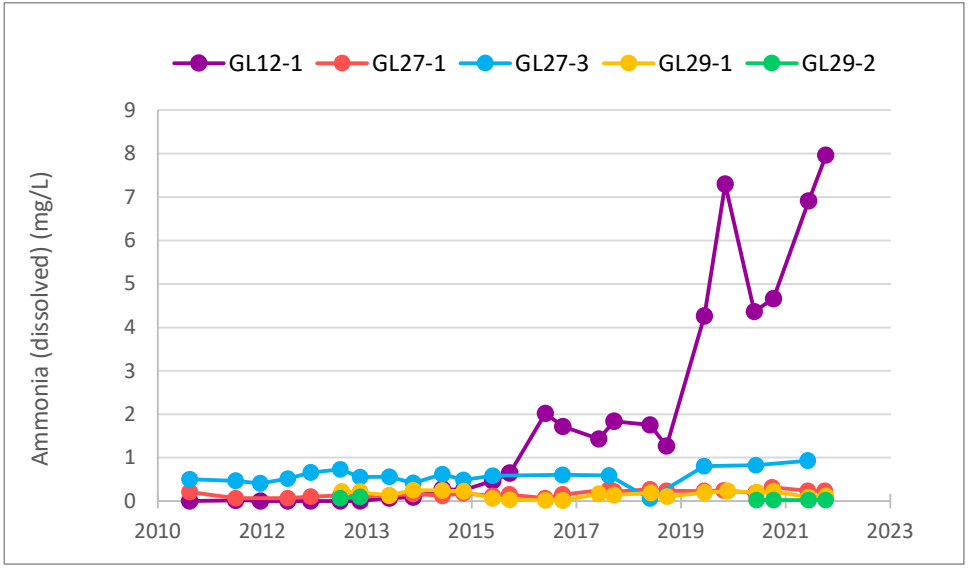
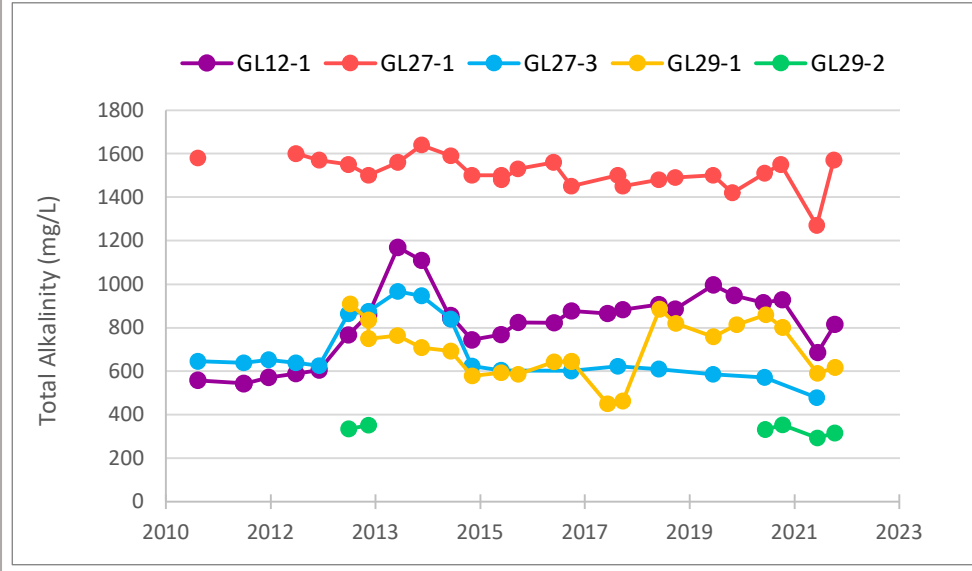
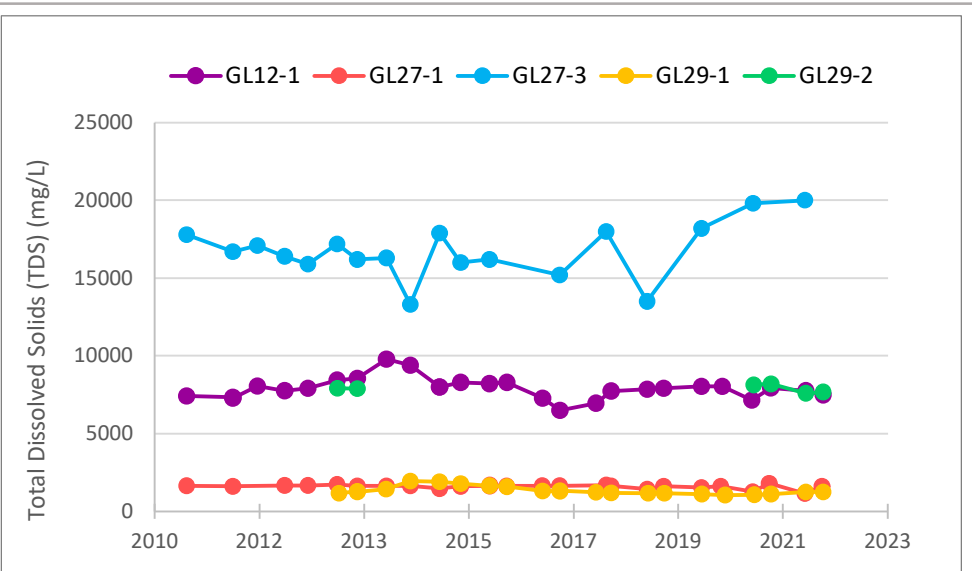
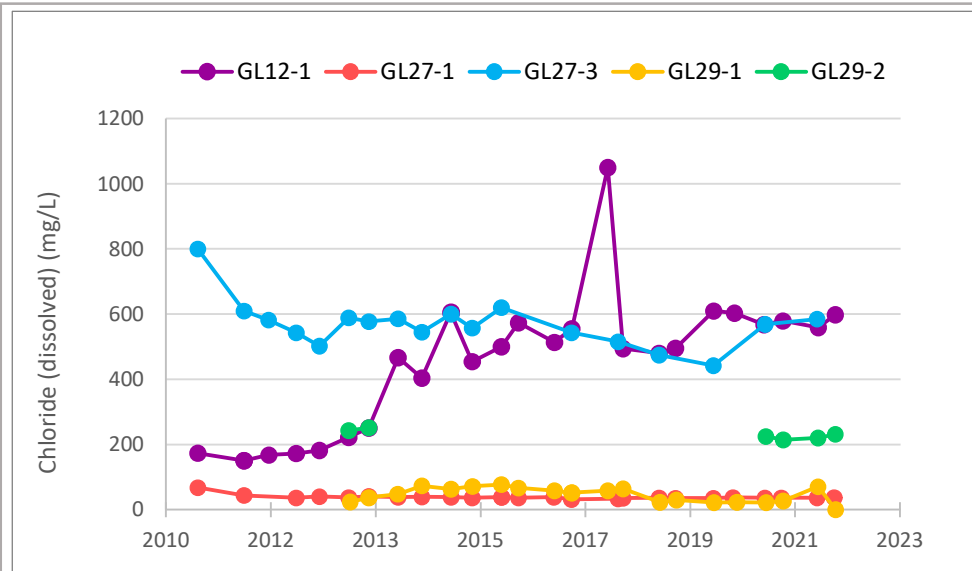
FIGURE H-3



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 LANDFILL VICINITY WELLS

Project No. 12605725  
 Date October 2023

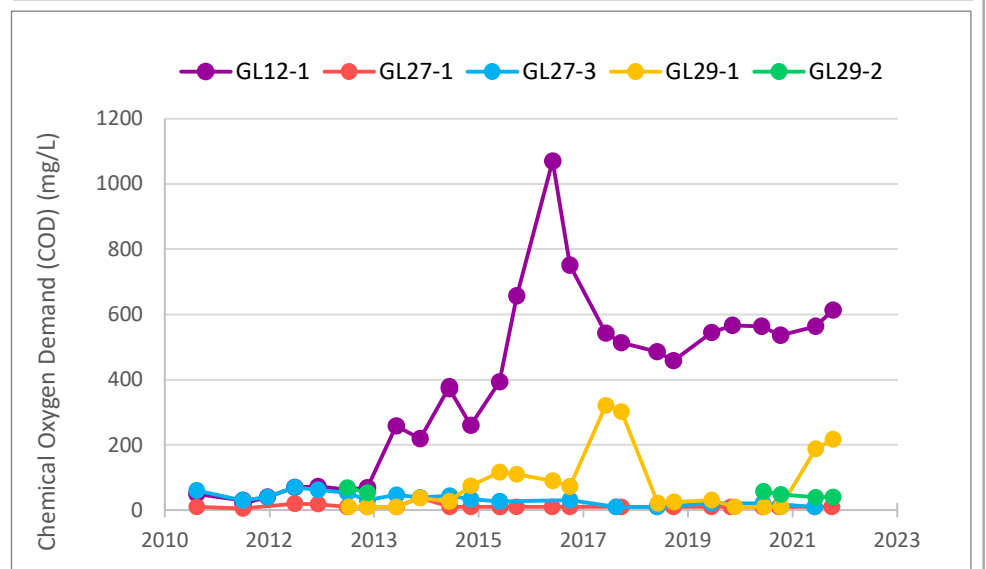
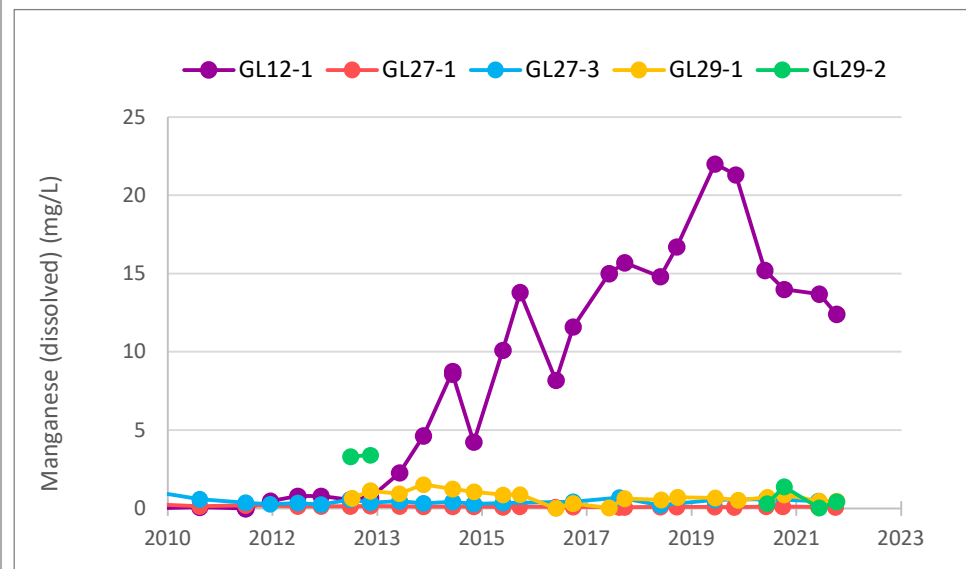
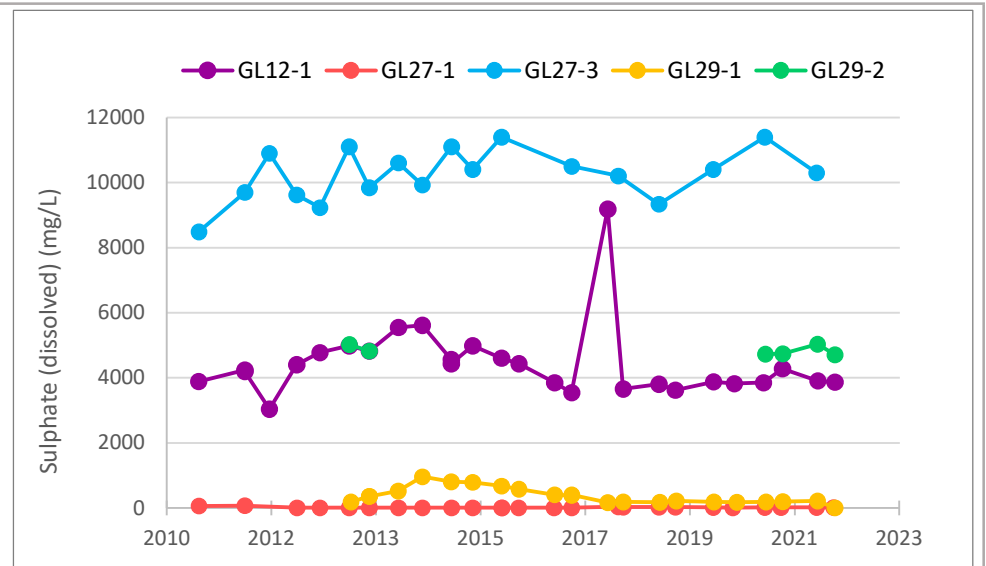
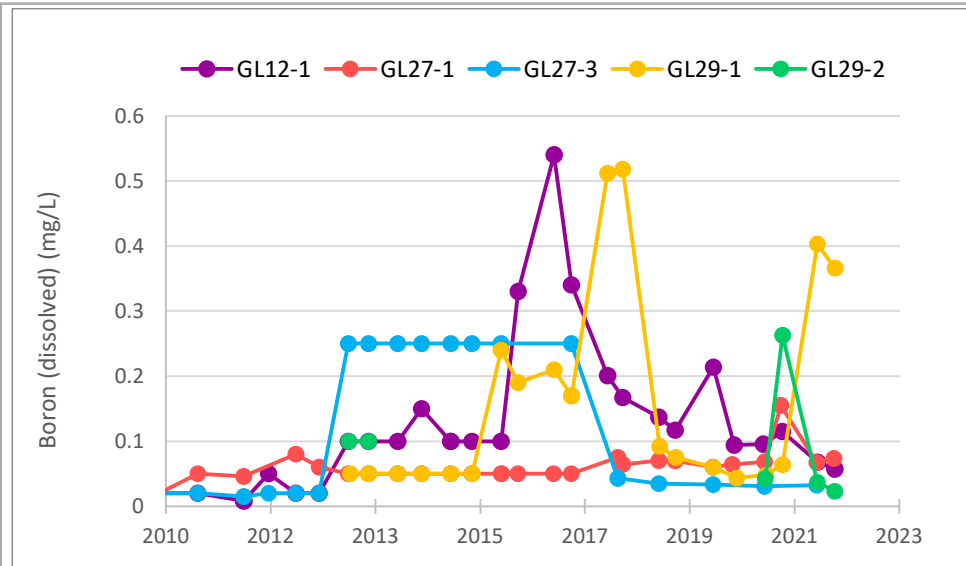
FIGURE H-4



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 COMPOST VICINITY WELLS

Project No. 12605725  
 Date October 2023

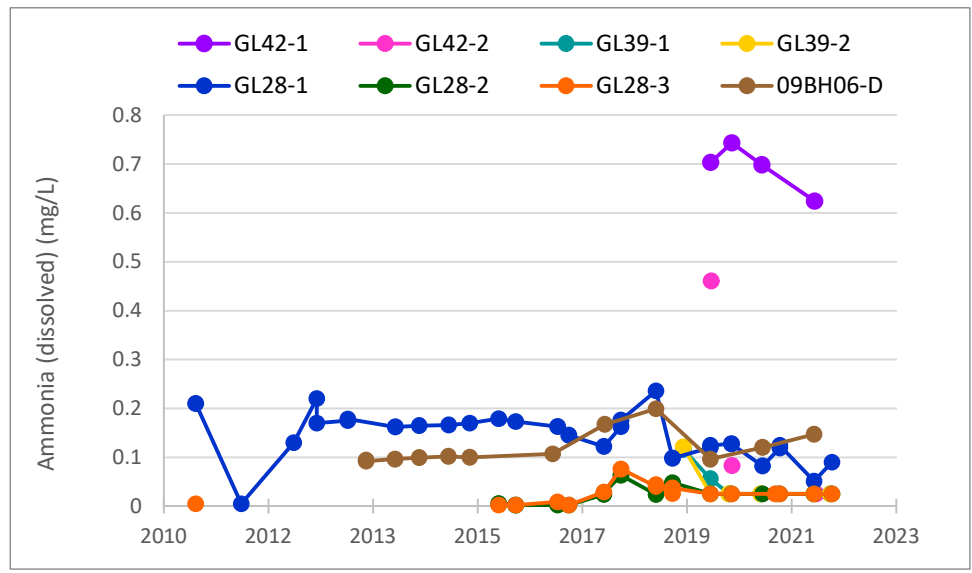
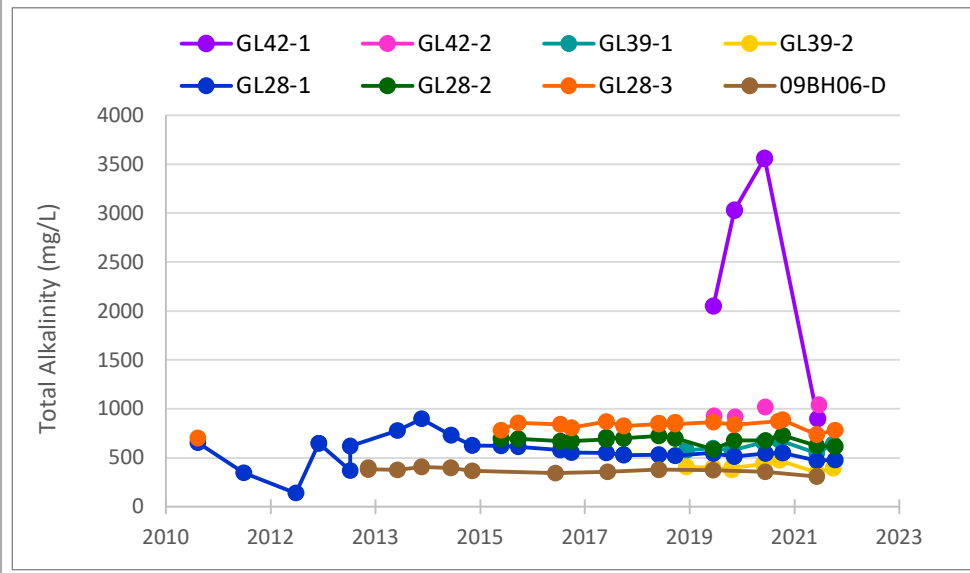
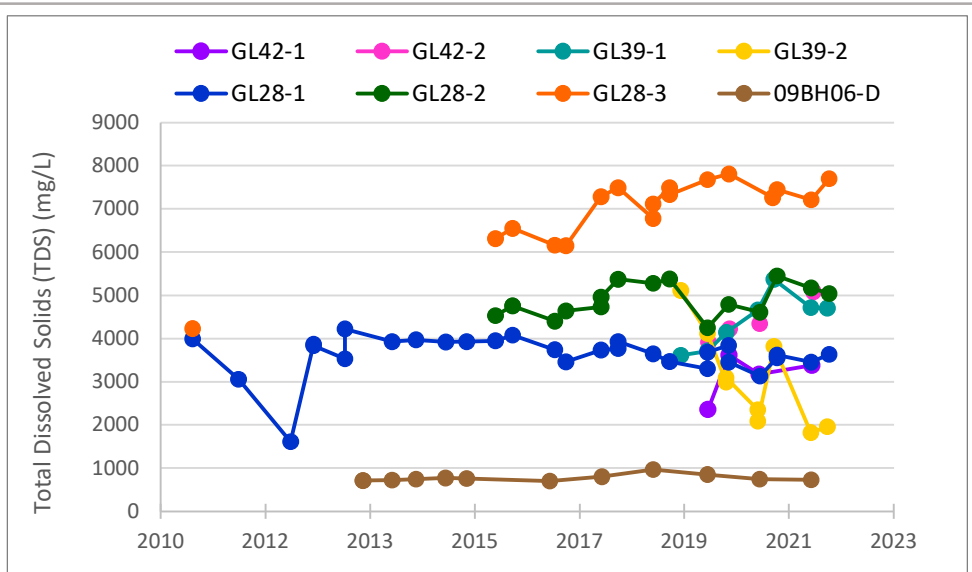
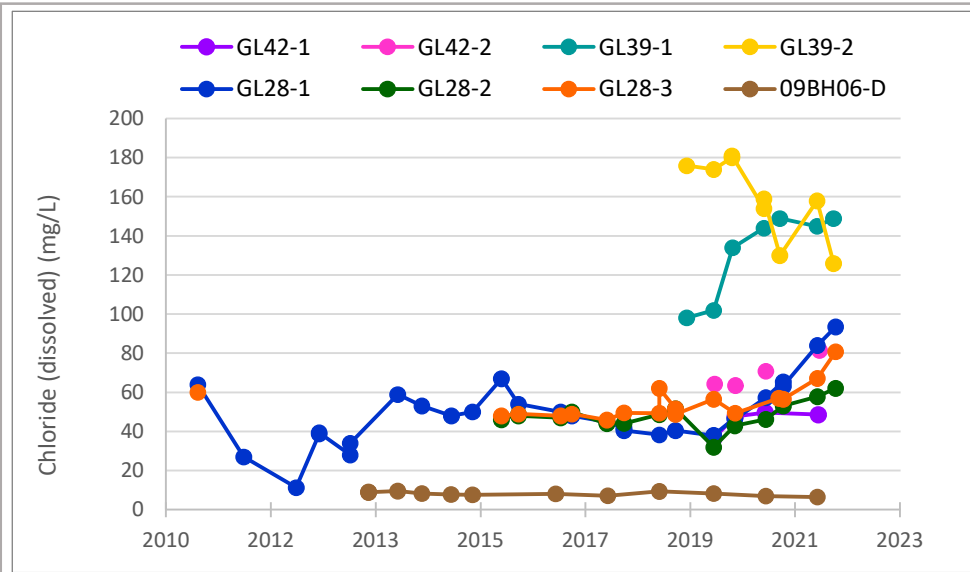
FIGURE H-5



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 COMPOST VICINITY WELLS

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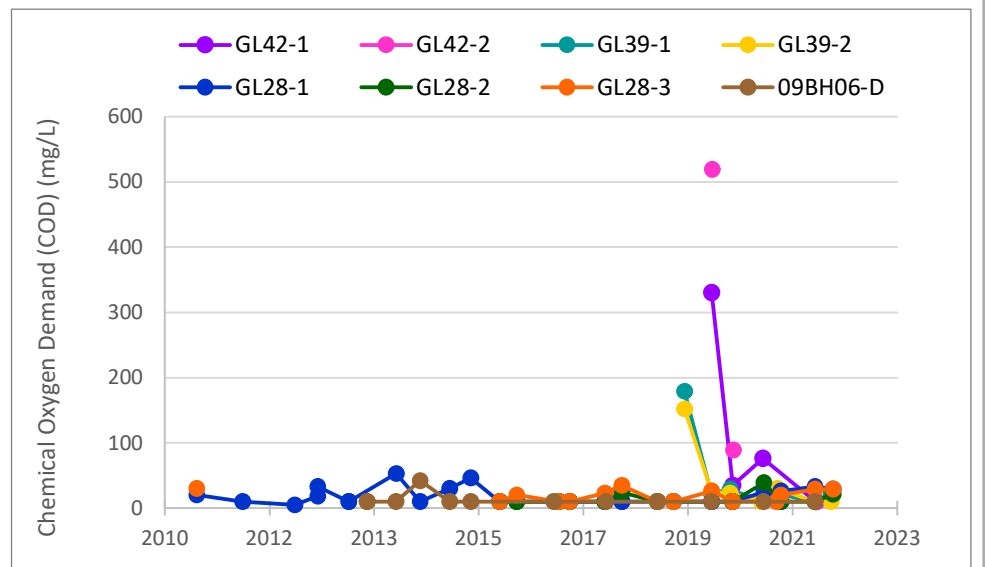
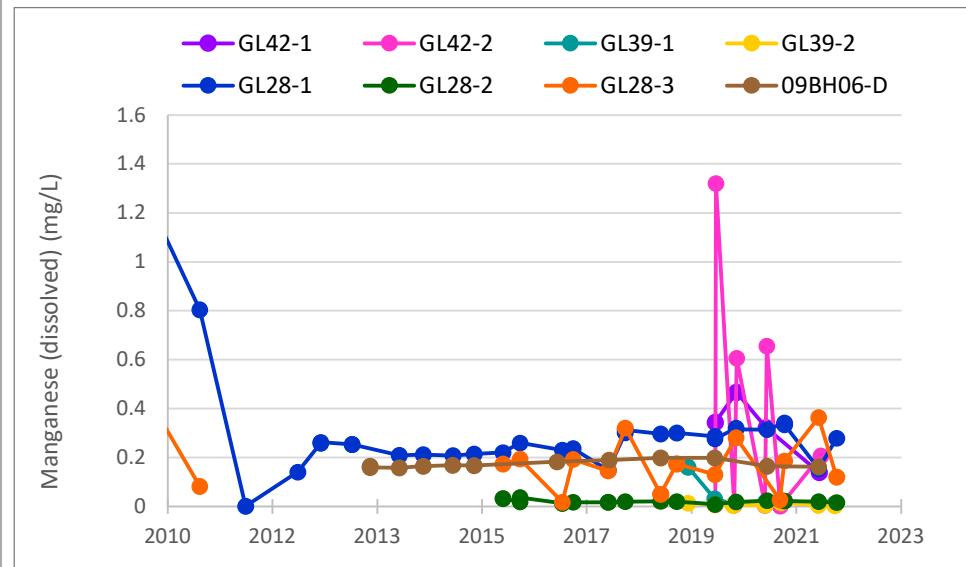
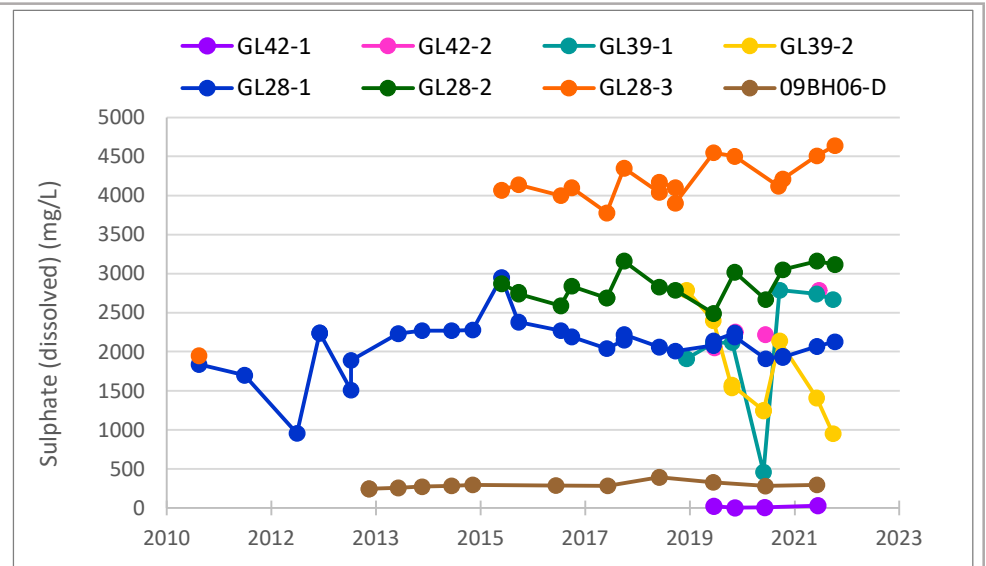
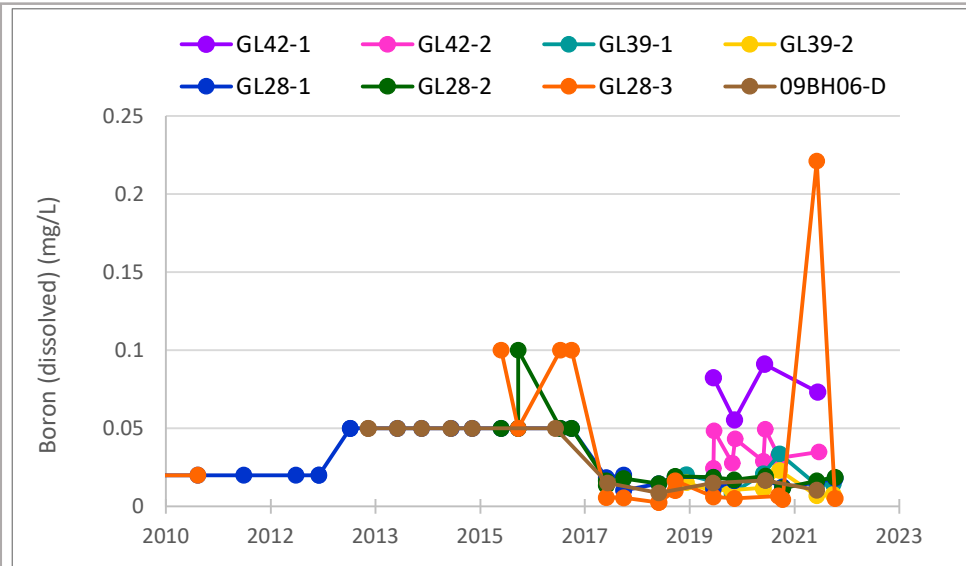
**FIGURE H-6**



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 DOWNGRADIENT WELLS

Project No. 12605725  
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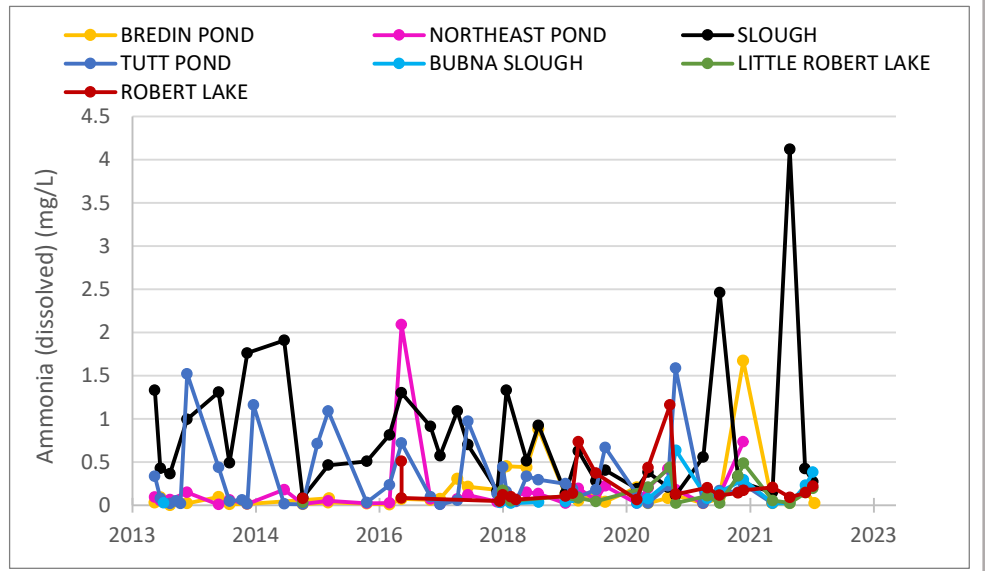
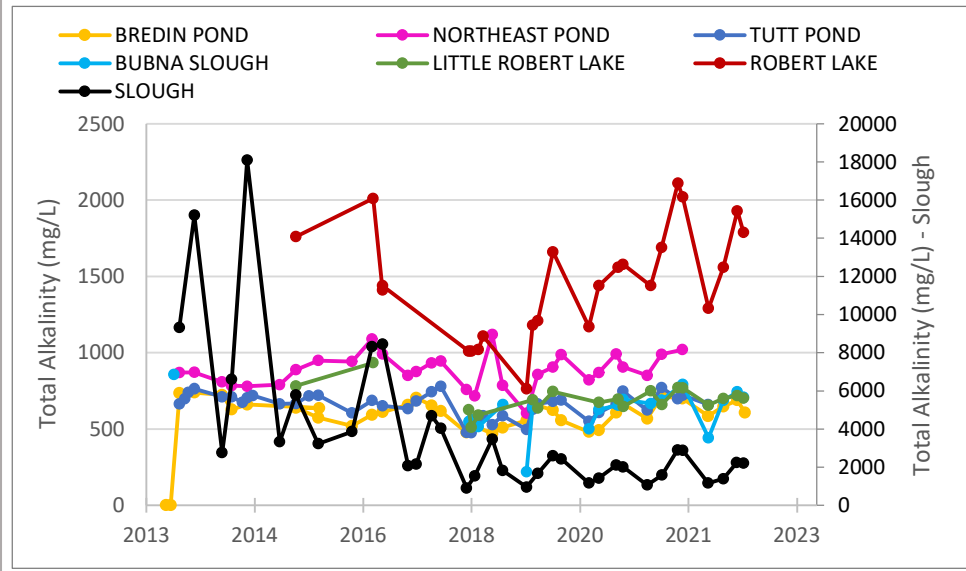
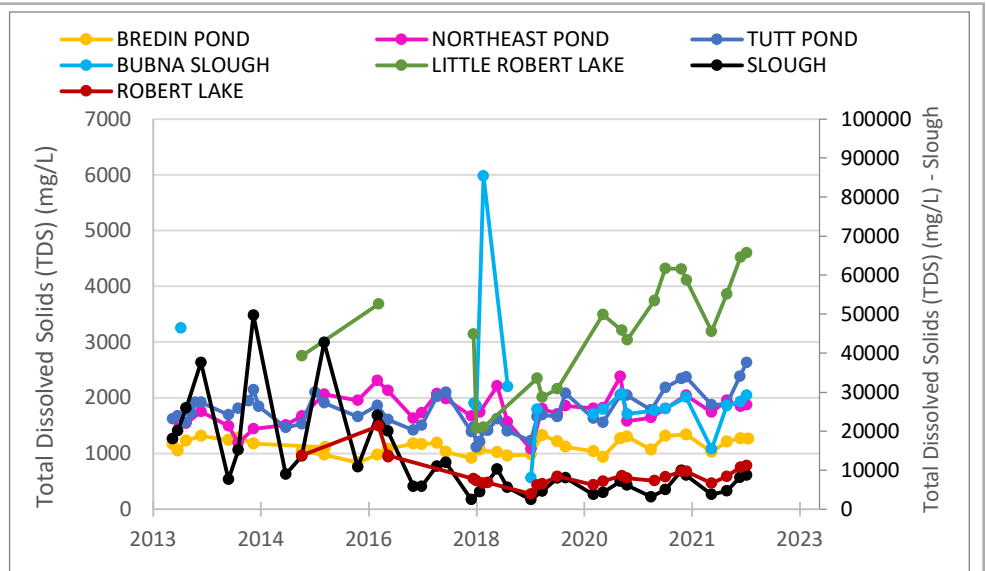
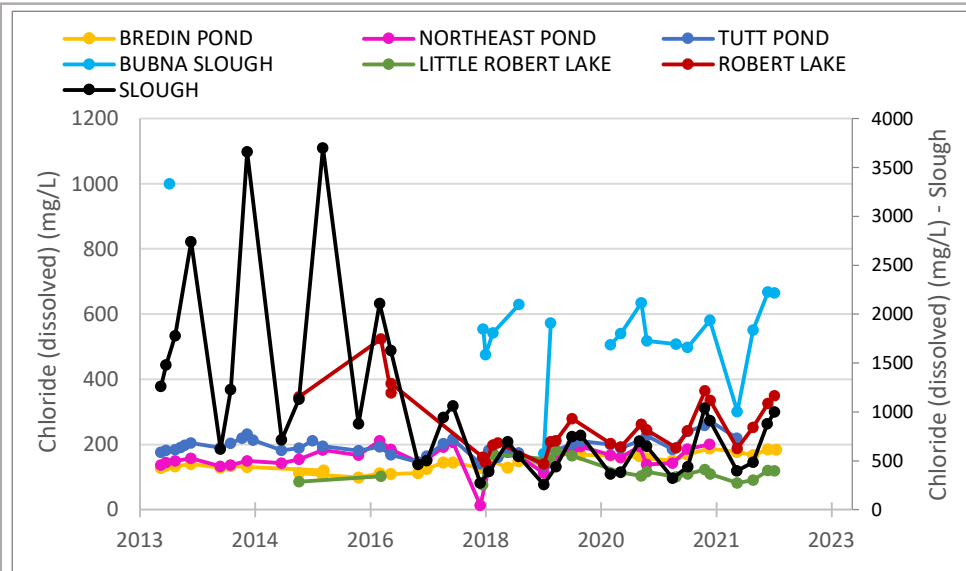
FIGURE H-7



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 DOWNGRAIDENT WELLS

Project No. 12605725  
 Date October 2023

**FIGURE H-8**

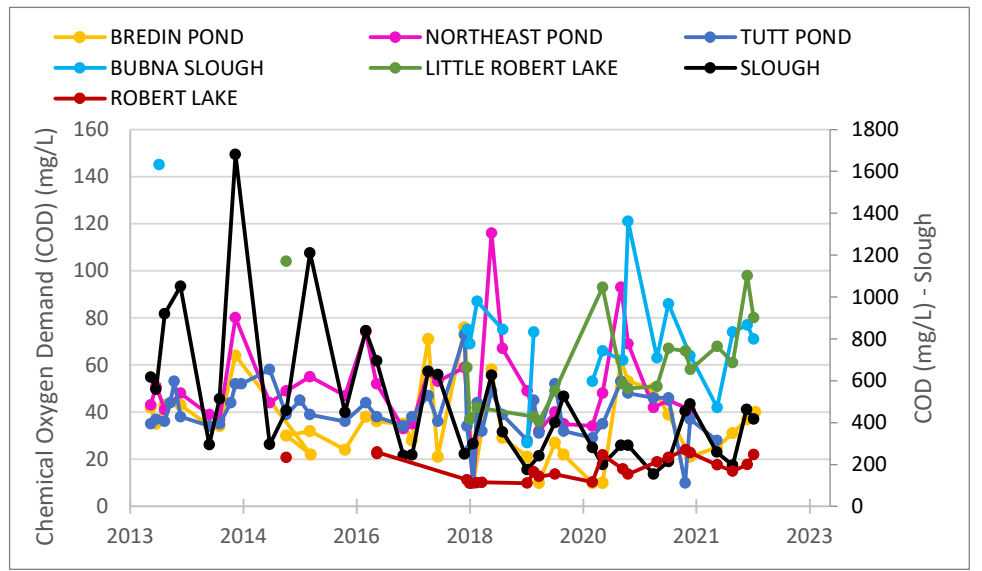
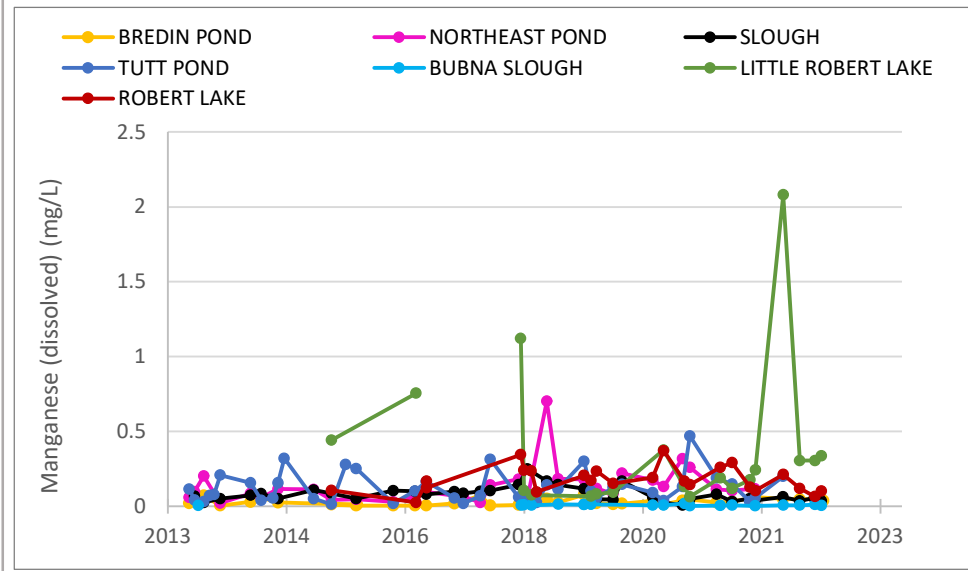
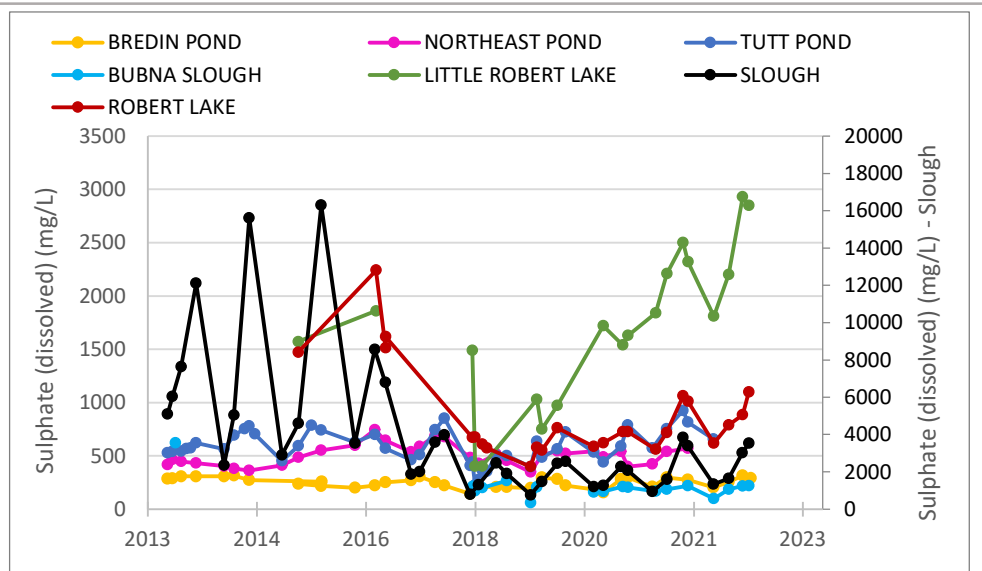
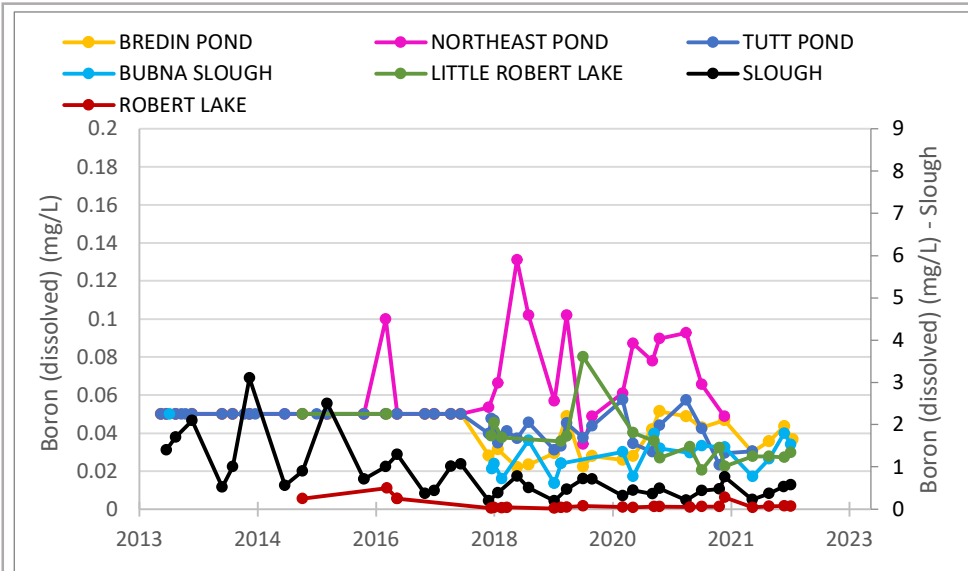


CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 SURFACE WATER

Project No. 12605725  
 Date October 2023

**FIGURE H-9**





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 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY CHARACTERIZATION REPORT  
 CONCENTRATION VERSUS TIME PLOTS  
 SURFACE WATER

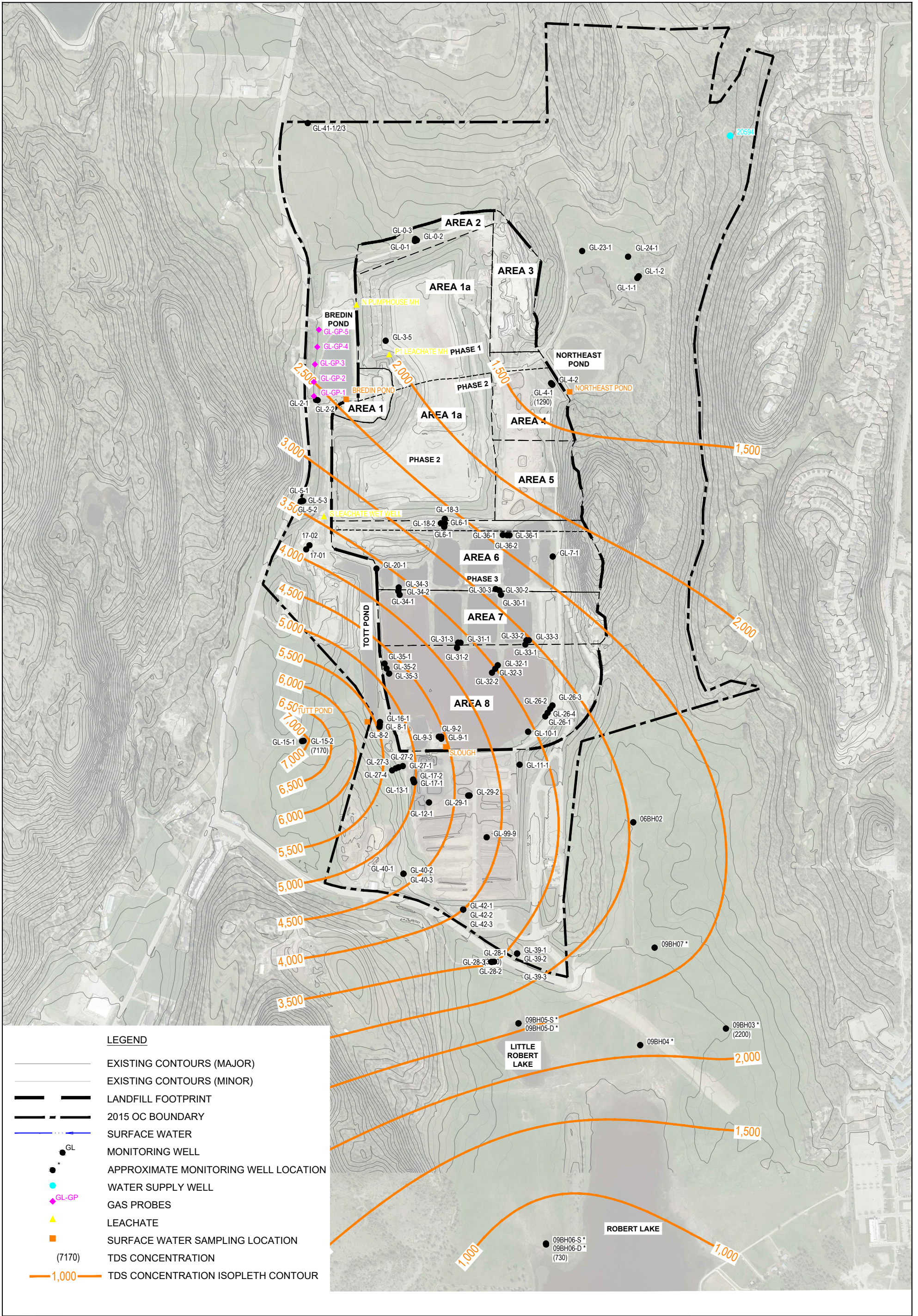
Project No. 12605725  
 Date October 2023

**FIGURE H-10**

# **Appendix I**

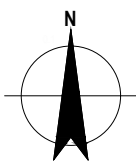
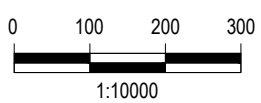
## **Concentration Isopleth Figures**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) TDS CONCENTRATION
- 1,000 TDS CONCENTRATION ISOPLETH CONTOUR

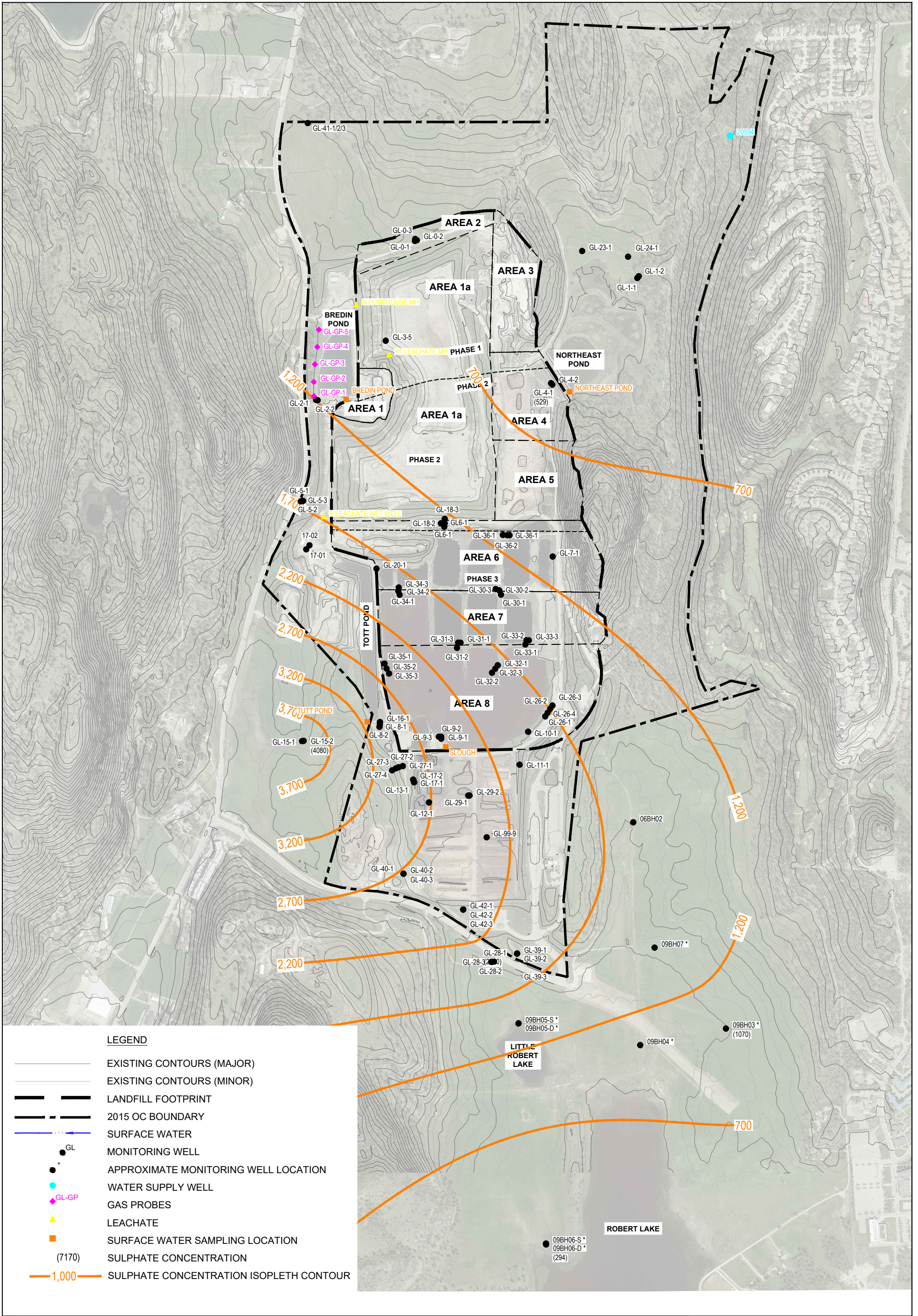


CITY OF KELOWNA  
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 CHARACTERIZATION REPORT  
 SAND AND GRAVEL UNIT  
 TDS CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

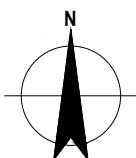
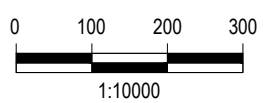
**FIGURE I-1**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) SULPHATE CONCENTRATION
- 1,000 — SULPHATE CONCENTRATION ISOPLETH CONTOUR

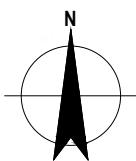
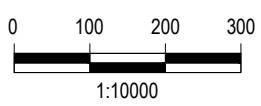
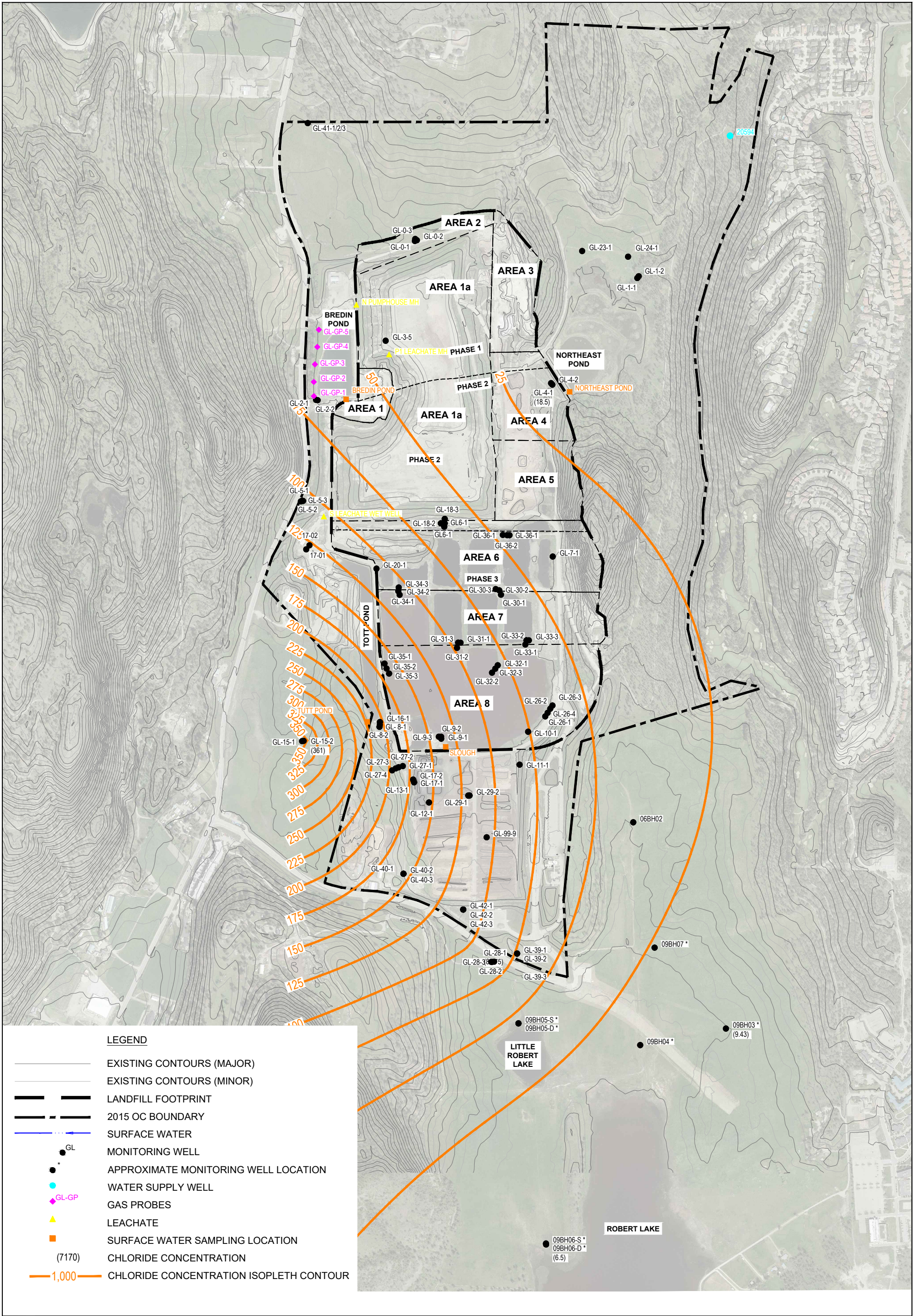


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 SAND AND GRAVEL UNIT  
 SULPHATE CONCENTRATION ISOPLETHS

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 Date October 2023

**FIGURE I-2**



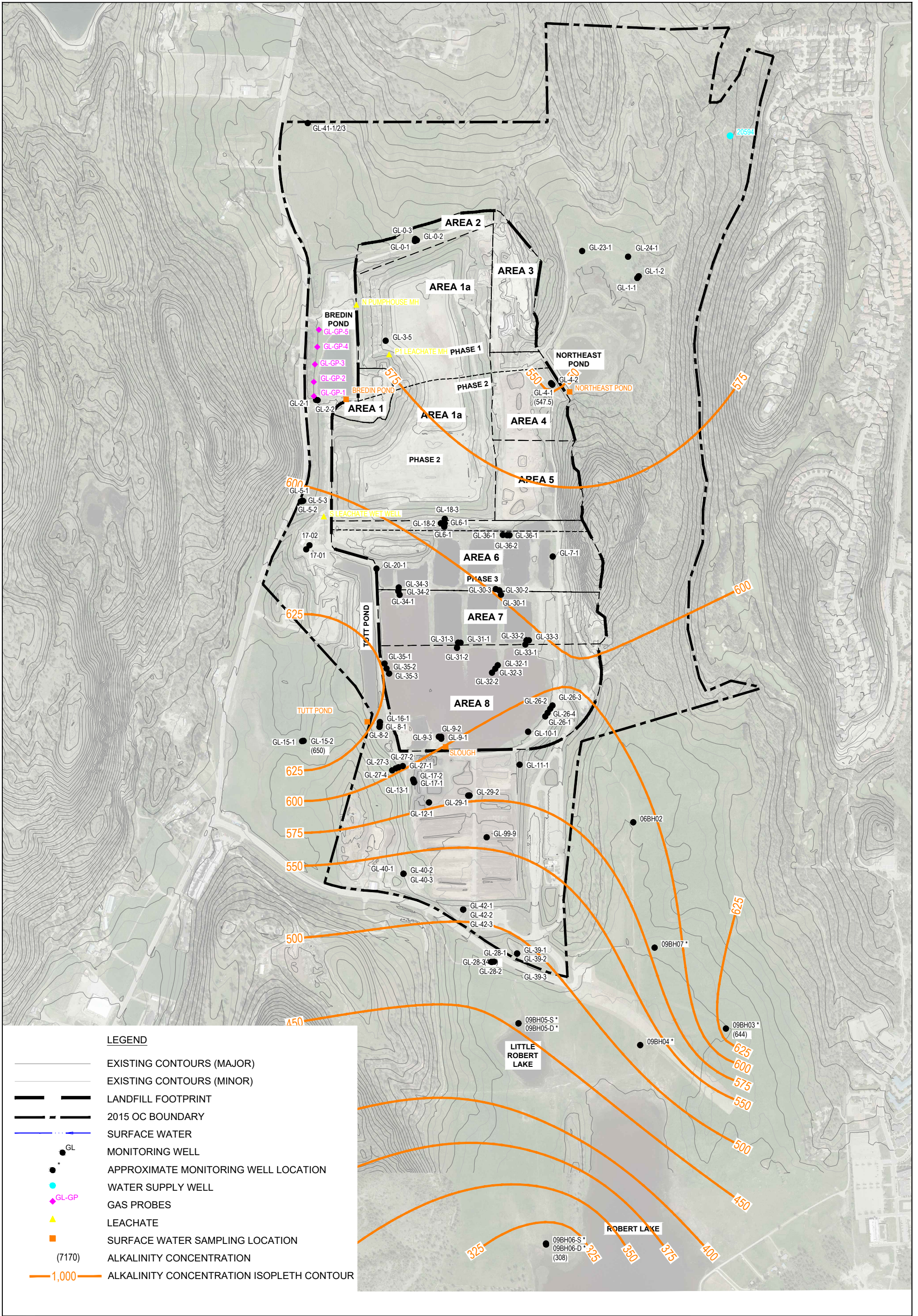


CITY OF KELOWNA  
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 CHARACTERIZATION REPORT  
 SAND AND GRAVEL UNIT  
 CHLORIDE CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

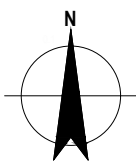
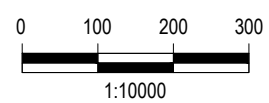
FIGURE I-3





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) ALKALINITY CONCENTRATION
- 1,000 ALKALINITY CONCENTRATION ISOPLETH CONTOUR

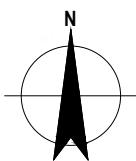
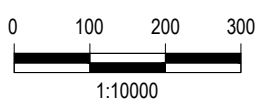
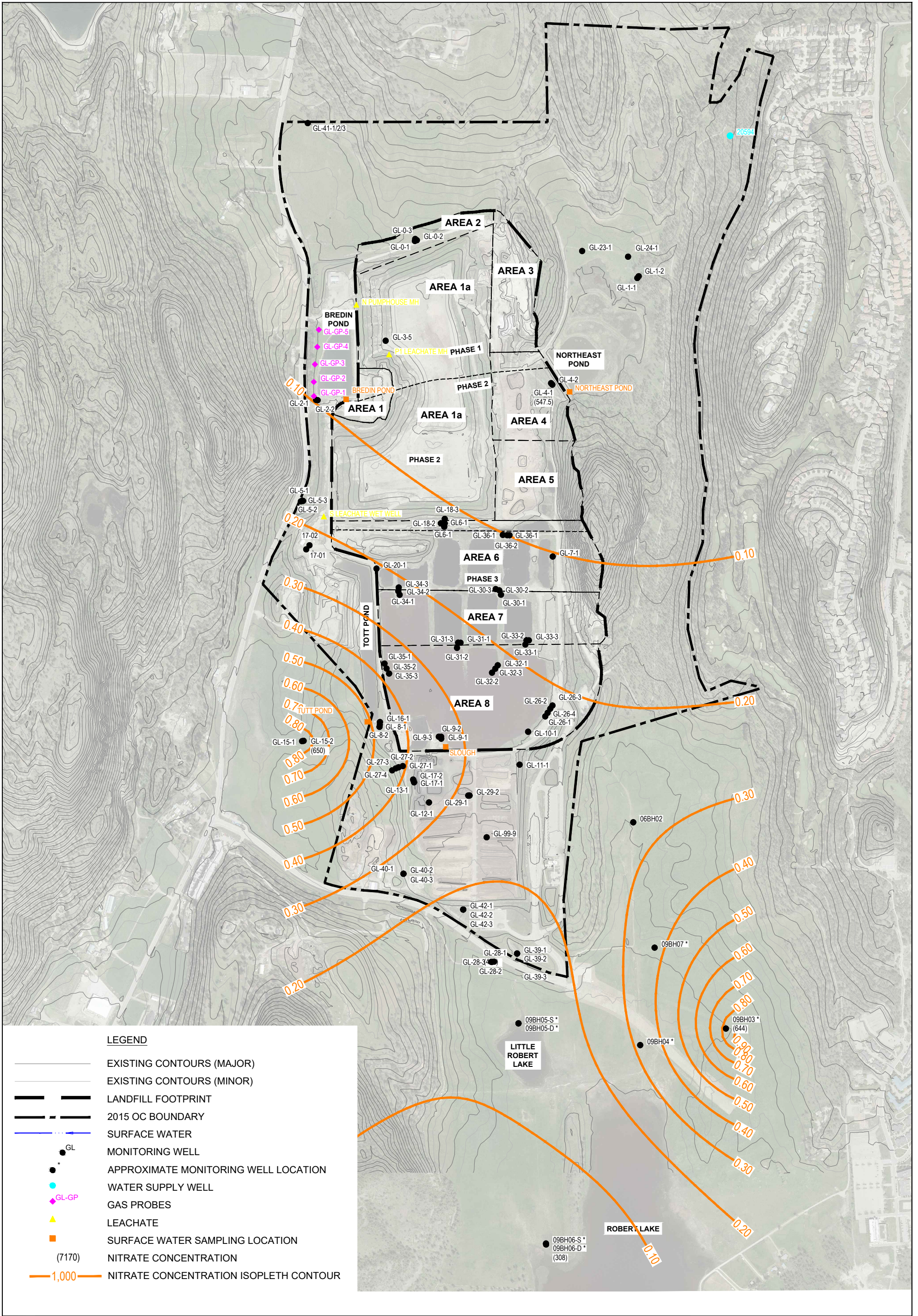


CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 SAND AND GRAVEL UNIT  
 ALKALINITY CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

**FIGURE I-4**



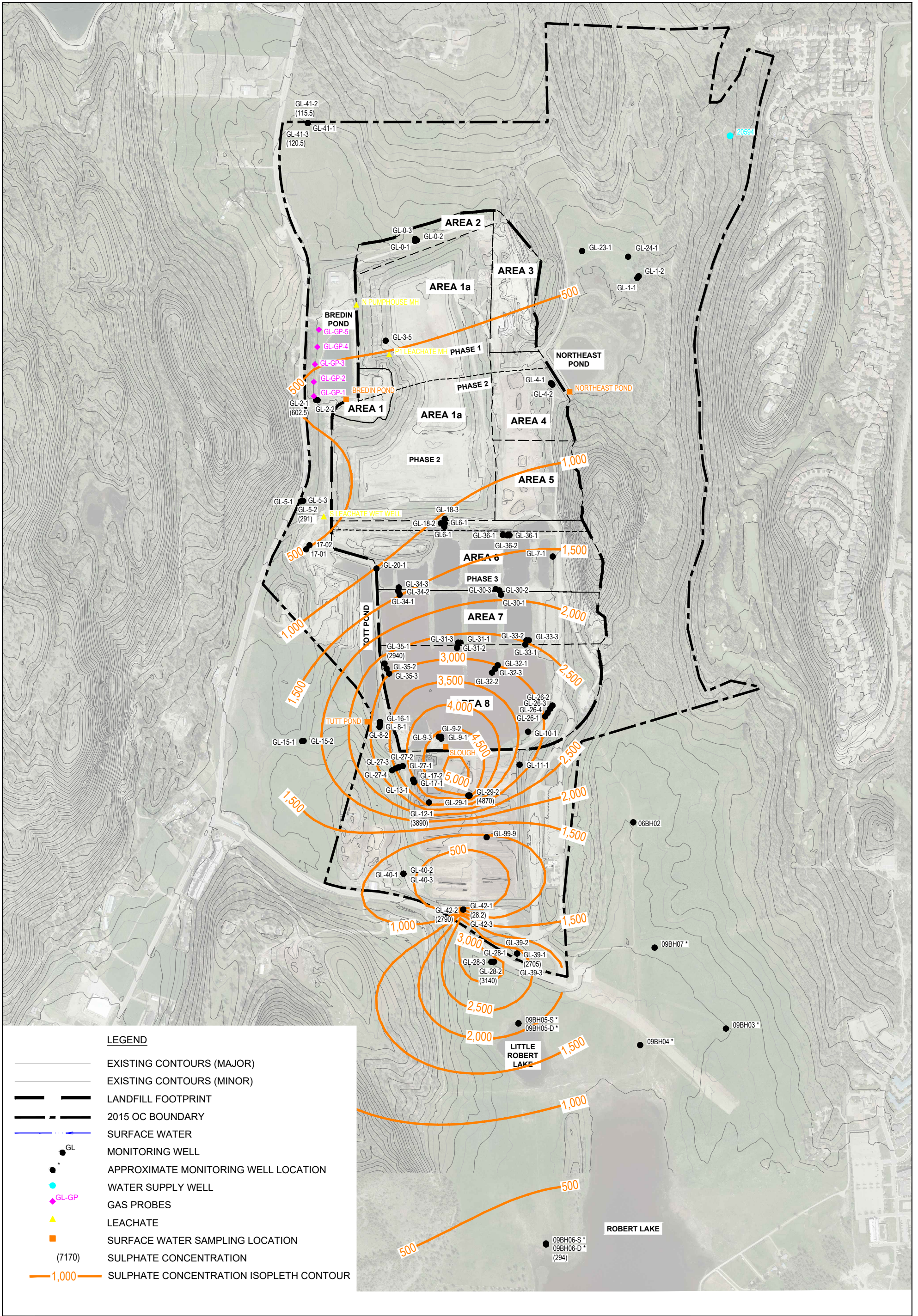


CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 SAND AND GRAVEL UNIT  
 NITRATE CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

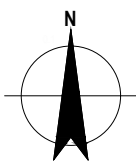
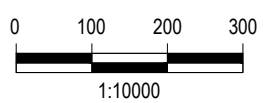
FIGURE I-5





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) SULPHATE CONCENTRATION
- 1,000 — SULPHATE CONCENTRATION ISOPLETH CONTOUR

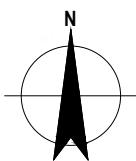
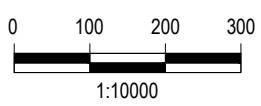
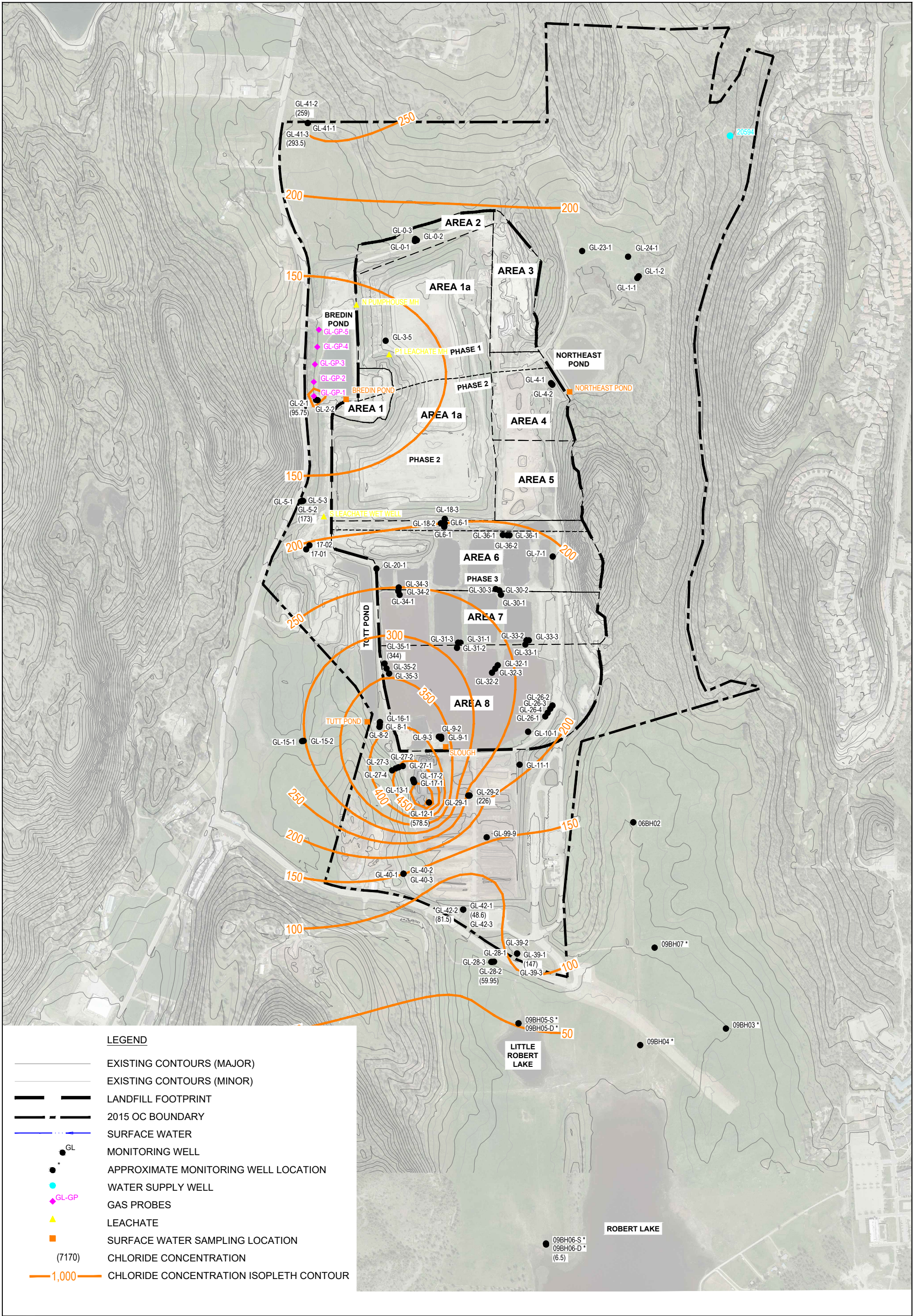


CITY OF KELOWNA  
 GLENMORE LANDFILL  
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 CHARACTERIZATION REPORT  
 TILL UNIT  
 SULPHATE CONCENTRATION ISOPLETHS

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**FIGURE I-7**





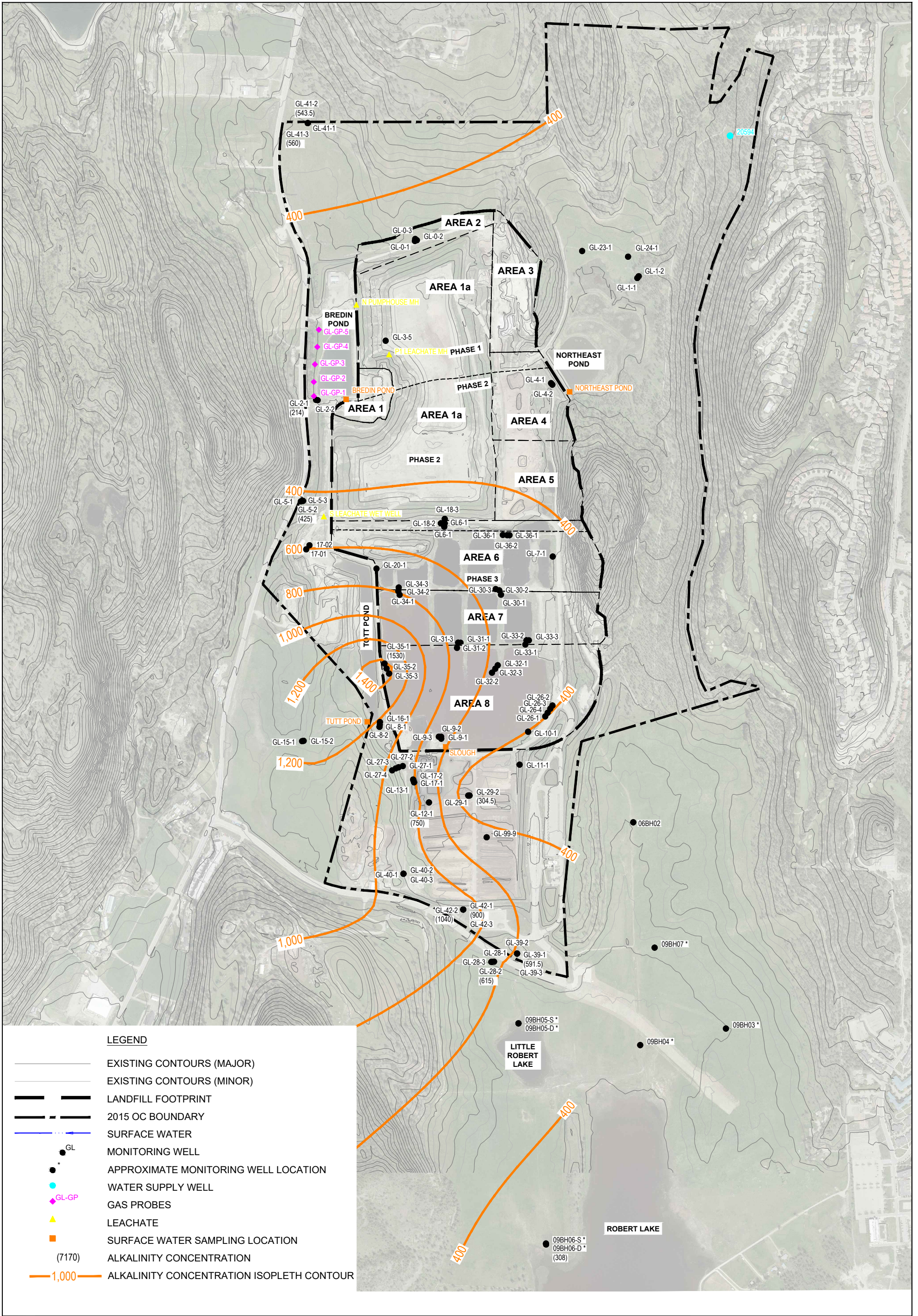
CITY OF KELOWNA  
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 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT

TILL UNIT  
 CHLORIDE CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

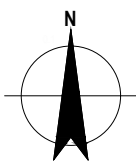
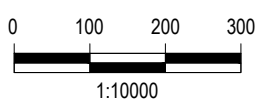
FIGURE I-8





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) ALKALINITY CONCENTRATION
- 1,000 ALKALINITY CONCENTRATION ISOPLETH CONTOUR

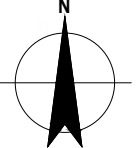
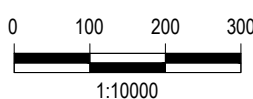
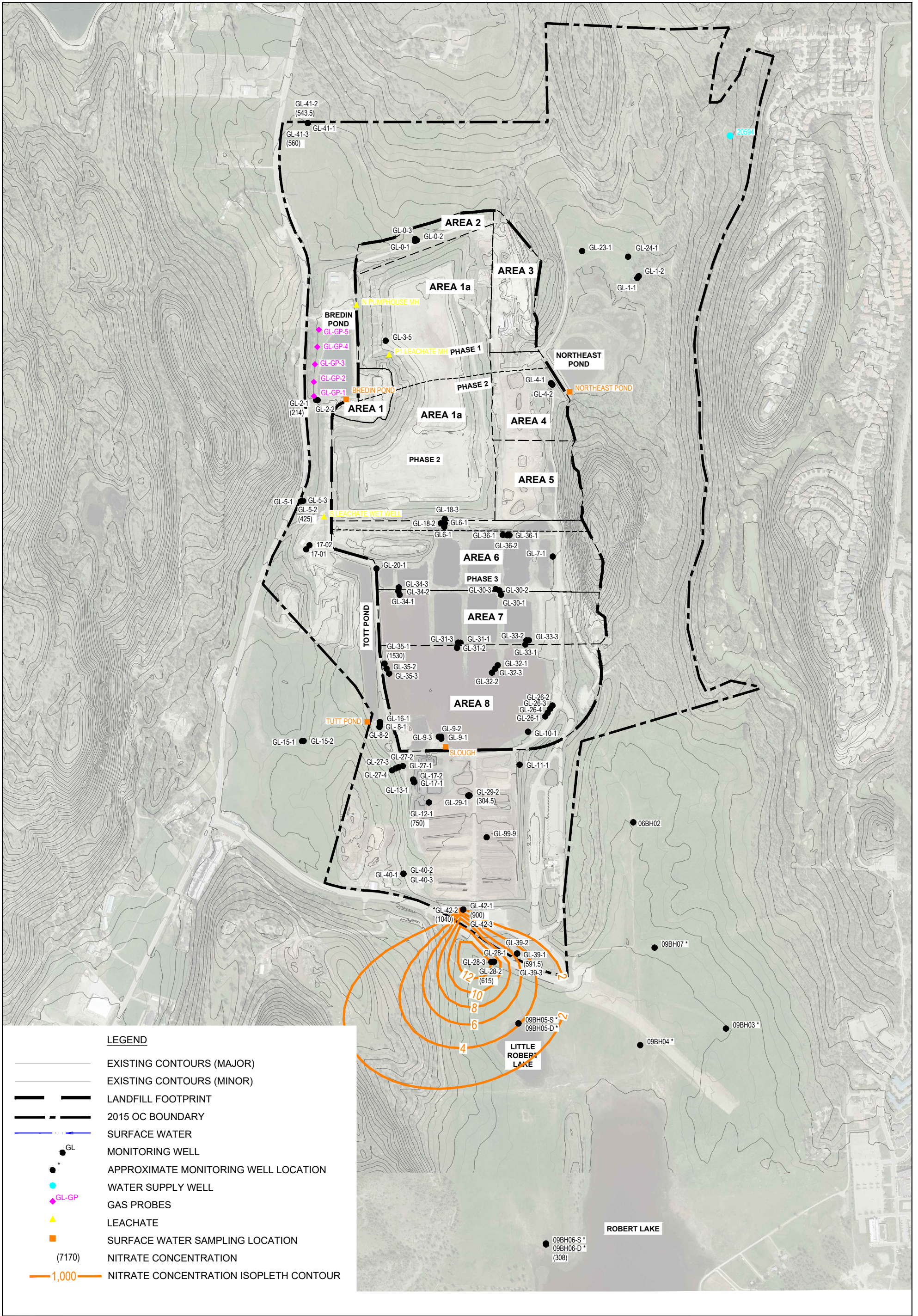


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 CHARACTERIZATION REPORT  
 TILL UNIT  
 ALKALINITY  
 CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

**FIGURE I-9**





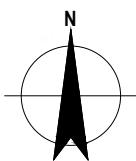
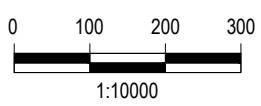
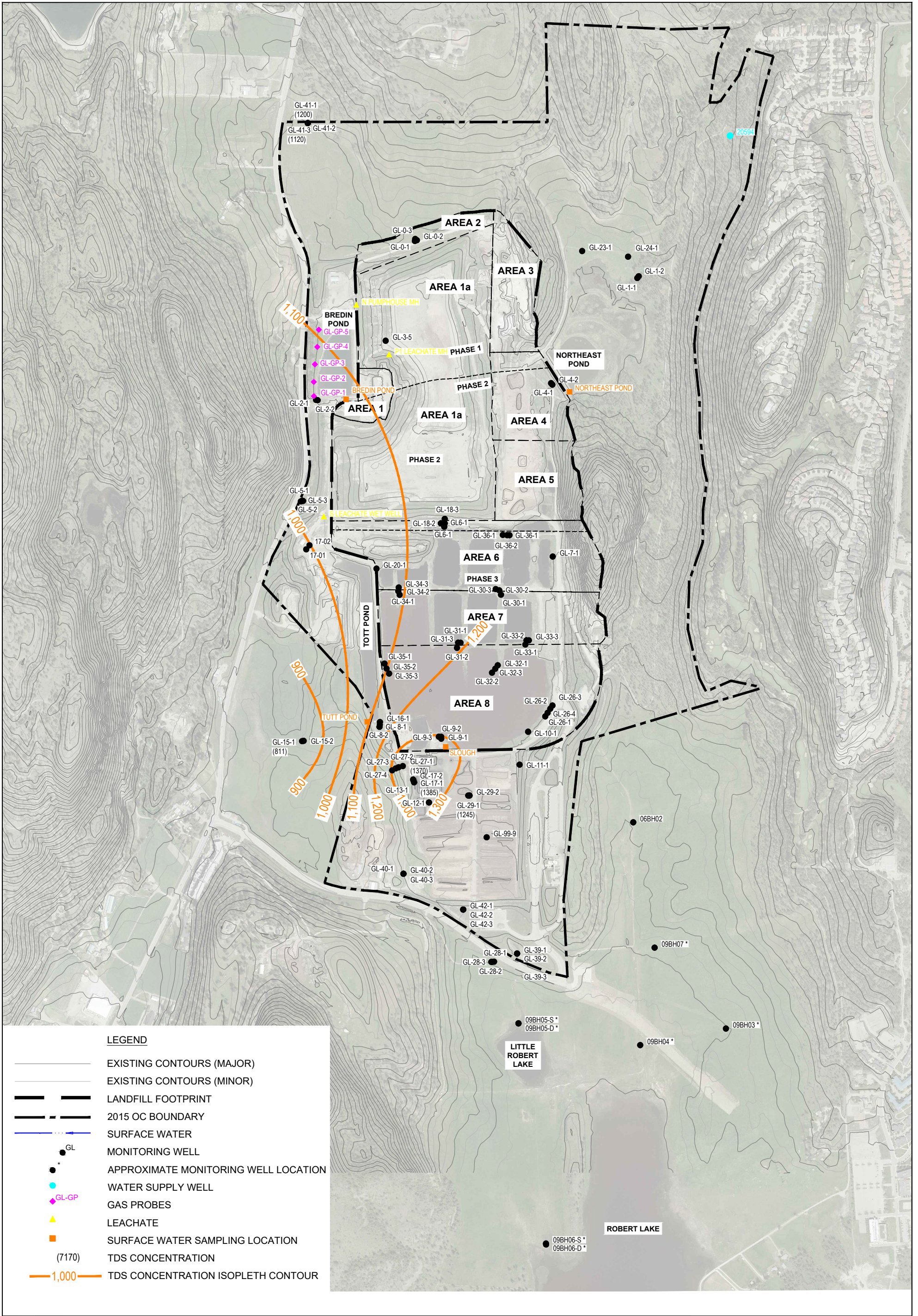
CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT

TILL UNIT  
 NITRATE CONCENTRATION ISOPLETHS

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 Date October 2023

FIGURE I-10



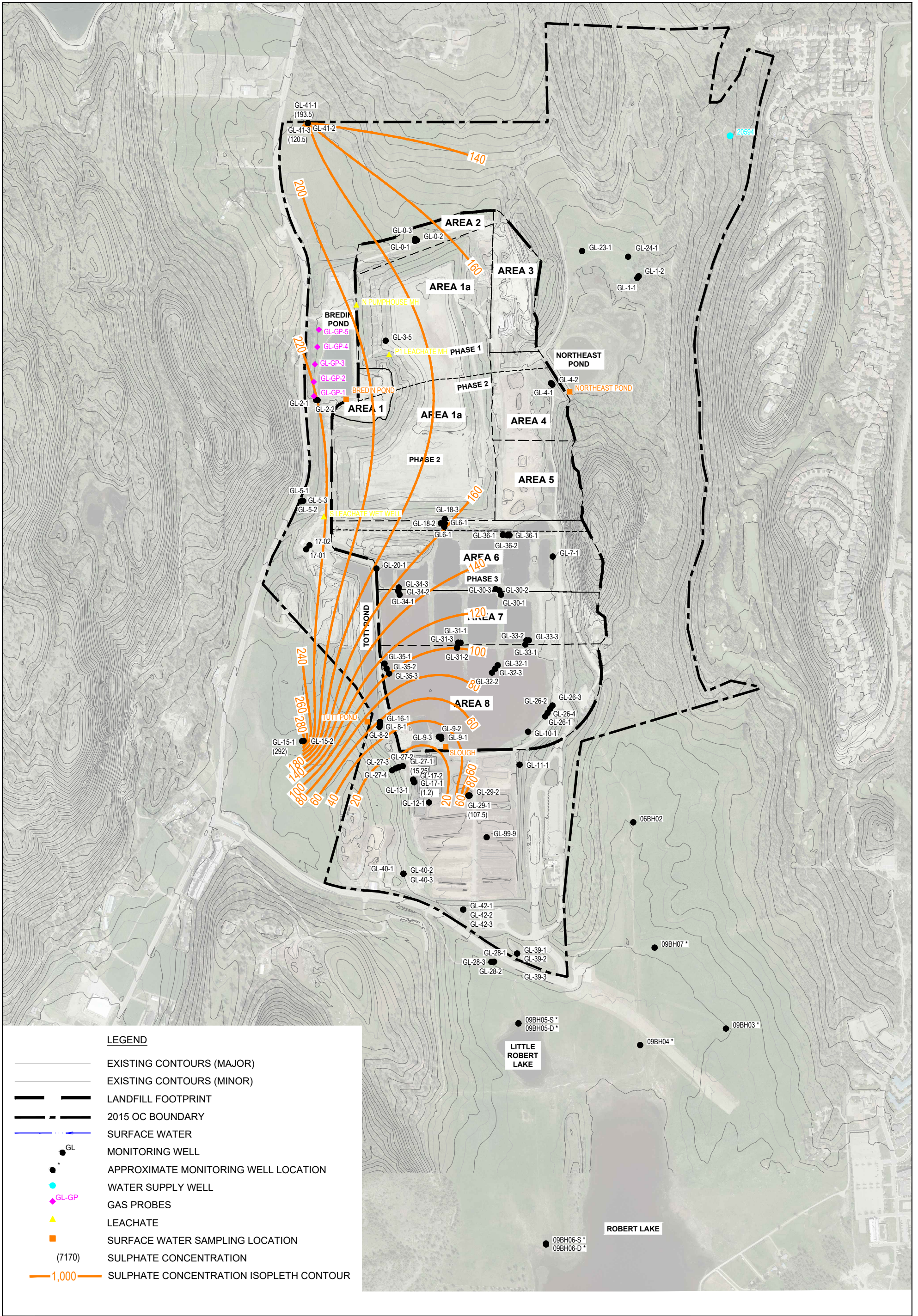


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 CHARACTERIZATION REPORT  
 BEDROCK UNIT  
 TDS CONCENTRATION ISOPLETHS

Project No. 12605725  
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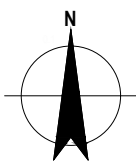
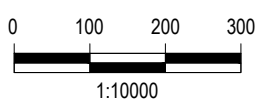
FIGURE I-11





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) SULPHATE CONCENTRATION
- 1,000 — SULPHATE CONCENTRATION ISOPLETH CONTOUR

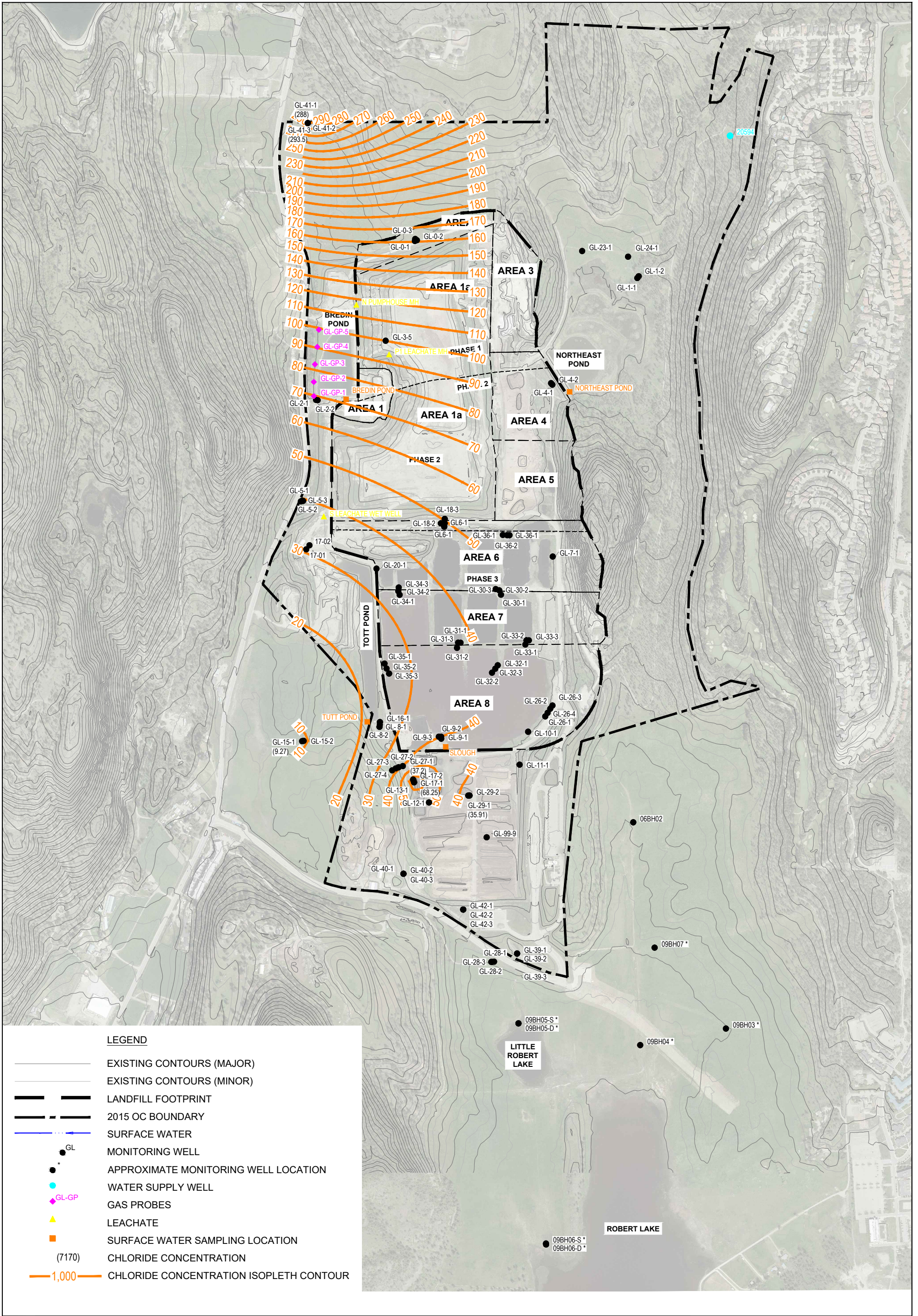


CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 BEDROCK UNIT  
 SULPHATE CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

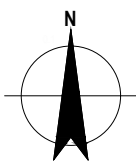
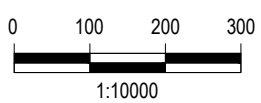
**FIGURE I-12**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- - - 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) CHLORIDE CONCENTRATION
- 1,000 CHLORIDE CONCENTRATION ISOPLETH CONTOUR

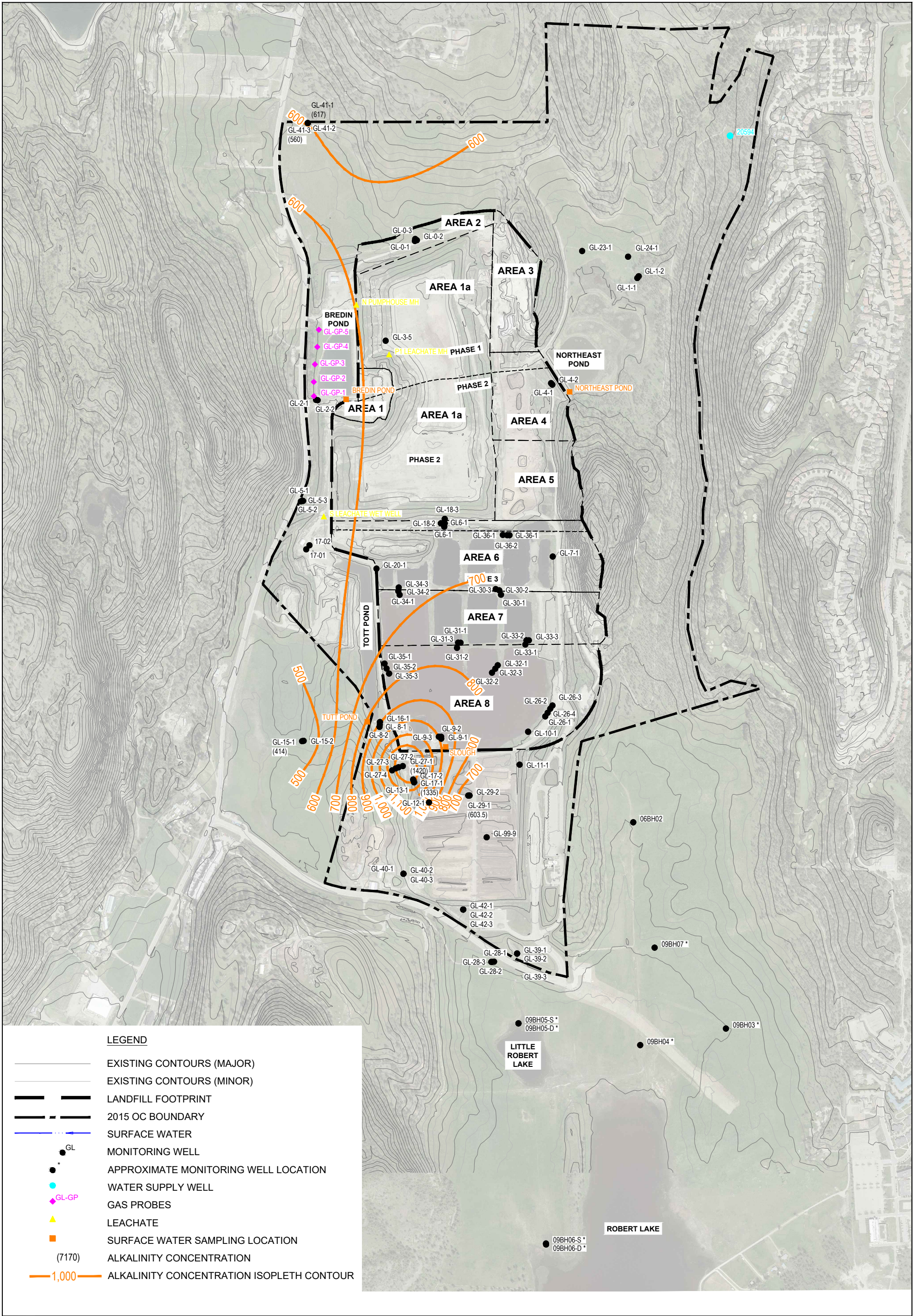


CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 CHLORIDE BEDROCK UNIT  
 CHLORIDE CONCENTRATION ISOPLETHS

Project No. 12605725  
 Date October 2023

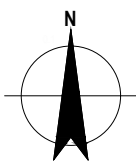
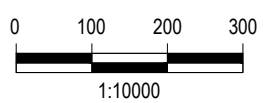
**FIGURE I-13**





**LEGEND**

- EXISTING CONTOURS (MAJOR)
- EXISTING CONTOURS (MINOR)
- LANDFILL FOOTPRINT
- 2015 OC BOUNDARY
- SURFACE WATER
- GL  
● MONITORING WELL
- APPROXIMATE MONITORING WELL LOCATION
- WATER SUPPLY WELL
- GL-GP  
● GAS PROBES
- ▲ LEACHATE
- SURFACE WATER SAMPLING LOCATION
- (7170) ALKALINITY CONCENTRATION
- 1,000 ALKALINITY CONCENTRATION ISOPLETH CONTOUR

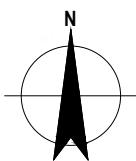
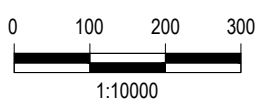
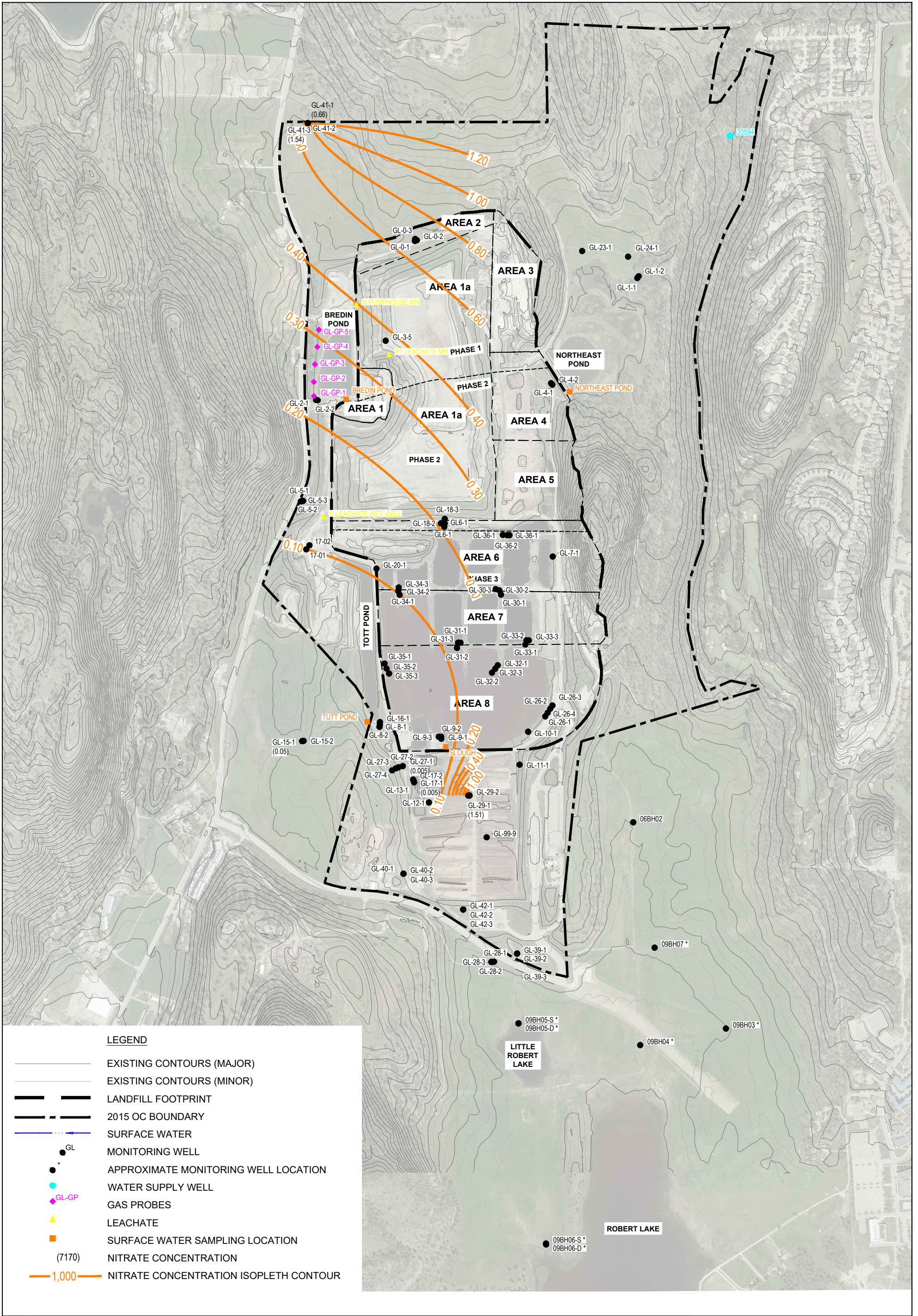


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 CHARACTERIZATION REPORT  
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 ALKALINITY CONCENTRATION ISOPLETHS

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**FIGURE I-14**





CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT

**BEDROCK UNIT  
 NITRATE CONCENTRATION ISOPLETHS**

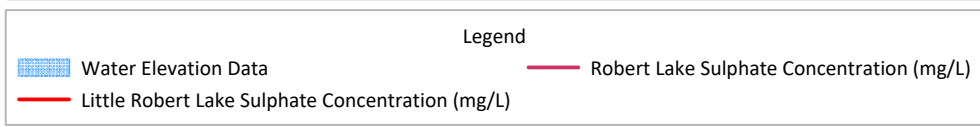
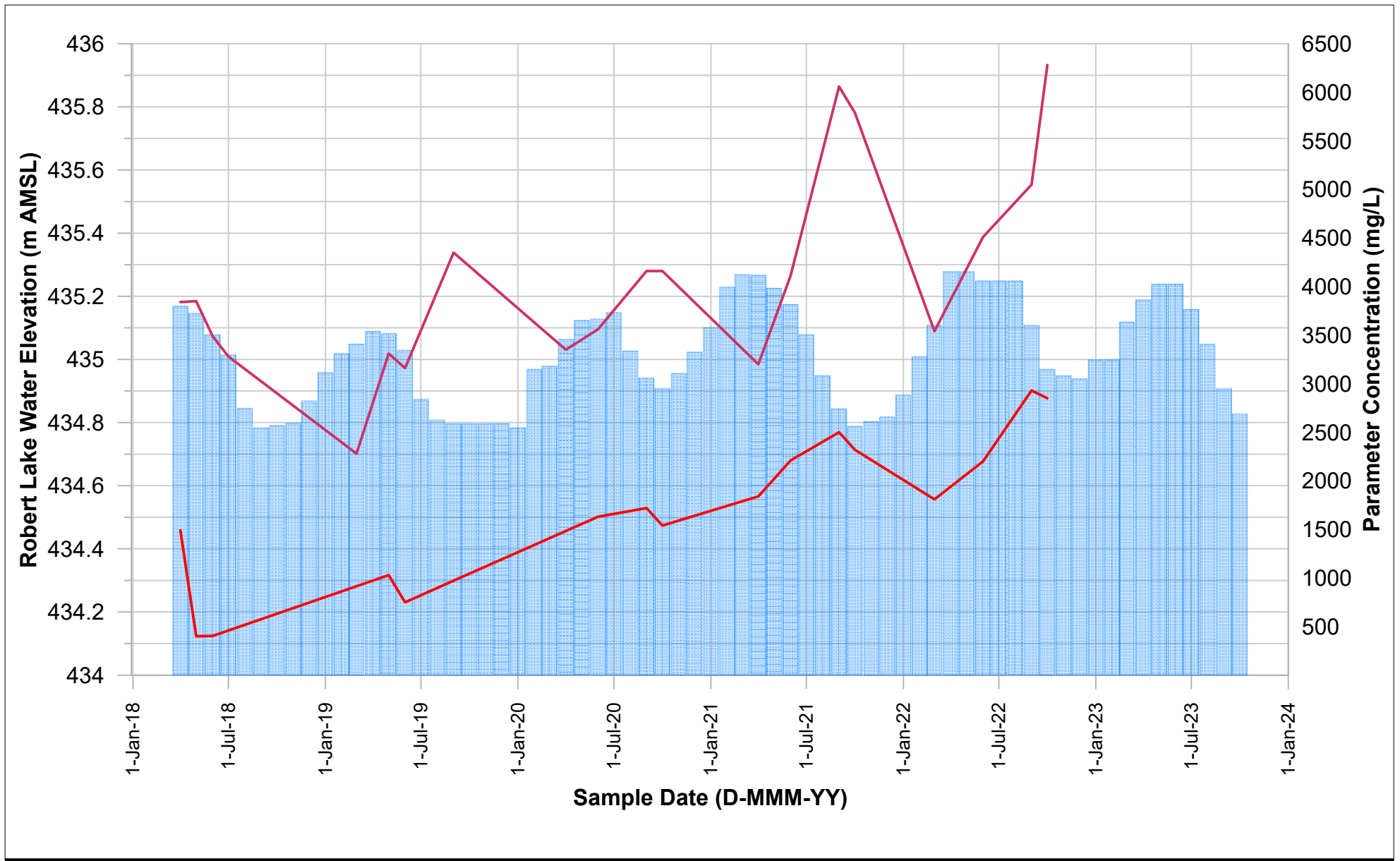
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 Date October 2023

**FIGURE I-15**



# **Appendix J**

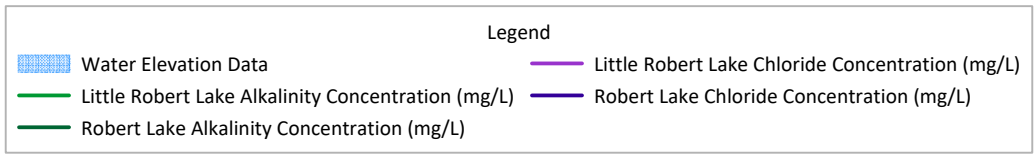
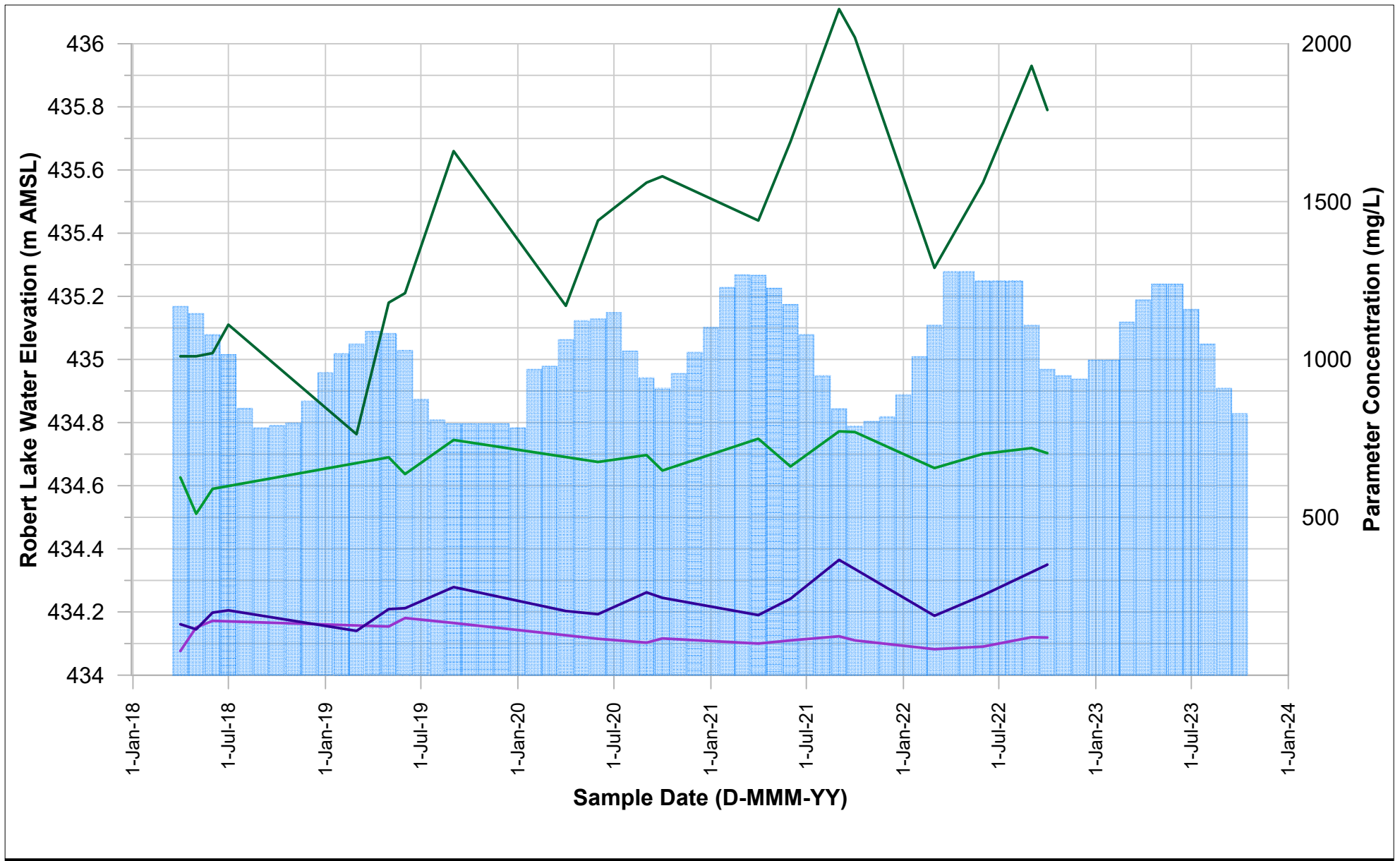
**Robert Lake Elevation versus Indicator  
Parameter Concentrations**



CITY OF KELOWNA - GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 Robert Lake Elevation vs Indicator  
 Parameter Concentrations in L. Robert Lake  
 and Robert Lake

Project No. 12605725  
 Date November 17, 2023

FIGURE J-1



CITY OF KELOWNA - GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 Robert Lake Elevation vs Indicator  
 Parameter Concentrations in L. Robert Lake  
 and Robert Lake

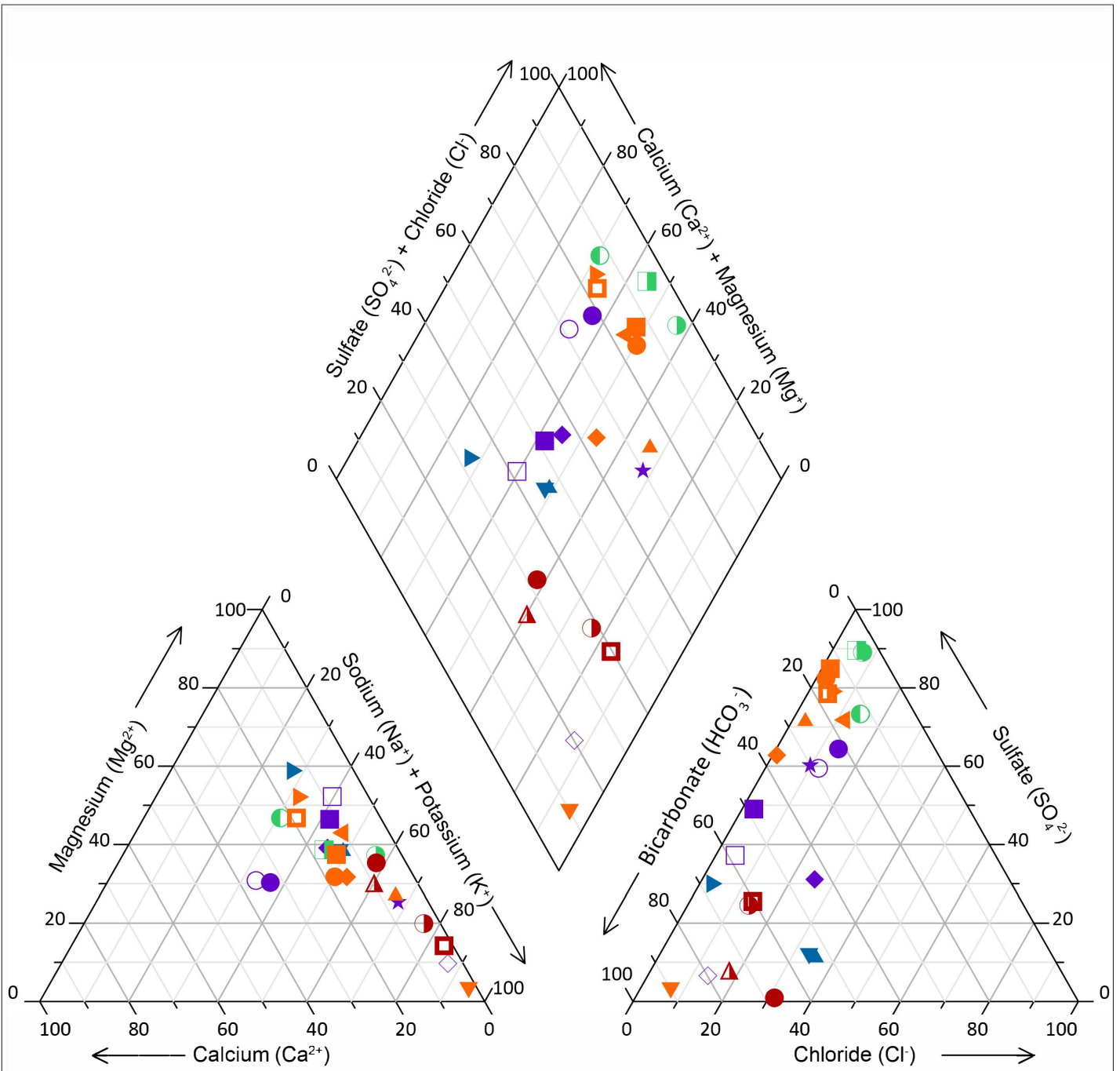
Project No. 12605725  
 Date November 17, 2023

FIGURE J-2



# **Appendix K**

## **Geochemical Analysis**



### LEGEND

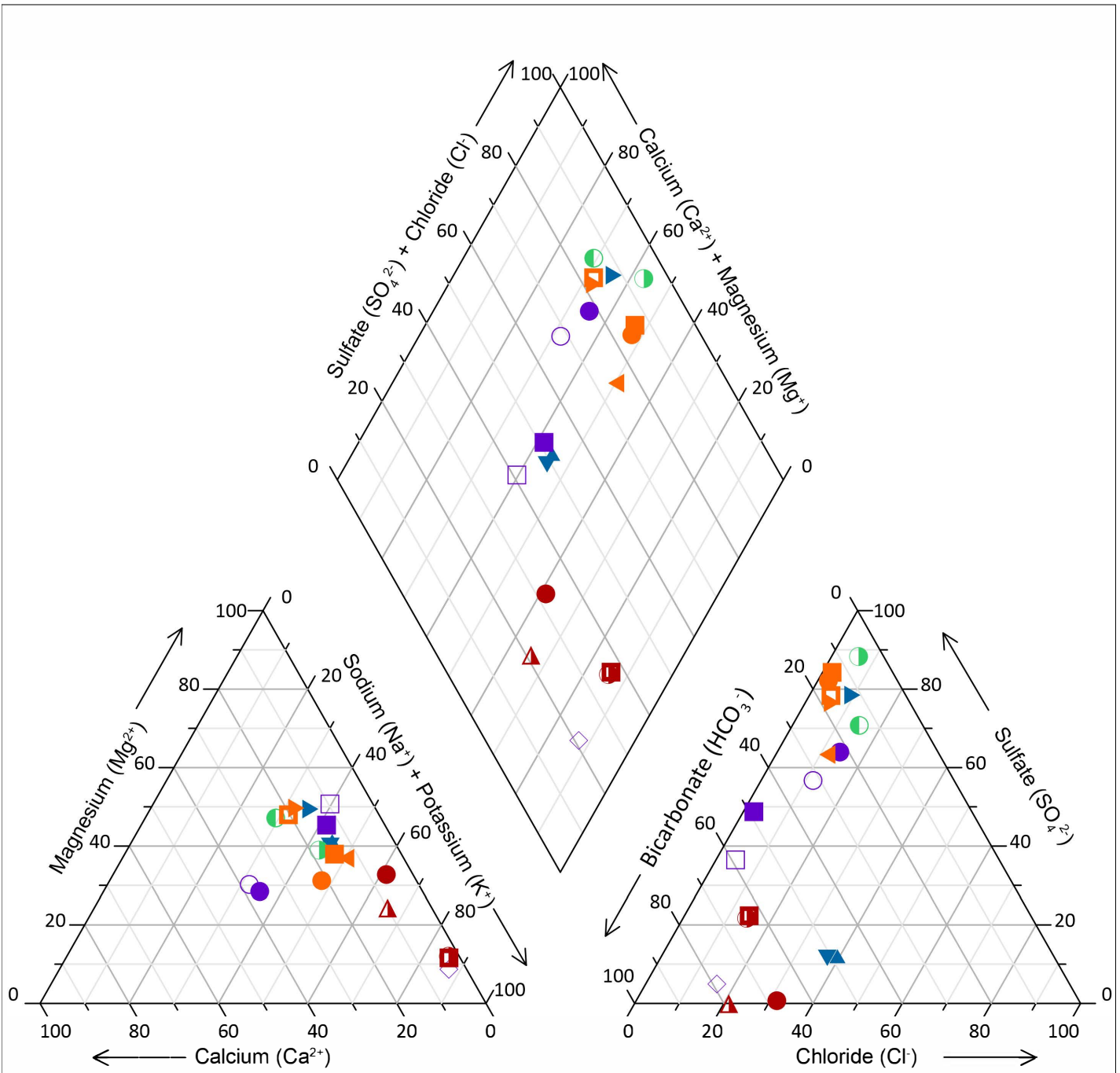
Upgradient	Landfill Vicinity	Compost Vicinity	Downgradient	Leachate
▼ GL41-2	● GL2-1	● GL12-1	▼ GL42-1	■ S Leachate Wet Well
▲ GL41-3	○ GL2-2	● GL27-3	▲ GL42-2	▲ P1 Leachate MH-2
▶ GL23-1	□ GL4-1	■ GL29-2	▶ GL39-1	● N Pumphouse MH
	□ GL4-2		▶ GL39-2	● P2 A2 Leachate MH
	◆ GL5-2		▶ GL28-1	
	◇ GL20-1		▶ GL28-2	
	☆ GL35-3		▶ GL28-3	
			▶ 09BH03	



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 GROUNDWATER OVERBURDEN WELL  
 PIPER PLOT - SPRING 2022

Project No. 12605725  
 Date November 2023

FIGURE K-1



**LEGEND**

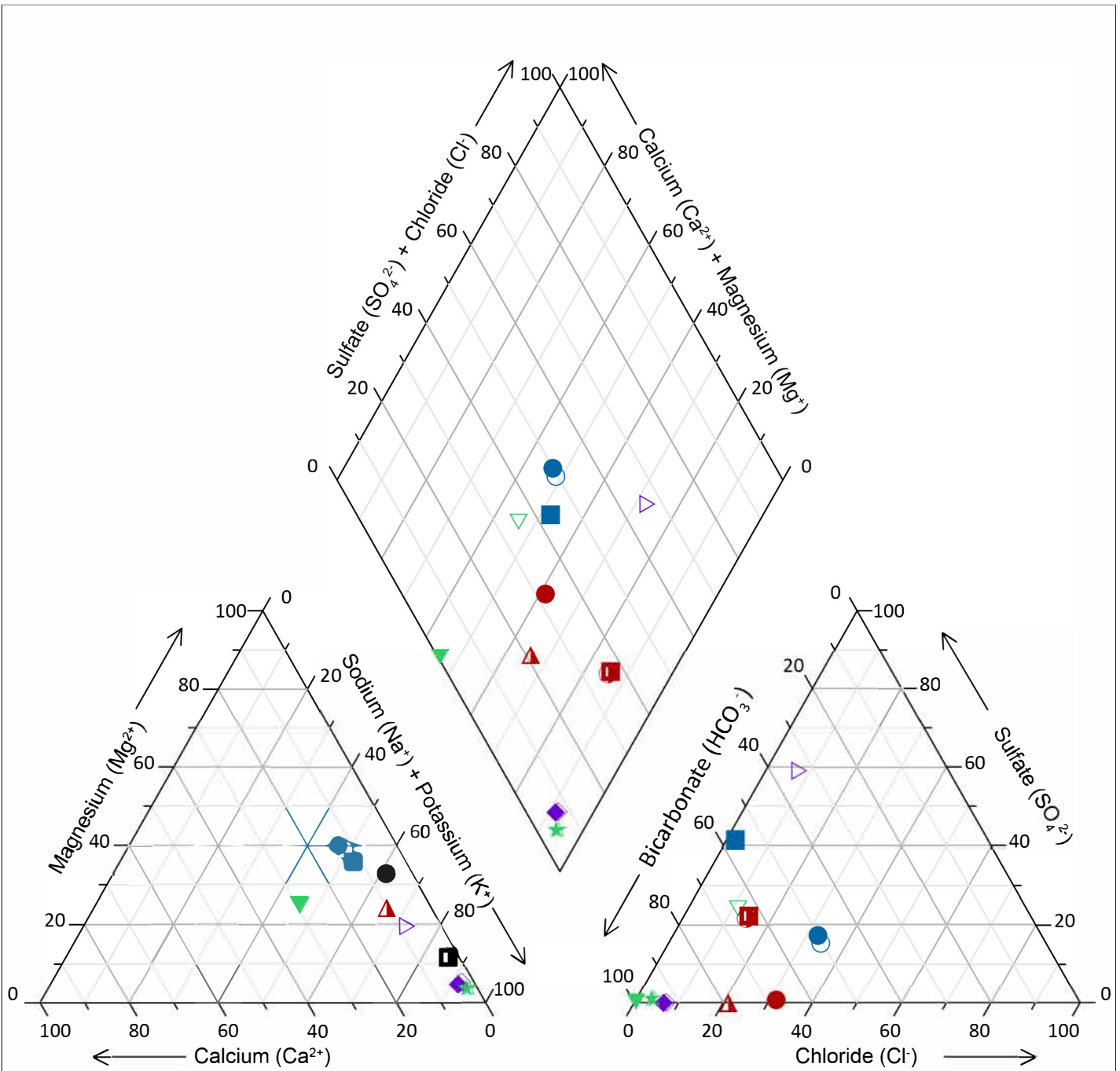
Upgradient	Landfill Vicinity	Compost Vicinity	Downgradient	Leachate
▼ GL41-2	● GL2-1	● GL12-1	▲ GL39-1	■ S Leachate Wet Well
▲ GL41-3	○ GL2-2	● GL29-2	▲ GL39-2	▲ P1 Leachate MH-2
▲ GL15-2	■ GL4-1		○ GL28-1	● N Pumhouse MH
	■ GL4-2		○ GL28-2	● P2 A2 Leachate MH
	◇ GL20-1		■ GL28-3	



CITY OF KELOWNA  
 GLENMORE LANDFILL  
 HYDROGEOLOGY AND HYDROLOGY  
 CHARACTERIZATION REPORT  
 GROUNDWATER OVERBURDEN WELL  
 PIPER PLOT - FALL 2022

Project No. 12605725  
 Date November 2023

**FIGURE K-2**



### LEGEND

#### Bedrock Monitoring Wells

##### Upgradient (Fall)

- GL41-1
- GL15-1

##### Upgradient (Spring)

- GL41-1

##### Landfill Vicinity (Fall)

- ◆ GL17-1

##### Landfill Vicinity (Spring)

- ◇ GL16-1
- ◇ GL17-1

##### Compost Vicinity (Fall)

- ★ GL27-1
- ▼ GL29-1

##### Compost Vicinity (Spring)

- ☆ GL27-1
- ▽ GL29-1

##### Leachate Median

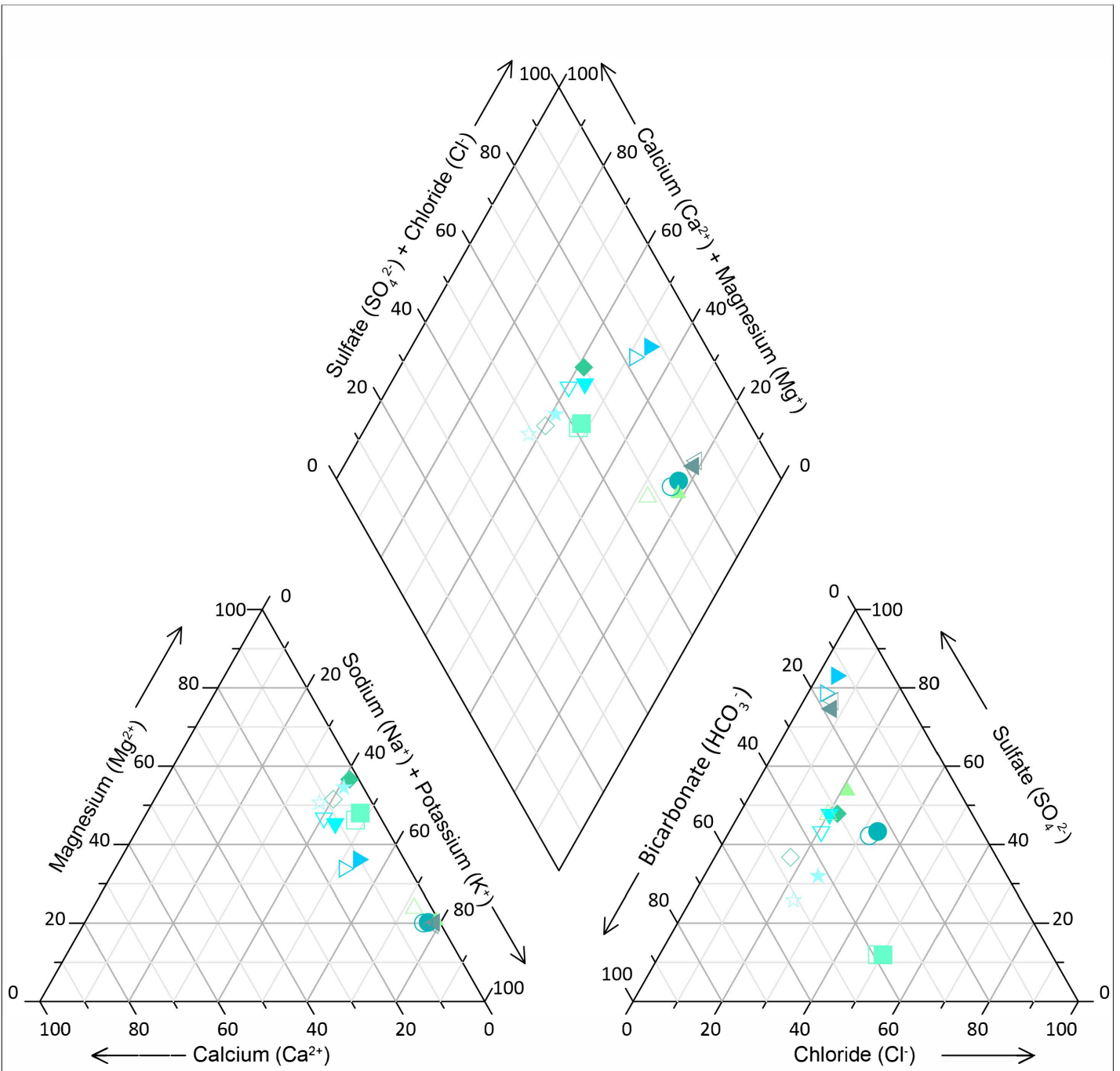
- S Leachate Wet Well
- ▲ P1 Leachate MH-2
- N Pumhouse MH
- P2 A2 Leachate MH



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 CHARACTERIZATION REPORT  
 GROUNDWATER BEDROCK WELLS  
 PIPER PLOT - 2022

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 Date November 2023

FIGURE K-3



### LEGEND

Surface Water	
September 2022	June 2022
● Slough #2	○ Slough #2
■ Bubna Slough	□ Bubna Slough
◆ NE Pond	◇ NE Pond
★ Bredin Pond	☆ Bredin Pond
▼ Tutt Pond	▽ Tutt Pond
▲ Slough	△ Slough
▶ Little Robert Lake*	▷ Little Robert Lake*
◀ Robert Lake*	◁ Robert Lake*

NOTES  
\* Offsite Surface Water Body



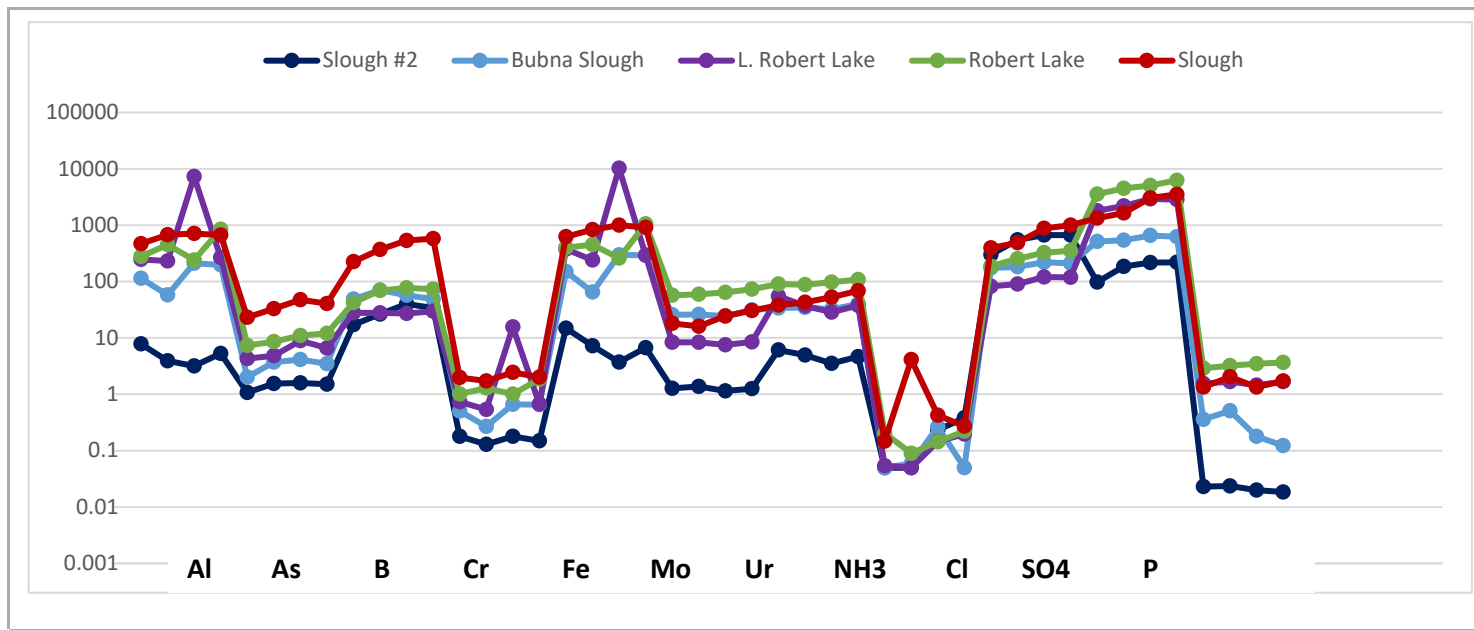
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FIGURE K-4





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SURFACE WATER GEOCHEMICAL PROFILE

Figure K-5



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